THE EFFECT OF DISK SPEED ON THE PERFORMANCE OF AN

EXPERIMENTAL CASTOR BEAN HULLER

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PREFACE

This study was undertaken to supply additional information on the subject of castor bean hulling so that the domestic production of castor beans can become economically practicable and feasible. At present castor beans are being produced to supply castor oil which is primarily needed for defense purposes.

The effectiveness and efficiency of the castor bean huller depends upon many factors, such as variety, maturity, and moisture content of the beans, disk speed, spacing between disks, width of disk, and hardness of rubber. The effect of these factors on the performance of the castor bean huller can be determined only through relentless research and experimentation. The author felt that there was a need for determining the effect of disk speed on the percent hulled beans and various other performance characteristics of the castor bean huller. No attempt was made to determine what effect the other factors have on the performance.

The author wishes to express his deepest appreciation to Professors E. C. Baker and J. G. Porterfield, under whose supervision this study was carried out. Professor Porterfield has given much of his time as guidance and has offered invaluable suggestions in the writing of this paper. He is also indebted to Dr. D. L. Vanhorn, agronomist for the United States Department of Agriculture and Oklahoma Agricultural Experiment station, who gave helpful advice and criticisms for the various problems involved and to Professor G. E. Marshall, Head of Statistics, who gave excellent advice in

iii

the sampling technique used in this thesis. The author is especially grateful to Professor E. W. Schroeder, Head of the Department of Agricultural Engineering, who made special efforts to provide the necessary facilities to carry out this study. The author would also like to thank all those who assisted him in performing the laboratory tests as it would have been impossible by himself to have obtained the data.

TABLE OF CONTENTS

CHAPT	ER	PAGE						
I.	INTRODUCT ION							
II.	OBJECTIVE							
III.	REVIEW OF LITERATURE							
	A. History of Castor Bean Production	4						
	B. Castor Beans and Their Uses	7						
	C. Development of Castor Bean Hulling Equipment	9						
IV.	APPARATUS AND EQUIPMENT							
¥.	METHOD OF MAKING TESTS AND OBSERVATIONS							
	A. Preliminary Investigations	25						
	B. Test Conditions	27						
	C. Technique Used	31						
	D. Sampling Technique	32						
VI.	ANALYSIS OF DATA	34						
	A. Determination of Performance Characteristics	34						
VII.	DISCUSSION OF RESULTS	65						
·	A. Per Cent Hulled Beans and Per Cent Beans in Unhulled Segments	65						
	B. Per Cent Unhulled Segments	66						
	C. Per Cent Cracked and Broken Beans	67						
	D. Capacity of Hulled Beans	68						
	E. Per Cent Losses	68						

V

TABLE OF CONTENTS (Cont'd)

CHAPTER	2		PAGE		
VIII.	SUM	MARY AND CONCLUSIONS	71		
	A .	Operating Disk Speed	71		
	в.	Type of Material	72		
	C.	Proposals For Further Study	73		
BIBLIOGRAPHY					
APPEND	CX.		77		
	A.	Results of Preliminary Investigations	78		

I. INTRODUCTION

Castor bean production, which was sizable in the United States during the last century, is being revived on a completely new basis of management. Public and private research, experimentation, and development is making this possible. Castor oil is listed as a strategic material and is needed in large quantities for both civilian and defense purposes.

Research by the agronomist, plant breeder, agricultural engineer, and the chemist has revolutionized production methods and decreased cultural costs to the point where domestic production is again practical. The agronomist made his contribution by finding where the plant preferred to be grown and what methods should be used in its culture. The plant breeder was charged with developing varieties of castor beans which would be suitable for commercial culture here. The breeder now has furnished types which are early-blooming, small-stemmed, short, high-yielding, and resistant to both shattering and dehiscence; therefore making them more suitable for mechanical harvesting. The agricultural engineer has aided in the development of satisfactory harvesting equipment and the design and manufacture of efficient hulling equipment, which put the hulling costs within range of economic practicability. Many of these machines are now in commercial production and are being used on the present donestic crop. The chemist has brought about the many uses of castor oil. These combinations of developments have now made possible the economic production of castor beans in this country.

The demand for castor beans as a major crop in the shifting pattern of

wheat, cotton, grass, grain sorghum and other crops is becoming popular in Oklahoma. This study was undertaken because it was felt that the need existed for new developments or modifications of farm machinery necessary for castor bean production and that the agricultural engineer should be increasingly responsible to any effort that looks to new discoveries to meet these needs.

II. OBJECTIVE

The objective of this study was to determine the effect of disk speed of a horizontal disk type castor bean huller on the following factors:

- 1. The per cent hulled beans.
- 2. The per cent beans in unhulled segments.
- 3. The per cent attached hulls in unhulled segments.
- 4. The per cent unhulled segments (beans plus attached hulls).
- 5. The per cent cracked and broken beans.
- 6. The capacity of hulled beans.
- 7. The per cent losses.
- 8. And to compare the above performance factors with three different materials, bulk or harvested, whole capsules, and segments, which were obtained from the same variety of castor beans.

III. REVIEW OF LITERATURE

A. HISTORY OF CASTOR BEAN PRODUCTION

The castor bean (Ricinus communis), seed of the castor plant, is not a true bean, nor a legume, but a member of the spurge family, a group of plants such as the rubber and tung oil trees. The name Ricinus is a Latin term meaning dog-tick which the seed was thought to resemble.

Tropical in its origin and native either to Africa or India, the castor plant has been carried by the many migrations of men in the course of ages to all parts of the tropical and subtropical world. In the tropics, the castor plant is a perennial that grows to a height of thirty or forty feet, but acclimated in cooler zones it becomes an annual, and attains a height of only from eight to twelve feet. In most areas of the United States they are grown as annuals.

Castor bean production is not new to American agriculture; however no records exist as to the exact date the first castor beans were produced in the United States. In the early 1800's¹⁹, limited production was reported in parts of the states of Illinois, Missouri, Kansas, and the territory of Oklahoma. Within the period 1825-1850¹⁹ there are occasional references that castor beans were produced in the coastal states from Virginia to Georgia and in Kentucky, Texas and California.

In 1850¹⁹ the first comprehensive data was recorded that indicated the extent of the crop. There were twenty-three castor oil mills in the United States in 1850. St. Louis was the commercial center in the west and seventy per cent of the domestic production of castor oil was produced there. In 1857¹⁹ a mill, the largest of its kind, was built in Jersey Gity, New Jersey. This mill processed some of the domestic production, but soon became the center for imported seed. Production became spasmodic and areas of production shifted and by 1870¹⁹ there were only six mills left in operation.

From about 1860 to 1916 Crooks⁵ and Sievers mention that extensive production occurred in southeastern Kansas and adjacent parts of Missouri and Oklahoma. Production to a lesser extent occurred in other parts of the United States mostly in the cotton belt.

During the first World War the production of castor beans was stimulated by the need for oil for special purposes. such as the lubrication of airplane engines. The castor bean industry did not survive after the war due to the economic factor of laborious and expensive hand-harvesting practices that limited production. During this period until 1940 no commercial acreage is reported in the United States and the United States was wholly dependent upon importations from the tropical countries. The earliest importations of castor beans used in the United States was supplied by India. During World War II imports were entirely from Brazil and Mexico, where castor beans have been grown under cultivation for at least fifty years. By 1939⁴ the United States was importing 150 million pounds of castor beans, of which almost the entire supply came from Brazil. World War II boosted the consumption to about double the peacetime level. A higher level of use carried over into peacetime and it appears now that the use of between 200 or 300 million pounds of beans per year will be normal. At the present the United States depends entirely on Brazil, taking about 80

per cent of her output.

In 1940⁵ castor bean production was again undertaken in the United States on a limited scale, particularly in the vicinity of Dallas, Texas. In June 194115 the United States Department of Agriculture started an energency castor bean program to furnish a supply of adapted seed stock for 1942. In the spring of 1942 this program was instituted through Texas, north to Kansas, east to Kentucky, and south to Tennessee. Out of scores of strains in hundreds of experimental plantings, the seed of two or three varieties, having more or less the desired characteristics as to plant growth and nonshattering factors were accepted, and one of them, called Conner, turned out to be well adapted to the region around Texas, Oklahoma, and Arkansas. It grew four to eight feet high and the hulls were reasonably resistant to shattering. The need for domestic castor beans did not materialize and this government work was virtually discontinued in 19444. Some state agricultural colleges went on with the work and eventually came up with improvements; however the big push after the war came from the Baker Gastor 011 Company⁴, one of the oldest and largest companies processing the oil.

Since 1947⁴ the Baker Castor Oil Company have brought about the development of several new varieties of castor beans of the low growing type of around four feet high, with vastly increased yields and more shatterresistant hulls. The Baker Castor Oil Company also recognized that economic production required proper machinery and they have assisted greatly in the development of harvesting and hulling machinery. The entire commercial castor bean acreage in the United States from 1947 to 1950 was grown under contract with the Baker Castor Oil Company. That acreage increased during that period from zero to about nine thousand acres in 1950.

In 1951¹³, after the outbreak of the Korean war, the Munitions Board realized the importance of castor oil as a strategic commodity which was in demand for military purposes and at their request, the Department of Agriculture was authorized to install a program for the domestic production of castor beans to be carried out by the Commodity Credit Corporation by a commitment of funds by the Defense Production Administration. The program was made available to farmers who enter into contracts either with Commodity Credit Corporation or with private companies under contract with Commodity Credit Corporation, in areas within Oklahoma, Texas, California and Arizona for which adapted seed is available. Harvesting machinery and technical guidance was made available to contracting farmers. The seed supply was the major limiting factor on the acreage planted.

In 1952⁴⁴ a program similar to that of 1951 to assure increased supplies for the national defense was authorized by the Secretary of Agriculture. At the present both the Baker Castor Oil Company and the Department of Agriculture are coordinating their efforts to carry on the now important crop of castor beans and the improvement of implements necessary to handle the crop.

B. CASTOR BEANS AND THEIR USES

Castor beans have shiny brittle coats of black, brown, tan and all sorts of mottled effects varying according to different varieties. The size of castor bean seeds is variable; however those measuring about one-half inch long and about one-fourth inch in diameter are preferable, and uniformity of seed size facilitates the removal of hulls by mechanical means. On early varieties seed production begins about 120 days after planting. The seed occurs in clusters made up of capsules each containing three seeds. The plants which grow wild have capsules that split open very readily at maturity;

however improved varieties have been developed that are resistant to shattering. Castor bean yields of 500 pounds per acre are average in the nonirrigated land of the midwest and with irrigation, various varieties of beans yield from three to four times as much. Localities with the longer growing seasons can produce better yields because seed formation goes on until frost kills the plant. Castor bean plants are not affected by plant diseases or insect pests.

A bushel of castor beans weighs 46 pounds and good varieties of castor beans analyze by weight approximately as follows: oil--50 per cent, shells--23 per cent, and pomace--27 per cent. Pomace is the cake or remnant of the bean after oil extraction. The chemical structure of castor oil differs from other domestic vegetable oils in that its fatty acids contain a hydrozyl group. This gives castor oil a chemical versatility over all other oils. Chemists have found many ways that castor oils can be used. It is in demand for military purposes mainly for use in lubricating oil for jet planes, a fluid in control equipment, such as hydraulic brakes, shock absorbers, and retractable landing gears on planes and special plastics. In addition dehydrated castor oil is a quick-drying oil that is used in protective coatings. Some other essential uses of castor oil are: paints. varnishes, lacquers, medicinal oil, nylon, linoleum, rubber substitutes. ink, cosmetics, electrical insulations, fungicides, soaps, artificial leather and for many other purposes. Pomace contains 73 per cent protein but it also contains a poisonons substance that renders it unsuitable for cattle feed, but because of its high nitrogen value it is an excellent fertilizer. especially where ground insects are troublesome, since it serves the dual purpose of a fertilizer and destruction of some insects. The shells have no value as far as is known.

All plant parts of castor beans are poisonous to humans and to livestock. Pomace contains a very toxic albumin called ricin and the other parts of the plant as well as the seed contain a poisonous substance called ricinine, which is of an alkaloidal nature.

C. DEVELOPMENT OF CASTOR BEAN HULLING EQUIPMENT

When the beans, or more correctly capsules, have been harvested a hulling machine is necessary to separate the beans from the hulls. Several machines have been built which do a successful job with little damage to the beans. These will be discussed briefly in the following paragraphs.

In 1942 Arnold¹ and Sharp developed a vertical disk type huller at the agricultural experiment station of the University of Tennessee. The machine consisted of two rubber disks, one being stationary and the other rotated at a peripheral speed of about 1,570 feet per minute, or approximately 1,000 revolutions per minute for the 6-inch diameter disk. The rubber used on the faces of the disks was 3/8 inch thick, black, soft, abrasive-resistant sheet rubber, with a specific gravity of 1.15. The disks were spaced about 1/2 inch apart and adjusted so the beans would just fit endwise between them without being crushed. A cleaning duct connected to a suction fan was provided for the removal of the cleanings. This 6 inch machine hulled 95 to 98 per cent of the beans without injury to them at a capacity of about one bushel per hour, and has proven to be very satisfactory for experimental plot work. Arnold and Sharp found that the capacity was proportional to the area of the disks and later in 1942¹⁷ they constructed a similar machine with 12 inch diameter rubber-faced disks and vacuum-type cleaner. Rotating the rotor at 525 rpm gave a capacity of six bushels of hulled beans per hour and over 99 per cent hulled. At that time this machine was considered ade-

quate for individual farm use.

In 1942 Glay^3 built a homemade castor bean thresher. The threshing device consisted of a 32 x 6:00 10-ply truck tire slightly inflated and rotated at 50 to 100 rpm inside approximately 1/5 of a 9:00 x 36 tractor tire casing, with bead cut-off, mounted on a wood frame. An air blast was used to clean the chaff from the beans. The capacity of the hulling element was over 200 lb/hr and around 99 per cent of perfect beans were hulled with proper adjustments.

Late in 1943 Arnold² designed an improved castor-bean huller similar to the one in 1942. This machine had 24-inch-diameter rubber-faced hulling disks and an hourly capacity of 900 to 1,400 pounds of shelled beans. Because of its capacity it became known as the "commercial size". A suction fan was employed to remove the hulls and trash from the clean beans. Under ordinary conditions, the machine hulled from 95 to 98 per cent of the beans and cracked less than 2 per cent.

In the Great Plains of Texas in 1941 Gordon¹⁰ tried out several types of experimental hullers to devise a method of hulling which would do a good job without excessive damage to the beans.

A machine, developed previous to 1940, was tried. Its hulling element consisted of a horizontal cylinder, 12 inches in diameter and studded with steel spikes, 3/8 inch in diameter and 2 inches long, was rotated between a feeding hopper and a curved metal grate at about 250 rpm. The chaff was separated from the beans by the use of a screen and an air blast. This huller worked satisfactorily with some varieties of castor beans; however excessive breakage occurred with the Conner variety.

A small experimental model was tried which consisted of an inverted conical rotor, mounted vertically and covered with rubber matting. The rotor turned inside a funnel-shaped housing, lined with a smooth rubberized fabric underlain with a coating of sponge rubber 3/4 inch thick, at a close distance which diminished toward the small end. No cleaning device was provided for this experimental unit. Rotating the rotor at speeds ranging from 125 to 150 rpm cracked less than 1 per cent and hulled about 94 per cent, however the capacity of this unit was very low.

Gordon¹⁰ built a small huller of the double belt type in which two belts traveled parallel, close to each other, in the same direction. The top belt traveled 38 per cent slower than the bottom one whose surface speed was computed to be 1,200 fpm. The abrasive action of the belt surfaces traveling at different speeds removed the hulls from the beans and tests showed that about 72 per cent were hulled and 2 per cent were cracked and broken. The belt type huller had a capacity of 650 to 700 pounds of hulled beans per hour per foot of belt width.

Gordon¹⁰ investigated the possibility of using a small combine, Allis Chalmers 40 all crop Harvestor. equipped with a cylinder covered with heavy rubber matting having a slightly grooved pattern. The cylinder was rotated at about 400 rpm and results showed that 85 to 90 per cent or more beans of the US varieties were hulled and 1 to 5 per cent were cracked and broken, however the Conner variety was badly damaged by the cylinder action. The machine had a capacity of 2,400 lb/hr.

A small huller, Cardwell-Gordon¹⁰ unit, was built during the winter of 1941-42. The hulling element consisted of a rubber covered cylinder 8 inches in diameter and 24 inches long, and a rubber covered concave. Results showed that with the Conner and Kentucky 38 varieties less than 5 per cent were cracked and broken; however capacity was very low. A paddle wheel type fan and rotary screens were used for cleaning and separation.

This principle of cylinder-concave hulling resulted in the revision of the Gardwell-Gordon machine into a larger machine with greater capacity and it became known as the "USDA Gastor Bean Huller". The hulling unit consisted of a wooden cylinder, eight inches in diameter and twenty-four inches long, and a concave facing, which were covered with abrasion resistant rubber matting, Type A, Durometer No. 70. Separation and cleaning was accomplished by a vibrating screen and suction type fan. The vibrating screen was equipped with a reciprocating wiping device to prevent clogging and to aid separation of unhulled beans from hulled beans. The hulling cylinder had a capacity of 1,200 lb/hr with Conner or Kentucky thirtyeight varieties. Five of these machines, designed by the Bureau of Agricultural Chemistry and Engineering for the Commodity Credit Corporation, were built for use during the 1942-43 hulling season.

This huller was later improved by development work at the Tillage machinery Laboratory¹⁶ of the United States Department of Agriculture, at Auburn, Alabama. Simplification of this unit resulted in an improved USDA Castor Bean Huller which has a capacity between 1,600 and 1,850 pound per hour and under normal conditions cracks less than two per cent and hulls above ninety-eight per cent.

It should be recognized that no research has been recorded on a castor bean huller with horizontal disks and it is believed that the research in this study will bring out the merits of a horizontal disk type huller comparable to the above hullers.

IV. APPARATUS AND EQUIPMENT

The castor bean huller tested is shown in Figures 1, 2, 3, and 4. It is mounted on a trailer to facilitate transportation and to accommodate it for quick service as soon as it is pulled to the job. The complete unit consists essentially of the huller engine, a hopper and elevator unit with electric motor, a rotating drum feeder, a hulling element consisting of two horizontal adjacent rubber-faced disks, and a cleaning unit made up of a section fan powered by a gasoline engine. Any one of these parts can be adjusted independently of the others, thereby making it possible to adapt the huller to various conditions to get maximum effectiveness and efficiency under any conditions.

The huller engine is a four cycle, single cylinder air cooled gasoline engine, type PAC 184, Serial Number 7-41394, rated hp 4.3, and manufactured by the Lauson Company, New Holstein, Wisconsin. The engine speed is controlled by changing the setting of the governor and after the governor is set for a particular speed the engine operates at approximately constant speed and has good governing for any range of speed. The engine is connected by V-belts to the vertical shaft which drives the rotating disk.

The hopper was built large enough to hold several sacks of unhulled beans and it was equipped with a sliding gate and a rod mechanism for operating the gate opening so as to control the rate of feeding the unhulled material.

The belt-conveyor, flight-type-elevator, feed mechanism is a Porta-Loader Serial No. 260, manufactured by the Boardman Company, Oklahoma City,



Figure 1. Top View of Complete Castor Bean Huller Unit Showing Position of Elevator as Used in Tests.

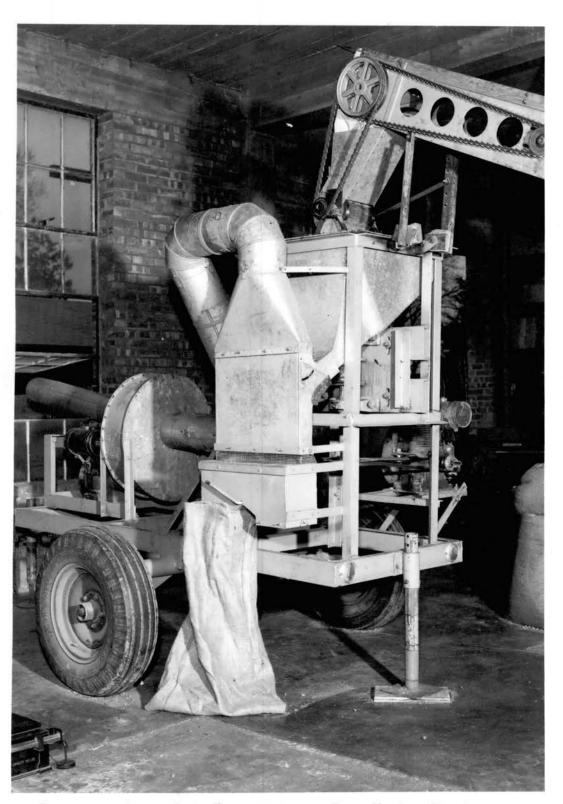


Figure 2. Right Side View of Castor Bean Huller Showing Arrangement of Rotating Drum Feeder, Cleaning Unit and Two Way Discharge Valve for Sacking.

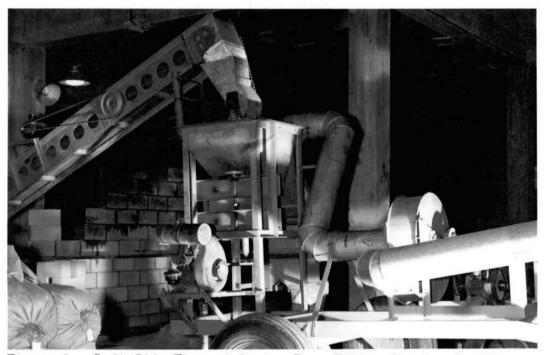


Figure 3. Left Side View of Castor Bean Huller Showing Position of Huller Engine and Handwheel Used to Adjust Spacing Between the Disks.

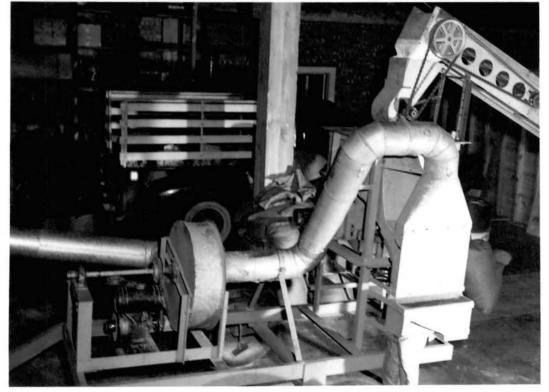


Figure 4. Right Side View of Castor Bean Huller Showing Position of Fan and Motor.

Oklahoma. The elevator is approximately 16 feet in length and has a channel width of 9 inches. The elevator belt runs at a peripheral velocity of about 5 fps and is driven by the top roller shaft which is powered by pulleys and V-belts connected to a 1/3 hp electric motor, integrally mounted on the elevator. The unbulled beans are conveyed to the rotating drum feeder by boards one inch by nine inches equally spaced on the belt.

The huller element consists essentially of two adjacent rubber-faced disks. One of the disks is stationary and the other rotates. The rotor is shown in Figure 5 and is attached on the end of the vertical shaft driven by the huller engine. This shaft is mounted in ball bearings and provided with large lubricant reservoirs. The rotor has an outside diameter of 18 inches and is faced with a 1-inch thickness of soft abrasive-resistant rubber with durometer hardness of 40, as based on company specifications and not on actual tests of rubber hardness. The rubber was cemented to a 1/4 inch steel plate with a good grade of rubber cement. The hulling surface of the rotor lies between a 14 inch diameter and the outside diameter of 18 inches. It consists of an area of around 100 square inches. The rubber disk facing on the rotor is provided with a 1-inch bevel at the center opening. The inner edge of the bevel is protected from being torn loose by a 1/16 inch steel plate fastened to the 1/4 inch plate by machine screws. This bevel is essential to break up the whole capsules into single segments small enough to enter the hulling space, to guide the beans between the disk, and to increase the capacity of the machine. Careful consideration should be taken in selecting the proper bevel since too much bevel will overload the disks, increase seed crackage, and permit large stones or other objects to go between the disks.

The stationary disk shown in Figure 6 is attached on the lower side of the top plate of the huller housing. The fixed disk has an outside diameter

prevent the miterial from weiging and passing between the top plate and No herel to a 1/4 inch steel plate which is factoned by four bolts to the top plate. cations sed not an actual tests of rubbar hardness. periotant dinater of 10 inches and is faced with a 1/4 inch thickness of abradivetened around the inside and outside diameters of the fixed disk housing to Fixed disk. is provided on the fixed rubber disk. rubber with duranter hundress of 55, as based on company specifi-A sheet-metal bank is fas-The rubber was curented

vided for by having the stationary disk spring tensioned to the top plate bly up or down on four supporting bolts; however once the spacing is set it to parent large objects to go between the disks without damaging them. the front of the huller. disk and vertical shaft assembly by means of a small threaded hand wheel on to the disks shanever a large object enters the disk. This might be proremains fixed since no provision was made on this machine to prevent damage The spacing or clearance between disks is adjusted by moving the rotor Turning the threaded hand wheel slides the assen-

the fixed disk, raising and lowering the screws and tightening the four bolts fastened to of the fixed dick. adjustable screws equally spaced on a square centered on the mean diameter inside the four hexagon suts welded to the top plate. All gument of the disks is provided on the fixed disk by means of four the proper disk alignment is obtained. The screws may be raised or lowered by turning then See Figure 7. 3

uniform feeding of the beans to the buller disks. roller 5 inches in diameter. through the opening and against the robary disk. the control opening on the top plate. Its privary function is to facilitate The rotating drum feeder shown in Figure 7 is essentially a moden The feeder and its housing are fastened over Then the retation of the The unhulled beans flow



Figure 5. View of 18 Inch Diameter Rotating Disk Equipped With 1-inch Thick Rubber Facing of Durometer Hardness No. 40 as Based on Company Specifications.



Figure 6. View of 18 Inch Diameter Stationary Disk Equipped With 1/4 Inch Thick Rubber Facing of Durometer Hardness No. 55 as Based on Company Specifications.



Figure 7. View of Rotating Drum Feeder and Two of the Four Adjusting Screws Used to Align the Disks.

rotor automatically feeds and circumfuses the beans between the disk faces, breaks up the capsules, removes the hulls and discharges the hulls and beans at the periphery. The feeding of the beans centrally between the disks causes the layer to spread or become thin as the beans move outward, thus reducing the chances of wedging.

The cleaning unit consists of a centrifugal type fan manufactured by the Belle City Manufacturing Company, Racine, Wisconsin. The fan is approximately 22 inches in diameter and is connected with 8 inch suction and discharge pipes at its housing. The 8 inch suction line is connected to the Y-cleaning duct, 3 inches by 20 inches in cross-sectional area which reduces the air velocity in the suction pipe. The Y-cleaning duct is equipped with an adjustable damper at the upper end which further restricts the air inlet but permits sound hulled beans to drop down through the throat area against the upward air stream and then into the sack. The damper permitted varying the throat cross-sectional area from 0 to 2 inches in width. Additional air inlet is provided by a screen area of 4 inches x 20 inches which may be adjusted by 4 shutters, each 1 inch x 20 inches, so as to provide additional air velocity to carry off the hulls. By closing one or more shutters it may be equally effective without requiring an increase in fan speed.

The mixture of hulls, beans and unhulled beans slides down a short incline to the Y-cleaning duct. The hulls, dust, and light undeveloped beans are carried up with the air through the fan which discharges them to the outside. The clean whole beans drop through the throat area and are sacked at the discharge spout which is equipped with a two way valve to facilitate the sacking operations.

The fan is driven by a 4 cycle single cylinder air cooled gasoline engine, rated 2 hp and manufactured by the Briggs and Stratton Corporation.

The engine speed is governed by changing the governor setting and maintains approximately constant speed after once set.

The number 16 cleaner shown in Figure 8 was used to separate the bulk or harvested material into whole capsules and segments. The cleaner was equipped with two screens, a top screen No. 28 with 7/16 inch oval perforations and a bottom screen No. 20 with 5/16 inch oval perforations. A wiping device of reciprocating brushes on the cleaner completely eliminated clogging the screen with hulls and segments. By proper adjustment of the fan practically all of the foreign material and light beans were removed by this cleaner. The cleaner removed all the cracked and broken, and hulled beans from the whole capsules; however part of the cracked and broken, and hulled beans were carried over with the segments. This is shown in Table 1.

The instruments used in testing the castor bean huller were a tachometer and stop watch, manufactured by M. DuCommun Company, New York. The hand tachometer, Type 25A Metron, Serial No. 1156, manufactured by Metron Instrument Company, Denver, Colorado, was very sensitive and was equipped with an adjustment for zeroing it before each run. Its smallest scale division was 20 rpm; however with careful observation it could be read accurately to increments of 5 rpm. A more precision instrument for obtaining the disk speed would have been by the use of a revolutions counter; however none was available.

The apparatus used in sampling is illustrated in Figure 9. The balance is a Model 4021Y, Serial No. 697, manufactured by Toledo Scale Company, Toledo, Ohio, and has a capacity of 5 kilogram with the smallest graduations of 1 gram. The balance was very sensitive and was read to within an accuracy of 1/2 gram for the measurements recorded during the sampling of the products.

The small hand operated clipper was used to separate the oil bearing

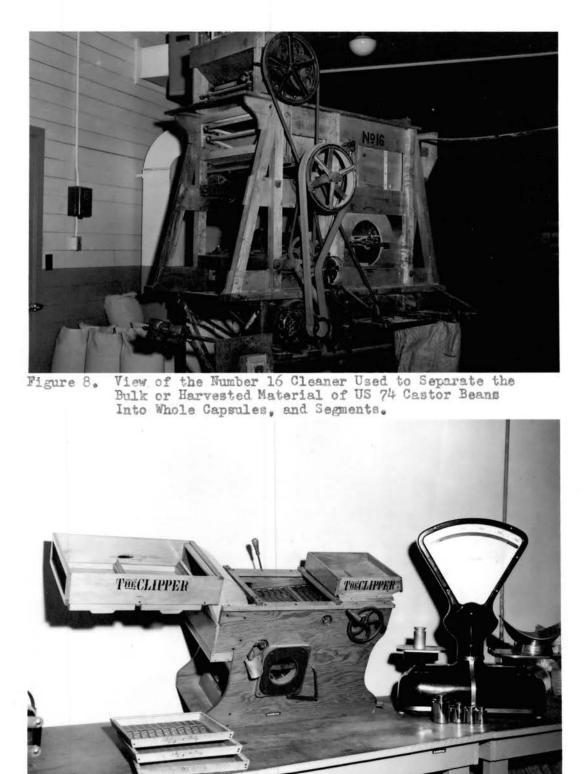


Figure 9. Sampling Apparatus Consisting of Toledo Scale Balance, Small Hand Clipper and 3 Separating Screens Used to Evaluate the Products in the Sack and in the Cleanings. material from the hulls and chaff, or cleanings. This small cleaner did a good job of separating the oil bearing material from the products of the cleanings.

The three screens shown in the foreground of Figure 9 were used in sampling the products from the sack. The top screen with holes $17/64 \times$ 3/4 inch separated the unhulled segments, the middle screen with $12/64 \times$ 3/4 inch holes separated the clean whole beans, cracked and broken, and the bottom screen or blank was used to collect the light undeveloped beans and the foreign material.

In Figure 10 is shown a small hand huller which was used to obtain the weight of the beans in the samples taken from the materials. Its hulling element consisted of a wooden drum faced with a 1/4 inch grooved rubber matting that turns close to another grooved rubber facing.

V. METHOD OF MAKING TESTS AND OBSERVATIONS

The technical aspects of making tests and observations to determine the effect of disk speed on the performance of the castor bean huller were considered in order that the results obtained would be reliable and acceptable. Such considerations included an understanding of the theory, precision, and accuracy of methods and measurements, and the practical limitations imposed by testing the castor bean huller.

A. PRELIMINARY INVESTIGATIONS

Preliminary investigations were made to find the best operating conditions for the different disk speeds so as to obtain data with as much accuracy as possible. These investigations were made with the bulk or harvested material of US 74 castor beans.

These investigations showed the following:

1. The minimum and maximum disk speeds that could be obtained with the Lauson engine were 150 and 750 rpm when the disk was loaded. Excessive heating of the disks occurred at the maximum disk speed of 750 rpm and this heating ruined the rubber and loosened the rubber cement so that it caused the rubber to peel from the disk plates. It was found that the top speed to prevent excessive heating was in the neighborhood of 650 rpm. The approximate setting of the disk speeds at intervals of 100 rpm are given in the results of preliminary investigations found in the appendix.

2. The proper adjustments of fan speed, damper opening, and position

of shutters to obtain the best cleaning performance for the different disk speeds were established by the following analysis. If the fan ran too slow it would not elevate the hulls and chaff, if too fast it would carry the good beans over with the hulls and chaff. When the removal of the hulls and light beans was not accomplished, even with the damper properly adjusted, the shutters could be closed over the screen area at the upper part of the Y-cleaner duct to provide additional air velocity to carry off the hulls. Making the cross-section area of the screen area smaller by closing one or more of the 1 inch x 20 inch shutters increases the air velocity in the duct so that it may be equally effective without requiring an increase in fan speed.

Additional air inlet into the cleaner duct is adjusted by raising or lowering the damper in the Y-duct. This opening should be as small as possible without letting light beans and hulls come down with the sound beans. Too much air entering through the screen area and damper causes poor elevation of the hulls and foreign material unless the fan speed is high.

The fan speed, position of shutters and position of damper are given in the results of preliminary investigations found in the appendix.

3. The selection of the proper spacing of the disks for good hulling of the variety of castor beans used was found to be 5/16 inch. This was determined by observing the number of beans remaining in the hulls and the number cracked and broken. If too many beans remained in the hulls the spacing was decreased by turning the hand wheel clockwise and if too many beans were cracked and broken the spacing

was increased by turning the hand wheel counterclockwise.

4. If the machine, after adjusting the spacing for 5/16 inch, failed to hull the material without crackage, the disks required checking for alignment. This was done by means of a round rod or dowel, with a diameter of 5/16 inch and 9 inches long, placed radially between the disks through the feed inlet, or opening. The disks were adjusted by changing the effective length of the four screws between the top plate of huller housing and the fixed disk so that both disks barely touched the dowel at all points.

B. TEST CONDITIONS

The testing conditions for determining the effect of disk speed upon the per cent hulled with the castor bean huller were controlled such that all variables except speed were held constant.

The variety of castor beans used in this study was US 74. US 74 are medium in height and is a recommended variety of castor beans for Oklahoma. The castor beans used were harvested with a combine modified to do a satisfactory job. The castor beans were stored in a bin and no preliminary drying was employed in testing the effect of speed on the per cent hulled.

Two other types of material in addition to the bulk or harvested material were obtained from the bulk material by the use of the No. 16 cleaner. The three materials are shown in Figure 10 and consist of the following: (1) The original harvested or bulk material taken from the bin, (2) Whole capsules or all material separated by the cleaner that contained only a small percentage of segments and (3) Segments or all material consisting of 1/3 of a capsule. All three of these materials were used to determine what effect they had upon the per cent hulled with different disk speeds. In order to correct for the deviations from the test operating conditions of the per cent hulled and the per cent cracked and broken in the materials before they were run through the huller, five one quart samples were taken at random during the sacking of each material tested. Correction factors, C_s (Pounds of sound hulled beans in test weight) and C_{cb} (Pounds of cracked and broken beans in the test weight) were determined from the data obtained from these five samples. Since a 100 pound test weight was used, C_s and C_{cb} are numerically equal to their percentages as found in the test weight. For bulk or harvested material, $C_g = 4.06$ lbs. and $C_{cb} = 0.57$ lbs.. This data is recorded in Table 1.

It should be recognized that there is a wide variation within the five samples taken from the bulk material and to arrive at a more accurate estimation of the per cent hulled and the per cent cracked and broken in the bulk material, more samples should have been taken until a smaller deviation was obtained. The variation obtained with the whole capsules and segments have less deviation from the mean and give a more approximate estimation of the corrections to be applied to the total population. These corrections are used in computing the test results for the actual conditions at which the machine performed.

The intended test conditions for each material were as follows:

- The test weight of the different materials used in each run was 100 pounds and this established the duration of operation under test conditions for the different disk speeds.
- Disk spacing to be held at 5/16 inch for all runs and disks checked for alignment.
- 3. Six different disk speeds with increments to be held as close as possible to 100 rpm so as to cover the speed range determined in

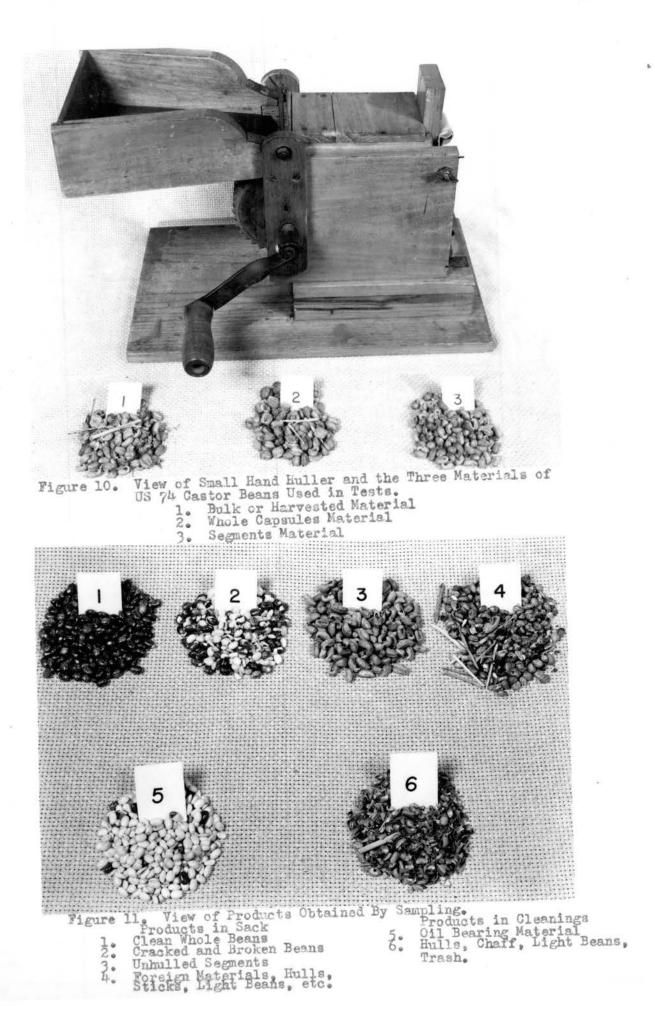


TABLE 1

Determination of Correction Factors, Cs and Ccb, In Materials Tested

From US 74 Castor Beans.

1. Bulk or Harvested Material

Sample No.	Weight	Weight Whole Capsules	hole Two	Weight Single Segments	Shelled Beans		Cracked and Broken Beans		Foreign Material	Weight Beans
	grams	grams	grams	grams	wt. grams	no.	wt. grams	no.	grams	grams
1 2	255 285.5	32.0 40.0	17.0 28.0	172 167	8.0 4.5	35 19	2.0	9 4	24 18	172 177
345	280 260.5 263	13.5 18.5 38.5	9.5 27.0 26.5	182 180.5 161	21.0 13.0 7.0	90 47 29	2.0 1.5 1.0	8 7 5	52 20 29	175 180.5 170
Total Per Cent	1317.0 100	142.5 10.8	108.0 8.2	862.5 65.52	53.5 4.06		7.5 0.57		143 10.85	874.5 66.4
				2.	Whole Capsul	<u>es</u>				
1 2 3	219 225 222	93 94 95	87.5 78.0 87.5	35.5 50.0 37.5	-	ī	-	1	3.0 3.0 2.0	149 156 152
4 5	223 212.5	90 81	92.0 87.5	38.0	-	1	-	-	3.0	150 142.5
Total Per Cent	1101.5	453 41.1	432.5 39.3	202.0 18.33	ō		ō		14.0 1.27	749.5
				3	. <u>Segments</u>		1			
1 2 3 4 5 Total Per Cent	299 299 257 280 <u>309</u> 1444 100			284 290 249 266 296 1385 95.92	13 7 6 11 11 48 3.32	53 28 24 43 44	1 - 1 1 0.21	41100	1.5 2.0 2.0 1.5 1.0 8.0 0.55	233 229 195 216.5 239 1112.5 77.0

the preliminary investigations.

- 4. The fan speed, damper opening and position of shutters set as found in the preliminary investigations.
- 5. The feed regulated manually by means of the rod mechanism that controls the gate opening in the hopper; thereby operating the disks at loaded conditions for all runs.

Every effort was made to carry out the tests as nearly as possible to the above conditions and thus reduce to a minimum any deviations from the specified conditions.

C. TECHNIQUE USED

The huller engine was regulated to give the desired disk speed under operating conditions and the fan speed, damper opening and position of shutters adjusted according to the preliminary investigations to give good performance at this disk speed. One hundred pounds of unhulled material was dumped into the hopper and the elevator started. The feed was regulated manually by the gate opening in the hopper on the elevator, so that there was always an adequate supply of unhulled material to keep the disks at loaded conditions throughout each run. The gate was opened and the beans conveyed to the rotating drum feeder. When the first beans dropped down on the disks the stop watch was started. During each run at various intervals five samples of the products in the sack were taken at random by means of the two-way valve at the discharge spout and three samples were taken at random from the products in the cleanings at the discharge side of the fan. Three readings of disk speed were taken with the tachometer and the average value recorded for each run. After all the one hundred pounds of unhulled material had passed through the disks, the stop watch was stopped and the

length of time was recorded. Three runs or similar observations were made for each disk speed tested except where there was variation in the desired disk speed, an extra run was made.

D. SAMPLING TECHNIQUE

The sampling technique was planned so that the data obtained could be analyzed on a statistical basis. The equipment used in obtaining data by sampling is shown in Figure 9 and the products obtained by sampling are shown in Figure 11.

The technique employed consisted of inspecting five samples, each one a 200 gram sample, taken from the products in the sack during each run. The procedure in inspecting the samples from the products in the sack was to separate and weigh the clean whole beans and the cracked and broken beans from each sample and to save the unbulled segments and foreign material from each individual sample until all five samples were inspected and then weigh them. Measurements of these products were recorded to the nearest 1/2 gram weight. From these five samples the mean percentages of clean whole beans, cracked and broken beans, unbulled segments, and foreign material were found. With these mean percentages the weight in pounds of each product was found by multiplying its mean percentage times the weight of products in the sack.

The same technique was used in sampling the three samples, each a 300 gram sample, taken from the cleanings. The mean percentages of oil bearing material, hulls, light beans, and foreign material were found and from these the weight in pounds was computed from the weight of the products in the cleanings. The oil bearing material was used to designate what few beans were whole and those cracked and broken that contained oil and were pulled over by the fan. This term was used since the fan tends to crack the largest percentage of whole beans passing through it; therefore making it impossible to separate the whole beans and cracked and broken beans in the products of the cleanings. Corrections for this could have been found by making a device to catch samples before they entered the fan.

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VI. ANALYSIS OF DATA

The method of analyzing the data obtained was to select the bean weight basis as the standard for computation of all results. Correction factors, resulting from deviations in the materials from the test operating conditions specified, were applied in computing the results. The method employed in computing the results from the observed data was to compute all values for each individual run. Calculations of these values were rounded off to two decimal places. The results obtained from the three different materials are summarized in Tables 2, 3, and 4. These values were then plotted graphically and curves constructed through the averages of the three points obtained for each speed.

A. DETERMINATION OF PERFORMANCE CHARACTERISTICS

The procedure followed in calculating these values from the observed data is explained in detail in the succeeding paragraphs. In order to simplify this analysis a flow diagram of the products, symbols for terms, and values of constants are employed. In reference to the flow diagram, the number of light beans left in the sack will depend upon the adjustment of the damper opening, position of shutters over screen area and fan speed.

The products and the symbols used in the following analysis are the weight in pounds found from the mean percentages obtained from the sampling data.

Let R = Total Weight in pounds of beans that went through huller. Then R = A + B + KC + E, where K is the ratio of the weight of beans in the unhulled segments to the total weight of beans plus the hulls in

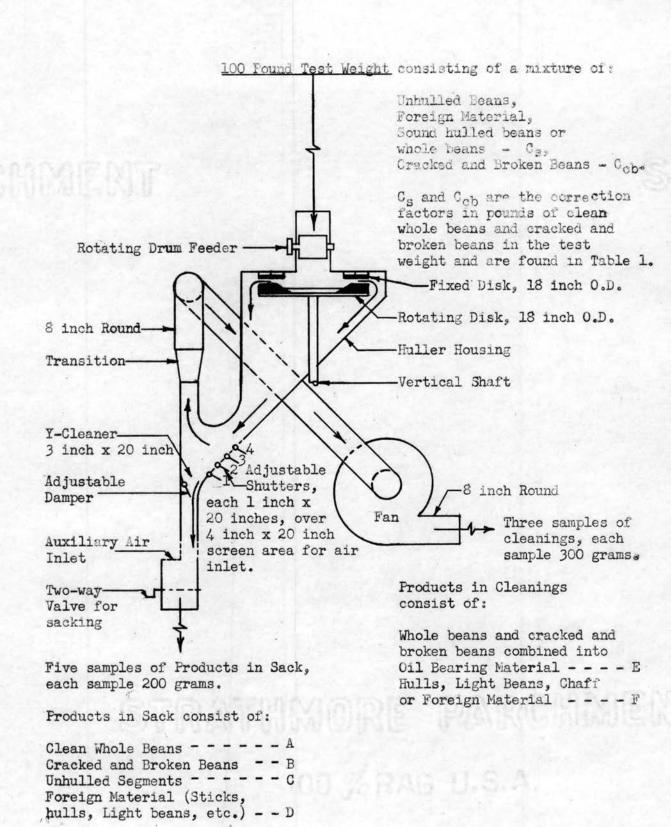


FIGURE 12. Flow Diagram of Products through Huller.

TABLE 2

Effect of Disk Speed and Spacing of 5/16 Inch on Bulk or Marvested

Material of US 74 Castor Beans.

Run No.	Time	Average Disk Speed	Fan Speed	Weight Of Beans		Unhulled	Attached Hulls in Unhulled	Unhulled Segments	Gracked and Broken	Per Cent Losses	Capacity of Hulled Beans
1A 1B 1C	Second s 49 3 512 528	RPM 185 180 175	RPM 900 900 900	Lds. 68.06 67.99 68.79	\$ 99 .79 99 .87 99 .83	% 0.21 0.13 0.17	Segments % 0.06 0.04 0.05	\$ 0.27 0.17 0.22	Beans % 0.46 0.41 0.36	% 0.84 0.51 0.79	Lb/Er 497 478 469
2A	356	255	900	67.51	99 .61	0.39	0.10	0.49	0.62	0.55	683
2B	325	260	900	67.19	99 .61	0.39	0.11	0.50	0.72	0.61	744
2C	361	255	9 00	67.54	99 .66	0.34	0.09	0.43	0.45	0.55	674
3A	210	355	960	66.12	99 : 56	0.44	0.11	0.55	0.83	0.80	1133
3B	211	355	940	67.92	99 : 44	0.56	0.15	0.71	0.96	0.60	1159
30	214	355	940	67.64	99 : 57	0.43	0.11	0.54	1.00	0.52	1138
4A	147	45 5	980	68.01	99.40	0.60	0.16	0.76	1.50	0.87	1666
4B	147	455	980	66.19	99.32	0.68	0.18	0.86	1.12	2.19*	1621
4C	135	460	980	67 .57	99.22	0.78	0.21	0.99	1.49	0.77	1802
5 A	100	550	1010	68.59	98 .75	1.25	0.33	1.58	2.16	0.83	2469
5 B	103	550	1010	67.93	99 .00	1.00	0.26	1.26	2.12	0.80	2374
5℃	109	545	1010	67.61	98 .70	1.30	0.35	1.65	2.24	0.81	2233
6A	79	635	1200	67.98	98 .53	1.47	0.39	1.86	3.70	1.06	3098
6B	70	640	1200	67.89	98 .54	1.46	0.39	1.85	4.17	1.12	3492
6C	73	640	1200	68.29	98 .5 8	1.42	0.35	1.79	4.04	1.22	3368

* Screen area for air inlet clogged with trash.

DATA SHEET 1.

Mean Percentages and Pounds of Products Evaluated From Samples

Taken From Bulk or Harvested Material

Products in Sack Sample Weight - 200 Gram

Products in Cleanings Sample Weight - 300 Gram

Run No.	Wt. of Sample Products No. in Sack	Clean Whole Beans	Gracked and Broken Beans	Unhulled Segments	Foreign Material	Wt. of Sam Products No in Cleanings	mple Oil 9. Bearing Materia	
14	Lbs. 68.69 1 2 3 4 5	Grams 194 192 193 195 <u>194</u>	Grams 2.5 3.0 2.5 2.0 2.5	Grams	Grams	Lbs. 31.31 1 2 3 Tot Mean Per Ce	5.5 5.1 16.5	Grams 293.5 295.5 294.5 883.5 98.17
	J Total Mean Per Cent Lbs.	96.8 96.49	12.5 1.25 0.86	2.5 0.25 0.17	17.0 1.70 1.17		os. 0.57	30.74
18	69.09 1 2 3 4 5	195 190 194 195 <u>192</u>	2.0 3.5 2.0 2.0 2.5			30.91 1 2 3 Tot Mean Per Ce	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	297 296 <u>297</u> 890 98.89
	Total Mean Per Cent Lbs.	966 96.6 66. 7 4	12.0 1.20 0.83	1.5 0.15 0.10	20.5 2.05 1.42	τр	os. 0,34	30.57
10	69.31 1 2 3 4 5 Total	193 195 193 194 <u>196.5</u> 97 1.5	3.0 2.0 3.0 2.0 <u>1.5</u> 11.5	2.0	15.0	30.69 1 2 3 Tot Mean Per Ce Lb	tal 16.0	296 293 <u>295</u> 884 98.22 30.14
	Mean Per Cent Lbs.	97.15 67.33	1.15 0.80	0.20 0.14	1.50 1.04		, €, €, 8 , 9 , 9 , 9 , 9 , 9 , 9 , 9 , 9 , 9 , 9	ل ف ال لي

		oducts in Sack Weight - 200 Gram	Products in Cleanings Sample Weight - 300 Gram				
Run No.	Wt. of Sample Products No. in Sack	Clean Cracked Whole and Beans Broken Beans	d Unhulled Foreign Segments Material	Wt. of Sample Oil Hulls, Products No. Bearing Light Beans, in Material Foreign Cleanings Material			
24	Lbs. 68.46 1 2 3 4 5	GramsGrams1914.01933.01942.01913.01942.0	Grams Grams	Lbs. Grams Grams 31.54 1 4.5 295.5 2 3.0 297 3 3.0 297 Total 10.5 889.5 Mean Per Cent 1.17 98.83			
	Total Mean Per Cent Lbs.	963 14.0 96.3 1.40 65.93 0.96	4.5 18.5 0.45 1.85 0.31 1.27	Lbs. 0.37 31.17			
2B	68.24 1 2 3 4 5	1913.51923.01923.01923.01923.01932.5		31.7612.5297.525.0295.034.0296.0Total11.5888.5Mean Per Cent1.2898.72			
	Total Mean Per Cent Lbs.	960 15.0 96.0 1.50 65.51 1.02	4.5 20.5 0.45 2.05 0.31 1.40	Lbs. 0.41 31.35			
20	68,36 1 2 3 4 5	194 2.0 193 3.0 194 2.0 193 2.5 193 3.0		31.64 1 3.5 296.5 2 3.0 297 3 <u>4.0 296</u> Total 10.5 889.5 Mean Per Cent 1.17 98.83			
	Total Mean Per Cent Lbs.	967 12.5 96.7 1.25 66.10 0.86	4.0 16.5 0.40 1.65 0.27 1.13	Lbs. 0.37 31.27			

			ducts in Weight -					Products in Cleanings Sample Weight - 300 Gram				
Run No.	Wt. of Products in Sack	Sample No.	Clean Whole Beans	Cracked and Broken Beans	Unhulle Segnent	d Foreig s Nateri		Wt. of Products in Cleanings	No.		Hulls, Light Beans Foreign Material	
	Lbs.	·	Grams	Grams	Grams	Grams	1	Lbs.		Grams	Grams	
3A	67.27	1	194	2.5				32.73	1	5.0	295	
-	* -	2	191	3.0		÷	• .		2	ū.5	295.5	
		3 4	189	3.5					3	5.0	295	
			189	3.5					Total	14.5	885.5	
		5	192	3.5			•	Mean Per		1.61	98.39	
		Total	955	16.0	5.0	24			Lbs.	0.53	32.20	
	Mean Pe		<u>95.5</u>	1.60	0.50	2.40						
		Lbs.	64.24	1.08	0.34	1.61						
3B	69.22	1	191	3.0				30.78	1	3.5	296.5	
		2	191	3.0			2 2 2		2	3.5	296.5	
		3	191	4.0					3	5.0	295.0	
		4	1 9 0	4.0					Total	12.0	888.0	
		5	<u>190</u>	3.0			•	Mean Per	Cent	1.33	98.67	
		Total.	95 3	17.0	6.5	23.5			Lbs.	0.41	30.37	
	Nean Pe		95 .3	1.70	0.65	2.35						
		Lbs.	65.97	1,18	0.45	1.63						
30	68 .63	1	192	4.0		4	•	31.37	1	4.0	296	
		2	19 2	3.0					2	2.0	298	
		3 4	19 3	3.5				0	3	4.0	296	
			192	3.0					Total	10.0	890	
		5	<u>190</u>	4.0			•	Mean Per	Cent	1.11	98.89	
		Total	959	17.5	5.0	18.5			Lbs.	0.35	31.02	
	Mean Pe		95.9	1.75	0.50	1.85						
		Lbs.	65.82	1.20	0.34	1.27						

	Sample	e Weight -	200 Gram			Sample Weight - 300 Gram				
aun 90.	Wt. of Sampl. Froducts No. in Sack	Clean Whole Beans	Cracked and Broken Beans		Foreign Naterial	Nt. of Products in Cleaning		0il Bearing Naterial	Eulls, Light Beans, Foreign Material	
	Lbs.	Grams	Grams	Grans	Grams	Libs.		Grams	Grams	
4A	68.97 1	192	4.5			31.03	1	6.0	294	
		193	3.0				2	4.5	295.5	
	3	189	4.5				3	6.5	293.5	
	2 3 4	190	4.0			,	Total	17.0	883.0	
	5	186	6.0			Hean P	er Cent	1.89	98.11	
	Total	950	22.0	7.0	21.0		Lbs.	0.59	30.44	
	Mean Per Cent	95.0	2.20	0.70	2.10					
	Lbs.	65.52	1.52	0.48	1.45					
4B	66.24 1	190	4.0			33.76	l	5.0	295	
	2	190	4.0			•••	2	5.5	294.5	
	3	191	3.5		·		3	28.0	272.0	
	4	190	4.0				Total	38.5	861.5	
	5	191	3.5		11111-1	Nean P	er Cent	4.28	95.72	
	Total	952	19.0	8.0	21.0		Lbs.	1.45	32.32	
	Mean Per Cen	t 95.2	1.90	0.80	2.10					
	Lbs	. 63.06	1.26	0.53	1.39					
40	68.84 1	186	5.5			31.16	1	5.0	295	
		190	4.0			7	2	5.0	295	
	2 3 4	190	4.0				3	5.0	295	
	<u></u> ц	189	4.5				Potal	15.0	885	
	5	190	4.0			Mean P	er Cent	1.67	98.33	
	Total	945	22.0	9.0	24.0		Lbs.	0.52	30.64	
	Mean Per Cen	t 94.5	2.20	0.90	2.40			-		
	Lbs		1.51	0.62	1.65					

Products in Sack

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Products in Cleanings

		Weight - 200		Sample Weight - 300 Gram					
Run No.	Wt. of Sample Products No. in Sack	Whole Beans I		Unhulled Segments	*	Nt. of S Products in Cleanings	Sample No.	0il Bearing Material	Hulls, Light Beans, Foreign Material
• •	Lbs.	Grams (lrams	Grams	Grams	Lbs.		Grams	Grams
<u>5</u> & .	69.73 1 2 3 4 5 Total Mean Per Cent Lbs.	93.6 2	5.0 5.5 7.0 5.5 5.0 28.0 2.80 2.80	14.5 1.45 1.01	21.5 2.15 1.50	30.27 Mean Per	l 2 3 Fotal Cent Lbs.	6.0 5.0 <u>6.0</u> 17.0 1.89 0.57	294 295 <u>294</u> 883 98.11 29.70
5B	69.58 2 3 4 5 Total Mean Per Cent Lbs.	93.2 2	5.5 5.0 7.0 5.0 5.0 5.0 27.5 2.75 2.75	11.5 1.15 0.80	29.0 2.90 2.02	30.42 Mean Per	l 2 3 Fotal Cent Lbs.	5.5 5.0 16.0 1.78 0.54	294.5 294.5 295.0 884.0 98.22 29.88
50	69.38 1 2 3 4 5 Total Mean Per Cent Lbs.	92.6 2	6.5 5.5 5.0 5.0 6.5 28.5 2.85 1.98	15.0 1.50 1.04	30.5 3.05 2.12	30.62 Mean Per	l 2 3 Fotal Cent Lbs.	6.0 4.0 <u>6.0</u> 16.0 1.78 0.55	294 296 294 884 98.22 30.07

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Products in Sack

Products in Cleanings

			ducts in Weight -			Products in Cleanings Sample Weight - 300 Gram					
Run No.	Wt. of Products in Sack	Sample No.	Clean Whole Beans	Cracked and Broken Beans		l Foreign Material		Wt. of Products in Cleaning	No.	Oil Bearing Material	Hulls, Light Beans, Foreign Material
64	Lbs. 69.20	1 2 3 4 5	Grams 182 177 186.5 185.0 186	Grams 8.0 11.0 7.0 8.5 7.5	Grams	Grams		Lbs. 30.80 Mean Pe	l 2 3 Total r Cent	Grams 7.0 6.0 8.0 21.0 2.34	Grams 293 294 292 879 97.66
	Mean Per	Total Cent Lbs.	916.5 91.65 63.42	42.0 4.20 2.91	17.0 1.70 1.18	24.5 2.45 1.69			Lbs.	0.72	30.08
68	69.00	1 2 3 4 5	186 187 184 176 180	10.0 7.5 7.0 10.0 12.0				31.00 Mean Pe	1 2 3 Total r Cent	7.0 8.0 <u>7.0</u> 22.0 2.45	293 292 293 878 97•55
	Nean Per	Total	913 91.3 63.00	46.5 4.65 3.21	17.0 1.70 1.17	23.5 2.35 1.62			Lbs.	0.76	30.24
60	68.94	1 2 3 4 5	185 185 184 183 183	8.5 9.0 10.5 9.0				31.06 Mean Pe	1 2 3 Total r Cent	9.5 7.5 <u>7.0</u> 24.0 2.67	290.5 292.5 293 876 97.33
	Mean Per	Total	920 92.0 63.42	45.5 4.55 3.14	16.5 1.65 1.14	18.0 1.80 1.24		- Coll I C	Lbs.	0.83	30.23

TABLE 3

Effect of Disk Speed and Spacing of 5/16 Inch on Whole Capsule

Material of US 74 Castor Beans.

Run No.	Time	Average Disk Speed	Fan Speed	Weight Of Beans	Per Cent Hulled Beans	Unhulled		Unhulled Segments		Per Cent Losses	Capacity of Hulled Beans	
140	Seconds	RPM	RPM	Lbs.	de as	\$	%	%	s	%	Lb/Hr	
1AC 1BC 1CC	722 726 724	180 180 180	900 900 900	65.16 66.30 65.54	99.88 99.88 99.92	0.12 0.12 0.08	0.03 0.03 0.02	0.15 0.15 0.10	0.45 0.60 0.50	0.38 0.33 0.35	325 329 326	
240	450	270	900	65.46	99.92	0.08	0.02	0.10	0.71	0.49	524	
2BC 200	503 504	250 250	900 900	65.70 66.01	99.92 99.92	0.08	0.02	0.10 0.10	0.66	0.49 0.46	470 471	
3AC 3BC	305 374	370 340	960 960	65.07 64.81	99.76	0.24 0.16	0.06	0.30	0.86	0.52	768 624	
300	300	370	960	65.34	99.84	0.16	0.04	0.20	0.66	0.58	784	
4AC	158	500	1000	65.23	99.68	0.32	0.08	0.40	1.66	1.20	1486	
4BC 4CC	229 215	450	1000	64.33 63.87	99.80 99.84	0.20	0.05	0.24	1.25	1.97 1.78	1011 1069	
4DC	210	450	980	64.66	99.72	0.28	0.07	0.35	1.46	0.93	1108	
5AC 5BC	132 134	560 560	1000	65.93 65.20	99.60 99.64	0.40	0.11 0.10	0.51	2.71 2.38	0.71* 1.49*	1798 1752	
500	133	560	1000	66.69	99.52	0.48	0.12	0.60	2.71	1.39	1805	
6AC	85	680	1150	64.76	98.79	1.21	0.32	1.53	6.22	1.12	2740	
6B0 6CC	83 84	680 680	1150 1150	66.42 66.30	99.00 98.97	1.00	0.26 0.28	1.26 1.31	6.26 608	1.43 1.84	2880 2842	

* No. 4 Shutter over screen area of air inlet partially closed. * No. 4 Shutter over screen area of air inlet closed.

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DATA SHEET 2.

Mean Percentages and Pounds of Products Evaluated From Samples

Taken From Whole Capsules Material

Products in Sack Sample Weight - 200 Gram

Run No.	Wt. of Products in Sack	Sample No.	Clean Whole Beans	Cracked and Broken Beans		Foreign Material	Wt. of Products in Cleanings	Sample No.	Oil Bearing Material	Hulls, Light Beans, Foreign Material
lac	Lbs. 65.39	1 2	Grams 197 197	Grams 1.0 1.0	Grams	Grams	Lbs. 34.61	1 2	Grams 2.5 1.5	Grams 297.5 298.5
		2 3 4 5 Total	198 198 <u>197</u> 987	0.5 1.0 <u>1.0</u> 4.5	16		Mean Pe		2.5 6.5 0.72	<u>297.5</u> 893.5 99.28
	Mean Pe		98.7 64.54	0.45 0.29	1.5 0.15 0.10	7.0 0.70 0.46		Lbs.	0.25	34.36
180	66.94	1 2 3 4	196.5 195.5 196.5 194.5	1.0 1.0 1.0 1.5			33.06	1 2 3 Total	2.5 2.0 <u>1.5</u> 6.0	297.5 298.0 298.5 894.0
	Mean Pe		<u>197.0</u> 980.0 98.0	1.5 6.0 0.60	1.5 0.15	12.5 1.25	Mean Per		0.67 0.22	99.33 32.84
100	66.05	Lbs. 1 2 3 4	65.60 196 197 196 197 197	0.40 1.0 1.5 0.5 1.0	0.10	0.84	33.95 Mean Per	1 2 3 Total Cent	2.0 2.5 <u>1.5</u> 6.0 0.67	298 297.5 298.5 894.0 99.33
	Mean Pe	Total r Cent Lbs.	983 98.3 64.93	5.0 0.50 0.33	1.0 0.10 0.07	11.0 1.10 0.73	Moan A GI	Lbs.	0.23	33.72

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Products in Sack Sample Weight - 200 Gram								Products in Cleanings Sample Weight - 300 Gram					
Run No.	Wt. of Products in Sack	Sample No.	Clean Whole Beans	Cracked and Broken Beans	Unhulled Segments	Foreign Material	Prod	lucts	Sample No.	0il Bearing Material	Hulls, Light Beans, Foreign Material		
240	Lbs. 66.15	1 2 3 4 5	Grams 195.5 196.0 194.0 195.5 196.0	Grams 1.5 1.5 1.0 1.5 1.5	Grams	Grams	33.8		1 2 3 Total Cent	Grams 3.5 3.0 <u>2.0</u> 8.5 0.94	Grams 296.5 297.0 298.0 891.5 99.06		
	Mean Pe	Total	977.0 97.7 64.63	7.0 0.70 0.46	1.0 0.10 0.07	15.0 1.50 0.99			Lbs.	0.32	33.53		
2BC	66.23	1 2 3 4 5	196 196 197 195 196	1.0 1.5 1.0 1.5 1.5			33.7 Mea		l 2 3 Total • Cent	2.5 3.0 <u>3.0</u> 8.5 0.94	297.5 297.0 297.0 891.5 99.06		
	Mean Pe	Total r Cent Lbs.	980 98.0 64.90	6.5 0.65 0.43	1.0 0.10 0.07	12.5 1.25 0.83			Lbs.	0.32	33.45		
200	66.59	1 2 3 4 5	195 196 197 197 195	1.5 1.0 1.0 1.0 1.5			33.4 Ma		1 2 3 Total er Cent	3.0 2.0 <u>3.0</u> 8.0 0.89	297 298 <u>297</u> 892 99.11		
	Mean Pe	Total	980 98.0 65.26	6.0 0.60 0.40	1.0 0.10 0.07	13.0 1.30 0.87		rolt + C	Lbs.	0.30	33.11		

Pro	ducts	in	Sacl	K	
Sample	Weight	; -	200	Gram	

Products in Cleanings Sample Weight - 300 Gram

Run No.	Wt. of Sample Products No. in Sack	Whole Beans	Gracked and Broken Beans	Unhulled Segments	Foreign Material	Wt. of Products in Cleaning	Sample No.	0il Bearing Material	Hulls, Light Beans, Foreign Material
3A0	Lbs. 65.62 1 2 3 4 5	Grams 194 196 195 195 195.5	Grams 1.5 1.0 2.5 2.0 1.5	Grams	Grams	Lbs. 34.38 Mean Per	l 2 3 Total r Cent	Grams 2.5 3.5 <u>3.0</u> 9.0 1.00	Grams 297.5 296.5 297.0 891.0 99.00
	Total Mean Per Cent Lbs.	975.5 97.55	8.5 0.85 0.56	3.0 0.30 0.20	13.0 1.30 0.85		Lbs.	0.34	34.04
3BC	65.31 1 2 3 4	196 193 197 196 196	1.5 1.5 1.0 1.5 1.0			34.69 Mean Pe	1 2 3 Total	5.0 3.0 <u>2.5</u> 10.5 1.17	295 297 297.5 889.5 98.83
	Total Mean Per Cent Lbs.	978 97.8	6.5 0.65 0.43	2.0 0.20 0.13	13.5 1.35 0.88	MCan x 0.	Lbs.	0.41	34.28
300	65.95 1 2 3 4	196 196 195 196	0.5 1.5 1.0 1.5			34.05	1 2 3 Total	3.5 2.5 <u>4.0</u> 10.0	296.5 297.5 296.0 890.0
	5 Total Mean Per Cent Lbs.	<u>194</u> 977 97.7 64.43	2.0 6.5 0.65 0.43	2.0 0.20 0.13	14.5 1.45 0.96	Mean Pe	r Cent Lbs.	1.11 0.38	98 .8 9 33.67

		ducts in Sack Weight - 200 Gram		Products in Sample Weight	
Run No.	Wt. of Sample Products No. in Sack	Clean Cracked Whole and Beans Broken Beans	Unhulled Foreign Segments Material	Wt. of Sample Products No. in Cleanings	Oil Hulls, Bearing Light Beans, Material Foreign Material
4AC	Lbs. 65.72 1 2 3 4 5 Total Mean Per Cent Lbs.	Grams Grams 191 4.0 192 3.0 192 4.0 192 2.0 194 3.5 961 16.5 96.10 1.65 63.16 1.08	Grams Grams 4.0 18.5 0.40 1.85 0.26 1.22	Lbs. 34.28 1 2 3 Total Mean Per Cent Lbs.	Grams Grams 6.5 293.5 7.0 293.0 7.0 293.0 20.5 879.5 2.28 97.72 0.78 33.50
480	64.31 1 2 3 4 5 Total Mean Per Cent Lbs.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2.5 19.0 0.25 1.90 0.16 1.22	35.69 1 2 3 Total Mean Per Cent Lbs.	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$
400	64.01 1 2 3 4 5 Total Mean Per Cent5 Lbs.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2.0 19.5 0.20 1.95 0.13 1.25	35.99 1 2 3 Total Mean Per Cent Lbs.	11.0 289.0 9.5 290.5 8.0 292.0 28.5 871.5 3.17 96.83 1.14 34.85
4DC	65.09 2 3 4 5 Total Mean Per Cent Lbs.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.35 15.0 0.23 0.98	34.91 1 2 3 Total Mean Per Cent Lbs.	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$

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		oducts in Sack Weight - 200 Gra	am				n Cleaning t - 300 Gr		
Run No.	Wt. of Sample Products No. in Sack	Clean Crack Whole and Beans Broke Beans	d Segments en	d Foreign s Material	Wt. of Products in Cleanings	No.	0il Bearing Material	Hulls, Light Beans, Foreign Material	
540	Lbs. 67.38 1 2 3 4 5	GramsGrams1895.51895.01904.51875.51866.0		Grams	Lbs. 32.62 Mean Per	1 2 3 Total Cent	Grams 5.0 4.5 <u>3.5</u> 13.0 1.44	Grams 295 295.5 296.5 887.0 98.56	
	Total Mean Per Cent Lbs.	941 26.5 94.1 2.65 63.40 1.79	5.0 0.50	27.5 2.75 1.85		Lbs.	0.47	32.15	
580	65.88 1 2 3 4 5	1905.01894.01905.01895.01904.5			34.12 Mean Per	1 2 3 Total Cent	9.0 7.5 9.0 25.5 2.83	291.0 292.5 291.0 874.5 97.17	
	Total Mean Per Cent Lbs.	948 23.5 94.8 2.35	4.5 0.45	24.0 2.40 1.58		Lbs.	0.97	33.15	•
500	67.05 1 2 3 4 5	1905.51887.01914.01904.51906.0			e 32.95 Mean Per	1 2 3 Total Cent	7.5 10.0 <u>8.0</u> 25.5 2.83	292.5 290.0 <u>292.0</u> 874.5 97.17	
	Total Mean Per Cent Lbs.	949 27.0 94.9 2.70 63.63 1.81	6.0 0.60	18.0 1.80 1.21		Lbs.	0.93	32.02	

m No.	Wt. of Products in Sack	Sample No.	Clean Whole Beans	Cracked and Broken Beans		l Foreign Material	Wt. of Products in Cleanings	No.	0il Bearing Material	Eulls, Light Beans, Foreign Material
	Lbs.		Grams	Grans	Grams	Grams	Lbs.		Grams	Grams
C	65.82	1	177	15			34.18	1	7.0	293
		2	178	13				2	6.0	294
		3	184	10.5				3	6.0	294
		2 3 4	176	13.5				Total	19.0	881
		.5	185	9.0		the second s	Mean Per		2.11	97.89
		Total	900	61.0	15.0	24		Lbs.	0.72	33.46
	Mean Per	r Cent	90.0	6.10		2.40			and the second second	a and the second second
		Lbs.	59.24	4.02		1.58				
BC	67.02	1	183	11.0			32.98	1	8.0	292
		2	181	12.5				2	11.0	289
		2 3 4	179	14.0				3	7.0	293
			179	13.5				Total	26.0	874
		5	183	11.0			Mean Per	Cent	2.89	97.11
		Total	905	62.0		20.5		Lbs.	0.95	32.03
	Mean Per	r Cent	90.5	6.20		2.05				
		Lbs.	60.65	4.16	0.84	1.37				
500	66.63	1	183	11.0			33.37	1	7.0	293
		2	178	15.0				2	12.0	288
		3	180	12.5				3	14.0	286
		4	185	9.5				Total	33.0	867
		5	180	12.5			Mean Per	· Cent	3.67	96.33
	1	Total	906	60.5	13.0	20.5		Lbs.	1.22	32.15
	Mean Per	Cent	90.6	6.05		2.05				
		Lbs.	60.37	4.03		1.37				

TABLE 4

Effect of Bisk Speed and Spacing of 5/16 Inch on

Segment Material of US 74 Castor Beans.

Run No.	Time	Average Disk Speed	Fan Speed	Weight Of Beans	Per Cent Hulled Beans	Beans in Unhulled		Unhulled Segments		Per Cent Losses	Capacity of Hulled Beans
	Seconds	RPM	RPM	Lbs.	B	ø	- CELICITOS	7	- Casso	Þ	Lb/Hr
las	410	180	900	76.59	99.75	0.25	0.06	0.31	0.55	0.34	672
1BS	450	160	900	76.84	99.83	0.17	0.04	0.21	0.97	0.57	615
1CS	423	175	900	76.48	99 •79	0.21	0.05	0.26	0.66	0.30	650
2AS	249	285	920	76.41	99.67	0.33	0.09	0.42	0.77	0.24	1105
2BS	302	240	920	76.37	99 •75	0.25	0.07	0.32	0.66	0,24	9 10
205	331	220	920	76.48	99.75	0.25	0.07	0.32	0.60	0.31	832
2DS	263	260	920	76.84	99.71	0.29	0.08	0.37	0.66	0.29	1052
3AS	177	360	960	76.68	99 •59	0.41	0.11	0,52	1.08	0.31	1560
3BS	174	365	960	76.54	99.58	0.42	0.11	0.53	1.08	0.34	1584
30 S	170	370	960	76.31	99•58	0.42	0.11	0.53	1.18	0.33	1616
4AS	114	440	1000	76.70	99 .50	0.50	0.13	0.63	1.28	0.81	2422
4BS	114	440	1000	76.24	99.42	0.58	0.15	0.73	1.44	0.96	2407
4CS	124	430	1000	76.20	99 •55	0.45	0.13	0.58	1.28	0,92	2 212
5AS	72	550	1000	76.12	99,21	0.79	0.21	1.00	2.45	0.55	3806
5BS	72	550	1000	76.71	99.17	0.83	0.22	1.05	2.08	0,61	3836
5CS	72	550	1000	76.33	99 .18	0.82	0.22	1.04	2.34	0.79	3816
6AS	62	650	1150	76.87	98 .92	1.08	0.28	1.36	5.64	1,08	4463
6BS	62	650	1150	76.46	98 .76	1.24	0.33	1.57	4.26	1.11	4440
6 CS	62	6 50	1150	76.06	98.92	1.08	0.29	1.37	5.91	1,22	4417

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DATA SHEET 3.

Mean Percentages and Pounds of Products Evaluated From Samples

Taken From Segment Material

Products in Sack Sample Weight - 200 Gram

Products in Cleanings Sample Weight - 300 Gram

Run No.	Wt. of Sample Products No. in Sack	Clean Crack Whole and Beans Broke Beans	l Segnents Material en	Wt. of Sample Products No. in Cleanings	0il Hulls, Bearing Light Beans, Material Foreign Material
145	Lbs. 76.54 1 2 3 4 5	GramsGrams1971.51972.51981.01981.01972.0	s Grams Grams	Lbs. 23.46 1 2 3 Total Mean Per Cent	Grams Grams 3.5 296.5 3.0 297 3.5 296.5 10.0 890.0 1.11 98.89
	Fotal Nean Per Cent Lbs.	987 8.0 98.7 0.80 75.54 0.61	3.0 2.0 0.30 0.20 0.23 0.16	Lbs.	0.26 23.20
1B\$	76.74 1 2 3 4	196 2.0 197 2.0 196 3.0 197 2.0		23.26 1 2 3 Total	5.0 295 3.0 297 9.0 291 17.0 883
	Total Mean Per Cent Lbs.	197 2.0 196 3.0 982 12.0 98.2 1.20 75.36 0.92	2.0 4.0 0.20 0.40 0.15 0.31	Mean Per Cent Lbs.	1.89 98.11 0.44 22.82
105	76.56 1 2 3 4	197 1.5 197 2.0 196 2.5 197 1.5		23.44 1 2 3 Total	3.0 297 3.0 297 3.0 297 9.0 891
	5 Total Mean Per Cent Lbs.	198 1.5 985 9.0 98.5 0.90 75.41 0.69	2.5 3.5 0.25 0.35 0.19 0.27	Mean Per Cent Lbs.	1.00 99.00 0.23 23.21

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		ducts in S Weight - 2			Products in Cleanings Sample Weight - 300 Gram					
Run No.	Wt. of Sample Products No. in Sack	Clean Whole Beans	Gracked and Broken Beans	Unhulled Segments	Foreign Material	Wt. of Products in Cleanings	Sample No.	0il Bearing Material	Hulls, Light Beans, Foreign Material	
2AS	Lbs. 76.76 1 2 3 4 5	Grams 196 195 197 197 195	Grams 1.5 3.0 1.5 1.5 2.5	Grams	Grans	Lbs. 23.24 Mean Per	l 2 3 Total Cent	Grams 2.0 2.5 2.5 7.0 0.78	Grams 298 297.5 297.5 893.0 99.22	
	Total Mean Per Cent Lbs.	980 98.0 75.22	10.0 1.00 0.77	4.0 0.40 0.31	6.0 0.60 0.46		Lbs.	0.1 8	23.06	
BS	76.55 1 2 3 4 5	196 196 198 197 197	2.0 1.5 1.0 2.0 1.5			23.45 Mean Per	l 2 3 Total Cent	2.5 2.0 2.5 7.0 0.78	297.5 298.0 <u>297.5</u> 893.0 99.22	
	Total Mean Per Cent Lbs.	984 98.4 75.32	9.0 0.9 0.69	3.0 0.30 0.23	4.0 0.40 0.31		Lbs.	0.18	23.27	
205	76.52 1 2 3 4 5	197 196 197 197.5 	2.0 2.0 1.5 1.0			23.48 Mean Per	l 2 3 Fotal Cent	3.0 3.5 2.5 9.0 1.00	297 296.5 297.5 891 99.00	
	Total Nean Fer Cent Lbs.	985.5 98.55 75.41	8.5 0.85 0.65	3.0 0.30 0.23	3.0 0.30 0.23		Lbs.	0.24	23.24	
2DS	76.87 1 2 3 4 5 Total	197 197 196 199 196	2.0 1.5 2.5 1.0 2.0			24 .1 3 Mean Per		3.5 2.5 <u>2.0</u> 8.0 0.89	296.5 297.5 298.0 892.0 99.11	
	Total Mean Per Cent Lbs.	985 98.5 75.72	9.0 0.90 0.69	3.5 0.35 0.27	2.5 0.25 0.19		Lbs.	0.22	23.91	

		roducts in Weight -				Products in Cleanings Sample Weight - 300 Gram				
 Run No.	Wt. of Sample Products No. in Sack) Clean Whole Beans	Gracked and Broken Beans		l Foreign Material	Wt. of Sample Products No. in Cleanings	0il Bearing Material	Hulls, Light Beans, Foreign Material		
3 8 5	Lbs. 76.91 1 2 3 4 5	Grams 196 194 194 196 195	Grams 2.5 2.0 3.5 2.5 2.5	Grams	Grams	Lbs. 23.09 1 2 3 Total Mean Per C ent	Grams 3.0 4.0 2.5 9.5 1.06	Grams 297 296 <u>297.5</u> 890.5 98.94		
	Total Mean Per Cent Lbs.	977 97•7 75•14	13.0 1.30 1.00	5.0 0.50 0.38	5.0 0.50 0.38	Lbs.	0.24	22.85		
3BS	76.86 1 2 3 4 5	193 194•5 196 196 196	3.5 3.0 2.0 2.0 2.5	۵		23.14 2 3 Total Mean Per Cent	2.5 4.0 <u>3.5</u> 10.0 1.11	297•5 296 <u>296•5</u> 890 98•89		
	Total Mean Per Cent Lbs.	9 75•5 97•55 74•98	13.0 1.30 1.00	5.0 0.50 0.38	6.5 0.65 0.50	Lbs.	0.26	22.88		
308	76.61 1 2 3 4 5	195 196 .5 195 194.5 194	3.5 2.0 3.0 3.0 2.5			23.39 1 2 3 Total Mean Per Cent	4.5 2.5 <u>2.5</u> 9.5 1.06	295.5 297.5 297.5 890.5 98.44		
	Total Mean Per Cent Lbs.	975 97•5 74•69	14.0 1.40 1.07	5.0 0.50 0.38	6.0 0.60 0.46	Lbs,	0.25	23.14		

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Products in Sack Sample Weight ~ 200 Gram							Products in Cleanings Sample Weight - 300 Gram					
Run No.	Wt. of Products in Sack	Sample No.	Clean Whole Beans	Cracked and Broken Beans	Unkulled Segments	Foreign Material	Wt. of Products in Cleanings	Sample No.	0il Bearing Material	Hulls, Light Beans, Foreign Material		
	Lbs.		Grams	Grams	Grams	Grams	Lbs.		Grams	Grams		
4AS	76.64	1	193	4.0			23.36	1	8.0	292		
		2	195	3.5				2	7.0	293		
		3 4	195	2.5			·	3	9.0	291		
			196	2.5			-	Total	24.0	876		
		_ 5	194	2.5			Mean Per		2.67	97.33		
	6 ग	Total	973	15.0	6.0	6.0		Lbs.	0.62	22.74		
	Mean Pe		97•3	1.50	0.60	0.60						
		Lbs.	74.57	1.15	0.46	0.46						
4BS	76.19	1	194	3.0			23,81	1	9.0	291		
	,	2	194	3.5				2	10.0	290		
		3	193	4.0				3	8.5	291.5		
		4	195	2.5			, i	Potal	27.5	872.5		
		5	193	3.5			Mean Per	Cent	3.06	96.94		
		Total	969	16.5	7.0	7.5		Lbs.	0.,73	23,08		
	Mean Pe	r Cent	96.9	1.65	0.70	0.75			- -			
		Lbs,	73.83	1.26	0.53	0.57						
4 C S	76.09	1	194	3.0			23,91	1	11.5	288.5		
• • •	1-0-0	2	195	4.0			~	2	7.0	293		
		3	195	2.5				3	.8.0	292		
		4	194	3.0			ł	Total	26.5	873.5		
		5	195	2.5			Mean Per		2.94	97.06		
		Total	973	15.0	5.5	6.5		Lbs.	0.70	23.21		
	Mean Pe		97.3	1.50	0.55	0.65				* • • • •		
		Lbs.	74.03	1.14	0.42	0.49						

Products in Sack

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Products in Cleanings

Products in Cleanings Sample Weight - 300 Gram

Run I	No. Wt. of Products in Sack	Sample No.	Clean Whole Beans	Cracked and Broken Beans	Unhulled Segments	Foreign Material	Wt. of Products in Cleanings	Sample No.	0il Bearing Material	Hulls, Light Beans, Foreign Material
5AS	Lbs. 76.51 Mean Per	l 2 3 4 5 Total Cent Lbs.	Grams 192 193 191 190 <u>190</u> 956 95.6 73.14	Grams 5.0 4.5 5.0 6.5 5.0 26.0 2.60 1.99	Grams 9.5 0.95 0.73	Grams 8.5 0.85 0.65	Lbs. 23.49 Mean Per	l 2 3 Total Cent Lbs.	Grams 4.5 5.5 <u>6.0</u> 16.0 1.78 0.42	Grams 295.5 294.5 294 884 98.22 23.07
5BS	77.06 Mean Per	l 2 3 4 5 Total	192 193 190 192 <u>192</u> 959 95.9 73.90	4.0 4.5 5.0 4.5 4.5 22.5 2.25 1.73	10.0 1.00 0.77	8.5 0.85 0.65	22.94 Mean Per	l 2 3 Total Cent Lbs.	5.0 6.0 <u>7.5</u> 18.5 2.06 0.47	295 294 292.5 881.5 97.94 22.47
505	76.43 Mean Per	1 2 3 4 5 Total	191 191 193 190 <u>193</u> 958 95.8 73.22	5.5 5.0 4.5 5.5 4.5 25.0 2.50 1.91	10.0 1.00 0.76	7.0 0.70 0.54	23.57 Mean Per	l 2 3 Total Cent Lbs.	8.5 8.0 <u>6.5</u> 23.0 2.56 0.60	291.5 292 <u>293.5</u> 877 97.44 22.97

Products in Sack Sample Weight - 200 Gram

		oducts in Weight -			Products in Cleanings Sample Weight - 300 Gram					
Run No.	Wt. of Sample Products No. in Sack	Clean Whole Beans	Cracked and Broken Beans		Foreign Material	Wt. of Products in Cleanings	Sample No.	0il Bearing Material	Hulls, Light Beans, Foreign Naterial	
645	Lbs. 76.90 1 2 3 4	Grans 180 185 188 187	Grams 15.0 11.5 8.0 8.0	Grams	Grams		l 2 3 Total	Grams 10.5 11.0 <u>11.0</u> 32.5	Grams 289.5 289 289 867.5	
	5 Total Mean Per Cent Lbs.	<u>182</u> 922 92 .2 70.90	14.0 56.5 5.65 4.35	13.0 1.30 1.00	8.5 0.85 0.65	Mean Per	Lbs.	3.61 0.83	96 .3 9 22 .27	
6 B S	76.20 1 2 3 4 5	189 186 187 190 <u>185</u>	7.5 10.0 9.5 7.5 9.0			23.80 Mean Per	l 2 3 Total Cent	9.0 15.0 <u>8.0</u> 32.0 3.56	291 285 <u>292</u> 868 96.44	
	Total Mean Per Cent Lbs.	937 93.7 71.40	43.5 4.35 3.31	15.0 1.50 1.14	8.5 0.85 0.65		Lbs.	0.85	22.95	
605	76.18 1 2 3 4 5	188 1 7 9 180 188 182	9.0 16.5 15.0 8.0 10.5			23.82 Mean Per	l 2 3 Total Cent	14.0 7.0 <u>14.0</u> 35.0 3.89	286 293 <u>286</u> 865 96.11	
	Total Mean Per Cent Lbs.	917 91.7 69.86	59.0 5.90 4.49	13.0 1.30 0.99	11.0 1.10 0.84		Lbs.	0.93	22.89	

the unhulled segments. K is the term commonly referred to as the hulling percentage of the material or variety of beans. The value of K was found from an actual population of unhulled segments that were saved during the sampling of the products. A sample of 300 grams of unhulled segments was used in which the actual weight of beans found by hulling with the small hand huller was 237 grams. This gave a value of K = 237/300 = 0.79, which was used in all computations.

Let R = Actual weight in pounds of beans in test weight that were unhulled. Then $R' = R - (C_s + C_{cb})$.

Let H = Actual weight in pounds of beans hulled by the disks in machine.

 $\mathbb{H} = \mathbb{A} + \mathbb{B} + \mathbb{E} - (\mathbb{C}_{s} + \mathbb{C}_{cb})$

Then PER CENT HULLED REANS = $H/R' \ge 100$ Also the PER CENT HULLED BEAMS = $(1 - KC/R') \ge 100$, where $KC/R' \ge 100$ equals PER CENT BEAMS IN UN-EVALUED SEGMENTS, which is also equal to $(1 - K/R') \ge 100$. Both the above values, per cent hulled beams and per cent beams in unhulled segments give the same relationship on the effect of disk speed except that one expresses the performance on a high percentage level (per cent hulled beams) and the other on a low percentage level (per cent beams in unhulled segments). Since they are generally found expressed either way, both values were included in this study.

PER CENT ATTACHED HULLS IN UNHULLED SEGMENTS = $(C - KC/R^{\dagger}) \times 100$. This value was included in the results because after the foreign material has been removed the attached hulls are the only material remaining which tend to lower the quantity of oil obtained from the beans. This per cent should be kept as low as possible.

PER CENT UNHULLED SEGMENTS (beans plus attached hulls) = $C/R' \times 100$. PER CENT CRACKED AND BROKEN BEANS = $\frac{B - C_{CD}}{R'} \times 100$.

It should be recognized that this per cent cracked and broken neglects the small percentage that is cracked and broken which may have been pulled off in the cleanings by the air velocity. This small percentage is included in the oil bearing material.

CAPACITY OF HULLED BEANS (LB/RR) = $\frac{R \times 3600}{\text{Time(Sec)}}$

The capacity is computed on the total weight in pounds of beans that went through the huller without correcting for the beans hulled in the test weight.

PER CENT LOSSES OR PER CENT OIL BEARING = E/R x 100.

This value was included to show the overall performance of the machine cycle for the various settings of disk speed, fan speed, shutter and damper openings, because even though the disks may be doing a good job of hulling the complete unit may be performing very poorly.

An example of the calculation of these values is taken from Run 1A.

From Data Sheet 1: Clean whole beans -A = 66.49 lbs. Cracked and broken beans -B = 0.86 lbs. Unhulled segments -C = 0.17 lbs. Oil bearing material -E = 0.57 lbs.

From Table 1: $G_{s} = 4.06$ lbs. $G_{cb} = 0.57$ lbs.

R = A + B + KC + E = 66.49 + 0.86 + (0.79)(0.17) + 0.57 = 68.06 lbs. $R' = R - (C_s + C_{cb}) = 68.06 - (4.06 + 0.57) = 63.43 lbs.$ $H = A + B + E - (C_s + C_{cb}) = 66.49 + 0.86 + 0.57 - (4.06 + 0.57) = 63.29 lbs.$ Per cent Hulled Beans = H/R' x 100 = 63.29/63.43 x 100 = 99.79%

$$= (1 - KC/R') \times 100 = (1 - 0.79 \times 0.17) \times 100 = 99.79\%$$
63.43

Per cent Beans in Unhulled Segments = KC/R' x 100

$$= \frac{(0.79)(0.17)}{63.43} \times 100 = 0.21\%$$

or

$$= (1 - H/R^{1}) \times 100$$

$$= (1 - 0.9979) \times 100 = 0.21\%$$

Per cent Attached Hulls in Unhulled Segments = (C - KC/R') x 100

$$= (0.17 - 0.79 \times 0.17) \times 100 = 0.06\%$$

Per cent Unhulled Segments = 0/R' x 100 = 0.17/63.43 x 100 = 0.27%

Per cent Gracked and Broken Beans = $\frac{B - C_{cb}}{R!} \times 100 = \frac{0.86 - 0.57}{63.43} \times 100^{-2} = 0.46\%$

Capacity of Hulled Beans (1b/hr) = $\frac{R \times 3600}{Time} = \frac{68.06 \times 3600}{493} = 497$ 1b/hr

Per cent Losses = $E/R \ge 100 = 0.57/68.06 \ge 100 = 0.84\%$

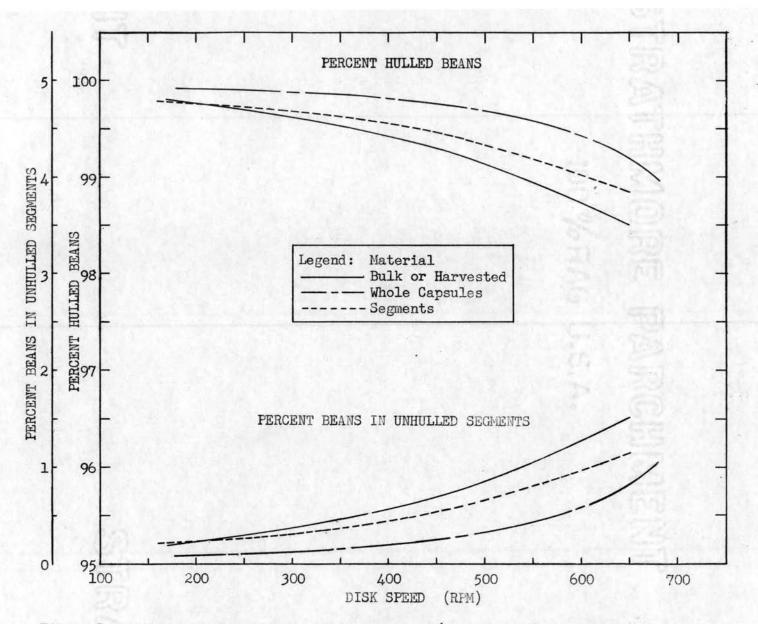


Figure 13. Effect of Disk Speed and Spacing of 5/16 inch on Percent Beans In Unhulled Segments and Percent Hulled Beans.

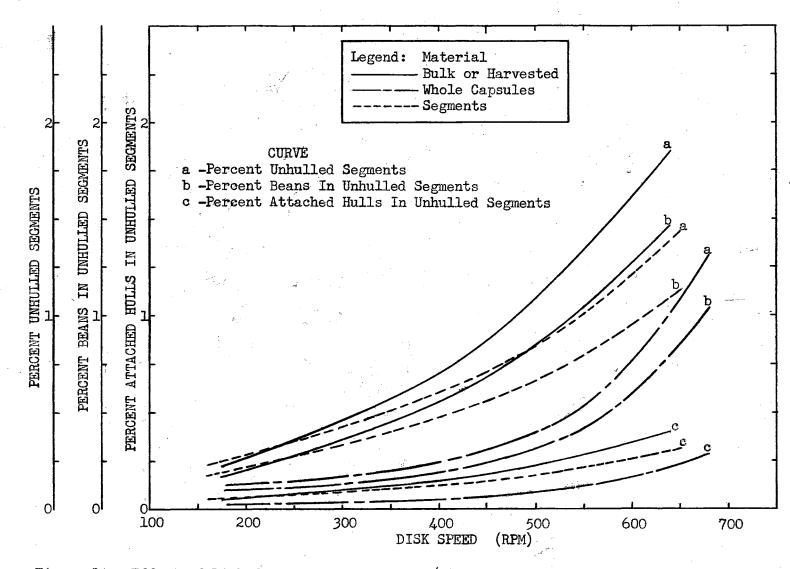


Figure 14. Effect of Disk Speed and Spacing of 5/16 inch on Percent Unhulled Segments, Percent Beans in Unhulled Segments, and Percent Attached Hulls in Unhulled Segments.

6

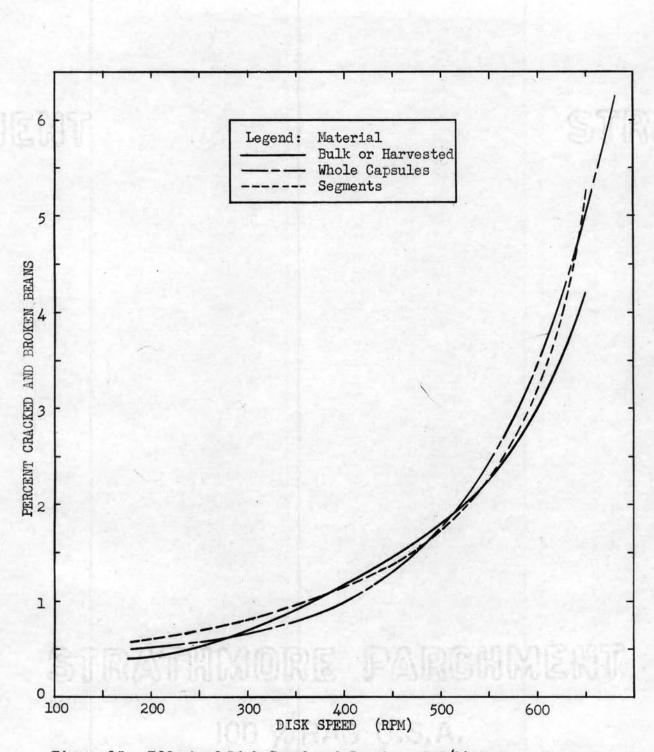
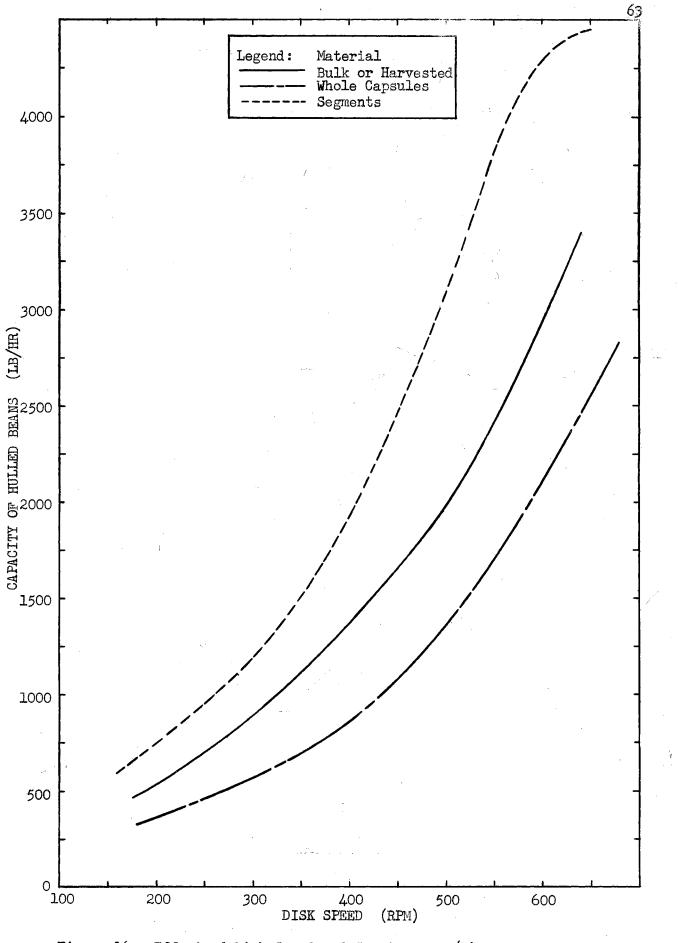
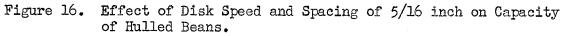


Figure 15. Effect of Disk Speed and Spacing of 5/16 inch on Percent Cracked and Broken Beans.





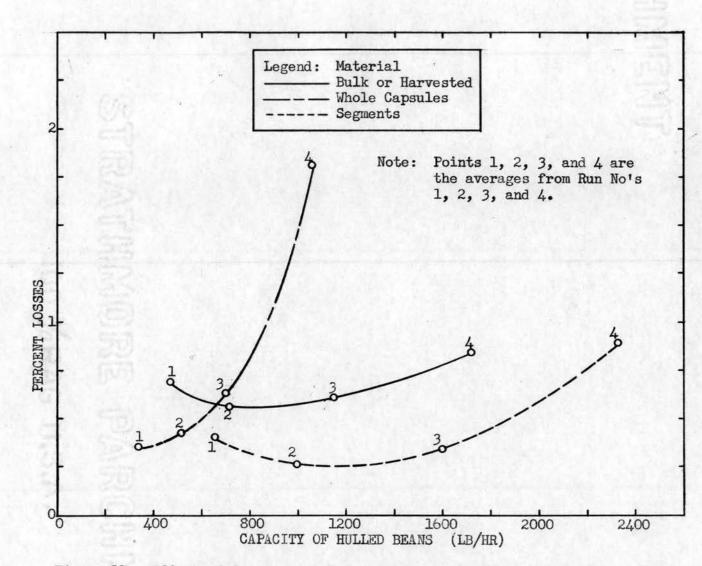


Figure 17. Effect of Capacity on Percent Losses obtained with Settings of Fan Speed, Shutter Openings, and Damper Opening for Runs 1, 2, 3, and 4.

VII. DISCUSSION OF RESULTS

In discussing the effect of disk speed on the various factors recorded in the analysis of the data, it should be kept in mind that these values were obtained under the controlled testing conditions as listed in Part V, methods of making tests and observations.

The results obtained from the sampling data sheets are recorded in Tables 2, 3 and 4. As was mentioned previously the sampling technique for obtaining the sampling data was planned so that a statistical analysis could be made if it was considered necessary. It is believed that the values obtained from the three runs for each disk speed give as accurate an estimation of the actual population as is required in this study; hence no statistical analysis was made to determine whether or not a sufficient number of samples were taken from the products in the sack and in the cleanings for each run. A study of these results shows that perhaps the greatest error in the reported values would be from failure to obtain enough representative samples; however no relation as to the per cent of error in sampling was made on the recorded data.

A. PER CENT HULLED BEANS AND PER CENT BEANS IN UNHULLED SEGMENTS

The factors determined in the analysis of the data are presented graphically in Figures 13 through 17. Figure 13 shows the effect of disk speed on per cent hulled beans and per cent beans in unhulled segments and the effect the different materials have on these percentages. At low disk speeds the per cent hulled beans has a maximum value of 99.75 to 99.90% and

it is obvious that the per cent unhulled beans will have a minimum value of 0.10 to 0.25% for any of the three materials tested. As the disk speed is increased the per cent hulled beans tends to decrease and the per cent beans in unhulled segments will increase. Whole capsules material had the highest per cent hulled, followed by segments and then the bulk or harvested materials. An important cause contributing to the fact that a higher per cent hulled is obtained with the whole capsules is that the capacity of hulled beans at a given disk speed is much lower than that of either the segments and bulk or harvested material. Referring to Tables 2, 3, and 4 or to Figure 16 and comparing the materials at the same capacity of hulled beans for different disk speeds, the per cent hulled beans obtained with the whole capsules is more nearly equal to that of the segments and the bulk or harvested material. Considering the lowest permissible per cent of hulled beans to be around 98%, none of the disk speeds used in this study are limited by this factor since the actual performance of the castor bean huller showed a minimum of 98.50% with the bulk or harvested material at the maximum disk speed of 650 rpm.

B. PER CENT UNHULLED SEGMENTS

Figure 14, shows the effect of disk speed on the per cent unhulled segments and its component parts, per cent beans in unhulled segments and per cent attached hulls in unhulled segments. Hence for any particular disk speed and material the ordinate of curve c plus the ordinate of curve b must equal the ordinate for curve a. The per cent unhulled segments was divided into these two parts for the purpose of illustrating how small the actual per cent of attached hulls are that the unhulled segments contain. At high disk speeds a maximum value of 0.40% of attached hulls was found with the bulk or harvested material. This percentage should be kept as

low as possible as the attached hulls on the unhulled segments are the only foreign material which tend to lower the quantity of oil obtained at the extraction mills. These values are minimum at low disk speeds and gradually increase as the disk speed increases.

The poorest performance occurred with the bulk or harvested material and since it contained more trash and foreign material than the whole capsules and segments, it would seem that this additional trash may have influenced the values obtained with the bulk or harvested material. However, if 2% unhulled segments is considered as the maximum value acceptable for good performance with this type of huller, any disk speed with the speed range tested will give satisfactory results.

C. PER CENT CRACKED AND BROKEN BEANS

Figure 15 shows the relationship of disk speed on the per cent cracked and broken beans for the three types of material tested. It is evident that the different materials have very little effect on the per cent cracked and broken beans as the disk speed is varied. At the lowest disk speed between 0.40 to 0.60% was cracked and broken and at the highest disk speed between 4 to 6% was cracked and broken for the materials tested. At the higher disk speeds the capacity tends to increase and it is possible that there is a definite relation between the per cent cracked and broken to the capacity of the disks. Some evidence of this possibility is found by studying Tables 2, 3, and 4.

If 2% cracked and broken is arbitrarily selected as the maximum permissible value for satisfactory performance of the hulling disks, the maximum speed at which the disk should be operated is 525 rpm. The per cent cracked and broken should be kept as low as possible since whenever the seed coat is cracked rapid deterioration of the oil in the bean itself

occurs before it reaches the extraction mill.

D. CAPACITY OF HULLED BEANS

Figure 16 shows the effect of disk speed on the capacity of hulled beans in pounds per hour and the effect of the different materials tested on the capacity of the disks. There is a difference between the various materials and from Figure 16 the order of materials of increasing capacities for a particular disk speed is whole capsules, bulk or harvested material, and segments. An important cause of the larger capacity with the segments is the fact that the segments will pass directly between the hulling surfaces where the bulk or harvested material and whole capsules require a time interval to break the material into segments before they can pass through the disks. In addition to this time required a higher degree of wedging action occurs that tends to lower the capacities of these materials below that obtained with segments. The whole capsules material had a lower capacity than the bulk or harvested material and by referring to Table 1 it is seen that the bulk or harvested material consisted primarily of segments; therefore causing the capacity of the bulk or harvested material to be greater than the whole capsules material. A capacity of 2825 lb/hr at a disk speed of 680 rpm was obtained with the whole capsules while a capacity of 3400 lb/hr at a disk speed of 640 rpm was obtained with the bulk or harvested material. The curve for the segments tends to level off at a disk speed around 550 rpm and at the maximum disk speed of 650 rpm a capacity of 4450 lb/hr was obtained. The leveling off of this curve may indicate that the hulling area of the disks is approaching its maximum capacity.

E. PER CENT LOSSES

Figure 17 shows the effect of capacity on per cent losses as obtained

with the settings of fan speed, shutter openings over screen area, and damper or opening for runs 1, 2, 3, and 4. The settings correspond to those that were determined from the results of the preliminary investigations with bulk or harvested material. The per cent losses is a function of the air velocity and the air velocity required is a function of the capacity. The air velocity is dependent upon the fan speed, shutter openings over screen area, and damper opening. The curves were plotted for only the first four runs since with these runs the fan speed alone was varied to try to maintain approximately constant per cent losses as the capacity increased. With runs 5 and 6 the position of shutters and damper opening as well as the fan speed were changed to provide the necessary air velocity for removal of the hulls and chaff.

These curves give the overall performance of the castor bean huller for each setting. By comparing the points corresponding to the same settings for each run number, the effect of air velocity on the per cent losses for the different capacities can be determined. For example by considering the points numbered 4 where the air velocity is the same for all three curves it is evident that for the whole capsules the air velocity was too high for the capacity obtained; thereby resulting in a higher per cent losses than with either the bulk or harvested and segment materials. This indicates that preliminary investigations should have been made separately with each material tested so as to obtain the proper air velocity corresponding to the capacity of the disk at the different disk speeds. A maximum of 1.85% losses was obtained at run number 4 for the whole capsules material.

The per cent losses for the segments follow a curve similar to that of the bulk or harvested material; however the per cent losses are some-

what smaller than that obtained with the bulk or harvested material. A minimum of 0.25% losses was obtained with the segment material. Since smaller per cent losses were obtained with the segments it is evident that the fan speed for each setting was greater than was needed for the capacities of the bulk or harvested material.

Referring to Table 2, Run 4B shows the effect of decreasing the area of air inlet which increases the air velocity in the Y-cleaner and tends to pull over a higher percentage of material. The same effect occurred in Table 3 in Runs 5AC and 5BC.

Since the preliminary investigations were made with only the bulk or harvested material the per cent losses for this curve approached a straight line. With this evidence at hand it would seem that, regardless of the material tested, the air velocity could be maintained so that the per cent losses could be held approximately constant as the capacity increases. This air velocity can be obtained by correct settings of the fan speed shutter openings over screen area, and damper opening. The per cent losses with the bulk or harvested material were held under 1%.

VIII. SUMMARY AND CONCLUSIONS

In summarizing the information contained in this study it is evident that the effect of disk speed is an important cause on the per cent hulled, per cent cracked and broken, and the capacity of the machine; however these characteristics are also affected by other variables which were held constant in this study. These variables are: moisture content of the beans, spacing or clearance between the disks, width of disk and hardness of rubber used on the disks. Since these variables were kept constant the conclusions drawn from this study pertain only to the effect of disk speed. To facilitate arriving at conclusions for these other variables requires further research.

The conclusions made from the present investigation are as follows: A. OPERATING DISK SPEED

1. The per cent hulled beans was above 98% and it is obvious that the per cent beans in unhulled segments was lower than 2% for any disk speed between the range investigated.

The per cent attached hulls in the unhulled segments was low for all the disk speeds; therefore this factor will have very little effect on the quantity of oil obtained at the extraction mills.

The per cent unhulled segments (beans plus attached hulls) was less than 2% for all speeds. Since 2% unhulled segments or 98% hulled is established commercially as the maximum and minimum permissible values, the selection of any disk speed within the range tested is acceptable.

- 2. The per cent cracked and broken beans varied from 0.50% to 6% as the disk speeds increase for the range of disk speeds used. The selection of the proper disk speed for a certain per cent cracked and broken is dependent upon an economic balance between the spoilage of the cracked and broken beans and the capacity of the disks. If a minimum amount of spoilage is desired this per cent should be kept as low as possible. On the other hand if capacity is desired additional spoilage of the cracked and broken beans is considered maximum to prevent excessive losses through spoilage, a maximum permissible disk speed should be around 500 rpm.
- 3. The capacity of the disks increased for the three materials tested as the speed increased. At a capacity of 4250 lb/hr the capacity of the hulling surfaces of the disks tend to approach a maximum value.
- 4. After selecting a desirable operating disk speed the relationship of per cent losses can be controlled by proper adjustments of the fan speed, shutter openings over screen area and damper opening so as to control the necessary air velocity to give good cleaning at the capacity at which the disks are operating,

B. TYPE OF MATERIAL

1. There is no important difference between the per cent hulled beans since 98% can be obtained with any of the materials. However it is seen that the whole capsules have the highest per cent hulled and an important cause is that the bevel on the rotating

disk tends to hull them before they pass through the disks.

- 2. There is no essential difference between the per cent cracked and broken beans with the different materials.
- 3. There is a difference between the capacities of the materials. The segments have a much greater capacity than either the whole capsules and bulk material; therefore it would be desirable to increase the bevel on the rotating disk so as to increase the capacity of these other materials.
- 4. There is no effect upon the per cent losses with different materials if the machine is properly adjusted.

C. PROPOSALS FOR FURTHER STUDY

Since in this study the performance of the castor bean huller dealt only with the effect of disk speed under the specified test conditions, it is obvious that further research is necessary to determine the performance of the castor bean huller when tested at different conditions. Much information is needed to determine the relationship of other factors on the performance of the castor bean huller.

The proposals for further work for determining the overall performance of the castor bean huller when operated at different conditions are as follows:

- 1. To determine the effect of the variety, maturity, and moisture content of the beans.
- 2. To determine the effect of spacing or clearance between the disks.
- To determine the effect of the width of the rubber facing on the disks, amount of bevel, size and hulling area of the disks.
 To determine the effect of rubber hardness used on the disks.
 To determine the effect of the rate of feeding the unhulled beans.

6. To determine the size of cleaning unit to provide the proper air velocity to give minimum per cent losses at various capacities.

Any one of the above variables should be determined independently of the others, so as to make it possible to evaluate its effect on the performance of the castor bean huller.

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APPENDIX

RESULTS OF PRELIMINARY INVESTIGATIONS WITH BULK OR HARVESTED MATERIAL

FOR DETERMINING OPERATING CONDITIONS.

See Flow Diagram of Products For Shutter Numbers

Run No.	Desired Disk Speed Under Operating Conditions	Approximate Setting Of Disk Speed When Empty	Approximate Fan Speed Under Operating Conditions	Position of Shutters	Approximate Damper Opening
	RFM	RPM	RPM		
1	150	180	900	All Open	1"
2	250	280	900	All Open	1"
3	350	380	96 0	All Open	1"
4	450	480	1000	All Open	1#
5	550	590	1000	4 Closed	1 5 "
6	650	740	1200	4 Closed	2 [#]

and Damper Opening

It should be recognized that in order to obtain the desired disk speeds under operating conditions the approximate setting of disk speed when empty had to be set fast enough to account for the losses in belt friction, bearings, and the torque-speed characteristic of the huller engine.

THESIS TITLE: THE EFFECT OF DISK SPEED ON THE PERFORMANCE OF AN EXPERIMENTAL CASTOR BEAN HULLER

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