MODIFICATION OF A MATTAUCH-HERZOG GEOMETRY MASS

SPECTROMETER FOR IMPROVED RESOLUTION

ION KINETIC ENERGY

SPECTROMETRY

Ву

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CHAPTER I

INTRODUCTION

According to the theory of mass spectra developed by Rosenstock, et al., (1) the ionization process via electron impact is assumed to be a vertical process, following the Franck-Condon principle. The molecular ions formed have finite amounts of excitational energy distributed in their electronic, vibrational and/or rotational degrees of freedom. It is assumed that the excited molecular ion does not decompose immediately but undergoes several crossings to intersecting hypersurfaces. During these vibrations there is a high probability of nonradiative randomization of the excess energy over the available states. At ion source pressures usually encountered, the mean free path of the molecular ion is sufficient to rule out intermolecular energy randomization. Decomposition of the molecular ion occurs whenever sufficient energy is localized in a vibrational mode. The observed mass spectrum is thus composed of molecular ions and fragment ions produced by consecutive and competive unimolecular fragmentations of vibrationally excited ions.

For the unimolecular decomposition

$$m_{1}^{+} \rightarrow m_{2}^{+} + (m_{1}^{-}m_{2}^{-})$$
 (I-1)

The phenomenological rate constant k(t) is given by Equation (I-2)(2)

$$k(t) = \frac{\int_{0}^{\infty} P(E)k(E)e^{-k(E)t}dE}{\int_{0}^{\infty} P(E)e^{-k(E)t}dE}$$
(I-2)

where k(E) is the microscopic unimolecular rate constant for ions of energy E and P(E) is the probability of m_1^+ having internal energy between E and E + dE.

In most mass spectrometers, ions spend approximately 1 microsecond in the ion source and 10 microseconds traversing the instrument prior to collection (3). Therefore, ions with unimolecular rate constants exceeding 10^6 /second decompose in the ion source while ions with rate constants of less than 10^5 /second are collected without further decomposition. Ions with unimolecular rate constants within the range 10^5-10^6 / second decompose during or after acceleration but prior to collection. These decompositions are termed *metastable* and the parent ions of such decompositions are *metastable ions*. The recorded signal of the daughter ions formed from the fragmentation of metastable ions have become known as *metastable peaks*.

Metastable ions have received much attention in single focusing mass spectrometers since their original description by Hipple (4,5) who correctly interpreted them as resulting from dissociations occurring in the field-free drift region following acceleration. More recently, interest has reintensified in metastable ions as a result of studies using double focusing instruments. Metastable decompositions can occur along the entire ion flight path of a double focusing instrument. As depicted in Figure 1, such a mass spectrometer has six discrete regions. In three of the regions there are no electrostatic or magnetic forces acting on the ions; these are the *field-free* regions. During accelera-



Distinct regions acceleration 1 2 first field-free 3 electrostatic field 4 second field-free 5 magnetic field 6 final field-free

Figure 1. Double-focusing Mass Spectrometer of the Mattauch-Herzog Geometry (From Mass Spectrometry, Ed., Charles A. McDowell, McGraw-Hill, 1963, pp. 19)

tion, electrostatic and magnetic deflection, fields are present; therefore, these regions are referred to as *fielded*. Extensive mathematical treatment has been given to the motion of ions resulting from decompositions in the fielded (6) and field-free (7) regions of double focusing mass spectrometers. In this discussion singly charged ions are considered; however, multiply charged metastable decompositions have received considerable attention (8). When m_1^+ decomposes to m_2^+ as in Equation (I-1), the daughter ion retains a fraction, m_2/m_1 , of the kinetic energy and momentum. This assumes no vibrational energy from the bond rupture appears as translation energy. When this decomposition occurs in the accelerating region before falling through a large potential difference, discriminations will be small and if the daughter ions pass through the electrostatic analyzer, they will appear in the mass spectrum as a tail on the low mass side of m_2^+ . The actual apparent mass is given by (5)

$$m^{\star} = \frac{m_2^2}{m_1} \left[1 + \frac{(m_1 - m_2)(V - V_1)}{m_2 V} \right]$$
 (I-3)

where V is the accelerating voltage and V_1 is the potential difference through which the ion of mass m_1 falls before decomposing. Metastable decomposition occurring after falling through nearly the entire acceleration (V₁ slightly smaller than V) will appear in the mass spectrum in the tail on the high mass side of m^* if allowed to pass the electrostatic analyzer.

Daughter ions from metastable decompositions formed within the acceleration region, electrostatic sector, or magnetic field will not be collected at discrete masses but will become part of the background.

The daughter ions from metastable decompositions which are formed after passing through the collector slit are likewise of little interest since they are collected with the parent ions unless a specialized detector is used (9). The ions formed in the field-free region(s) preceding the magnetic sector of single or double focusing instruments can be observed at discrete masses. The ions formed just prior to magnetic deflection appear in the mass spectrum at m* given by Equation (I-4)

$$m^* = \frac{\frac{m_2^2}{m_1^2}}{m_1^2}$$
 (I-4)

as would any ions formed in the first field-free region if permitted to pass through the electrostatic sector at the normal accelerating potential. Equation (I-4) follows from Equation (I-3) when V_1 equals V.

Decoupling the electrostatic sector voltage from the acceleration potential in order to pass ions formed in the first field-free region is termed *defocusing*. Techniques for defocusing the Nier-Johnson (10) or Mattauch-Herzog (11) double focusing instruments are well established. With the mass spectrometer set to focus stable ions at the collector (as is the case for conventional mass analysis) the electrostatic field between the electric sector plates is such that ions which received the full acceleration energy will follow a central path through the sector. Daughter ions from metastable decompositions, m_2^+ , will have a smaller radius of curvature in the field and will not be transmitted because they possess only a fraction, m_2/m_1 , of the necessary energy. The daughter ions from metastable decompositions can be made to follow the central path by either increasing the accelerating voltage by a factor m_1/m_2 (holding the electric sector voltage constant), or by reducing

the electric sector voltage by a factor m_2/m_1 (holding the ion accelerating voltage constant). In either case, the main ion beam is not transmitted through the electrostatic sector.

The first method of defocusing has two disadvantages: as the ion accelerating voltage is changed, the tuning conditions within the ion source are altered due to changes in field penetration; and second, the voltage cannot be changed without bound, which consequently limits the ratios of m_1/m_2 that can be studied. This method has the advantage that the mass scale of the instrument is unchanged because the daughter ion of any first field-free decomposition now possesses what would be the normal acceleration energy. The magnet current can be set to observe ions at $m/e = m_2$ in the conventional mass spectrum, and as the accelerating voltage is scanned, a series of peaks are observed, each corresponding to a different metastable ion which decomposes into the m_2^+ ion.

The second defocusing method has the disadvantage that the mass scale changes during the scan of electric sector voltage, and any ions being collected will appear at m* (Equation I-4). The advantage is that all the daughter ions, without limit, can be made to pass the electric sector. In either defocusing technique described, the ion current may be monitored at the β -slit, Figure 1. The ion current plotted as a function of kinetic energy of the daughter ion constitutes the Ion Kinetic Energy Spectra, IKES (12). The observed metastable peaks in the IKES may be unambiguously assigned by setting the electric sector voltage (second defocusing method) to maximize the individual ion current at the beam monitor (β -slit) and scanning the magnetic field until m* is determined. The daughter ions will pass the electric sector when

$$\frac{E'}{E} = \frac{\frac{m_2^+}{m_1^+}}{m_1^+}$$
 (I-5)

where E is the electric sector voltage needed to pass the main ion beam, m_1^+ , and E' the voltage necessary to pass the daughter ion, m_2^+ . By knowing E, E', and m* equations (I-4) and (I-5) may be used to calculate unique values for m_1^+ and m_2^+ .

The uses of metastable ions and IKES for elucidation of fragmentation pathways in mass spectrometry have been summarized in an excellent review (13). The literature has increased vastly within the last few years as the application of IKES to ion fragmentation studies has become more common. Among the recent applications are the following: consecutive metastable decompositions in the two field-free regions (14); analysis of mixtures (15); isotope measurements and effects (16); release of kinetic energy in unimolecular decompositions (17); collision-induced dissociations and charge transfer reactions (18); reverse geometry instruments (19); appearance potential measurements of metastable peaks (20); thermochemistry and energy partitioning (21); non-zero scattering angle reactions (22); and analysis of geometric isomers (23-27). In all of these IKES applications, the energy resolving power of the mass spectrometer is important.

A large percent of the double focusing instruments presently used for IKES are of either a Nier (28) or a Mattauch-Herzog (29) geometry. The Nier-Johnson mass spectrometer has a 90 degree electrostatic analyzer followed by a 90 degree magnetic sector (e.g. M.S.9 manufactured by GEC/AE1) (30). A modified Nier-Johnson geometry instrument, the RMH-2 (31) (manufactured by Hitachi-Perkin Elmer) has a 70 degree degree electrostatic sector and a 70 degree magnetic field. The important aspect of the Nier-Johnson geometry instrument for IKES is the formation of an ion source energy image in the second field-free region at the β -slit. In Figure 2, ions of two slightly different energies but equal masses are energy focused in the plane containing the β -slit. By closing the β -slit and scanning the voltage on the electric sector plates at fixed accelerating potential, the IKES can be monitored with a detector behind the β -slit. The ability of the electrostatic sector to focus ions of the same energy to a point allows routine IKES of better than 0.5% energy resolution while recording peaks which make up only 10^{-7} to 10^{-8} of the total ion current (32). The maximum energy resolution with commercial Nier-Johnson geometry instruments for IKES is better than 0.025% (32).

In the Mattauch-Herzog geometry the ion source is located at the focal point of the $\Pi/4\sqrt{2}$ electrostatic sector forming an image at infinity. In Figure 1 ions of two slightly different energies and significantly different masses traverse the second field-free region with trajectories parallel to each other. By closing down the β -slit and scanning the voltage on the electric sector plates at fixed accelerating potential, the IKES can be monitored; however, the peaks observed will be broader than in the case of Nier-Johnson geometry with a significant loss in resolution due to the width of the intermediate image. One of the primary objectives of this research was to increase the applicability of Mattauch-Herzog mass spectrometers for IKES by increasing the energy resolution without affecting the performance of the instrument for routine mass analysis.

Once an improvement in energy resolution was realized it was a



Figure 2. Double-focusing Mass Spectrometer of the Nier Geometry (From A. O. Nier, *Rev. Sci. Instr.*, <u>31</u>, 1127 (1960))

further aim of this research to investigate the applicability of IKES as a structural probe. It was intended to investigate similarities or differences between normal ion abundances and those produced by decompositions in the first field-free region for a group of substituted thiophenes. Because the metastable decompositions are processes with halflives of approximately 10^{-5} seconds these are molecular ions that have received a relatively small amount of excess energy on ionization. Ions that have received a large excess of excitation energy will decompose in the ionization chamber while those receiving less excitational energy than necessary for decomposition will reach the detector intact. The mass spectrometer is thus acting as an energy filter since the first field-free region metastable decompositions are studied by rejecting all ions that undergo rapid reaction and allow only those undergoing slow reaction to be analyzed. Because the metastable ions possess less excitational energy than their counterparts which fragment in the ion source it is becoming evident that these ions are of more importance in obtaining correlations between fragmentation patterns and ion structure. The applications of IKES to analysis of structural isomers has included the following: N. R. Daly et al. (23) with the cis- and trans-butenes, R. M. Caprioli, et al. (24) with ortho-, meta-, and para-phenylenediamines, E. M. Chait and W. B. Askew (25) with camphor and trans-8methylhydrindan-2-one, H. W. Majors (26) with cis-, and trans-dimethyl maleate, and more recently S. Safe et al. (27) with isomeric chlorobenzenes and polychlorinated biphenyls. Some compounds have identical fragmentation patterns; no differences in IKES has been observed for meta-, and para-isomers of fluorophenylacetylene or for l-butene and *cis*-2-butene (25). The lack of differences in the spectra in many cases

is probably due to common structure for the molecular ion prior to metastable decomposition.

CHAPTER II

LOW RESOLUTION ION KINETIC ENERGY SPECTRA

Part I - Experimental Modifications

All spectra were obtained with a Mattauch-Herzog double focusing mass spectrometer (model DuPont/CEC 21-110B). For conventional mass analysis the accelerating potential of the instrument is slaved to the positive half of the electrostatic sector dual-purpose power supply. An approximate 20:1 voltage relationship exists between the acceleration and positive electrostatic sector plate (i.e. $V_{\text{sector}} = \pm \frac{V_{\text{accel.}}}{20}$). The electric sector plate potentials are not continuously variable but rather six discrete voltages can be supplied from the mass measurement chassis. It was required for metastable observation that the power supplies be separated and that the electrostatic plate potentials be continuously variable and independent of the accelerating potential. This decoupling of the power supplies was done by the addition of the circuit in Figure Switch #1 (S1) is a three position multilayer rotary switch. Posi-3. tion #1 of S1 bypasses most of the circuit and applies the ± voltage from the mass measurement chassis to the sector plates. Switch #1 should be in position #1 for mass spectral analysis. Position #2 is an off position and applies no voltage to the electric sector plates. Position #3 applies \pm 750 volts through wafers C and D to S2-A and S2-B respectively. The voltage is dropped along the fixed resistor string and



Figure 3. Circuit Diagram for Decoupling and Scanning the Electric Sector Voltage of a DuPont/CEC 21-110B Mass Spectrometer

the tandem potentiometer (Beckmann instruments precision Helipot, model #7603, R650K) where it is picked off and applied to the electric sector plates via S1-A and S1-B position #3. The electric sector voltage was monitored with Hewlett-Packard $4\frac{1}{2}$ digit multimeter (model #34702A). Switch #2 electronically inverts the position of the potentiometer and the fixed resistor string and allows a low (\pm .8 to 375 volts) or a high (± 741 to 333 volts) range of voltages to be applied to the electric sector plates. A multiratio gearmotor (Apcor, model #2201-010) was used to drive the 10-turn tandem potentiometer at speeds of 10, 5, 2, 1, 1/2, and 1/5 RPM. The ion signal was taken off the beam monitor vacuum feedthrough by a Keithley high speed picoammeter (model #417) and displayed on a Keithley recorder (model #370). The spectra were usually scanned with a potentiometer speed of 1/2 RPM (sector plates changed at \pm 18 volts/min.) and a chart speed of .75 in/min. The majority of the spectra were measured from 0% through 100% electrostatic sector voltage; however, peaks were generally observed in the 50% - 100% region. Precise measurement of the energy of peaks in the IKE spectra was obtained by manually scanning the electric sector voltage to maximize the peak intensity while monitoring the digital multimeter.

The ion source temperature and pressure were noted on the spectra. Other ion source conditions were as follows except where otherwise noted: electron energy, 70 eV; trap current, 80µ amps; bilateral source slits, open maximum; and focus electrode, maximum signal at beam monitor for the main beam.

Part II - Results and Discussion

The Ion Kinetic Energy Spectra of n-decane recorded with a Nier

geometry mass spectrometer (RMH-2) by Beynon, et. al. (33) is given in Figure 4. The metastable peak assignments are indicated in Table I. The energy resolution in Figure 4 is between .6 - .9% depending upon the metastable peaks selected (peaks F and G, C and D respectively). Chait, et. al. (25) has recorded the IKES of n-decane on a Mattauch-Herzog instrument (DuPont 21-110B), Figure 5. The metastable peak assignments refer to Table I. The lower energy resolution is indicated in the latter spectra by the complete loss of the C-D doublet as well as peaks E, F, G, the shoulder on the low energy side of I, and M. The calculated energy resolution is approximately 3% based on the B, C-D doublet. Both spectra were obtained by scanning the voltage on the electrostatic sector plates at fixed acceleration potential and recording the ion intensity at the β -slit. In the Nier geometry instrument with the presence of an energy image in the second field-free region, a narrow β -slit was used to yield the high energy resolution. The instrument's sensitivity and detectibility were increased for IKES by incorporation of an electron multiplier behind the energy resolving slit (12). In the Mattauch-Herzog instrument there is no intermediate image and the signal was recorded with an electrometer behind the wide (0.250 inch) β -slit.

The n-decane IKE spectra recorded with the O.S.U. mass spectrometer is given in Figure 6. Figures 5 and 6 are essentially identical except for intensity variations (e.g. peaks H, I, and J) which could be due to ion source pressure or temperature discrepancies. The authors do not indicate the ion source conditions under which Figure 5 was obtained.

To check further the performance of the O.S.U. instrument, the IKES of benzene was recorded, Figure 7. The daughter ions were mass analyzed and the metastable transitions were identified using Equations I-4 and

TABLE I

METASTABLE PEAKS AND TRANSITIONS IN THE IKES OF n-DECANE (TAKEN FROM A. H. STRUCK & H. W. MAJOR JR., ASTM E-14, 1969)

Metastable	Peak	Assigned Transition	Calculated m ₂ /m ₁
a		43 → 41	.953
		41 → 39	.951
b		84 → 69	.821
С		142 →113	.796
d		142 →112	.789
		70 → 55	.786
е		113 → 85	.752
f		113 → 83	. 735
		57 → 42	.737
q		112 → 83	. 741
<u> </u>		56 → 41	.732
1-			
11		$\begin{array}{c} 98 \neq 70 \\ 57 \neq 41 \end{array}$. /14
			•723
i		142 → 99	.697
j		127 → 85	.669
		85 → 5 7	.671
	•	85 → 56	.659
k		113 → 71	.628
1		71 → 4 3	.606
m		142 → 85	.599
n		99 → 57	.576
0		55 → 29	.527
р		142 → 71	.500
_		113 → 57	.504
		85 → 4 3	.506
		57 → 29	.509
		55 → 27	.491



Figure 4. Ion Kinetic Energy Spectrum of n-decane With a Nier Geometry Mass Spectrometer (From Beynon, et al., Chem. Commun., 723 (1969))



Figure 5. Ion Kinetic Energy Spectrum of n-decane With a Mattauch-Herzog Mass Spectrometer (From Chait, et al., Org. Mass Spectrom., <u>5</u>, 147 (1971))







Peak # (low ESA → Hi E SA)	ESA (obs.)	m * from Plate	Transition	ESA (calc.)	m* (calc.)
1 2 3 4	.503 .599 .670 .670 .671 .671 .968	19.58 23.27 34.72 35.39 33.98 33.98 72.98	$78^{+} \rightarrow 39^{+} + 39$ $65^{+} \rightarrow 39^{+} + 26$ $78^{+} \rightarrow 52^{+} + 26$ $79^{+} \rightarrow 53^{+} + 26$ $76^{+} \rightarrow 51^{+} + 25$ $77^{+} \rightarrow 51^{+} + 26$ $77^{+} \rightarrow 75^{+} + 2$.500 .600 .667 .670 .671 .662 .974	19.50 23.4 34.67 35.56 34.22 33.78 73.05
4	.970	73.19	$78^+ \rightarrow 76^+ + 2$.974	73.05

Figure 7. Ion Kinetic Energy Spectrum of Benzene Below the Main Ion Beam

I-5. The IKE spectra agreed well with that of Chait, et. al. (25); however, the assignment of the metastable peak at 67% of the electrostatic analyzer voltage was incorrectly reported in the literature. The transition was reported as $78^+ \rightarrow 63^+ + 15$. If this decomposition does occur in the first field-free region, the daughter ion would be detected when the electric sector plates are lowered to 81%, not 67%, of the voltage necessary to pass the main ion beam. Our identification was obtained by measuring the apparent mass, m*, of the daughter ions passed at an electrostatic sector energy of 67%. An apparent mass of 34.7 uniquely determined the transition as $78^+ \rightarrow 52^+ + 26$.

The energy resolving limitations of the Mattauch-Herzog mass spectrometer were investigated computationally on an IBM 360/65 computer (Appendix B, Program #1). For computational purposes the ions were treated as point particles at ion fluxes low enough to neglect space charging effects. All metal surfaces were considered as ideal in that no charge build-up or screening was considered although this can be of considerable importance (34). The results of these computations presented in Figure 8 are for ions exiting the infinitely narrow ion source slit with divergent angles from the central axis of the instrument as indicated by α . The maximum acceptance angles of the entrance slit to the electric sector in the O.S.U. instrument is \pm 0.00045 radians. The ions treated computationally in the first field-free region were those moving in the plane orthogonal to the electric sector entrance slit. In Figure 8 the final position of the ions in the plane of the exit slit of the electrostatic sector (measured from the vertex of the sector) is given as a function of the accelerating voltage and the angle of entrance (in radians) to the sector. The arrows at 63.84





and 63.69 cm mark the extremes of the 0.060 inch exit slit. Opening the adjustable ion source slit by 0.001 inch has the effect of broadening each of the lines in Figure 8 by approximately that amount.

From Figure 8 it is clear that ions resulting from metastable decompositions in the first field-free region entering the electrostatic sector with differences in their translational energies greater than about 5 percent can be completely separated and detected at the β -slit using different electric sector voltages. Each group of daughter ions, although translationally monoenergetic, exit the electric sector at a fixed sector voltage at radial distances determined entirely by the angle of entrance to the sector. If the daughter ions differ in translational energy by less than about 5%, the groups of ions are not completely resolved. This accounts for the wide metastable peaks and low energy resolution observed in the IKES with the Mattauch-Herzog mass spectrometer. With an ion source slit of .002 inches, entrance and exit slit widths of the electric sector of .016 and .060 inches respectively, and an accelerating potential of 7500 eV, the computed overlap of IKE peaks on the DuPont/CEC 21-110B mass spectrometer are as follows: 80% overlap at energy differences of 1.3%; and a 10% overlap at an energy difference of 2.3%.

The energy resolution of the Mattauch-Herzog mass spectrometer can be improved by decreasing the width of the entrance slit to the electric sector. This decreases the acceptance angle α , Figure 8, narrowing the width of the ion beam at the exit slit of the sector. The energy resolution of the IKE spectra can also be improved by narrowing the exit slit to the electrostatic sector. Both methods unfortunately also decrease the sensitivity of the instrument and correspondingly limit its utility

as a general purpose mass spectrometer. Hence, it was decided to attempt further improvement of the energy resolution by designing a variable β -slit which could be completely removed from the ion path during normal mass spectrometric operation of the instrument.

CHAPTER III

MEDIUM ENERGY RESOLUTION ION KINETIC ENERGY SPECTRA

Part I - Experimental Modifications

The second field-free region of a Mattauch-Herzog mass spectrometer (DuPont/CEC 21-110B) was fitted with a bellows assembly to insert a variable β -slit and an electron multiplier (Bendix Continuous-Dynode, Model 4700) into the ion beam traversing the region, Figure 9. The bellows assembly had a travel of greater than 3½ cm allowing the slit and electron multiplier to be completely removed from the ion beam when not in use. One end of the continuous-dynode resistor was grounded to the mass spectrometer. The front of the resistor string (also the entrance to the electron multiplier) was connected to a vacuum feed-through placed in the auxiliary pump-out flange behind the photoplate holder. The negative high voltage (1000 - 2800v) for the continuous-dynode electron multiplier was supplied by the power supply for the instrument's discrete dynode electron multiplier.

The slit was positioned in front of the continuous-dynode electron multiplier and was continuously variable in width from closed to approximately 0.5 cm open. With the electron multiplier-slit assembly positioned in the ion beam the variable slit acts as an adjustable β -slit. However, because the adjustable β -slit was physically connected to the





electron multiplier it cannot be inserted into the ion beam independently.

The signal from the anode of the electron multiplier was connected to the conventional beam monitor vacuum feed-through via a wiper arm. The wiper arm contact introduces a larger than normal dark current into the detection system. At 2500v a dark current of 1×10^{-12} amps was detected. The signal from the vacuum feed-through was fed into a high speed picoammeter (Keithley Model 417) and recorded on a strip chart recorder (Keithley Model 370). In order to avoid perturbations of the secondary electron trajectories within the multiplier by fringing magnetic fields the magnetic sector current was set to the minimum.

Part II - Results and Discussion

The increase in energy resolution of the mass spectrometer using the adjustable β -slit-electron multiplier is illustrated with n-decane, Figure 10. The metastable transitions and peak assignments correspond to those in Table I. The IKES of n-decane using only the electrometer detector behind the wide (~ 0.250 inch) β -slit is given in Figure 6. The increased energy resolution for IKES in Figure 10 is apparent with the splitting of additional metastable peaks from the main ion beam with daughter ions retaining 98.5% and 97.7% of the kinetic energy. Further indications of the increased energy resolution and sensitivity are the resolution of the C-D doublet; the appearance of peaks e, f, and g; the splitting of peak i; and the appearance of the m doublet. The energy resolution of n-decane in Figure 10 is comparable to that reported with a Nier geometry instrument, Figure 4; however, in the former case the adjustable β -slit was set for maximum energy resolution


Figure 10. Ion Kinetic Energy Spectrum of n-decane With the Adjustable β -slit and Electron Multiplier

whereas in the latter this was not the case.

The minimum detectability of our Mattauch-Herzog mass spectrometer for IKES peaks was not as low as the Nier geometry. Beynon et. al. (12) have investigated electron transfers to multiply charged argon ions in the first field-free region. For the transition $\operatorname{Ar}^{+4} \rightarrow \operatorname{Ar}^{+}$ (1), $\operatorname{Ar}^{+3} \rightarrow \operatorname{Ar}^{+}$ (39), $\operatorname{Ar}^{+2} \rightarrow \operatorname{Ar}^{+}$ (820), $\operatorname{Ar}^{+3} \rightarrow \operatorname{Ar}^{+2}$ (123), $\operatorname{Ar}_{3}^{+2} \rightarrow \operatorname{Ar}_{2}^{+2}$ or $2Ar^+$ (9), and $Ar_2^{+2} \rightarrow Ar^{+2}$ (28) the relative intensities are given in parentheses. At maximum sensitivity we have been able to observe only $Ar^{+2} \rightarrow Ar^{+}$, and $Ar^{+3} \rightarrow Ar^{+2}$ on our instrument. Electric sector potentials required for $Ar^{+3} \rightarrow Ar^{+}$ have not been attempted due to limitations in our dual-purpose power supply; however, $\operatorname{Ar}_{2}^{+2} \rightarrow \operatorname{Ar}_{3}^{+2} \rightarrow \operatorname{Ar}_{2}^{+2}$ or Ar have not been observed. The difference in the minimum detectability is attributed to the presence in the Nier and lack in the Mattauch-Herzog geometry of a focal point for metastable daughter ions in the second field-free region. An additional factor is the increased dark current introduced by using the wiper arm in our installation of the electron multiplier in the second field-free region.

The occurrence of multiply charged metastable decompositions are well documented in double focusing mass spectrometers. Beynon, et. al. (8) have reported dish shaped peaks resulting from the large amounts of translational energy imparted to the ionic fragments upon bond rupture. In the IKES of benzene a dish shaped peak at electrostatic sector voltage above the main ion beam can be found at 162% of the energy. This peak corresponds to the singly charged daughter ion at m/e 63 resulting from the doubly charged molecular ion decomposing in the first fieldfree region. The Mattauch-Herzog instrument with an adjustable β -slit and electron multiplier has the necessary energy resolution and sensitivity to resolve the dish shaped metastable in benzene, Figure 11.

The interest in substituted thiophene compounds has been intensified recently by their presence in fossil fuels. An analysis using the 70 eV mass spectra of a liquification product mixture from coal is complicated by the predominance of common fragment ions. Due to the mass defect of sulfur, thiophene compounds with molecular weights of 200 or greater require very high mass resolution to separate their molecular ions from those of many hydrocarbons at the same nominal mass. An incomplete series of alkyl- and benzo- thiophene compounds were obtained from the ERDA laboratory in Bartlesville, Oklahoma. Two additional compounds, 2-heptylthiophene and 2-butylthiophene, were prepared by previously reported synthetic routes (35). All of the thiophene compounds were vacuum distilled and found to be 99+% pure by gas chromatography and field ionization mass spectrometry (36). The mass spectra of all of the thiophene compounds obtained have been reported (37). The IKES of the thiophene compounds were undertaken to investigate the types and number of transitions present and determine whether it would be possible to distinguish the presence of thiophene compounds generally (or specific thiophene compounds) in a mixture on the basis of their IKES. An additional aim of the analysis of the thiophenes was to determine whether structural isomers, which give similar mass spectra, could be characterized better on the basis of their IKES.

The sensitivity and energy resolution of the Mattauch-Herzog mass spectrometer using the adjustable β -slit and electron multiplier was further illustrated with 2-heptylthiophene. In Figure 12, the IKES was recorded using only the electrometer, whereas in Figure 13 the electron multiplier and adjustable β -slit was used. The spectra in Figure 12 was





β







Figure 13. Ion Kinetic Energy Spectrum of 2-heptylthiophene Using the Adjust-able β -slit and the Electron Multiplier

ω

recorded with the bilateral ion source slits opened for maximum sensitivity. In Figure 13, although the source slits were left open the adjustable β -slit, electron multiplier, and electrometer were all reduced to bring the peaks on scale. The additional energy resolution in Figure 13 is apparent in the C-D doublet as well as many of the lower intensity peaks. The electron multiplier-adjustable slit assembly was removed from the beam and the apparent masses, m*, of the daughter ions were obtained from the photographic plate. Plate exposures of approximately $10^{-12} - 10^{-11}$ coulombs were taken. Using Equations (I-4) and (I-5) the metastable transitions in Table II were assigned. No attempt was made to quantify the metastable transitions since generally several daughter ions were present in a recorded metastable peak and the photographic plate was exposed at the metastable peak maximum. The metastable peak maximum corresponds to the maximum intensity resulting from superposition of all metastable peak contributions at that point.

The IKE spectra of the remaining thiophene compounds are reported in Figures 14-26. The metastable transitions were assigned on a basis of the electrostatic sector voltage; however, for major and pertinent peaks for the discussion the apparent mass of the daughter ions were checked with the photographic plate or the electron multiplier following magnetic deflection. The percent electrostatic sector energies indicated are the experimentally determined values. The IKES of thiophene in Figure 14 illustrates the fragmentation of the unsubstituted ring. The molecular ion undergoes multiple bond rupture to lose mass 45, $84^{+} \rightarrow$ $39^{+} + 45$, as well as hydrocarbon loss from the molecular ion to form the daughter ion at m/e 45. Loss of sulfur, m/e 32, is common from the molecular or fragment ions as are rearrangements or multiple bond rup-

TABLE II

METASTABLE PEAKS AND TRANSITIONS IN THE IKES OF 2-HEPTYLTHIOPHENE

Metastable	Peak	Assigned	Tran	sition	Calculated m_2/m_1	
a		97	→ 4	5	.464	
b		85	→ 4	3	.506	
С		182	→ 9	7	.533	
		183	→ 9	8	.536	
		84	$\rightarrow 4$	5	.536	
		55	→ 2°	9	.527	
đ		100		2		
u		180	→ 9a	8	.544	
		97	\rightarrow 5.	3	.546	
P		6 E		2		
C		20	→ 3:	9	.600	
		110	→ 6	/ ~	.604	
		100	> 60	-	.600	
	•	108	→ 6:		.602	
		97	$\rightarrow 58$	3	.598	
f		67		,		
Ť.		102	~ 41		.612	
		102			.610	
		102	→ II(.604	
q	· · ·	43	→ 27	7	620	
		,	2,		• 020	
h		71	→ 45	5	634	
		153	→ 97	,	634	
					.034	
i		97	→ 63	1 P	649	
					• • • • •	
j		84	→ _58		.690	
		181	→ 125		.691	
		111	→ 77		.694	
k		55	→ <u>39</u>	· · ·	.709	
		97 -	→ 69		.711	
1		153 -	→ 111		.726	
	•	· -				
m		182	→ 139		.764	
		139 -	→ 105		.755	
		110 -	→ 84		.764	
n		148 -	→ 119		.804	
		149 -	→ 120		.805	

TABLE	II	(Continued)	
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Metastable Peak	Assigned	Tr	ansition		Calculated	^m 2 ^{/m} 1
0	182	→	148		.813	- <u></u>
	183	→	149		.814	
	100		150		0/1	
p	102		150		-041 9/2	
	T03	7	104		.042	
q	97	\rightarrow	84		.866	
r	110	\rightarrow	96		.873	
S	29	\rightarrow	26		.897	
t	43	÷	39		.907	
11	27	→	25		926	
u i	28	, ->	26		.920	
	29	÷	27		.931	
	41		38		.927	
•	57	→	53	•	.930	
	20	<u>بد</u>	27		931	
•	30		28		. 931	
	43	→	41		.953	
	43	, ,	40		.952	
	42	->	45		.957	
	41	→	39		.951	
	44	→	42		.955	
W	27	→	26		. 963	
••	28	→	27		.964	
	30	→	29		.967	
,	39	÷	38		.974	
	40	→	39		.975	
	44	\rightarrow	43		.977	
· · · ·	46	→	45		.978	
	55	→	53		.964	
	53	\rightarrow	51		.962	
	67	\rightarrow	65		.970	
	68	\rightarrow	66		.971	
	69	\rightarrow	67		.971	





tures to lose m/e 34 and m/e 26.

The mass spectra of 2-(2-methylpropyl)thiophene and 2-butylthiophene are similar (36). The differences that do exist in the mass spectra are in intensities at m/e 125 (1.23 vs. .17), m/e 111 (.42 vs. 3.66), m/e 110 (.64 vs. 1.19), m/e 85 (.61 vs. 1.66), m/e 84 (1.11 vs. 2.59), and m/e 77 (.95 vs. 1.72). The numbers in parentheses are the percent of the base peak, m/e 97, contributed to a given ion fragment by 2-(2-methylpropyl)thiophene and 2-butylthiophene respectively.

The differences in the mass spectral intensities can be explained by the metastable transitions in their respective IKE spectra, Figures 15 and 16. The loss of m/e 29 from the molecular ions to form m/e 111 is observed in the IKES at 79.3% of the electrostatic sector energy. The 79.3% peak in the IKES of 2-butylthiophene is a significant metastable transition. The m/e lll peak is small in the 2-(2-methylpropyl) thiophene mass spectra since it is probably not a simple fragmentation but requires at least one rearrangement; however, daughter ions at m/e 111 do occur in the IKES at 79.3% and 88.8% of the electrostatic sector energy. These fragmentations, although they do occur in 2-(2-methylpropyl)thiophene, do not have sufficiently large rate constants to be of any consequence in the time frame of the mass spectra. The metastable transition indicating the loss of a methyl group from the 2-(2-methylpropyl)thiophene molecular ion is present in the IKES as is the large peak indicating the loss of m/e 41 at 71.2% of the electrostatic sector energy. At an electron energy of 70 eV fragment ions resulting from rearrangements will be observed in the mass spectra; however, they may be minor peaks. In the IKES daughter ions resulting from transitions requiring rearrangements will generally account for a



Figure 15. Ion Kinetic Energy Spectrum of 2-(2-methylpropyl)thiophene



Figure 16. Ion Kinetic Energy Spectrum of 2-butylthiophene

larger part of the total ion current than the ions in the mass spectra. Examples of large metastable peaks in the IKES resulting from rearrangements are $140^+ \rightarrow 84^+$ and $97^+ \rightarrow 53^+$ in both 2-butylthiophene and 2-(2-methylpropyl)thiophene as well as $140^+ \rightarrow 99^+$, $125^+ \rightarrow 91^+$, and $140^+ \rightarrow 111^+$, in 2-(2-methylpropyl)thiophene and $110^+ \rightarrow 77^+$, $140^+ \rightarrow 84^+$, and $97^+ \rightarrow 53^+$ in 2-butylthiophene.

Analysis of mixtures of small amounts (a few percent) of either 2-butylthiophene in 2-(2-methylpropyl)thiophene or 2-(2-methylpropyl)thiophene in 2-butylthiophene can be done on any mass spectrometer which has good reproducibility of peak intensities (e.g. a Dempster mass spectrometer). The analysis could be done with the intensity variation at m/e 125 for the first mixture and m/e 111 for the second. The analysis using IKES could be done on small amounts of 2-butylthiophene in 2-(2-methylpropyl)thiophene using the $140^+ \rightarrow 111^+$ transition if it is shown to be a true first order decomposition. The analysis of small amounts of 2-(2-methylpropyl)thiophene in 2-butylthiophene using IKES would be more difficult. With higher energy resolution (.1% or better) the metastable decomposition, $111^+ \rightarrow 99^+$, in 2-butylthiophene could be separated from $140^+ \rightarrow 125^+$ in 2-(2-methylpropyl)thiophene; the $111^+ \rightarrow$ 99^+ transition could then be used for the analysis.

The IKES of the 2-(1,1-dimethylethyl)thiophene, Figure 17, is significantly different from that of either 2-(2-methylpropyl)thiophene or 2-butylthiophene; however, these mass spectra are also different. The base peak is at m/e 125 with large fragment ions at m/e 140 (25%), m/e 97 (17%), and m/e 85 (12.3%).

Figures 18-23 are IKES of alkylthiophenes substituted in the 2 or 2,5 positions. The daughter ions observed result in large part from







Figure 18. Ion Kinetic Energy Spectrum of 2-(3-methylbutyl)thiophene

₹3











Figure 21. Ion Kinetic Energy Spectrum of 2-ethyl-5-(2-methylpropyl)thiophene



Figure 22. Ion Kinetic Energy Spectrum of 2-(2-ethylbutyl)thiophene



Ion Kinetic Energy Spectrum of 2-decylthiophene

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decompositions of hydrocarbon fragment ions (e.g. $91^+ \rightarrow 65^+$, $65^+ \rightarrow 39^+$, $43^+ \rightarrow 41^+$, etc.) and loss of sulfur fragments (HS, H₂S, HCS, H₃C₂S, etc.) from the molecular ions and large fragments. Metastable decompositions from the molecular ions give daughter ions which predominately contain the sulfur atom. The alkylthiophenes substituted in the 2-position have large metastable transitions from the molecular ion to the base peak of the mass spectra, Figures 13-18, 22, and 23. The mono-substituted thiophenes which have large or branched alkyl groups have significant transitions from the molecular ion to m/e 111 (97+14) and m/e 125 (97+28).

The IKES of the 2,5-dialkylthiophenes rich in transitions usually exhibit significant transitions from the molecular ions. For example, 2-propyl-5-(3-methylbutyl)thiophene, Figure 20, and 2-ethyl-5-(2-methylpropyl)thiophene, Figure 21, unlike 2-ethyl-5-(3-methylbutyl)thiophene, Figure 19, have prominent metastable peaks from the molecular ions. A characteristic transition of dialkylthiophenes with molecular weights greater than 168 is $167^{+} \rightarrow 111^{+}$.

The IKES of benzo[b]thiophene, Figure 24, contains several intense metastable peaks which result from fragmentation of the molecular ion by multiple bond ruptures and/or rearrangements. The most intense metastable peak results from the loss of m/e 45 from the molecular ion. A similar fragmentation pattern occurs in 6-methylbenzo[b]thiophene and 2-benzylthiophene, Figures 25 and 26, with major metastable peaks resulting from the loss of m/e 45, 26, 32, 59, and 71 from the molecular ion.

As indicated previously, high mass resolution is required to separate the molecular ions of the large thiophene compounds from those of hydrocarbons at the same nominal mass. Specifically, 2-heptylthiophene



Figure 24. Ion Kinetic Energy Spectrum of Benzo[b]thiophene



Figure 25. Ion Kinetic Energy Spectrum of 6-methylbenzo[b]thiophene





has a molecular weight of 182.1129 and bibenzyl has a molecular weight of 182.1095. The mass resolution required to separate the molecular ions would be in excess of 53,000. Although the fragmentation patterns are guite different for the two compounds, in mixtures containing homologous compounds common ions would make identification difficult. The IKES could be helpful in identification of the two compounds in the mix-The IKES of 2-heptylthiophene, Figure 13, has several transitions ture. from the molecular ion (peak c, m, o, and p). In the IKES of bibenzyl, Figure 27, there are two transitions from the molecular ion. Whereas in the mass spectra identification of m/e 182 in the mixture would be difficult, requiring high mass resolution, the same problem is not present in the IKES. If sufficient energy resolution is not possible to resolve the transitions at the β -slit, the daughter ions at the specific electric sector voltage can be mass analyzed giving a unique assignment to each transition.

To explore the uses of IKES further, higher energy resolution and increased sensitivity would be beneficial. The increase in energy resolution and sensitivity was explored by theoretical modification of the ion optical path.



Figure 27. Ion Kinetic Energy Spectrum of Bibenzyl

CHAPTER IV

FURTHER IMPROVEMENTS IN ENERGY RESOLUTION FOR A MATTAUCH-HERZOG MASS SPECTROMETER

In the Mattauch-Herzog geometry the ion source is placed at the focal point of the electric sector giving rise to ions whose trajectories in the second field-free region are parallel to each other (38). The interdependence of the solid angle and energy bandwidth which was discussed quantitatively in Chapter II is represented in Figure 28. (39) In Figure 28(a), the β -slit is opened to transmit all ions of energy eU o that have passed the α -slit. The ions with energy $e(U_0 + \Delta U)$ exiting the electric sector also form a parallel beam but make a small angle with the beam of ions with energy eU o. The ions with the higher energy $e(U_0 + \Delta U)$ are partially cut off by the β -slit; for these ions the β -slit acts as a one-sided α -stop. In Figure 28(b) the β -slit is closed to allow only the ions at the extremes of the beams with energy $e(U_0 + \Delta U)$ to pass. In this second case the energy pass of the β -slit increases with the width of the α -slit.

A proposed solution to this problem of interdependence has been to use two radial electrostatic sectors instead of one (40). The β -slit could then be placed between the first and second electrostatic sector; if proper geometry is maintained, excellent energy resolution would be achieved. Although this solution is no doubt possible, it was not considered for two reasons: (1) it would require severe modification of



Figure 28. Interdependence of Solid Angle and Energy Bandwidth in a Mattauch-Herzog Mass Spectrometer

the optical bench and expense in obtaining an appropriate electrostatic sector; and (2) it would effectively exclude the Mattauch-Herzog portion of the instrument from the energy focusing for ion kinetic energy spectra.

A second approach to the problem of interdependence of the solid angle and energy bandwidth was that of Liebl (39). He had suggested the incorporation of a single linear three-element electrostatic lens in the second field-free region as indicated in Figure 29. Such lenses are often called *Einzel* lenses. There is one additional characteristic this electrostatic lens must have for ion kinetic energy spectra not considered by Liebl in his application to conventional mass spectrometry. With IKES, as the radial electrostatic voltage is decreased to pass daughter ions of lower energy, the voltage on the three-element electrostatic lens would also have to be changed. The voltage on the lens must be changed in such a way as to maintain a constant focal length for the ions with the proper energy (those ions whose energies are in the proper ratio to the radial electrostatic sector voltage). To avoid having to design a power supply for the three-element lens which would be scanned as some non-linear function of the radial electrostatic sector voltage, it would be desirable to design the lens such that its focal length would be constant as its applied voltage maintains a constant-ratio to the radial electrostatic sector voltage, i.e.

In this way as two daughter ions enter the lens system with kinetic





energies eU_{O} and $e(U_{O} + \Delta U)$, their focal length and hence their image size at the β -slit would be a function only of their kinetic energy. Although this modification would improve ion kinetic energy discrimination at the β -slit, the double focusing properties of the instrument would be lost if this lens were energized during conventional mass spectra analysis.

Experimental focal properties of linear three-element electrostatic lenses have been compiled and discussed by Septier (41), the essential properties of which are illustrated in Figure 30. The ratio of potentials for the single lens, R_{sl} , contains the potentials of the two outer and the inner electrodes as well as the kinetic energy of the incident particle, U_a , U_i , and U_o respectively. The inverse of the focal length of the lens, K, is given as a function of lens potentials, R_{sl} . For given U_a and U_i particles entering the lens normal, with a range of kinetic energies sufficient to give rise to R_{sl} values of .5 - .6 are focused to approximately equal focal lengths. However, if the potentials on the lens are adjusted to yield R_{sl} values of -0.1 to 0.1 (actual values depending upon the specific lens chosen), a small difference in ion energies yields a large difference in focal lengths. It is this later case that is of most interest in increasing the energy discrimination of the Mattauch-Herzog instrument for ion kinetic energy spectra.

Due to the demand on our instrument for conventional mass analysis, it was decided that the proposed incorporation of a linear three-element electrostatic lens be investigated computationally prior to any experimental modification. For computational purposes the ions were considered as point particles, and the influence of their charges on those of the electrodes, as well as other ions, was ignored so the focusing



Figure 30. Power Characteristics of Three Element Electrostatic Lenses. (Taken From Reference 41)

field could be calculated independently of the beam it is to focus. This approximation is acceptable in the case of low particle flux beams. Furthermore, all electrode surfaces were treated as ideal in that no charge build-up or screening was considered at the electrode surfaces (42).

In the calculation of the ion focal properties of slit-aperture electrostatic lenses, it is usually necessary to first determine accurately the potential distribution within the lens system. At present, the most widely used method involves computation of tens of thousands of potentials at mesh points by numerical relaxation and interpolation between points by either Lagrange formulas (43) or cubic splines (44). The present experimental methods, such as the electrolytic plotting tank (45) and the resistor network (46), require special equipment and are very time consuming if one is to obtain potentials of sufficient accuracy for trajectory analysis.

Despite the popularity of the numerical relaxation method, it requires substantial computer time and generates potentials at a large number of points outside the region of interest (47). For this reason the method of Conformal Mapping was used. With the knowledge of potentials and potential gradients throughout the lens system, ions with known mass and initial momentum were traced through the lens.

If the electrodes and slits of the three-element lens in Figure 31 are treated as infinite in the x and z directions, then the lens can be treated as two dimensional in the xy plane. The electrode system is now considered mathematically as a degenerate polygon in the complex z-plane (x + iy). As the boundary of the electrode system and the associated electrostatic field can be rather complicated, the region



COMPLEX Z-PLANE



between the projections of the slits was mapped on the positive imaginary half of a complex w-plane (u + iv) Figure 32. This conformal mapping is best accomplished by the Schwarz-Christoffel transformation (48,49) which is applicable to bounded polygons. In this transformation LaPlace's equation is invariant; so the same equation must be solved in the w-plane but with simplier boundary conditions.

The potential distribution along the center line of the lens system can be obtained in closed form (Appendix A) whereas off-axis potentials near the main axis are computed by series expansion (48).

$$V(\mathbf{x},\mathbf{y}) = V(\mathbf{0},\mathbf{y}) + \left(\frac{\partial V}{\partial \mathbf{x}}\right)_{\mathbf{0},\mathbf{y}} \mathbf{x} + \frac{1}{2}\left(\frac{\partial^2 V}{\partial \mathbf{x}^2}\right)_{\mathbf{0},\mathbf{y}} \mathbf{x}^2 + \cdots \qquad (\mathrm{IV-2})$$

For the case of a symmetrical potential distribution all odd derivatives are zero.

$$V(\mathbf{x},\mathbf{y}) = V(-\mathbf{x},\mathbf{y}) \quad (IV-3)$$

The partials of the potential with respect to x are not easily obtainable; however, by differentiation of LaPlace's equation all even derivatives can be found

$$\frac{\partial^2 V}{\partial x^2} = -\frac{\partial^2 V}{\partial y^2}, \text{ (LaPlace Equation)} \tag{IV-4}$$
$$\frac{\partial^4 V}{\partial x^4} = \frac{\partial^4 V}{\partial y^4},$$
etc.

From knowledge of the potential distribution along the center line, potentials near this line are given by:


Figure 32. Electrode System in Complex w-plane

$$V(\mathbf{x},\mathbf{y}) = V(\mathbf{0},\mathbf{y}) - \frac{\mathbf{x}^2}{2!} \left(\frac{\partial^2 \mathbf{v}}{\partial \mathbf{y}^2}\right) + \frac{\mathbf{x}^4}{4!} \left(\frac{\partial^4 \mathbf{v}}{\partial \mathbf{y}^4}\right) - + \cdots$$
(IV-5)

Numerically, the ray tracing can be simplified by calculating the gradients of the potential at the points of interest. Equations (IV-6) and (IV-7) are obtained by differentiation of Equation (IV-5).

$$(\frac{\partial V}{\partial x}) = -x (\frac{\partial^2 V}{\partial y^2}) + \frac{x^3}{6} (\frac{\partial^4 V}{\partial y^4}) - \frac{x^5}{120} (\frac{\partial^6 V}{\partial y^6}) + \cdots (IV-6)$$

$$(\frac{\partial V}{\partial y}) = (\frac{\partial V}{\partial y})_{0,y} - \frac{x^2}{2} (\frac{\partial^3 V}{\partial y^3})_{0,y} + \frac{x^4}{24} (\frac{\partial^5 V}{\partial y^5})_{0,y} - \frac{x^6}{720} (\frac{\partial^7 V}{\partial y^7})_{0,y} + \cdots (IV-7)$$

It is thus possible to calculate the potential (Equation IV-5) or the gradients of the potential (Equations IV-6 and IV-7) at any point in the lens system with only the knowledge of the potential as well as the derivatives of the potential at that y-coordinate on the central axis.

The principle of the Schwarz-Christoffel method is to treat the electrode array as the limiting case of a polygon; in so doing no provisions are made to calculate potential distributions on the outer sides of the electrode system, Figure 31. Since it is intended to ground the outer electrodes, field penetration of the center electrode potential out of the lens system is of concern. By incorporation of two extra apertured planes as in Figure 33, ion trajectories into and out of the central three apertured planes can be considered. The conformal mapping of this larger lens follows identically that of the three apertured case; however, the size and number of the actual equations for the transformation increase.





The thickness of each electrode must be considered if the lens is to be realistic. In the Schwarz-Christoffel transformation the electrodes are represented as infinitely thin. Wallington (50) has found that accurate theoretical representation of an electrode requires the use of two or more planes of infinitesimal thickness with the outermost planes separated by distances equal to the real thickness of the electrode. The potential on each plane is the same as the real electrode. In the case of *Einzel* lenses (three-element electrostatic lenses in which the outer two electrodes are at the same potential; usually ground) the thickness of the center electrode is most important for the lens properties (50,51).

To simulate trajectories of ions leaving the exit slit of the radial electrostatic sector in the mass spectrometer and entering an *Einzel* lens, the potentials and notation indicated in Figure 34 are used. Four electrodes are used to represent the "thick" electrode instead of two; so a wide range of electrode thickness can be investigated without adversely affecting potentials near the center line between the "thick" electrodes. The potentials at x-positions up to 30% of the slit widths were plotted as a function of y in the vicinity of the "thick" electrode; no effects of multiple thin electrodes were apparent.

The conformal map constants as well as calculated geometry (using Program #3, Appendix B, Statement #40-69) are given in Table III for the electrostatic lens in Figure 34. The calculated geometry compares to better than 1 part in 10^5 to the initial geometry which was used to compute the conformal mapping constants. This is well within machining tolerances for construction of lenses.





TABLE III

CONFORMAL MAPPING CONSTANTS AND CALCULATED GEOMETRY FOR AN EIGHT APERTURED ELECTROSTATIC LENS

	Conformal Map	Constants	
a =	$.50024775480706 \times 10^{-1}$	o = .18082807808053 x	10 ⁻⁶
b =	$.19300864069821 \times 10^{-2}$	p = .10108731694186 x	10 ⁻⁶
с =	$.75029876030201 \times 10^{-4}$	q = .54139569185460 x	10 ⁻⁷
d =	$.11355285860026 \times 10^{-4}$	r = .90256235746935 x	10 ⁻⁸
e =	$.18930615960949 \times 10^{-5}$	s = .13659682395425 x	10 ⁻⁸
f =	$.10138808939371 \times 10^{-5}$	t = .53100422724127 x	10-10
g =	$.56679183410157 \times 10^{-6}$	u = .20487528999131 x	10-11
h =	$.32014561619614 \times 10^{-6}$		

Calculated Geometry (cm)

Sl = 0.1000	· · ·	S6 = 0.1000	D3 = 0.0872
S2 = 0.1000		S7 = 0.1000	D4 = 0.0871
S3 = 0.1020		S8 = 0.1000	D5 = 0.0872
S4 = 0.1020		D1 = 2.0306	D6 = 0.5000
S5 = 0.1020		D2 = 0.5000	D7 = 2.0306

Computed trajectories were carried out on monoenergetic positive ions entering the lens system parallel to the y-axis. The time step (δt) used in all calculations was determined by first selecting a large time interval and calculating the final position of the particle at the seventh apertured slit. The time interval was then reduced in steps until the position of the ion at the seventh electrodes remained constant to five significant figures with successive changes in δt . Consistency in the final position was obtained with δt values of approximately .75 nanoseconds; however, time intervals of .1 nanoseconds were typically used to insure that the trajectories would be well within achievable experimental accuracy.

The final x-coordinates of the ions are indicated as a function of initial ion kinetic energy as well as initial x-coordinates in Figure 35. All ions enter the lens system parallel to the y-axis. The final x-coordinates for the 7300 eV ions form a sharp image at the seventh apertured plane at -0.0004 cm, -0.0005 cm, -0.0004 cm, and +0.0006 cm for ions with initial x-coordinates of +0.0025 cm, +0.0050 cm, +0.0075 cm, and +0.0100 cm respectively. The apparent discrepancy of the fourth final x-position from the previous three is an artifact of the calculation. The symmetry of the lens system about the y-axis was tested by using initial values for the ions of -0.0025 cm, -0.0050 cm, -0.0075 cm, and -0.0100 cm; the final x-coordinates at the seventh apertured plane agreed in magnitude but differed in sign from the previous results.

In using the conformal transformation method for calculations of the forces acting on the ions, the series expansion for the gradients of the potentials given in Equations (IV-6) and (IV-7) were used. Wallington (50) has found that by including terms up to and including



Figure 35. Trajectory Analysis of 7300 eV Ions in an Eight Apertured Symmetric Lens

the fourth partial of the potential, the paraxial trajectories calculated are good approximations to the true trajectories only when the starting x-coordinates of the trajectories are less than approximately 1/10 of the width of the apertures. Therefore, in the present calculations a starting position of \pm 0.0100 cm for the ions represents the x-coordinates extrema as partial derivatives up to and including only the fourth were included. The calculations of paraxial trajectories with starting positions greater than 0.0100 cm were considered for purposes of comparison. Figure 36 is a point-by-point ray trace of 7300 eV positively charged ions through the eight apertured lens with +7440 volts on the "thick" electrodes. With starting positions of \pm 0.0100 cm the ions reach maximum off-axis values of \mp 0.0181 cm. At this offaxis point the second term in Equation (IV-7) was less than 1% of the first term. If the starting x-coordinate of the paraxial trajectory is increased to \pm 0.015 cm or \pm 0.020 cm (the ions reaching maximum off-axis x-coordinates of \mp 0.0276 cm and \mp 0.0378 cm), the second term in the series expansion (Equation (IV-7) now represents 4% and 9% respectively of the first terms. Because $(\frac{\delta^5 v}{5})$ is positive in the δy o,y vicinity of the maximum x-coordinates of a trajectory in Figure 36, the calculated $(\frac{\delta V}{\delta y})$ and hence the force in the y-direction is smaller than it should be. The ion therefore spends too much time in the lens system subject to the forces acting in the x-direction and appears at increasingly larger final x-coordinates at the seventh apertured plane with increasing starting x-coordinates. The second term in Equation (IV-6) approaches only 1% of the first term as the starting x-coordinate for the paraxial trajectory is increased to ± 0.0200 cm. To use starting x-coordinates for the paraxial trajectories in the range 0.010 to



Figure 36. Ray Trace of a 7300 eV Positive Ion Through the Eight Apertured Lens

0.020 would therefore require the inclusion of an additional term in Equation (IV-6) as it must be significant. Starting x-positions greater than 0.0200 cm would no doubt require additional terms in both Equations (IV-6) and (IV-7).

The introduction of an apertured plane with an adjustable slit into the Einzel lens was considered in order to determine whether this would adversely affect the final positions of the trajectories or the image size. A second lens was conformally mapped to give the constants and calculated geometry in Table IV. This second lens is identical in calculated geometry to the first lens (Table III) except for the much smaller aperture in the seventh plane (S7). Ray traces were carried out for positive ions with paraxial trajectories as previously described. The results of the final x-coordinates of the ions are illustrated in Figure 37 as well as trajectory analysis in Figure 38 through Figure 40. Figure 37 illustrates the path of ions with the proper as well as improper energy to pass the lens at a given potential on the "thick" electrodes. Figure 38 when compared to Figure 35 illustrates the minor focusing change when the seventh aperture is changed from a large to a narrow slit. The image size of a 7300 eV beam of ions compares favorably with the image size of the first lens. The final x-coordinates at the seventh apertured plane for the second lens are -0.0004 cm, -0.0004cm, -0.0005 cm, and +0.0006 cm for initial x-coordinates of 0.0025 cm 0.0050 cm, 0.0075 cm, and 0.0100 cm respectively. Therefore, changes in the size of the collector slit do not significantly change focal properties of the Einzel lens.

It was previously established that in order for the *Einzel* lens to be useful as an energy selective device for ion kinetic spectra,

TABLE IV

CONFORMAL MAP CONSTANTS AND CALCULATED GEOMETRY FOR AN EIGHT APERTURED LENS WITH A NARROW SEVENTH APERTURE

	Conformal Map Constant	.s
$a = .50024774723523 \times 10^{-1}$	1 o =	= $.17963624022968 \times 10^{-6}$
b = .19300862635880 x 10	2 p =	= $.10027910788180 \times 10^{-6}$
$c = .75028372396914 \times 10^{-1}$	4 q :	$= .53657306727246 \times 10^{-7}$
d = .11354848732495 x 10	4 r :	$= .91460386857642 \times 10^{-8}$
e = .18924732492200 x 10	5 s :	$= .28076474096165 \times 10^{-10}$
$f = .10121472509559 \times 10^{-1}$	5 t :	$= .86093522158906 \times 10^{-13}$
$g = .56494427727956 \times 10^{-1}$	6 u	$= .13306465669631 \times 10^{-13}$
$h = .31856328547029 \times 10^{-1}$	6	

Calculated Geometry (cm)

S1 = 0.1000	S6 = 0.1020	D3 = 0.0874
S2 = 0.1000	S7 = 0.0020	D4 = 0.0874
S3 = 0.1020	S8 = 0.1000	D5 = 0.0874
S4 = 0.1020	D1 = 2.0306	D6 = 0.5000
S5 = 0.1020	D2 = 0.5000	D7 = 0.5000



Figure 37.

 Ray Trace of Ions Focused (a) in Front, (b) at, and
 (c) Behind a Narrow Slit in an Eight Apertured Lens



Figure 38. Trajectory Analysis of an Eight Apertured Lens With a Center Electrode Potential of 7440 Volts and a Narrow 7th Slit



Figure 39. Trajectory Analysis of an Eight Apertured Lens With a Center Electrode Potential of 5952 Volts and a Narrow 7th Slit



Figure 40. Trajectory Analysis of an Eight Apertured Lens With a Center Electrode Potential of 4464 Volts and a Narrow 7th Slit

there must exist a linear relationship between the energy of the ions focused and the voltage on the "thick" electrodes. This relationship is illustrated in Figure 39 and Figure 40 where the potential on the "thick" electrodes is reduced to 5952 volts and 4464 volts respectively. The arrow in the figures indicates the required focal point for a linear relationship; i.e. V(center electrode)/V(focus) = 1.0192.

The final problem is to calculate the energy resolution of the combination $\Pi/4\sqrt{2}$ radial electrostatic analyzer followed by the linear electrostatic lens. The method used in calculation of trajectories restricted analysis of the three element electrostatic lens to the center 10%. Fortunately, when two beams of ions with similar energy exit the radial electric sector, the width of the combined beam is only 0.139 cm (Chapter II); thus the analysis uses approximately 15% of the combined beam in the calculated trajectories through the three element The ions entering the Einzel lens have initial trajectories lens. parallel to each other and perpendicular to the plane of each of the apertures. The ions entering the lens along the center line (x = 0.0)experience no deflection regardless of their energy or the potential on the "thick" electrodes of the lens. The further off-axis an ion of a given energy enters the lens, the more deflection it experiences at the energy resolving slit. To obtain the energy resolution of the Einzel lens, the final x-coordinates at the seventh apertured plane were plotted as a function of the initial x-coordinates for various energy paraxial trajectories, Figure 41. Linear extrapolations were then made to the full beam width. The energy resolution calculated will serve only as an approximation to the true energy resolving power of the lens due to the uncertainty in the extrapolation beyond the data points.



Figure 41. Energy Discriminating Properties of an Eight-apertured Electrostatic Lens With a Narrow Seventh Slit

The calculations indicate that the energy resolution using the *Einzel* lens described would be approximately .13% with a .0005 inch β -slit and .26% with a .002 inch β -slit and a 10% valley. No attempt has been made to optimize the energy resolution of the *Einzel* lens by changing geometries.

The energy resolution of the Mattauch-Herzog mass spectrometer without the β -slit modification was approximately 3-5%. It has been shown that because of the poor energy resolution and sensitivity the instrument is limited as a research tool for the study of first field-free region metastable decompositions. Modification of the β -slit and insertion of an electron multiplier increased the energy resolution to .6% while also increasing the detectibility and sensitivity of the instrument. Calculations have shown the feasibility of using an *Einzel* lens to further increase the energy resolution of the instrument while maintaining its utility as a general purpose mass spectrometer. The use of such a lens would give an energy dispersed intermediate energy image in the second field-free region at the β -slit and would thus circumvent the inherent low energy resolution associated with the Mattauch-Herzog geometry mass spectrometer by providing an independent adjustment of the aperture and energy bandwidth for Ion Kinetic Energy Spectra.

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APPENDIX A

NUMERICAL CALCULATION OF THE POTENTIAL DISTRIBUTION IN AN EIGHT APERTURED PLANE LENS

APPENDIX A

NUMERICAL CALCULATION OF POTENTIAL DISTRIBUTION

The region between the projections of the electrodes was mapped conformally on the positive imaginary half of the complex w-plane. The Schwarz-Christoffel transformation was used because of its general applicability to regions bounded by straight lines (52). For the calculations in Appendices A and B, the variable names a,b,c,\ldots,u (excluding i-n) are attributed successively to the internal and infinite ends of the electrodes as indicated in Figure 42. The conformal mapping of the planar lens system from the complex z-plane (z = x + iy) to the complex w-plane (w = u + iv) was performed by the inverse of the function (47, 53)

$$z = \int_{W_0}^{W} \frac{(x^2 - a^2) (x^2 - c^2) (x^2 - e^2) (x^2 - g^2) (x^2 - o^2) (x^2 - q^2) (x^2 - s^2) (x^2 - u^2)}{(x^2 - b^2) (x^2 - d^2) (x^2 - f^2) (x^2 - h^2) (x^2 - p^2) (x^2 - r^2) (x^2 - t^2)} dx$$
(A-1)

The function was decomposed into partial fractions, integrated, and the boundary conditions ware applied (48). The resulting equations contain the physical constants of the lens and the parameters governing the conformal mapping, Table V. From the nature of the problem the conformal mapping constants a,b,c,...,u are real and subject to the constraints a>b>c>d>e>f>g>h>o>p>q>r>s>t>u. The restrictions limit the solutions to one which is not obvious without further approximations.



Figure 42. Cross Section of Eight Element Lens System

r ₁ =	$\frac{(a^2-b^2)(b^2-c^2)(b^2-e^2)(b^2-g^2)(b^2-o^2)(b^2-q^2)(b^2-s^2)(b^2-u^2)}{2b(b^2-d^2)(b^2-f^2)(b^2-h^2)(b^2-p^2)(b^2-r^2)(b^2-t^2)b^2}$	
r ₂ =	$\frac{(a^2-d^2)(c^2-d^2)(d^2-e^2)(d^2-g^2)(d^2-o^2)(d^2-q^2)(d^2-s^2)(d^2-u^2)}{2d(b^2-d^2)(d^2-f^2)(d^2-h^2)(d^2-p^2)(d^2-r^2)(d^2-t^2)d^2}$	
r ₃ =	$\frac{(a^{2}-f^{2})(c^{2}-f^{2})(e^{2}-f^{2})(f^{2}-g^{2})(f^{2}-o^{2})(f^{2}-q^{2})(f^{2}-s^{2})(f^{2}-u^{2})}{2f(b^{2}-f^{2})(d^{2}-f^{2})(f^{2}-h^{2})(f^{2}-p^{2})(f^{2}-r^{2})(f^{2}-t^{2})f^{2}}$	
r ₄ =	$\frac{(a^{2}-h^{2})(c^{2}-h^{2})(e^{2}-h^{2})(g^{2}-h^{2})(h^{2}-o^{2})(h^{2}-q^{2})(h^{2}-s^{2})(h^{2}-u^{2})}{2h(b^{2}-h^{2})(d^{2}-h^{2})(f^{2}-h^{2})(h^{2}-p^{2})(h^{2}-r^{2})(h^{2}-t^{2})h^{2}}$	
r ₅ =	$\frac{(a^{2}-p^{2})(c^{2}-p^{2})(e^{2}-p^{2})(g^{2}-p^{2})(o^{2}-p^{2})(p^{2}-q^{2})(p^{2}-s^{2})(p^{2}-u^{2})}{2p(b^{2}-p^{2})(d^{2}-p^{2})(f^{2}-p^{2})(h^{2}-p^{2})(p^{2}-r^{2})(p^{2}-t^{2})p^{2}}$	
r ₆ =	$\frac{(a^2-r^2)(c^2-r^2)(e^2-r^2)(g^2-r^2)(o^2-r^2)(q^2-r^2)(r^2-s^2)(r^2-u^2)}{2r(b^2-r^2)(d^2-r^2)(r^2-r^2)(h^2-r^2)(p^2-r^2)(r^2-t^2)r^2}$	
r ₇ =	$\frac{(a^{2}-t^{2})(c^{2}-t^{2})(e^{2}-t^{2})(g^{2}-t^{2})(o^{2}-t^{2})(q^{2}-t^{2})(s^{2}-t^{2})(t^{2}-u^{2})}{2t(b^{2}-t^{2})(d^{2}-t^{2})(f^{2}-t^{2})(h^{2}-t^{2})(p^{2}-t^{2})(r^{2}-t^{2})t^{2}}$	
s ₁ =	$a + r_1 \ln \frac{a+b}{a-b} + r_2 \ln \frac{a+d}{a-d} + r_3 \ln \frac{a+f}{a-f} + r_4 \ln \frac{a+h}{a-h} + r_5 \ln \frac{a+p}{a-p}$	+ $r_6 \ln \frac{a+r}{a-r}$ + $r_7 \ln \frac{a+t}{a-t}$ + $\frac{ac^2 e^2 g^2 o^2 g^2 s^2 u^2}{b^2 d^2 f^2 h^2 p^2 r^2 t^2}$

TABLE V

EQUATIONS TO DETERMINE THE PARAMETERS GOVERNING THE CONFORMAL MAPPING

r,

TABLE V (Continued)

s ₂) — 1	с +	- r_lr	h b+e b-e	+ :	r ₂ ln	<u>c+d</u> c−d	+	r ₃ ln	c+f c-f	+	r_4^{ln}	<u>c+h</u> c-h	+	r ₅ ln	c+p c-p	+ r	6^{ln}	<u>c+r</u> c-r	+ r ₇ ln	<u>c+t</u> c-t	$+\frac{a^2}{b}$	$e^2g^2o^2$ d^2f^2h	$\frac{2q^2s^2u^2}{2p^2r^2t^2}$	2
sg	=	e -	r lr	h <u>b+e</u> b-e	· + :	r_ln	<u>d+e</u> d-e	+	r ₃ ln	<u>e+f</u> e−f	+	r_4 ln	<u>e+h</u> e-h	+	r ₅ ln	<u>e+p</u> e-p	+ r	6 ^{ln}	<u>e+r</u> e-r	+ r ₇ ln	<u>e+t</u> e-t	$+\frac{a^2}{b}$	$\frac{2^2 \text{eg}^2 \text{o}^2}{2^2 \text{f}^2 \text{h}^2}$	$\frac{2}{q} \frac{2}{s} \frac{2}{u} \frac{2}{u}$	2
s		g -	r rlı	h b+g b-g	· + :	r ₂ ln	<u>d+g</u> d-g	+	r ₃ ln	<u>f+g</u> f-g	+	r_4 ln	<u>g+h</u> g-h	+	r ₅ ln	<u>g+p</u> g-r	+ r	6 ^{ln}	<u>g+r</u> g-r	+ r ₇ ln	<u>g+t</u> g-t	$+\frac{a^2}{b^2}$	$\frac{2^2 e^2 go}{2^2 d^2 f^2 h}$	$\frac{2q^2s^2u^2}{2p^2r^2t^2}$	2
s	=	0 -	+ r_l1	h <u>b+o</u> b−o	• + :	r ₂ ln	<u>d+o</u> d-o	+	r ₃ ln	<u>f+o</u> f−o	. +	r ₄ ln	<u>h+o</u> h-o	+	r_ln	<u>о+р</u> о-р	+ r	6 ^{ln}	o+r o-r	+ r ₇ ln	<u>o+t</u> o-t	+ $\frac{a^2}{b}$	$\frac{2^2 e^2 g^2}{2^2 d^2 f^2 h}$	$\frac{2^2 s^2 u^2}{2^2 r^2 t^2}$	2
se	=	d -	⊦r_lr	b+q	• + :	r_ln	<u>d+q</u> d-q	+	r ₃ ln	<u>f+q</u> f-q	+	r_4^{ln}	<u>h+q</u> h-q	; +	r ₅ ln	<u>p+q</u> p-q	+ r	6 ^{ln}	<u>q+r</u> q-r	+ r ₇ ln	<u>q+t</u> q-t	$+\frac{a^2}{b}$	$\frac{2}{2} \frac{2}{e} \frac{2}{g} \frac{2}{g}$	$\frac{2}{2} \frac{2}{p} \frac{2}{r} \frac{2}$	2
s,	, =	s -	⊦r_l	$\frac{b+s}{b-s}$	· + '	r ₂ ln	<u>d+s</u> d-s	+	r ₃ ln	<u>f+s</u> f-s	+	r ₄ ln	<u>h+s</u> h-s	+	r ₅ ln	<u>p+s</u> p-s	+ r	6 ^{ln}	<u>r+s</u> r-s	+r ₇ ln	<u>s+t</u> s-t	$+\frac{a^2}{b}$	$\frac{2^2 e^2 g^2}{2^2 f^2 h}$	$\frac{2^2 q^2 s u^2}{2^2 r^2 t^2}$	2
s ٤	3 =	u -	r lı	b+u b-u	+	r2 ^{ln}	<u>d+u</u> d-u	+	r ₃ ln	<u>f+u</u> f-u	+	r ₄ ln	<u>h+u</u> h-u	+	r ₅ ln	<u>p+u</u> p-u	+ r	6 ^{ln}	<u>r+u</u> r-u	+ r ₇ ln	<u>t+u</u> t-u	$+\frac{a^2}{b}$	$\frac{2^2 e^2 g^2}{2^2 d^2 f^2 h}$	$\frac{2^2 q^2 s^2}{2^2 q^2 s^2}$	$\frac{1}{2}$

Part I - The Transformation Constants

Boerboom (47) has introduced a general method for obtaining the transformation constants for linear electrostatic lens systems where all slit dimensions are smaller than the distances between successive apertured planes $(\frac{1}{4}\pi r_{\#}>2s_{\#}, \text{ Figure 42})$. Although this was not the case for the lenses in the present study, the approximation will serve as a basis for procedures to obtain the transformation constants. Subject to the constraint $\frac{1}{4}\pi r_{\#}>2s_{\#}, a^2>>b^2>>c^2>>\text{etc.};$ therefore, a>>c> e>>g>>o>>q>>s>>u and likewise b>>d>>g>>h>>p>r>>t. Using the series expansion

$$\ln \frac{a+b}{a-b} = 2 \frac{b}{a} \left\{ 1 + \frac{1}{3} \frac{b^2}{a^2} + \frac{1}{5} \frac{b^4}{a^4} + \cdots \right\}$$
 (b

and neglecting terms of order higher than one, the following equations clearly follow from Table V.

- $a + 2r_1 \left(\frac{b}{a}\right) = s_1$ (A-3) $r_1 = \frac{a^2}{2b}$ (A-11) $2r_1 \left(\frac{c}{b}\right) + 2r_2 \left(\frac{d}{c}\right) = s_2$ (A-4) $r_2 = \frac{r_1 c^2}{bd}$ (A-12)
- $2r_2(\frac{e}{d}) + 2r_3(\frac{f}{e}) = s_3$ (A-5) $r_3 = \frac{r_2e^2}{df}$ (A-13)
- $2r_{3}(\frac{g}{f}) + 2r_{4}(\frac{h}{g}) = s_{4}$ (A-6) $r_{4} = \frac{r_{3}g^{2}}{fh}$ (A-14)

$$2r_4(\frac{o}{h}) + 2r_5(\frac{p}{o}) = s_5$$
 (A-7) $r_5 = \frac{r_4}{hp}$ (A-15)

$$2r_{5}\left(\frac{q}{p}\right) + 2r_{6}\left(\frac{r}{q}\right) = s_{6} \quad (A-8) \qquad r_{6} = \frac{r_{5}q}{pr} \qquad (A-16)$$

$$2r_{6}\left(\frac{s}{r}\right) + 2r_{7}\left(\frac{t}{s}\right) = s_{7} \quad (A-9) \qquad r_{7} = \frac{r_{6}s^{2}}{rt} \qquad (A-17)$$

$$2r_{7}\left(\frac{u}{t}\right) + \frac{\frac{2}{a}\frac{2}{c}\frac{2}{e}\frac{2}{g}\frac{2}{o}\frac{2}{q}\frac{2}{s}\frac{2}{u}^{2}}{\frac{2}{b}\frac{2}{d}\frac{2}{f}\frac{2}{h}\frac{2}{p}\frac{2}{r}\frac{2}{t}\frac{2}{t}^{2}}$$
(A-10)

The approximate equations (A-3)-(A-17) were solved to obtain expressions for the transformation constants, Table VI. Equations (A-5) - (A-17) were made exact by adding the terms ignored when Equation (A-2) was used to approximate the solutions. For example, Equation (A-3) was re-written

$$a + 2r_1(\frac{b}{a}) = s_1 - (r_1 \ln \frac{a+b}{a-b} - 2r_1(\frac{b}{a})) - r_2 \ln \frac{a+d}{a-d} - r_3 \ln \frac{a+f}{a-f} - r_4 \ln \frac{a+h}{a-h} - r_4 \ln \frac{a+h}{a-h}$$

$$r_{5}\ln \frac{a+p}{a-p} - r_{6}\ln \frac{a+r}{a-r} - r_{7}\ln \frac{a+t}{a-t} - \frac{ac^{2}e^{2}g^{2}c^{2}q^{2}s^{2}u^{2}}{b^{2}d^{2}f^{2}h^{2}p^{2}r^{2}t^{2}}$$
(A-3a)

To avoid repetition, the *exact* presentation of Equations (A-3a) -(A-17a) are listed in Appendix B, Program 2, Subroutine CONMP8, Statements #0112 - #0126. The values generated for S11,S22,...,S88,R11,..., R77 were used to replace $s_1, s_2, \ldots, s_8, r_1, \ldots, r_7$ respectively in Equations (A-3) - (A-17). The new equations were solved for the transformation constants a,b,c,...,u in terms of S11,S22,...,S88,R11,...,R77 and $s_1, s_2, \ldots, s_8, r_1, \ldots, r_7$. The equations are given in Appendix B, program 2, Subroutine CONMP8, statements #0143 - #0157. The variable names in the computer program A1,B1,...,RB1,SB1,...,U1 correspond to the transformation constants a,b,...,r,s,...,u.

The new values of the constants were substituted into the *exact* equations (Appendix B, Program 2, Subroutine CONMP8, Statements Oll2 -0l26) to generate new values for Sll,...,S88,Rll,...,R77 which were in turn used to calculate better values for the transformation constants

a =	$=\frac{\frac{s_1}{2}}{2}$		•		$q = \frac{s_6}{2^2}$	$\begin{array}{c} & 2 & 2 & 2 & 2 & 2 \\ & 5 & 5 & 4 & 3 & 5 & 2 \\ 1 & 2 & 2 & 2 & 2 & 2 \\ r & 5 & r & 4 & 3 & 2^{1} \end{array}$	$\frac{1}{2}$
b =	$\frac{s_1}{2^3r_1}$				$r = \frac{s}{2^2}$	$\begin{array}{c} 2 & 2 & 2 & 2 \\ \underline{6^{s}5^{s}4^{s}3^{s}2^{s}} \\ 3 & 2 & 2 & 2 \\ \mathbf{r_{6}r_{5}r_{4}r_{3}}^{r} \end{array}$	$\frac{2}{\frac{1}{2}}$
c =	$= \frac{\frac{s_2 s_1}{2}}{2 r_1}$				$s = \frac{s_7}{2^2}$	$\begin{array}{c} 2 & 2 & 2 & 2 \\ \frac{2}{5} & 2 & 2 & 2 \\ \frac{5}{5} & 2 & 2 & 2 \\ 5 & 2 & 2 & 2 & 2 \\ 5 & 2 & 2 & 2 & 2 \\ \end{array}$	2^{2} 2 2^{2} 1 2^{2} 2
d =	$=\frac{\frac{s_{2}^{2}s_{1}^{2}}{\frac{r_{2}^{7}r_{2}r_{1}^{2}}{r_{2}r_{1}}}$				$t = \frac{s}{2}$	$^{1}6^{1}5^{1}4^{1}3^{1}$ $^{2}2^{2}2^{2}2^{2}$ $7^{5}6^{5}5^{4}4^{3}3^{5}$	$\frac{2^{2}1}{\frac{2^{2}2^{2}}{\frac{2^{2}1}{2}}}$
e =	$=\frac{\frac{2^{2}}{3^{3}}\frac{2^{2}}{2^{9}}\frac{1}{2^{2}}}{\frac{2^{9}}{2^{2}}\frac{2^{2}}{2^{1}}}$, ,			2 ² 	$r_{7}r_{6}r_{5}r_{4}r_{7}r_{7}r_{6}r_{5}r_{7}r_{7}r_{7}r_{7}r_{7}r_{7}r_{7}r_{7$	$\frac{2}{3}$ $\frac{2}{2}$ $\frac{2}{1}$ $\frac{2}{3}$ $\frac{2}{2}$ $\frac{2}{1}$
f =	$\frac{s_{3}^{2}s_{2}^{2}s_{1}^{2}}{s_{1}^{2}r_{3}r_{2}^{2}r_{1}^{2}}$				$u = \frac{0}{2^2}$	9 2 2 2 2 2 ⁹ 7 ⁷ 6 ^r 5 ^r 4 ¹	2 2 2 ² 3 ² 2 ¹
g =	$=\frac{{}^{s_{4}}{}^{s_{3}}{}^{s_{2}}{}^{s_{1}}{}^{1}}{{}^{2}}{}^{13}{}^{r_{3}}{}^{2}{}^{r_{2}}{}^{r_{1}}{}^{2}}$						•
h =	$=\frac{s_4^2s_3s_2s_1}{2^{15}r_4r_3r_2r_1^2}$						
0 =	$=\frac{\frac{s_{5}s_{4}s_{3}s_{2}s_{1}}{s_{1}r_{4}r_{3}r_{2}r_{2}r_{2}}}{r_{4}r_{3}r_{2}r_{2}r_{2}}$	4				•	
p =	$=\frac{\frac{2}{5} + \frac{2}{5} + \frac{2}{3} + \frac{2}{5} + \frac$	2 L		• •			

SOLUTIONS TO APPROXIMATE EQUATIONS (A-3)-(A-17)

(Program 2, Subroutine CONMP8, Statements 0143 - 0157). The iteration process was terminated when two successive values of <u>e</u> differed by less than 10^{-9} . In general convergence is within a few iterations; however, for certain lens geometries successive values of the transformation constants oscillated with increasing divergence about their respective true values. Wallington (46) found that by employing an additional sequence to the iteration scheme the oscillation could be damped. The modified procedure was to carry out the first two iterations in the normal manner, and for the third iteration to use as the latest values the mean of the values generated in the previous two iterations. The fourth iteration, but the fifth used the mean of the third and fourth iterations. By use of this weighting procedure, convergence was obtained within 30 iterations for all lens geometries studied.

Up to this point lenses have been considered in which slit dimensions were smaller than the distances between successive apertured planes. In lens systems where the slit dimensions are large compared to distances between successive apertures, Wallington (46) and Boerboom (53) have developed special mathematical procedures for approximating and refining the transformation constants. Although these procedures are general, for large lens systems (over 3 or 4 electrode pairs) the mathematics becomes extensive. It was therefore decided to develop a simplier procedure which would be generally applicable. The procedure was to first obtain the transformation constants for a lens which had the proper slit widths and reasonably large spacing between adjacent slits (i.e. $\frac{1}{4}\pi r_{\#}^{>}2s_{\#}$). For this system Equations (A-3) - (A-17) were applicable; so approximate, then *exact* solutions were possible. The

lens system was then changed slightly by decreasing the distances between apertured planes. Approximate solutions were not obtained for this second lens but rather the more accurate solutions from the previous lens were used as approximate solutions. The transformation constants were refined by iterations with the more exact equations (Program 2, Subroutine CONMP8, Statements 112 - 126) until constant values were obtained. A third lens was then considered in which the distances between adjacent planes was further decreased. The approximate transformation constants for the third lens were the *exact* values from the second lens. This procedure was repeated until the desired lens geometry was obtained.

Part II - Determination of Potentials in the Lens System

The central axis of the lens system coincides with the imaginary axis in both the z-plane and the w-plane. The equation which couples points on one imaginary axis to those on the other was obtained from Equation (A-1)(47).

$$y = v + 2r_{1} \tan^{-1} \frac{v}{b} + 2r_{2} \tan^{-1} \frac{v}{d} + 2r_{3} \tan^{-1} \frac{v}{f} + 2r_{4} \tan^{-1} \frac{v}{h} + 2r_{5} \tan^{-1} \frac{v}{h} + 2r_{5} \tan^{-1} \frac{v}{c} + 2r_{6} \tan^{-1} \frac{v}{r} + 2r_{7} \tan^{-1} \frac{v}{t} - \frac{a^{2}c^{2}e^{2}g^{2}c^{2}q^{2}s^{2}u^{2}}{b^{2}d^{2}f^{2}h^{2}p^{2}r^{2}t^{2}} / v$$
 (A-18)

where r_1, \ldots, r_7 and a,b,...,u correspond to the distances between apertured planes and the conformal mapping constants respectively, Figure 42. Equation (A-18) was solved iteratively for <u>v</u> at specified <u>y</u> positions along the imaginary axis in the z-plane. The total potential acting at

(A-19)

the y-coordinate is the sum of the contributions of each individual electrode and in the case of symmetric potentials, each electrode pair.

$$\begin{aligned} v_{\text{total}} &= \frac{8}{12} \ v_1' \\ v_1' &= \frac{2v_1}{\pi} \ \tan^{-1} \frac{v}{b} \\ v_2' &= \frac{2v_2}{\pi} \ (\tan^{-1} \frac{v}{d} - \tan^{-1} \frac{v}{b}) \\ v_3' &= \frac{2v_3}{\pi} \ (\tan^{-1} \frac{v}{f} - \tan^{-1} \frac{v}{d}) \\ v_4' &= \frac{2v_4}{\pi} \ (\tan^{-1} \frac{v}{h} - \tan^{-1} \frac{v}{f}) \\ v_5' &= \frac{2v_5}{\pi} \ (\tan^{-1} \frac{v}{p} - \tan^{-1} \frac{v}{f}) \\ v_6' &= \frac{2v_6}{\pi} \ (\tan^{-1} \frac{v}{r} - \tan^{-1} \frac{v}{p}) \\ v_7' &= \frac{2v_7}{\pi} \ (\tan^{-1} \frac{v}{t} - \tan^{-1} \frac{v}{p}) \\ v_8' &= \frac{2v_8}{\pi} \ (\frac{\pi}{2} - \tan^{-1} \frac{v}{t}) \end{aligned}$$

and V_1, V_2, \ldots, V_8 are the potentials on each electrode pair.

The potentials at off-axis points were calculated with Equation (IV-5). The necessary first, second, third, and fourth derivatives of

where,

the potential required by Equations (IV-5) - (IV-7) are calculated in subroutines 'FSTPOT', 'SNDPOT', 'TRDPOT', and 'FRHPOT' respectively (Program 3, Appendix B).

PLEASE NOTE:

Appendix B has extremely small print. Filmed in the best possible way.

UNIVERSITY MICROFILMS.
APPENDIX B

COMPUTER PROGRAMS

PROGRAM #1 * * *

ION TRAJECTORY CALCULATIONS THROUGH A 31.8 DEGREE ELECTROSTATIC SECTOR BASED ON A CEC 21-110B MASS SPECTROMETER

THE CALCULATION STARTS WITH THE ION AT THE FINAL (ADJUSTABLE) THE CALCULATION STARTS WITH THE ION AT THE FINAL (ADJUSIABLE) SLIT OF THE ION SOURCE. A MASS, ANGULAR DIVERGENCE ALPHA (IN THE X-Y PLANE], AND ACCELERATING POTENTIAL ARE ASSIGNED TO THE ION. THE ION TRAVERSES THE FIRST FIELD-FREE REGION AND IF IT HAS THE CORRECT CORDINATES ENTERS THE ELECTROSTATIC ANALYZER. BY KNOWING THE POSITION AND THE FORCES ACTING ON THE ION NEW VELOCITIES ARE CALCULATED EVERY DT (DELTA TIME).

EVERY DT (DELTA TIME). TERMINATION OF THE PROGRAM OCCURS WHENEVER THE ION FAILS TO ENTER THE ELECTROSTATIC SECTOR, HITS EITHER SECTOR PLATE, OR COMPLETES THE TRIP THROUGH THE SECTOR. THE OUTPUT CONSISTS OF ALL INPUT DATA, A MESSAGE INDICATING WHY PROGRAM WAS TERMINATED, WHETHER THE ION REACHES THE SECOND FIELD-FREE REGION, AND FINALLY THE POSITION AND THE VELOCITY OF THE TON AT ITCLASE DOINT. AND THE VELOCITY OF THE ION AT ITS LAST POINT.

CALCULATED PROGRAM VARIABLE NAMES V = TOAL RELOCITY OF THE ION IN THE FIRST FIELD-FREE REGION (CM/SEC) VX = TOAL RELOCITY OF THE ION IN THE FIRST FIELD-FREE REGION (CM/SEC) VY = Y-COMPONENT OF VELOCITY OF ION IN THE FIRST FIELD-FREE REGION (CM/SEC) T = TIME TO TRAVERSE THE FIRST FIELD-FREE REGION (SEC) Y = V-POSITION OF THE PARTICLE AT THE ENTRANCE OF THE ELECTRIC SECTOR -- REFERENCED TO THE CENTER LINE OF THE FIRST FIELD-FREE REGION. THEN TO THE VERTEX OF THE ELECTROSTATIC FIELD-FREE REGION. THEN TO THE VERTEX OF THE ELECTROSTATIC SECTOR (CM) R = RADIAL DISPLACEMENT OF ION IN THE ELECTRIC SECTOR (CM) VTHETA = VELOCITY OF ION IN ELECTRIC SECTOR IN THE THETA DIRECTION (RADIANS/SEC) THETA = ANGULAR POSITION OF THE PARTICLE AT ANY TIME (RADIANS) VR = VELOCITY OF THE ION IN SUFCTRIC SECTOR IN THE RADIAL DIRECTION (CM/SEC) AA = ELECTROSTATIC FORCE ACTING ON THE ION IN THE ELECTRIC AA = ELECTRUSTATIL FURLE ACTING ON THE TON IN THE ELECTRIC SECTOR (ERGS) BB = CENTPIPETAL FORCE OF THE TON IN THE ELECTRIC SECTOR (ERGS) FNET = NET FORCE ACTING ON THE ION IN THE ELECTRIC SECTOP (ERGS) ER = ELECTRIC FIELD STRENGTH AT A GIVEN R (VOLTS/CH) VX2 = x-COMPDVENT OF VELOCITY OF THE ION AFTER LEAVING THE EVERTIC SECTOP (ENVER) VY2 = LECTRIC SECTOR (CM/SEC) VY2 = Y-COMPANENT OF VELOCITY OF THE ION AFTER LEAVING THE ELECTRIC SECTOR (CM/SEC) XKEX2 = KINETIC ENERGY OF THE ION IN X-DIRECTION AFTER LEAVING THE ELECTRIC SECTOR (VOLTS) XKEY2 = KINETIC ENERGY OF ION IN Y-DIRECTION AFTER LEAVING THE ELECTRIC SECTOR (VOLTS)

VARIABLES FOR A GIVEN RUN DT = TIME INTERVAL FOR INCREMENT (SEC)

c

ANU = MASS OF ION (AMU) YISS = Y-COORDINATE OF ION IN ION SOURCE SLIT ZERO TAKEN AS CENTER (CM) XKE = KINETIC ENERGY OF ION - ACTUALLY ACCELERATING XKE = KINETIC EMEMOT UP IUN - ACTUALLY ACCELERATING VOLTAGE (VOLTS) ESP = ELECTRIC SECTOR POTENTIAL, POSITIVE PLATE WITH RESPECT TO INSTRUMENT GROUND (VOLTS) ALPHA = ANGULAR DIVERGENCE OF ION FROM THE NORMAL X-Y PLANE (POSITIVE OR NEGATIVE RADIANS) INSTRUMENT AND PHYSICAL CONSTANTS AE = RADIUS OF CURVATURE OF ELECTRIC SECTOR (CM) XTHETA = ELECTRIC SECTOR CURVATURE = (PI/(4*SQRT(2)) RADIANS) R1 = RADIUS TO INNER ELECTRIC SECTOR PLATE (CM) R2 = RADIUS TO OUTER ELECTRIC SECTOR PLATE (CM) SEI = ENTRANCE SLIT WIDTH TO ELECTROSTATIC SECTOR (CM) SEO = SXIT SLIT FROM ELECTROSTATIC SECTOR (CM) XLE = LENGTH OF FIRST FIELO-FREE REGION (CM) E = ELECTRON CHARGE = 1.6021917 E-19 COUL. ONE AMU = 1.66043 E-24 GRAMS --------------

IMPLICIT REAL*8 (A-H,D-Z) SOR T(X)=D SOR T(X) SIN(X)=DSIN(X) COS(X)=DCOS(X) ALOG(X)=DLOG(X) ARSIN(X)=DARSIN(X) ESP=372 DO 69 LL=1,3 ALPHA=-.00044 DO 110 J=1.3 XKE=7525.0 DO 112 JJ=1,3 XKE=XKE+.5 VARIABLES FOR THIS RUN DT=1.0D-10 AMU=39.948D 00 YISS=0.00 00 INSTRUMENT AND PHYSICAL CONSTANTS AE=64D 00 XTHETA=. 555360367 SEI=.04064

c

C

c

С č

c C

с

с

0001

0002

C003

0004 0005

0006

0007

0008

0009

001.0

0011

0012

0013

0014

0015

C016

0017

0018

0019

0021

0022

0024

0025

0026

0028

SE0=.15240 XLE=AE/SQRT(2.00 00) R1=62.40615 R2=65.59385 E=1.60219170-19

CONVERSIONS AND OTHER USEFUL QUANTITIES XMASS=AMU*(1.66043D-24) THET A=0.0 AAA=AE-SEO/2. BBB=AE+SEO/2.

	C	INITIALIZATION OF VARIABLES TO ZERO	0044	
C029		VX2=0.0	0004	THE TA = THE TA + VTHE TA + DT
0030		VY2=0.0		C C
0031		XK EX2=0.0		C CHECK TO SEE TE TON HAS HIT ELECTRIC SECTOR WALL
0022			0065	TE(R=AE111.12.12
0052			0066	
0033 .		X=0.0	0067	12 IFIN-X1/14,14,12
C034		Y=0.0	0001	13 1F (R2-R) 14, 14, 12
0035		R=0.0		
0036		1=0		C CHECK TO SEE TE TON IS AT EXIT OF THE TOP THE
	r		0068	12 IF(XTHETA-THETA) 20, 20, 21
	č		0069	21 69 10 10
	L	VELOCITY OF ION	0070	
0037		V=SQRT((2.D 00*E*XKE*1.0D 07)/XMASS)	0071	14 #R1(E (6,25)
	С		0073	25 FURMAT(IH , ION HIT PLATE IN ELECTROSTATIC SECTOR:)
	С	COMPONENT DE VELOCITY IN X AND Y DIRECTIONS	0072	GO TO 121
0033				C C
0030				C CHECK TO SEE TO UTIL OWNER STORES
0054	•	VI-V+SIN(ALPHA)		ELECTRIC SECTOR INTO SECOND FIELD
	Ĺ		. 0073	C FREE REGION
	С	TIME TO REACH THE ELECTRIC SECTOR	0.071	20 IF(R-AE)31,32,33
0040		T=XLE/VX	0074	31 IF(R-AAA)34,34,32
	r		0075	33 IF(BBB-R)34,34,32
	č		0076	32 WRITE(6, 60)
00/1	6	POSITION OF IGN AT ELECTRIC SECTOR	0077	
6041		Y=YISS+VY*T	0011	40 FORMATTIN , ION HAS PASSED THROUGH EXIT SLIT OF ELECTRIC SECTOR ()
0042		X=XLE		
	С			C X- AND Y-COMPONENTS DE VELOCITY DE TON IN SECOND STELD STEL
	c	CHECK TO SEE TE TON WITH ENTER ELECTRIC SECTOR		C REGION FIELD FREE
0043	•	TEIVIL 2 3	0078	
0043			0079	
0044		3 1F(Y-SE1/2)2,2,4	0080	ANEX2=(AMASS*VX2*VX2)/(2.0D 00+E*1.0D 07)
0045		1 IF(Y+SEI/2)4,2,?	0080	VY2=VR
0046		4 WRITE(6,5)	0081	XKEY2=(XMASS*VY2*VY2)/(2.D 00*F*1.0D 07)
0047		5 FORMAT(1H ION FAILED TO MAKE ENTRANCE TO ELECTRIC SECTOR:)	C082	WRITE(6,102) XKE, YISS ESP. ALDHA, AND DE SET CEO H H P THERE
004.9		CO TO TO TO TO TO TALE OF ON TAKE INTRANCE TO ELECTRIC SECTORY		2XKFX2, W2, WEW2, T
0040	~	55 15 121	0083	
	6			TO A WARTIN , // +' INITIAL CONDITIONS', /, * XKE + , F7.2. /, * YISS + .
	C	CHANGE ORIGIN TO VERTEX OF ELECTRIC SECTOR		2=12-4+/ ESP= +,F6-1+/+ ALPHA= +,F8-5+/+ AMU= +,F8-6+/+ DT+ +
004 9		2 X=0.0		3E15.7./. SEI= '.F7.5./. SEO= '.F7.5.////. ETNAL VALUES
0050		Y=AE+Y		4' X= ',F10.6./.' Y= '.F10.6./.! P= 1.510.6./.! THE TALLES !!!
	r			5' VX2= 1,514.6.5X.1VKEV2= 1.50 2.4 1 10.077, 1HE1A= ',F8.67/,
	ř	ELECTRIC FIELD IN ELECTROSTATIC SECTOR		6F8-2-/-+ 1- + T0)
0051	C C	COL CONTRICTION FLECTRUSTATIC SECTOR	0084	
0051	•	-25T=-F25	0085	
0052		XK1=(ESP1-ESP)/ALOG(R2/R1)	0005	34 WRITE(6,41)
	С		0086	41 FORMAT(1H + TON HAS COMPLETED PASS THROUGH ELECTRIC SECTOR OUT FILE
	С	CHANGE TO CYLINDERICAL COORDINATES		2LED TO PASS EXIT SITTI
0052				C
005/				Y- AND Y CONCURSES USE
0054		VIHEIA=VX/R		A AND F-COMPONENTS OF VELOCITY OF ION IN SECOND FIELD-FREE
0055		VR=VY	0087	C REGION
0056	1	0 ER=XK1/R	0087	100 VX 2=R* VTHETA
0057		I=I+1	0089	XKEX2=(XMASS*VX2*VX2)/(2-00 00*5*1 00 07)
	r		C089	VY2=VR
	č		0090	XKE V2- CYNA CCHNWARWAAL COM A SAME AND A SAME
	C	FORCES ACTING IN RADIAL DIFECTION	0091	10 TT (10 12 V12 V12) / (2.0 00 + E + (.00 07)
0058		44 = E*ER*1.00 07	007.8	WEITERS, 1021 XKE, YISS, ESP, ALPHA, AMU, DT, SEI, SED, X, Y, R, THETA, VX2.
0059		BB=XMASS*R*VTHETA*VTHETA		2XKEX2, VY2, XKEY2, I
0060		FNET=AA+BB	0092	GO TO 112
	r		0093	121 WRITE(6+1)1)XKE, YISS, ESP, ALPHA ANU DI SET CEO M M - EVEL
	č	NEW RADIAL TON VELOCITY	C094	101 FOP MAT (1H -//-) INITIAL CONDITION OF A BURNET, SEU, A, T, R, IHETA, I
	c	NEW RADIAL ION VERGENT		2512 4 (1 55) + THITTAL CONDITIONS , /, * XKE= , F7.2, /, * YISS= *,
1001		VK= 1FNE! +DI J/XMA35+VK		ALL TT SPE ', FO.1,/,' ALPHA= ', F8.5,/,' AMU= ', F8.4./.' DT= '.
	С			3CL3+(+/+ SEI= +,F7+5+/+ SEO= +,F7+5+///+ FINAL VALUES+-/-
	С	POSITION OF ION AFTER TIME INTERVAL DT		4' X= ',F10.6,/,' Y= ',F10.6,/,' R= ',F10.6,/,' THETAL LOA
0062	•	VTHETA=VX/R		5' I= ',I8)
0063			0095	112 CONTINUE
0005		1-11 HA (2)	0096	

.

69 ESP≭ESP+3 STOP END

* * * PROGRAM #2 * * *

CONFORMAL MAPPING USING THE SCHWARZ-CHRISTOFFEL TRANSFORMATION

CONFORMAL MAPPING USING THE SCHWARZ-CHRISTOFFEL TRANSFORMATION THE PROGRAM DETERMINES TRANSFORMATION CONSTANTS FOR A LINEAR EIGHT APPERTURED ELECTROSTATIC LENS, THE MAIN PROGRAM SUPPLIES THE LENS GEOMETRY TO SUBROUTINE "COMMPD". THE SUBROUTINE CALCULATES THE CONFORMAL MAPPING TRANSFORMATION CONSTANTS USING APPROXIMATE AS WELL AS THE "EXACT" EQUATIONS, AFTER THE CONSTANTS FOR THE FIRST GEOMETRY ARE CALCULATED AND PRINTED, THE MAIN PROGRAM SUPPLIES A SECOND GEOMETRY TO THE SUBROUTINE. "COMMPS" DOES NOT CALCULATE APPROXIMATE CONSTANTS FOR THIS SECOND AND SUBSEQUENT GEOMETRIES BUT USES THE "EXACT" SOLUTION FROM THE PREVIOUS GEOMETRY AS A FIRST APPROXIMATION, AFTEN HA NEGATIVE LOG ARGUMENT. AT THE MAPPENDENT OF A CHANGE IN GEOMETRY IS ENCOUNTERED, THE PROGRAM WILL BOMB - USUALLY WITH A NEGATIVE LOG ARGUMENT. AT THIS POINT "XHOVE" SHOULD BE DECREASED AND THE PROGRAM RE-INITIATED STARTING AT THE LAST SET OF TRANSFORMATION CONSTANTS.

IMPLICIT REAL*8 (A-H,O-Z) COMMON PI,A,B,C,D,E,F,G,H,O,P,Q,R,S,T,U,XS1,XS2,XS3,XS4,XS5,XS6, ZXS7,XS8,R1,R2,R3,P4,R5,R6,R7,XMESS,IFLAG

c		2X31, X38, R1, R2, R3, P4, R5, R6, R7, XMESS, IFLAG
ċ		INITIAL LENS GEOMETRY
		XSI=.1
		XS2=.1
		XS3=.1
		XS4=.1
		XS5=.1
		X\$6=.1
		XS7=.1
		XS8=.J
		X01=•5
		XD2=.557
		XD3=.234
		XD4=.234
		XD 5=, 234
		XD6=.557
		XD 7=. 5
		Z= • 000000001
		PI=3.141592653589793
		XMOVE=.055
		NUM=11
		IFLAG=0
		DO 1 I=1,NUM
		CALL CONMP8 (XD1, XD2, XD3, XD4, XD5, XD6, XD7, 7)
		IFLAG=1
C		
6		CHANGES IN LENS GEOMETRY
		XD 2= XD 2- XMOVE
		XD3=XD3-2*XMOVE/3
		XD4= XD4-2* XMOVE/3
		XD5=XD5-2*XMOVE/3
	1	XD6=XD6-XMOVE

0001 0002

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0000000

STOP END

SUBROUTINE CONMP8 (XD1,XD2,XD3,XD4,XD5,XD6,XD7,Z) IMPLICIT REAL®8 (A-H,O-Z) COMMON P1 4A.0,C,D+E+F,G,H+O,P,Q,R+S,T,U,XS1,XS2,XS3,XS4,XS5,XS6, 2X57,XS8,R1,R2,R3,K4,R5,R6,R7,XMESS,IFLAG ABS(X)=DABS(X) 0001 0002 0004 0005 0006 ABS(X)=DABS(X) ALOG(X)=DLOG(X) WRITE(6,5)XS1,XS2,XS3,XS4,XS5,XS6,XS7,XS8,XD1,XD2,XD3,XD4,XD5,XD6, ZN07 5 FORMAT(1H0,' USING THE FOLLOWING INPUT PARAMETERS ---',//,5X,'S1 =' 2,F7,4,7,5X,'S2 =',F7.4,7,5X,'S3 =',F7.4,7,5X,'S4 =',F7.4,7,5X,'S5 3=',F7.4,7,5X,'S2 =',F7.4,7,5X,'S7 =',F7.4,7,5X,'S4 =',F7.4,7,5X,'S 41 =',F7.4,7,5X,'D2 =',F7.4,7,5X,'S7 =',F7.4,7,5X,'S4 =',F7.4,7,5X,'S 41 =',F7.4,7,5X,'D2 =',F7.4,7,5X,'S7 =',F7.4,7,5X,'S4 =',F7.4,7,5X,'S 5'D5 =',F7.4,7,5X,'D6 =',F7.4,7,5X,'D7 =',F7.4,3 0007 00000 IF "IFLAG=1" THE SUBROUTINE DOES NOT CALCULATE APPROXIMATE TRANSFORMATION CONSTANTS, THEY MUST ALREADY EXIST IN MEMORY --EITHER FROM THE PREVIOUS GEOMETRY OR READ IN VIA THE MAIN . PROGRAM 0008 0009 0010 0011 0012 0013 0014 0015 0016 0017 0018 0019 0020 0021 0022 0023 0024 0025 4A=0 N=0 IF(IFLAG.EQ.1) GO TO 55 S1=XS1 S2=XS2 S2=XS2 S3=XS3 S4=XS4 S5=XS5 S6=XS6 S7=XS7 S8=XS8 R1=XD1/PI R2=XD2/PI R3=X03/PI R 4= XD 4 /P I R5= XD5 /P I R6=XD6/PI R6=XD6/PI R7=XD7/PI I A=S1/2 0026 N=S1/2 V1=S1/(4*R1) B=V1*A V2=S2/(4*R1) 0028 0029 V2=S2/(4*R1) C=V2*B V3=S2/(4*R2) D=V3*C V4=S3/(4*R2) 0031 0032 0033 0034 0035 0036 V4=337(4+R2) E=V4+D V5=S37(4+R3) F=V5+E 0037 0038 0039 V6=S4/(4*R3) G=V6*F V7=S4/(4*R4) H=V7*G V8=S5/(4*R4) D=V8*H 0040 0041 0042 0043 0044 V9=S5/(4*R5) P=V9*0 V10=S6/(4*R5) 0045 0046 0047 Q=V10*P V11=S6/(4*R6)

0048	P=V11+0		
0049		00.00	
0050		0098	R6=XD6/PI
0051	2-41246	0099	R7=XD7/PI
0052	VI3=S77(4=R7)	0100	S1=XS1
0052	1=V13+S	0101	S2=XS2
0053	V14=S8/(4*R7)	0102	S3=XS3
0054	U=V14*T	01 03	S4=X S4
	C CHECK FOR CONVERGENCE OF "A" VALUE	0104	55±¥55
0055	DIFF=ABS (AA-A)	0105	S4=¥S4
0056	IF(DIFF.GT.Z) GD TD 2	01.06	
0057	WRITE(6+6)N+A+B+C+D+F+F+G+H+D+P+O+P+S+T+H	01 07	
0058	6 FORMAT(1)H0.//. AFTERLIA, I TERATOR OF THE	0108	30-838
	25 1.//.5X. A =1.514.6.15V IN THERATIONS OF THE APPROXIMATE EQUATION	0109	
	3.F14.6./.5X.IE	0110	NEO
	4# F14.6/ 5/ 5/ 5/ 5/ 5/ 5/ 5/ 5/ 5/ 5/ 5/ 5/ 5/	0111	JFLAG=0
	5p =1 =1 4 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	0111	KFLAG=-1
0059	S1 - + = + = C1 + = Of / + > X, * S = * + E1 4=6 + / + 5 X, * T = * + E1 4=6 + / + 5 X + * U = * + E1 4=6		
0060	31 = A + Z + K + B / A		C • EXACT · EQUATIONS
0041	32= 2=K 1=C /B+2=K2=B/C	0112	11 $S11=S1-(R1+ALOG((A+R)/(A-R))-2+R1+R(A))$
0061	53=2=R2*E/D+2*R3*F/E		$2 = R^2 + A \log((A+D)) / (A-D)) = D^2 + A \log(A+D) / (A-D) = D^2 + A \log(A+D) / (A-D)) = D^2 + A \log(A+D) / (A-D) = D^2 + A \log(A+D) / (A-D)) = D^2 + A \log(A+D) / (A-D) = D^2 + A \log(A+D) / (A-D)) = D^2 + A \log(A+D) / (A-D) = D^2 + A \log(A+D) = D^2 $
0062	54=2*R3*G/F+2*R4*H/G		3)-R5+ALOG((A+P)/(A-P))-R6+ALOG((A+F)/(A-F))-R6+ALOG((A+H)/(A-H)
0063	S5=2*R4*0/H+2*R5*P/0		4A*C*C/(B*B))*(E*C/(D*D))*(A*ALUG((A+R)/(A-R))-R7*ALOG((A+T)/(A-T))-(
0064	S6 ≠2 *R 5 * Q/ P+ 2 * R6 *R/Q		5(R+R) 1*(1+1/(T+T)) *(G+G/(F+F))*(G+G/(H+H))*(Q+Q/(P+P))*(S+S/
0065	S7=2*R6*S/P+2*R7*T/S		C
0066	\$8=2*R7*U/T+(A*A/(B*B))*{[?*C/(D*D)]*/F*F//F*F\}*/***	0113	522-52-5-51 + 1 - 2014 - 2014
	2P+P))+(Q+Q/(R+R))+(S+S/(T+T))+U		2
0067	R1=A*A/(2*B)		$\frac{1}{2} = \frac{1}{2} $
0068	R2=R1+C+C/(B+D)		<pre>S+ALUG((C+F)/(C-F))-R4*ALUG((C+H)/(C-H))-R5*ALUG((C+P)/(C-P)</pre>
0069	R3=R2*E*F/(D*F)		= -ROF ALOG((C+R)/(C-R)) - R7 + ALOG((C+T)/(C-T)) - (A + A + C/(B + B)) + (E + C/(D + C))
0070	R4=R3+G+G/(F+H)		5U]] *{G*G/(F*F))*(0*0/(H*H))*(Q*Q/(P*P))*(S*S/(B*P))*(U+U+U+U+U)
0071	R S = R A + O + O / (H + O)	0114	
0072	R6=R5=0/(h+p)	0114	S33=S3-E-R1+ALCG((B+E)/(B-E))-(R2+ALCG((D+E)/(D-E)), 2+C + E + C
0073			
0074			
0075			4)-R6*ALDG((E+R)/(E-R))-R7*ALDG((E+T)/(E-T))/(E-R)*ALDG((E+P)/(E-P)
0074			5)*(E*G*G/(F*F))*(0*)/(H#H))*(0*0/(D*D))*(C*C/(D*D))*(C*C/(D*D))
0077		·	C
0079	SI=A+2=RI+B/A	0115	\$44=\$4=G=R1+A1 DG((B+G)/(B=C))=0.2+41 DG((D=0.0))
0070	S2=2=R1+C/B+2+R2+D/C		2(F-G))-2*83*6/F)
0079	53=2#R 2*E /D+2*R 3*F /E		3(G-H))-2*R4*H/G) -(R4*ALOG((G+H)/
0080	S4=2*R3*G/F+2*R4*H/G		4)-8 6#ALOG((G+P)/(G-P))-0.7+ALOG((A)-1.44
0081	S5≠2≠R4+C/H+2≠R5+P/0		5)*(F*F/(F*F))*(C*C/(D*D)
0082	S6=2*R5*Q/P+2*R6*R/Q		C
0083	S7=2*R6*S/R+2*R7*T/S	0116	\$55±\$5=0=81±41 00110.00110.00110
0084	SB=2*R7*U/T+(A*A/(B*B))*(C*C/(D*D))*(F*F/(F*F))*(C*C/(U+U))*(C*C /		2E-011-(26++1-200((B+0)/(B-0))-R2+ALOG((D+0)/(D-0))-R3+ALOG((E+0)/(
•	2P*P))*(Q*Q/(R*R))*(S*S/(T*T))*(3 - (R+ 4 20(((H+U)) (H-U)) - 2*R 4*0/H)
0085	$R1 = A \neq A / (2 \neq B)$		<pre></pre>
0086	R2=R1*C*C/(B*D)		<pre>F(0+R)/(0-R)/-R7*ALOG((0+T)/(0-T))-(A*A/(B*B))*(C*C/(0+D))</pre>
0087	R3=R2+E+F/(D+F)		51+(E+E/(F+F))*(G+G/(H+H))*(O+Q+Q/(P+P))*(S+S/(R+R))*(Im(1/(T+T))
0088	R4=R3+G+G/(F+H)	0117	
0089	R 5 = R 4 + (1 + 1) (1 + 2)		566=56-Q-R1*ALDG((B+Q)/(B-Q))-R2*ALDG((D+Q)/(D+Q))-R2*ALDG((C+Q))-R2*ALDC((C+Q))-R2*ALDC((C+Q))-R2*ALDC((C+Q))-
0090	R6=R5=A0=(//D=P)		2F-Q) - P4 * AL OG((H+Q)/(H-Q)) - (R5 * AL OG((P+Q)/(P-Q)) - 2*P5 * AL OG((F+Q)/(P+Q)) - 2*P5 * AL OG((P+Q)) - 2*P5 * AL OG((P+Q)
0091			$-(R_0 + AL DG((0+R)/(0-R)) - 2 + 0 + 0)$
0092			$-\mathbf{R} 7 \mathbf{A} \mathbf{I} \mathbf{D} \mathbf{G} \mathbf{I} \mathbf{O} \mathbf{T} \mathbf{V} \mathbf{I} \mathbf{O} \mathbf{T} \mathbf{V} \mathbf{I} \mathbf{I} \mathbf{D} \mathbf{T} \mathbf{V} \mathbf{I} \mathbf{I} \mathbf{D} \mathbf{T} \mathbf{I} \mathbf{I} \mathbf{I} \mathbf{I} \mathbf{I} \mathbf{I} \mathbf{I} I$
			5)*(E*E/(F*F))*(G*G/(H*H))*(O+C/(B*D))*(O+C/(D*D))*(C*C/(D*D))
0093	SE OT AND	A	C C C C C C C C C C C C C C C C C C C
0004	22 R. #AUL/P1	0118	577 = 57 - 5 - 81 + ALDG((8+5)) (8-5)) = 8.2 + 41 DG((8-5)) = 8.2 + 41 DG((8+5)) = 8.2 + 41
0005	K2=XU2/P1		2F-S))-P6*ALDG[(H+S)/(H-S))-P5*ALUG((D+S)/(D-S))-R3*ALUG((F+S)/(
0095	K3=XU3/PI		351)-2*R6*5/R)
0040	R4=XD4/PI		4)-2*R7*T/S) -(R7*ALOG((S+T)/(S-T)
0097	R5=XD5/PI		5) * (E*E / (E*E)) * (C*C / (U*U)) * (O*C / (D*D)) * (C*C / (D*D)
			C

.

0119		\$88=\$8-U-R1*ALOG((8+U)/(8-U))-R2*ALOG((0+U)/(D-U))-R3*ALOG((F+U)/(2F-U))-R4*ALOG((U+H)/(H-U))-R5*ALOG((P+U)/(P-U))-R6*ALOG((R+U)/(R-U 3))-(8F*ALOG(10+U)/(1-U)-2*A274U2)-2*A274U2)
	r	517 (RITAL GG([1+0])(1-0])-2*R/*U/1)
0120	c	Rll=Rl+((8+8-D*D)/(8+8-C*C))*((8+8-F*F)/(8+8-E*E))*((8+8-H*H)/(8+8 2-O+G1)*((8+8-P*F)/(8+8-O+O))*((8+8-R*R)/(8+8-Q+Q))*((8+8-T*T)/(8+8 3-5*5)*(8+8/(8+8)/(8+0-U+Q))*A/2
	ι.	
0121	C	R2Z=R2*{(C*C/{(C*C-D*D)}*((B*B-D*D)/(B*B))*{(D*D-F*F)/(D*D-E*E)}*((D 2*D-H*H)/(D*D-G*C))*{(D*D-P*P)/(D*D-O*O)}*((D*D-R*R)/(D*D-Q*Q))*((D 3*D-T*T)/(D*D-S*S))*(D*D/(D*D-U*U))*(D*C*C)/(Z*B*B)
01 22	C C	
0122		K33=K3#{C#C/{C#C=F#F]}#{[B#B=F#F]/{B#B]}#{E#F/[E#E=F#F]}#{[D#D=F#F 2}/{D#D]}#{[F#F=H#H]/[F#F=G#G]}#{[F#F=P#P]/{F#F=D#D]}#{[F#F=R#R]/{F 3#F=Q#D]}#{[F#F=T#T]/[F#F=S#S]]#{[F#F/{F#F=U#U]}}#{[F#C#C/{2#B#B]}#{[E# 4E/{D#D]}
	L	
0123	с	R44=R4*(C*C/IC*C=H+H1)*((B*B=H+H)/(B*B])*(E*E/(E*E=H*H)}*((D*D=H*H 2)/(D*D])*(G*G/(G*G=H*H))*((F*F=H*H)/(F*F])*((H*H=D*P)/(H*H=D*O])* 3((H*H=R*R)/(H*H=Q*Q))*((H*H=T*T)/(H*H=S*S))*(H*H+/(H*H=U*U))*(H*C*C 3/(2*G*B))*(E*E/(D*D))*(G*G/(F*F))
0124	-	
		2)/(D+D)/(D+(D+(D+P+P))*((B+B+P+P)/(B+B))*(E+E/(E+E-P+P))*((D+D-P+P))
		2;7(U+U);+(G+G/(G+G-P+P))+((F+F-P+P)/(F+F))+(O+O/(O+O-P+P))+((H+H-P
		5+P]/(H+H]]*((P*P-R*R)/(P*P-Q*Q))*((P*P-T*T)/(P*P-S*S))*(P*P/(P*P-U
	~	4*0]]+(P*C*C/(2*B*B))*(E*E/(D*D))*(G*G/(F*F))*(D*O/(H*H))
	6	
0125		R66=R6*(C*C/(C*C-R*R))*((B*8-R*R)/(B*B))*(F*F/(F*F-R*P))*/(D*D_P*P
		2)/(D*D))*(G*G/(G*G-R*R))*((F*F-R*R)/(F*F))*(0*0/(0*0-R*R))*((U*0-R*R))
		3*R]/(H*H)]*(0*0/(0*0-R*R))*((P*P-P*P)/(P*P))*((P*P))*
		4*(R*R/(R*R-U*U))+(R*C*C/(2*R*R))*(F*F/(D*D))*(C*C*C*C*C*C*C*C*C*C*C*C*C*C*C*C*C*C*
		5))*(Q*Q/(P*P))
	c	
0126		877=97=16=6/16=6-7=7=7.11=10=0.7=7=7.00=0.000
		2)/(D+D)/+/C+C/(C+C+C+T+T)/+((B+B+(+T+T)/(B+B))+((E+E/(E+E-T+T))+((D+D-T+T
		2 + T 1 () + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 +
		3+1)/(1+1))+(U+U/(U+U-T+T))+((P+P-T+T)/(P+P))+(S+S/(S+S-T+T))+((R+R
		4-1+1)/(R*R))*(T*T/(T*T-U*U))+(T*C*C/(2*B*B))*(E*E/(D*D))*(G*G/(F*F
	-	5))*(U*U/(H*H))*(Q*Q/(P*P))*(S*S/(R*R))
~ ~ ~	L,	
0127	·	VV1=S11/(2*(R1+R11))
0128		VV2=S22*R22/(2*(R1*R22+R2*R11))
0129		VV3=S22*R11/(2*(R1*R22+R2*R11))
0130		VV4=S33*R33/(2*(R2*R33+R3*R22))
0131		VV5=S33*R22/(2*(R2*R33+R3*R22))
0132		VV6=S44*R44/(2*(R3*R44+R4*R33))
01 33		VV7=S44+R33/(2+(R3+R44+R4+P4=R3))
0134		VV8=\$55+R55/(2+(R4+R55+D5+D4))
0135		
0136		VV10-5445441441744545444441
01 37		VV11~5440EE/12+183+800+864855)]
0138		V11-300TN33/12T1K3FK05+K6FK551]
0130		vv12x3(1/*K/1/12×(K6*R77+R7*R66))
01.59		VVLJ=S/(FK00/(2*(R6*R77+R7*R66))
0140		VVL4=S88/(2*(R7+R77))
0141		IF(N-GT-1000) GO TO 100
0142		IF (JFLAG.EQ.1)GO TO 56
01.43		A1=S11*R11/(R1+R11)
01.44		B1 ≠A1 * VV1
0145		C1=81+VV2

				÷			
0146		D1-C1+1010					
0147		DI=CI+VV3					
0149		E1=D1+VV4					
0148		F1=E1*VV5					
0149		G1=F1*VV6					
0150		H1=G1+VV7					
0151		01-11+1000					
01 52		01-11-448					
01 5 2		P1=01*VV9					
0155		Q1=P1*VV10	1				
0154		RB1=Q1+VV1	1				
0155		SB1=RB1+VV	12				
0156		T1=581+VV1	2				
0157		117-71+1114	5				
0158		01-11+0014					
0150		JF LAG=1					
01/0		DIF=ABS(AA-	-E1)				
0160		IF(DIF.GT.	Z) GD TO 20				
0161		A=A1					
0162		B=B1					
0163		C=C1					
01.64		0-01					
0165		0=D1					
0105		E=E1					
0100		F=F1					
0167		G=G1					
0168		H=H1					
0169		0=01					
0170		0-01					
0171		P=P1					
0170		Q=Q1					
01/2		0 0 0					
~		K=R B1					
0173		K=RB1 S≃SB1					
0173 0174		K≖RB1 S≖SB1 T≖T1					
0173 0174 0175		K=RB1 S=SB1 T=T1					
0173 0174 0175 0176		K=KBI S=SBI T=T1 U=U1					
0173 0174 0175 0176 0177	•	K=RB1 S=SB1 T=T1 U=U1 31 WRITE(6,60)	N,A,B,C,D,E,F	•G+H+0, P,Q,R,S,	, T ,U		
0173 0174 0175 0176 0177		K=RB1 S=SB1 T=T1 U=U1 31 WRITE(6,60) 60 FORMAT(1H0,	N,A,B,C,D,E,F //,' AFTER',I	•G+H+O+P+Q+R+S 5•' ITERATIONS	T,U		
0173 0174 0175 0176 0177	- - -	K=RB1 S=SB1 T=T1 U=U1 31 WRITE(6,60) 60 FORMAT(1H0, 20NFORMAL MA	N,A,B,C,D,E,F //,' AFTER',I P CONSTANTS A	•G+H+O+P+Q+R+S+ 5+' ITERATIONS RE'•//-5X-14	T,U OF "EXACT	EQUATIO	INS, THE C
0173 0174 0175 0176 0177		K=RB1 S=SB1 T=T1 U=U1 31 wRITE(6,60) 60 FORMAT(1H0, 20NFORMAL MA 3/,5X,*C =*,	N+A+B+C+D+E+F //+' AFTER'+I P CONSTANTS A E14-6-/+5X-+D	•G+H+O, P,Q+R,S, 5.' ITERATIONS RE',//,5X,+V =',-14.6./.5X	T,U DF "EXACT 1,E14.6	- EQUATIO	DNS, THE C =*,E14.6,
0173 0174 0175 0176 0177	•	K=RBI S=SBI T=T1 U=U1 31 WRITE(6,60) 60 FORMAT(1H0, 20NFORMAL MA 3/,5X,'C =', 46,/,5X,'G =	N,A,B,C,D,E,F //,' AFTER',I P CONSTANTS A E14.6,/,5X,'D '.E14.6,/.5X	•G•H•O•P•Q•R•S• 5•' I TERATIONS RE'•//,5x,•/ ≈'•El4•6•/,5X	.T.U OF "EXACT .=',E14.6 'E =',E14.	EQUATIO	DNS, THE C =',E14.6, F =',E14.
0173 0174 0175 0176 0177	•	K=KB1 S=SB1 T=T1 U=U1 31 WRITE(6,60) 60 FORMAT(1H0, 20NFORMAL MA 3/,5X,*C =:, 46,/,5X,*C =: 54.6,/,5X,*C =:	N,A,B,C,D,E,F //,' AFTER',I P CONSTANTS A E14.6,/,5X,'D '.E14.6,/,5X, ='.F14.6,/.5X,	•G•H•O,P•Q•R•S 5•' ITERATIONS RE',/,5X,' *'•El4-60/,5X 'H =',El4-6,/,5	•T•U OF ■EXACT \ ='•E14.6 •'E ='•E14. X•'O ='•E14.	EQUATIO	DNS, THE C =',€14.6, (F =',€14. (,'P =',€1
0173 0174 0175 0176 0177		K=KB1 S=SB1 T=T1 U=U1 31 wRITE(6,601 60 FORMAT(1H0, 20NFORMAL MA 3/,5X,*C=*, 46,/,5X,*C 54,6,/,5X,*Q 65146,6,5	N.A.B.C.D.E.F //.' AFTER'.I P CONSTANTS A E14.6./.5X.'D '.E14.6./.5X ='.E14.6./.5	•G•H•O•P•Q•R•S• 5•' ITERATIONS RE'•//•5X• **•El4-6•/•5X H ='•El4-6•/•5 X•'R ='•El4-60/	T,U OF "EXACT \=',E14.6 y'E =',E14. X,*0 =',E ',5X,*S =',E	<pre>EQUATIO //•5X,'B .6./.5X,' 14.6./,5 E14.6./,</pre>	DNS, THE C =*,E14.6, !F =*,E14. (,*P =*,E1 5X,*T =*.
0173 0174 0175 0176 0177		K=KB1 S=SB1 T=T1 U=U1 31 wRITE(6,60) 60 FORMAT(1H0, 20NFORMAL MA 3/,5X,*C =', 46,/,5X,*G = 54.6,/,5X,*G 6E14.6,/,5X, WPITE(6,4)	N,A,B,C,D,E,F //,' AFTER',I P CONSTANTS A E14.6,/,5X,'D ',E14.6,/,5X, 'U =',E14.6)	•G•H•O•P•Q•R•S• 5•' I TERATIONS RE',//,5X•f4 ='•El4.60-/,5X X•H ='•El4.60-/	T,U OF "EXACT = *,E14.6 "E = ',E14.6 X,*O = ',E ',5X,*S = *	EQUATIO	DNS, THE C =',E14.6, F =',E14. (,'P =',E1 5X,'T =',
0173 0174 0175 0176 0177 0177	•	K=KB1 S=SB1 T=T1 U=U1 60 FORMAT(1H0, 20NFORMAL MA 3/,5X,*C=*, 46,/,5X,*C=*, 6E14.6,/,5X,*Q 6E14.6,/,5X,*Q 6E14.6,/,5X,*Q	N,A,B,C,D,E,F //,' AFTER,I P CONSTANTS A !.E14.6,/,5X,:D '.E14.6,/,5X, =',E14.6,/,5X, U =',E14.6, A,B,C,D,E,F,G	•G•H•O•P•Q•R•S• 5•' ITERATIONS RE'•,//,5x,•/ ='•El4•6•/,5x /H ='•El4•6•/, x,•R ='•El4•6•/ *H•O•P•Q•R•S•T•	•T.U OF ■EXACT =*.E14.6 >*.E =*.E14.6 >*.F =*.E14. >*.F =*.E14. >*.F =*.E14. >*.F =*.E14. >*.F = *.E14. >*.F = *.F = *.	" EQUATIC +/+5X+18 +6+/+5X+1 14+6+/+5 +E14+6+/+	DNS. THE C =',E14.6, F =',E14. (,'P =',E1 5X,'T =',
0173 0174 0175 0176 0177 0177		K=KB1 S=SB1 T=T1 U=U1 31 wRITE(6,60) 60 FORMAI(H0, 20NFORMAL MA 3/,5X,'C =!, 46./,5X,'C =!, 54.66./,5X,'G 6214.6./,5X, WRITE(6,61) 61 FORMAT(H0,	N,A,B,C,D,E,F //,' AFTER,I,I P CONSTANTS A E14.6,/,5X,ID '.E14.6,/,5X, U =',E14.6,/ A,B,C,D,E,F,G (/.31622,14.1	•G+H+O,P+Q+R+S 5•' ITERATIONS RE•;//,5X+J •H =••E14+6+/,5X X+'R =••E14+6+/, •H+O+P+Q+R+S+T •SX1)1	T,U OF "EXACT \=',E14.6 ,'E =',E14.6 ,'E =',E14.6 X,'O =',E ',5X,'S =', U	<pre>" EQUATIO */•5X,*B *6•/•5X,* 14•6•/•5X,* 14•6•/•</pre>	DNS, THE C =*,E14.6, F =*,E14. (,"P =*,E1 5X,"T =*,
0173 0174 0175 0176 0177 0177	c	K=KBI S=581 T=T1 U=U1 31 WRITE(6,60) 60 FORMAL MA 3/,5%,*C=*, 46*,45%,*C=*, 46*,45%,*C=*, KRITE(6,61) 61 FORMAT(110), CALCULAT	N,A,B,C,D,E,F //. AFTER,J P CONSTANTS A E14.6,/,5X,D . E14.6,/,5X, . U = 1,E14.6,/,5 . U = 1,E14.6,/,5 . U = 1,E14.6,/,5 . J,3(E22.3)4.1 E0 VALUES DF 1	•G,H,O,P,Q,R,S, 5•I TERATIONS = •,V,5X,+J = •E14.66,/,5X, + = •,E14.66,/,5X, + += •,E14.66,/ + +,O,P,Q,R,S,T, = +,O,P,Q,R,S,T, = +,SX1J) = +YSICAL ASPERT	T,U OF "EXACT "E =',E14.6 "E =',E14.6 X,'O =',E14. X,'O =',E14. V U	EQUATION +/-5X,'B -6-/-5X,'B -6-/-5X,' 14-6-/-5 -E14-6-/- -50000000000000000000000000000000000	DNS, THE C =',E14.6, IF =',E14. ('P =',E1 5X,'T =',
0173 0174 0175 0176 0177 0177 0178 0179 0180	C	K=KBI S=SBI T=T1 U=U1 31 WRITE(6,60) 60 FORMAXIAN 3/,5X,'C =', 46./,5X,'C =', 54.6./,5X,'Q 6114.6./,5X, WRITE(6,61) 61 CORAT(1H0), CALCULAT	N, A, B, C, D, E, F //,' AFTER, J, I P CONSTANTS A E14.6, /, 55X, JD '.E14.6, /, 55X 'U ='.E14.6, /, 55 'U ='.E14.6, J A, B, C, D, E, F, G 5//, 3/E22.J4, J ED VALUES DF J ED VALUES DF J	• G, H, D, P, Q, R, S, 5 • I TERATIONS = • • E - • • • , • / • 5 × • 1 = • • E E 4 • 6 • / • 5 × × • * = • • E 14 • 6 • / × • * = • • E 14 • 6 • / • + • 0 • P, Q R, S, T, \$ × 1) HYSICAL ASPECT AI CIU ATE D VALU	T,U OF "EXACT I = ',E14.6 'E = ',E14.6 'X,'O = ',E ',5X,'S = ', U S OF LENS	" EQUATIC ,/,5X,'B ,6,/,5X,'B ,4.6,/,5 ,E14.6,/, SYSTEM	DNS, THE C =*,E14.6, F =*,E14. (,*P =*,E1 5X,*T =*,
0173 0174 0175 0176 0177 0178 0178 0179	c	K=KBI S=5BI T=T1 U=U1 31 WRITE(6,60) 60 FORMAL MA 3/,5X,*C =1, 46,/,5X,*C =1, 46,/,5X,*C =5 ,46,/,5X,*C 06E14,6,/,5X,*C 06E14,6,/,5X,*C CALCULAT 69 FORMAT(1H0), 256, 57, 58'	N.A.B.C.D.E.F //.' AFTER.J. P CONSTANTS A E14.6.7.45X, D :E14.6.7.45X, ='.E14.6.7.45X, a.B.C.D.E.F.G 5/7.31E22.314. E0 VALUES OF 1 //.' PRESENT (-/.' D1.2.1	•G,H,D,P,Q,R,S, 5• I TERATIONS =I,J,S,+J = •El4.66,/.5X, •H = •,El4.66,/.5X, •H = •,El4.66,/. •H,O,P,Q,R,S,T, •SXIJJ >H+O,P,Q,R,S,T, SXIJJ >HYSICAL ASPECT	T,U OF "EXACT 1 = 1, E14.6 2 = 1, E14.6	EQUATIO	DNS, THE C =',E14.6, F =',E14. (,'P =',E1 5X,'T =', S4, S5,
0173 0174 0175 0176 0177 0178 0179 0180	c	N=KBI S=5BI T=T1 U=U1 31 WRITE(6,60) 60 FORMAI MA 3/,5X,'C =' 54.6./,5X,'G = 54.6./,5X,'G 61146./,5X,'G 61246./,5X,'G 61246./,5X,'G 6154. 054. 054. 054. 054. 054. 054. 054. 0	N.A.B.C.D.E.F //. AFTER:,I P CONSTANTS A E14.6,/,5X,*D *.E14.6,/,5X,*D U =',E14.6]/ A:B.C.D.E.F.G E0 VALUES DF I E0 VALUES DF I /.' PRESENT ./.' D1, D2, [.G.H.D.P.Q.R.S. 5.' I TERATIONS # '-E14.6./.5X.' # -*.E14.6./.5X * H -*.E14.6./. X.'R ='.E14.6./ X.'R ='.E14.6./ X.'R ='.E14.6./ X.'J. X.'J. X.'J. X.'J. CALCULATED Y. A.C. D. O. D. O. S.	T,U OF "EXACT "E =',E14.6 "E =',E14.6 "S,'O =',E ",5X,'S =' U S OF LENS ES FOR S1, D7 RESPEC	 EQUATIO 	DNS, THE C =*,E14.6, f* =*,E14.6, f* =*,E14.6, f* = **,E14.7, f* = **,E14.7, S4, S5, -*,15(/,
0173 0174 0175 0176 0177 0178 0179 0180 0181	C	K=KBI S=SBI T=T1 U=U1 31 MRITE(6,60) 60 FORMAT(1H0, 200F0RMAL 3/,5X,*C=+, 46,/5X,*G=+, 54-6,/5X,*G 61 FORMAT(1H0, CALCULAT 69 61 69 69 60 60 75,75,75,75,75,75,75,75,75,75,75,75,75,7	N,A,B,C,D,F,F //, AFTER,I P CONSTANTS A E14.6,7,5X,D .E14.6,7,5X, U =1,E14.6,7,5X, U =1,E14.6,7,5X, A,RB,C,D,F,F,G E0 VALUES DF,I //, PRESENT (,, DI, D2, [.G.H.O.P.Q.R.S. 5. ITERATIONS RE	T,U OF "EXACT 1 = 1, E14.6 3 : E = 1, E14.6 3 : F = 1, E14.6 5 : S : S = 1 5 : S : S = 1 U S OF LENS ES FOR S1 07 RESPEC	 EQUATIO , /, 5X, 18 , 6, /, 5X, 14 , 6, /, 5) , 614 . 6, /, 5) , 614 . 6, /, 5) , 514 . 6, /, 5) , 52, 53, 53, 51 , 52, 53, 51 	DNS, THE C =',E14.6, F =',E14. (,'P =',E1 (,'P =',E1 (,'F =',E1 (,'F =',E1) S4, S5, -',15(/,
0173 0174 0175 0176 0177 0177 0179 0180 0181 0182	C	N=KBI S=5BI T=T1 U=U1 31 WRITE(6,60) 60 FORMAI MA 3/,5X,'C =' 46,/,5X,'G = 54,6,/,5X,'G 6E1446,/,5X, WRITE(6,61) 61 FORMAT(1H0), CALCULAT (59 FORMAT(1H0), 256, S7, S8' 35X,E14,61) GO TO 100	N.A.B.C.D.E.F //. AFTER:.I P CONSTANTS A E14.6.7.5X.TO 	,G,H,D,P,Q,R,S, 5,' I TERATIONS 8'1',/',SX,'/ 8' +E14-6,/5X 'H =',E14-6,/5 X,'R =',E14-6,/ X,'R =',E14-6,/ X,'R =',E14-6,/ H,D,P,Q,R,S,T, SX)1 PHYSICAL ASPECT ALCULATED VALU 37, D4, D5, D6,	T.U OF "EXACT "E ='.E14.6 X,'O ='.E14 X,'O ='.E3 ,'5X,'S ='. U S OF LENS ES FOR S1, D7 RESPEC	 EQUATIO 	DNS, THE C =',E14.6, F =',E14. (;'P =',E14. (;'P =',E14. (;'P =',E14. (;'P =',E14. (;'P =',E14.) S4, S5, -',15(/,
0173 0174 0175 0176 0177 0178 0179 0180 0181 0182 0183	C	K=KBI S=SBI T=T1 U=U1 31 WRITE(6,60) 60 FORMAXIA11H0, 20NFORMAL MA 3/,5X,'C =+, 466/,5X,'SC, 61 FORMAT(1H0, 256, 57, 581 (64 FORMAT(1H0), 256, 57, 581 (757)(757)(757)(757)(757)(757)(757)(757	N,A,B,C,D,E,F //, AFTER.I P CONSTANTS A E14.64,75X,10 =:E14.64,75X, U =: (14.64,75) A,B,C,D,E,F G,C,D,E,F E0 VALUES DF I C, P, C,	.G.H.O.P.Q.R.S. 5. ITERATIONS RE,/,5X.1, =',El4.6./,5X. H =',El4.6./,5X. X.*R =',El4.6./ ;H.O.P.Q.R.S.T. SX]] HYSICAL ASPECT VALCULATE VALU J3, D4, D5, D6,	T.U OF "EXACT **.414.6 *E =*.414.6 *.52.*S =* U S OF LENS ES FOR S1. D7 RESPEC	EQUATION (1,7,5,7,5,7,5,7,5,7,5,7,5,7,5,7,5,7,5,7,	DNS, THE C =',E14.6, F =',E14. ('P =',E4. ('P =',E4. ('P =',E4. ('P =',E4. ('P =',E4. ('P = ',E4. ('P = ',E4. ('P = ',E4. ('P = ',E4. ('P = ',E14.6, ('P = ',E14.6,('P = ',E14.6,
0173 0174 0175 0176 0177 0177 0177 0179 0180 0181 0182 0183 0184	C	K=KBI S=SBI T=T1 U=U1 31 WRITE(6,60) 60 FORMAINA 37,5X,*C =*, 46,75X,*G = 54,6,75X,*G = 54,6,75X,*G = 54,6,75X,*G = 54,6,75X,*G = 54,6,75X,*G = 54,6,75X,*G = 54,6,75X,*G = 54,6,75X,*G = 54,6,75X,*G = 54,75X,*G	N.A.B.C.D.F.F. //. AFTER:.I P CONSTANTS A E14.6.7.45X.TO 		T,U OF "EXACT "= *,E14.6 X,'O =',E ',5X,'S =', U S OF LENS ES FOR S1, D7 RESPEC	 EQUATIO ,/,5X,*B ,6/,5X,*B ,6/,6,/,52 ,14.6,/,52 ,14.6,/,52 ,514.6,/, ,52,53 ,714,00 	DNS, THE C =',E14.6, F =',E14. (;'P =',E14.
0173 0174 0175 0176 0177 0177 0178 0179 0180 0181 0182 0183 0184	c	N=KBI S=SBI T=T1 U=U1 31 MRITE(6,60) CONFORMAL MA 3/,5X,*C =+, 46,/,5X,*C =+, 54,6,7,5X,*G 6214,66,7,5X,*G 614,66,7,5X,*G 614,66,7,5X,*G 614,66,7,5X,*G 62,76,7X,*G 64,75,7X,*G 64,75,7X,*G 65,75,75,84 67,67,75,75,75,75,75 67,67,75,75,75,75,75,75,75,75,75,75,75,75,75	N,A,B,C,D,E,F //, AFTER:I P CONSTANTS 14.66,/5X,10 :=14.66,/5X, u=',E14.66,/5X, d=',E14.66,/ A,B,C,D,E,F,G f(/31E22,14,) ED VALUES DF 1 f(',' PRESENT (*/',' D1, D2, 1	•G,H,O,P,Q,R,S, 5.' I TERATIONS RE',/',5X,'' =',El4.66,/5X, 'H =',El4.66,/ X,'R =',El4.66,/ X,'R =',El4.66,/ SX)]] PHYSICAL ASPECT VALUATE VALU 33, D4, D5, D6,	T.U OF "EXACT **.414.6 *E =*.414.6 *.42,*0 =*.42 *.52,*5 =* U U S OF LENS ES FOR S1, D7 RESPEC	" EQUATIC /-5X,'B .6./-5X,'B .6./-5X .514.6./, .52.53, .71VELY -	DNS, THE C =',E14.6, F =',E14. (;' P =',E4. (;' P =',E4.
0173 0174 0175 0176 0177 0177 0177 0180 0181 0182 0183 0183 0184 0185	C	K=KBI S=SBI T=T1 U=U1 31 WRITE(6,60) 60 FORMAINA 3/,5X,'C=', 40,/,5X,'G= 5+,6,/,5X,'G=	N.A.B.C.D.F.F //. AFTER.I P CONSTANTS A E14.6.7.45X. ='.E14.6.7.45X. ='.E14.6.7.45X. *U ='.E14.6.7.45X. *U ='.E14.6.7.45X. *U ='.E14.6.7.45X. E0 Values DF 1 //.' PRESENT (*/.* D1, D2, 1	.G.H.D.P.Q.R.S. 5. ITERATIONS E, V., 5X, J. ='.El4.6, /.5X, 'H ='.El4.6, /. X, 'R ='.El4.6, / S, J.J. S, J.J. CALCULAP.Q.R.S.T. CALCULATED VALU J3. D4. D5. D6.	T.U OF "EXACT = 1,E14.6 'E = 1,E14.6 'S X,'O = 1,E14.7 '5 X,'S = 1 U S OF LENS ES FOR S1. D7 RESPEC	EQUATION (1, 1, 5, 7, 1) 64, 7, 57, 18, 66, 7, 53, 14, 66, 7, 53, 14, 66, 7, 53, 14, 66, 7, 53, 52, 53, 52, 53, 52, 53, 71, 17, 10, 10, 10, 10, 10, 10, 10, 10, 10, 10	DNS, THE C =* E14.6, (* = - + E14. (* + P = - + E14. (* + E14.
0173 0174 0175 0176 0177 0177 0177 0178 0179 0180 0181 0182 0183 0184 0185 0186	C	K=KBI S=SBI T=T1 U=U1 31 WRITE(6,60) 60 FORMAT(1H0, 20NFORMAL MA 3/,5X,*(C=*, 46,/,5X,*0 614,6,7,5X,*0 614,6,7,5X,*0 614,6,61) 61 FORMAT(1H0, 60 FORMAT(1H0, 60 FORMAT(1H0, 60 FORMAT(1H0, 35X,F14,61) GO T0 100 20 N=N*1 B=B1 C=C1 D=D1	N,A,B,C,D,E,F //, AFTER: I P CONSTANTS 1:466,/55,*D :E1466,/55,*D 1:21466,/5 1:0=7,61460 A;B,C,D,E,F,G 6//31622,144 ED VALUES DF I C/.' PRESENT (,',' D1, D2, (•G,H,D,P,Q,R,S, ST TERATIONS RE,/-SX,II =',EL4-6,/-SX, 'H =',EL4-6,/-SX, 'H =',EL4-6,/-SX, SX,'R =',EL4-6,/- SX,'R =',EL4-6,/- SX,'R =',EL4-6,/- SX,'R = ',EL4-6,/- CALCULATED VALU D3, D4, D5, D6,	T,U OF =EXACT =*,E14.6 *E =*,E14.6 *F =*,E14.6 *S,*S =*,E *5X,*S =*,U U S OF LENS ES FOR S1 O7 RESPEC	EQUATI(,/,5X,'6 .6,/,5X,'6 .4.6,/,5X,'5X,'5X,'5X,'5X,'5X,'5X,'5X,'5X,'5X,	DNS, THE C =',E14.6, F =',E14. (;'P =',E4. (;'P =',E4. (;'P =',E4. (;'P =',E4. (;'P =',E4. (;'P =',E4. (;'P = ',E4. (;'P = ','E4. (;'P = ','P = ','E4. (;'P = ','P = ','E4. (;'P = ','P = ','E4. (;'P = ','P = ','P = ','E4. (;'P = ','P
0173 0174 0175 0176 0177 0177 0177 0179 0180 0181 0182 0183 0184 0185 0185 0187	C	K=KBI S=SBI T=T1 U=U1 31 WRITE(6,60) 60 FORMAXI(1H0, 20NFORMAL MA 3/,5X,'C = *, 46,/,5X,'G 61 FORMAT(1H0, CALCULAT 69 FORMAT(1H0, CALCULAT 69 FORMAT(1H0, 256, 57, 58*, 35X,E14,60) 60 T0 1J0 20 N=N+1 B=B1 C=C1 0=D1 E=F1	N,A,B,C,D,F,F //, AFTER.I P CONSTANTS A E14.6,/5X,D .E14.6,/5X, U = 1,E14.6,/5X U = 1,E14.6,/5X .A,B,C,D,E,F,G 5//,3(E22.14, C) VALUES DF //, PRESENT (//, PRESENT (.G.H.O.P.Q.R.S. 5. ITERATIONS E, V., 5X, J. =', El4.66, / 5X, 'H =', El4.66, / X, 'R =', El4.66, / X, 'R =', El4.66, / S, J.J. H.O.P.Q.R.S.T. X, J.J. H.O.P.Q.R.S.T. X, J. X, J	T,U OF "EXACT 'E,E14.6 'E,E14.6 'E,E14.6 'E 'E 'S S S S.OF LENS ES FOR SL D7 RESPEC	EQUATI(//,5X,'B 66/,5X,'L 466/,5X, E14.66/, 514.66/, SYSTEM , S2, S3, TIVELY -	DNS, THE C =*,E14.6, F =*,E14. (*) =*,E14. 5x,*T =*, 5x,*T =*, S4, S5, -*,15(/,
0173 0174 0175 0176 0177 0177 0180 0181 0182 0183 0184 0185 0184 0185 0188	C	K=KBI S=SBI T=T1 U=U1 31 WRITE(6,60) 60 FORMAI T(1H0, 20NFORMAL MA 3/,5X,*(C=*, 466,/,5X,*0 614,6,/,5X,*0 614,6,/,5X, CALCULAT (6) FORMAT(1H0, CALCULAT (6) FORMAT(1H0, 20 FORM	N,A,B,C,D,E,F //, AFTER: I P CONSTANTS 1:E14.60/,5X,*D :E14.60/,5X,* 1:U = ',E14.60/,5X /U = ',E14.60/,5X //31E22.144. ED VALUES DF I ED VALUES DF I //.' PRESENT (,//.' D1, D2, (• G, H, D, P, Q, R, S, SR =:,//5X, I =',EL4.66,/5X, 'H =',EL4.66,/5X, 'H =',EL4.66,/ SX, 'R =',EL4.66,/ H, O, P, Q, R, S, T, SX) HYSICAL ASPECT VALUATE VALU J3, D4, D5, D6,	T,U OF =EXACT =*,E14.6 *E =*,E14.6 *F =*,E14.6 *F = *,E14.6 *F = *	<pre>■ EQUATI(,/,5X,'8, 66,/,5X,'8, 14.6,/,5X, 14.6,/,5X, E14.6,/, SYSTEM S2, S3, TIVELY -</pre>	DNS, THE C ='.E14.6, F ='.E14.6, ('P ='.E4.6, ('P ='.E4.6, ('P ='.E4.6, ('P ='.E4.6, ('P = '.E4.6, ('P = '.E4.6, ('P = '.E4.6, (
0173 0174 0175 0177 0177 0177 0177 0180 0181 0182 0183 0184 0183 0184 0185 0186 0187 0189	C	K=KBI S=SBI T=T1 U=U1 31 WRITE(6,60) 60 FORMAXIA11H0, 200FORMAL MA 3/,5X,'C = *, 46,/,5X,'G = *, 64,/,5X,'G = *, 64,/,5X,'G = *, 64,/,5X,'G = *, 64,/,5X,'G = *, 65, FORMAT(1H0, CALCULAT 69 FORMAT(1H0, 256, 57, 57, 35X,FI4,6) 60 T0 100 20 N=N+1 A=ABI C=C1 D=D1 E=E1 E=C1	N,A,B,C,D,F,F //, AFTER.I P CONSTANTS A E14.6,7,5X,D .E14.6,7,5X, U =1,E14.6,7,5X, U =1,E14.6,7,5X, A,B,C,D,E,F,G 5(7,3) E22.14, CO VALUES DF I //, PRESENT (//, D1, D2, [.G.H.O.P.Q.R.S. 5. ITERATIONS REF.4.6.7.5%.M H =E14.6.7.5% X.*R ='.E14.6.7. H.O.P.Q.R.S.T. H.O.P.Q.R.S.T. S.J)] HYSICAL ASPECT ALCULATE VALU J3. D4. D5. D6.	T,U = ".EL4.6 * E = '.EL4.6 * E = '.EL4.6 * E = '.EL4.6 * E = '.EL4.6 * S = '.EL4.6 * S OF LENS S OF LENS ES FOR SL D7 RESPEC	<pre>■ EQUATI(//,5X,'B 66/,5X,'L 466/,5X, E14*66/, SYSTEM , S2, S3, TIVELY -</pre>	DNS, THE C =*,E14.6, IF =*,E14. (19 =*,E14. 5x,*T =*, 5x,*T =*, 54, S5, -*,15(/,
0173 0174 0175 0176 0177 0177 0180 0181 0182 0183 0184 0185 0184 0186 0186 0188 0188 0188	C	<pre>K=KBI S=SBI T=T1 U=U1 31 WRITE(6,60) 60 FORMAI MA 3/,5X,*C =*, 46,/,5X,*G = 54,6,/,5X,*G = 54,6,/,5X,*G = 54,6,/,5X,*G 6614,6,/,5X, 61 FORMAT(1H0), CALCULAT (69 FORMAT(1H0), 256, S7, S8' (69 FORMAT(1H0), 20 N=N*I 60 TO 100 20 N=N*I CALCULAT CALCULAT BBI C=C1 D=D1 E=E1 F=F1 F=C1 CaCL</pre>	N.A.B.C.D.F.F //. AFTER.J P CONSTANTS A E14.6,/.5X.*D .E14.6/.45X. ".E14.6/.5X. U ='.E14.6] A:B.C.D.F.F.G E0 VALUES DF I E0 VALUES DF I ./.' PRESENT (./.' D1, D2, [•G,H,D,P,Q,R,S, 5*I ITERATIONS E,/-,/-,5X,+J = •EL4-6,/-5X, *H = •,EL4-6,/-5X, *H = •,EL4-6,/- X,*R = *,EL4-6,/- X,*R = *,E_4-6,/- X,*R = *,E_4-6,/-X,*R = *,E_4-6,/-X,	T.U OF "EXACT =*.E14.6 "E =*.E14.6 "E =*.E14.6 "E =*.E14.6 "S = 5 X,*S =*. U S OF LENS ES FOR S1. D7 RESPEC	EQUATIC //.5X.'B .6./.5X.'B .6./.5X.' k.6./,5X.' SYSTEM .52.'S3. TIVELY -	DNS, THE C =',E14.6, F =',E14. (;'P =',E14.
0173 0174 0175 0177 0177 0177 0177 0177 0180 0181 0182 0183 0184 0185 0185 0186 0187 0189 0189 0189	C	K=KBI S=SBI T=T1 U=U1 31 WRITE(6,60) 60 FORMAXIAIOO, 20NFORMAL MA 3/,5X,*(C=*, 466,/,5X,*0 61 4.60,/5X,*0 61 4.60,/5X,*0 61 4.60,/5X,*0 61 4.60,/5X,*0 63 4.60,/5X,*0 64 4.60,/5X,*0 74 5.60,/5X,*0 74 5.60,/5X,*0 74 5.60,/5X,*0 74 5.60,/5X,*0 74 5.	N,A,B,C,D,E,F //, AFTER:JI P CONSTANTS A E14.64,75X,D :.E14.64,75X 'U =',E14.61,5 5'U =',E14.61,5 5'U =',E14.61,5 5'U =',E14.61,5 5'U =',22,14,1 ED VALUES DF I '/'' PRESENT (*/'' D1, D2, D	.G.H.D.P.Q.R.S. 5. ITERATIONS RE://5X.Y. ='.El4.6.//5X. H ='.El4.6./ \$X.R ='.El4.6./ \$X.R ='.El4.6./ \$X.R ='.El4.6./ H.D.P.Q.R.S.T. \$X]] HYSICAL ASPECT VALCULATE VALU D3. D4. D5. D6.	T.U OF "EXACT =",E14.6 "E =",E14.6 "E =",E14.6 "E =",E14.6 "S OF LENS S OF LENS ES FOR S1 D7 RESPEC	EQUATION //5X,'B 60//5X,' Katop/ E14.64/, System System System S2, S3, TIVELY -	DNS, THE C =',E14.6, F =',E14. (') = '',E14. (') = '',E14. (') = '',E14. (') = '',E14. S4, S5, -'',15(/,
0173 0174 0175 0175 0177 0177 0180 0181 0182 0183 0185 0186 0185 0186 0187 0188 0187 0188 0187 0189 0189 0189 0189 0189 0189	C	K=KBI S=SBI T=T1 U=U1 31 WRITE(6,60) 60 FORMAXIANO, 20NFORMAL MA 3/,5X,'C='', 46./,5X,'G=' 54.6./,5X,'G 54.6./,5X,'G 54.6./,5X,'G 157.75 54.6./,5X,'G 55.7,58'' 169 FORMAT(1H0), 20 FORMAT(1H0), 20 FORMAT(1H0), 20 FORMAT(1H0), 20 FORMAT(1H0), 20 FORMAT(1H0), 20 FORMAT(1H0), 20 FORMAT(1H0), 20 FORMAT(1H0), 20 N=N+1 B=B1 C=C1 D=D1 E=E1 F=F1 G=G1 H=H1 D=01	N.A.B.C.D.F.F //. AFTER.J P CONSTANTS A E14.6,/.5X.*D '.E14.6,/.5X. ''.E14.6,/.5X. 'U ='.E14.6]/.5X fU ='.E14.6]/.5X fU ='.E14.6]/.5X fU ='.E14.6]/.5X fU ='.E14.6]/.5X fU ='.C.C.S.F fU ='.C.C.S.F fU ='.C.C.S.F fU = '.C.C.S.F fU = '.C.S.F fU = '.C.	.G.H.D.P.Q.R.S. 5.' I TERATIONS E:,/.5X.'J ='.El4.6./.5X.' 'H ='.El4.6./. X.'R ='.El4.6./. X.'R ='.El4.6./. X.'R ='.El4.6./. X.'R ='.El4.6./. ALCULATED VALU D3. D4. D5. D6.	T.U OF "EXACT **.€14.6 *E **.€14.6 *5 *5 U U S OF LENS ES FOR S1. D7 RESPEC	EQUATIC //.5X.'B .6./.5X.'B .6./.5X.' I.4.6./, SYSTEM .52. S3. TIVELY -	JNS, THE C =* E14.6, f =*,E14. (,'P =*,E14.
0173 0174 0175 0176 0177 0177 0180 0181 0183 0184 0183 0184 0185 0186 0187 0188 0189 0189 0189 0189 0190 0192	c	<pre>K=KBI S=SBI T=T1 U=U1 31 WRITE(6,60) 60 FORMAT(1H0, 20NFORMAL MA 3/,5X,'C = *, 466,/,5X,'G 614,66,/,5X,'G 614,66,/5X,'G 614,66,/5X,'G 60 T0 100 20 N=N+1 A=A1 B=B1 C=C1 D=D1 E=E1 F=F1 G=G1 H=H1 D=01 P=P1</pre>	N,A,B,C,D,E,F //, AFTER:I P CONSTANTS 1.E14.6,/,5X, 	•G,H,O,P,Q,R,S, 5. ITERATION RE,//,5X,*J =',El4.66,/5X, H =',El4.66,/5X, H =',El4.66,/ 5X,*R =',El4.66,/ SX,*R =',El4.66,/ SX,11 PHYSICAL ASPECT ALCULATED VALU J3 + D4 + D5 + D6 +	T,U OF "EXACT =',E14.6 'E =',E14.6 'E =',E14.6 'E =',E14.6 'S CF LENS CF LENS	EQUATIO //.5X,'B 60//.5X,' 14.62//.5X,' E14.64/, SYSTEM , S2, S3, TIVELY -	DNS, THE C =',E14.6, F =',E14. (;P =',E14. (;P =',E14. (;P =',E14. (;P =',E14. (;P =',E14. (;P =',E14. (;P = (;P =
0173 0174 0175 0177 0177 0177 0180 0181 0180 0181 0182 0183 0184 0185 0185 0185 0186 0187 0189 0189 0189 0189	C	R=RBI S=5BI T=T1 U=U1 31 WRITE(6,60) 60 FORMAXIAN 3/,5X,'C='' 54,6,/,5X,'G='' 54,6,/,5X,'G'' 54,6,/,5X,'G'' 54,6,/,5X,'G'' 54,6,/,5X,'G''' 54,0,75X,'G'''' 54,0,75X,'G'''''''''''''''''''''''''''''''''''	N.A.B.C.D.E.F //. AFTER:,I P CONSTANTS A E14.6,/.5X.*D :E14.6,/.5X. ".E14.6,/.5X. ".E14.6,/.5X. "", E14.6,/.5 :/.31E22.14. ED VALUES DF I :/.' PRESENT ./.' D1, D2.	.G.H.D.P.Q.R.S. 5.' I TERATIONS E:,/.5X.'J ='.El4.6./.5X.' 'H ='.El4.6./. X.'R ='.El4.6./ X.'R ='.El4.6./ X.'R ='.El4.6./ H.D.P.Q.R.S.T. SXIJJ PHYSICAL ASPECT CALCULATED VALU J3. D4. D5. D6.	T.U OF "EXACT **.€14.6 *E *'.€14.6 *5.7.*S ** U U S OF LENS ES FOR S1. D7 RESPEC	EQUATIC //.5X.'B .6./.5X.'B .6./.5X. J.6./. .52. SYSTEM .52. S3. TIVELY -	DNS, THE C =*,E14.6, (;*,P =*,E14. (;*,P =*,E1 .5X,*T =*, S4, S5, -*,15(/,
0173 0174 0175 0176 0177 0180 0181 0183 0184 0183 0184 0185 0186 0186 0187 0188 0189 0189 0189 0190 0191	C	<pre>K=KBI S=SBI T=T1 U=U1 31 WRITE(6,60) 60 FORMAITAT(1H0, 20NFORMAL MA 3/,5X,*(C=*, 466/,5X,*0 61 FORMAT(1H0, CALCUAF(6,61) 61 FORMAT(1H0, 256,57,58) 61 FORMAT(1H0, 256,57,58) 60 FORMAT(1H0, 256,57,58) 60 FORMAT(1H0, 35X,F14,61) GO TO 100 20 N=N+1 B=B1 C=C1 D=D1 E=E1 F=F1 G=G1 H=H1 0=01 P=P1 D=01 S=03</pre>	N,A,B,C,D,E,F //, AFTER:I P CONSTANTS 14.60,/5X, U =: 164.60,/5X, U =: 164.60,/5X, 0 =: 164.60,/5X, U =: 164.60,/5X, 0 =: 164.60, 0 =:	•G,H,O,P,Q,R,S, 5.' I TERATIONS RE',/',5X,'J =',El4.66,/5X, 'H =',El4.66,/ X,'R =',El4.66,/ X,'R =',El4.66,/ X,'R =',El4.66,/ X,'R =',El4.66,/ X,'R =',El4.66,/ H,O,P,Q,R,S,T SX)JJ PHYSICAL ASPECT VALUA DA, D5, D6,	T,U OF =EXACT =',E14.6 'E =',E14.6 'E =',E14.6 'E =',E14.6 'E =',E14.6 'S OF LENS S OF LENS ES FOR S1 D7 RESPEC	= EQUATIC //.5X,'B 60//5X,' Ka6./,5X, E14.64/, SYSTEM , S2, S3, TIVELY -	DNS, THE C =',E14.6, F =',E14. (;'P =',E4. (;'P =',E4. (;'P =',E4. (;'P =',E4. (;'P =',E4. (;'P = ',E4. (;'P = ',E4. (;'P = ',E4. (;'P = ',E14.6, (;'P = ',E14.6,(;'P = '
0173 0174 0175 0177 0177 0177 0180 0181 0182 0183 0184 0183 0184 0185 0186 0187 0188 0187 0189 0191 0193 0194 0195	C	K=KBI S=SBI T=T1 U=U1 31 WRITE(6,60) 60 FORMAXI(1H0, 200FORMAL MA 3/,5X,'C = *, 46,/,5X,'G 61 FORMAT(1H0, CALCULAT 69 FORMAT(1H0, CALCULAT 60 FORMAT(1H0, CALCUL	N,A,B,C,D,F,F //, AFTER.I P CONSTANTS A E14.6,/5X,D :.E14.6,/5X, U =: E14.6,/5X U =: F14.6 5//,31E22.14, E0 VALUES DF //, PRESENT (//, D1, D2, D	,G,H,D,P,Q,R,S, 5,' I TERATIONS 8'1',/',SX,'/ 8' +E14-6,/5X 'H =',E14-6,/5 X,'R =',E14-6,/ X,'R =',E14-6,/ X,'R =',E14-6,/ H,D,P,Q,R,S,T, SX)1 PHYSICAL ASPECT ALCULATED VALU 33, D4, D5, D6,	T,U OF "EXACT 'E,E14.6 'E,E14.6 'E,E14.6 'E 'S 'S S S.OF LENS CF LENS CF LENS D7 RESPEC	EQUATI(+/.5X.'8 6.7/.5X.' 4.6.7/.5X. E14.6.7, System 52.53, Tively -	DNS, THE C =* E14.6, [* = +, E14. (, * P = *, E1 .5X, *T = *, 5X, *T = *, S4, S5, -*, 15(/,

01.04		7-71				
0190		1-11				
0100						
0190						
0200						
0200		00 A2-311+K11/(K1+	(11)			
0201		BZ=AZ*VV1				
0202						
0203		02=02=04				
0204		E2≠U2¥ VV4				
0205		F2=E2*VV5				
0206		62=F2*VV6				
0207		H2=G2*VV7				
0208		02=H2=VV8				
0209		P2=U2+VV9				
0210		Q2=P2=VV10				
0211		RB2=02*VV11				
0212		282=K82* VV12				
0213		12=562=VV13				
0214		02=12=44414				
0215		DIFEABS(AA-E2)				
0210		IFIDIF .G .ZI GU	10 30			
0217		A=A2 B=02				
0210		B=02				
0217		0-02				
0220		5-52				
0222		5-62				
0223		6762				
0224		U=U2				
0225		0=02				
0226		P=02				
0227		0=02				
0228		R=RB2				
0229		5=582				
0230		T=T2				
0231		U=U2				
0232		GO TO 31				
0233	3	0 A1 = (A1 + A2)/2				
0234		B1=(B1+B2)/2				
0235		C1 = (C1 + C2)/2				
0236		D1 = (D1 + D2) / 2				
0237		E1=(E1+E2)/2				
0238		F1 = (F1 + F2)/2				
0239		G1=(G1+G2)/2				
0240		H]=(H1+H2)/2				
0241		01=(01+02)/2				
0242		P1=(P1+P2)/2				
0243		Q1=(Q1+Q2)/2				
0244		RB1=(RB1+RB2)/2				
0245		SB1=(SB1+SB2)/2				
0246		T1=(T1+T2)/2				
0247		U1 = (U1 + U2)/2				
0248		AA=E1				
0249		N=N+L				
0250		A=41				
0251		5=61				
0252						
0253		0=01				

0254 0255 0256 0257 0258 0260 0261 0262 0263 0264 0265 0264 0265 0266 0267 0268 0269 0271 0272 0271 0271 0272 0273 0274 0275 0276 0277 0276 0277 0277 0277 0277 0277	$ \begin{array}{l} E=E1 \\ F=F1 \\ G=C0 \\ H=H1 \\ 0=01 \\ P=P1 \\ 0=01 \\ R=R81 \\ S<81 \\ T=T1 \\ U=U1 \\ IF(K=LAG.EC0.0) GO TO 32 \\ IF(K=LAG.EC0.1) GO TO 32 \\ IF(K=LAG.EC0.1) GO TO 33 \\ GO TO 11 \\ SA=381 \\ B3=B1 \\ C3=C1 \\ O3=01 \\ P3=P1 \\ O3=01 \\ P3=P1 \\ O3=01 \\ P3=P1 \\ O3=01 \\ P3=P1 \\ SB=SB1 \\ SB=SB1$
0291	E1=(E1+ E3)/2
0293	G1 = (G1 + G3)/2
0295	H1=(H1+ H3)/2 01=(01+ 03)/2
0296 0297	P1=(P1+P3)/2
0298	RB1= (RB1+ RB3)/2
0300	SB1 = (SB1 + SB3)/2 T1 = (T1 + T3)/2
0301	U1=(U1+ U3)/2
0303	8=81
0304 0305	C=C1
0306	E=E1
0307	F=F1 G=G1
0309	H=H1
0310	0≠01 P≠P1
	· · · · ·

0312

S=SB1 T=T1 U≠U1 GO TO 11 100 RETURN END

0=01

R=RB1

PROGRAM #3 * * *

NUMERICAL CALCULATIONS OF THE POTENTIAL DISTRIBUTION AND ION TRAJECTORIES IN A SYMMETRIC LINEAR SIXTEEN ELEMENT ELECTROSTATIC LENS.

THE CONSTANTS OF THE TRANSFORMATION HAVING ALREADY BEEN DETERMINED ARE KEY-PUNCHED INTO THIS PROGRAM AND CHECKED BY CALCULATING THE PHYSICAL CONSTANTS OF THE LENS IN THE Z-PLANE. AFTER INITIALIZATION OF THE LENS VOLTAGES, ION POSITION, AND EMERGY, ROTS ARE FOUND FOR THE 'INVERSE FUNCTION'. THE FIRST THROUGH THE FOURTH DERIVATIVES OF THE POTENTIAL WITH RESPECT TO POSITION, AND RALALS POUND SO THE FORCES ACTING ON OFF-AXIS IONS CAN BE CALCULATED. BY KNOWING THE POSITION AND THE FORCES ATING ON THE ION, NEW VELOCITIES AND POSITIONS ARE CALCULATED EVERY DT (DELTA TIME).

MAIN PROGRAM VARIABLE NAMES

ABCC....U (EXCLUDING I-N) = CONFORMAL TRANSFORMATION CONSTANTS XMESS = THE LARGE CONSTANT IN THE 'INVERSE FUNCTION' XMASS = MASS OF THE ION. (GRAMS)

XMASS = MASS OF THE ION. (GRAMS) RRI_RR2....,RR7 = CALCULATED VALUES FOR THE PHYSICAL DISTANCES BETWEEN ELECTRODE PAIRS IN THE Z-PLANE (CM) SSI.SS2....SS8 = CALCULATED VALUES FOR THE PHYSICAL SLIT WIDTHS FROM THE CENTER LINE OF THE LENS SYSTEM (CM) Q2.03....OT = POTENTIAL ON A GIVEN ELECTRODE PAIR. (VOLTS) TOL = TOLERANCE TO WHICH SUCCESSIVE VALUES OF THE 'INVERSE FUNCTION' MUST MEET DEFORE A "ROOT" IS DECLARED. USED IN SUBROUTINE "FIND'

MUST MEET BEFORE A "ROOT" IS DECLARED. USED IN SUBROUTINE YFIND' XLNGTH = TOTAL LENGTH OF LENS. (CM) DT = TIME INTERVAL FOR SUCCESSIVE CALCULATIONS OF FORCES. (SEC) XKE = KINETIC ENREGY OF ION. (ELECTRON-VOLTS) V = TOTAL VELOCITY OF THE ION. (CM/SEC) VX = COMPONENT OF THE ION VELOCITY IN THE X-DIRECTION. (CM/SEC) XY = COMPONENT OF THE ION VELOCITY IN THE X-DIRECTION. (CM/SEC) X = COMPONENT OF THE ION IN THE LENS. (CM) Y = Y-CODORDINATE OF THE ION IN THE LENS. (CM) FORCEX = FORCE ACTING ON THE ION IN THE X-DIRECTION. (DYNES) FORCEY = FORCE ACTING ON THE ION IN THE Y-DIRECTION. (DYNES)

IMPLICIT REAL*8 (A-H,C-Z)

IMPLICIT REAL+8 (A-H, C-Z) COMMON PI, A, B, C, D, E, F, G, H, O, P, O, R, S, T, U, XS1, XS2, XS3, XS4, XS5, XS6, ZX57, XS8, R1, R2, R3, R4, R5, R6, R7, XMESS, OZ, O3, O4, O5, O4, O7, DVDR2, DVDR3, DVDR4, DVDR5, DVDR6, DVDR7, SVR22, SVR23, SVR24, SVR25, SVR26, SVR27, VTR32, 47VR33, TVR34, TVR35, TVR37, DVD27, DVDV33, DVDV54, DVDV53, DVDV56, DVD74, DVDR5, SVR27, TVR37, SVR27, DVDV32, TVV33, TVY34, TVY35, TVY35, GTVY37, DVDR, SYR27, TVR3, SVR7, DRDV, SR22, TVR32, FVR43, FVR44, FVR45, FVR46, FVR67, FVY42, FVY43, FVY44, FVY45, FVY46, FVY47, FYR4, FR44, FVR57, BTOTAL1, TOTAL2, TOTAL3, TOTAL4, ZB, ZD, ZF, ZH, ZT SQRT(X)=DSQRT(X) ABS(X)=DABS(X) SIN(X)=DSIN(X)

107

0001 0002

С Ċ с с с

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с

0007		COS (X) =DCDS (X)		
	С	······ ,		3((R*R-S*S)/(R*R-T*T))*((R*R-1)*()/(D*D))
	c	PHYSICAL CONSTANTS OF LENS SYSTEM IN THE 7-OLANG	0046	RR7 = ((A + A - T + T))/(2 + T) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T + T)) + ((C + C - T + T))/(2 + C - T))/(2 + T))/(2 + C - T))/(2
0008	-	XSI = 1		2((G*G+T*T)/(F*F+T*T))*((O*O+T*T))*((O*O+T*T))*((F*F+T))*((F*F+T))*((F*F+T))*((F*F+T))*((F*F+T))*((F*F+T))*((F*F+T))*((F*F+T))*((F*F+T))*((F*F+T))*((F*F+T))*((F*F+T))*((F*F+T)))*((F*F+T))*((F*F+T))*((F*F+T)))*((F*F+T)))*((F*F+T))*((F*F+T)))*((F*F+T))*((F*F+T)))*((F*F+T)))*((F*F+T))*((F*F+T)))*((F*F+T)))*((F*F+T)))*((F*F+T)))*((F*F+T))*((F*F+T)))*((F*F+T)))*((F*F+T)))*((F*F+T)))*((F*F+T)))*((F*F+T)))*((F*F+T)))*((F*F+T)))*((F*F+T)))*((F*F+T)))*((F*F+T)))*((F*F+T)))*((F*F+T)))*((F*F+T)))*((F*F+T)))*((F*F+
0009		YC2 = 1		3((\$*\$-T*T)/(P*P-T*T))*((T*C-T*T)/(P*P-T*T))*
0010			0047	R1=RR1
0011			0048	
0011		×34=-102	0049	
0012		xs5=•102	0050	
0013		XS6=•102	0051	K 4 = KK 4
0014		XS7=.002	0052	K5=KK5
0015		XS8=•1	0052	R6=RR6
0016		XD 1=2.0306	0053	R7=RR7
0017		XD2≖ •5	0054	SS1=A+R1*ALOG((A+B)/(A-B))+R2*AI/0G/(A+D)/(A-D))+R2*AI/0G/(A+D)/
0018		XD3=_0873		2) + R4 * AL OG ((A+H) / (A-H)) + R5 * AL OG ((A+H)) + R5 * A
0019		XD 4#- 0873		3R 7*AL (G((A+T)/(A-T)) + (A+C+C/(D+A)+(A+P))*R6*ALUG((A+R)/(A-R))+
0020		YD5+ 0973		4*H) + (0*O/(0*D) + (0*C/(0*D) + (0*D))*(G*G/(F*F))*(0*O/(H
0021			C055	\$2-C+U+AU+AU+AU+AU+AU+AU+AU+AU+AU+AU+AU+AU+A
0021				332-C+R1+ALUG((B+C)/(B-C))+R2+ALUG((C+D)/(C-D))+R3+ALUG((C+F)/(C-F
0022		XU /=• 5		211+R4+ALUG((C+H)/(C-H))+R5+ALOG((C+P)/(C-P))+R6+ALOG((C+R)/(C-R))+
0023		PI=3.141592653589793		3R (# AL UG[(C+T)/ (C-T)) + (A*A/(B*B))*(C*E*E/(D*D))*(G*G/(F*E))*(O*O//H
	C		005/	4*H))*(Q*Q/(P*P))*(S*S/(R*R))*(U*U/(T*T))
	С	FROM THE CONFORMAL MAP PROGRAM THE FOLLOWING CONSTANTS HERE OPTATHED	0056	SS3=E+R1*ALOG((B+E)/(B-E))+R2*ALOG((D+E)/(D-E))+R3*ALOG((F+E)/(C-E))
0024		A=. 50024774728523D-01		2))+R4* AL DG((E+H)/(E-H))+R5*AL DG((E+D)/(E-D))+R4*AL DG((E+H)/(E-H))
0025		B=, 19300862635880D-02		3R7*ALOG([E+T]/(E-T))+(A*A/(B*B))+(C+C)(C+D)+(C+C)(C+D)+
0026		(=,750283723969140-04)		4*H))*(0*0/(0*D))*(5*5/(0*0))*(0*0/)*(E*G*G/(F*F))*(0*0/(H
0027			0057	SS4=G+P1 = A1 OC/(P+G)/(R+R)/+(U+U/([+[]])
0028				2) + R + ALUG((B+G)/(B-G))+R2 *ALUG((D+G)/(D-G))+R3*ALUG((F+G)/(F-G
0020		10924/32492200D-05		211 TK+*ALOG((G+H)/(G-H))+R5*ALOG((G+P)/(G-P))+R6*ALOG((G+R)/(G-R))
0029		F= .101214725095590-05		5*R + AL UG((G+1)/(G-T))+(A*A/(B*B))*(C*C/(D*D))*(E*E/(F*F))*(G*D*D/(
0030		G=•56494427727956D-06	0050	4H+H])*(Q*Q/(P*P))*(S*S/(R+R))*(U+U/(T*T))
0031		H=• 31 8563 285 47 029D-0 6	0038	SS5=0+R1+ALOG((B+0)/(B-0))+R2+ALOG((D+0)/(D-0))+R3+ALOG((E+0)/(E-0)
0032		0=.17963624022968D-06		2) + R4 + ALOG((H+O)/(H+O)) + R5 + ALOG((O+P)/(O-P)) + R6 + ALOG((O+P)/(O+P)) + R6 + ALOG((O+P)/(O+P)/(O+P)/(O+P)) + R6 + ALOG((O+P)/(O+P)/(O+P)/(O+P)) + R6 + ALOG((O+P)/(O+P)/(O+P)/(O+P)) + R6 + ALOG((O+P)/(O+P)/(O+P)/(O+P)) + R6 + ALOG((O+P)/(O+P)/(O+P)/(O+P)/(O+P)/(O+P)) + ALOG((O+P)/
0033		P=• 10027910788180D-06		3R7*ALOG((0+T)/(0-T)) + (A*A/(B*B)) * ((*C/(0+D)) * (5+C/(C+T))) * (5+C/(C+T)) * (5+C/(C+T))) * (5+C/(C+T)) * (5+C/(C+T)) * (5+C/(C+T)) * (5
0034		Q=, 536573067272660-07		4)]*(0*Q*Q/(P*P))*(S*S/(B*P))*(1#U/(T+T))
0035		R=-91460386857643D=08	0059	SS6=0+R1 *ALDG((8+0)/(8=0))+P2*ALDG((D))
0036		S = 28076476061660-10		21)+84*AL DG((H+0)/(H=0)) AD FH2 ALUG((D+Q)/(D-Q))+R3*ALDG((F+Q)/(F-Q
0037				387*ALDG((0+T)/(0 T))++K3+ALDG((P+Q)/(P-Q))+R6*ALDG((Q+R)/(Q-R))+
0039		1-600733221389060-13		() + () + () + () + () + () + () + () +
0030		U=.13306465669631D-13	0060	+/) + (0+ 0/ (P=P)) + (0+ S+ S/ (R+R)) + (0+ 0/ (T+T))
0039	· · ·	XMESS=(A*A/(B*B))*(C*C/(D*D))*(E*E/(F*F))*(G*G/(H*H))*(D*D/(P*P))*	0000	55/=5+R1*ALOG((8+5)/(8-5))+R2*ALOG((0+5)/(D-5))+R3*ALOG((E+5)/(E-5)
		2(Q*Q/(R*R))*(S*S/(T*T))*(U*U)		2) + R4* AL OG((H+S)/(H-S))+R5*AL OG((P+S)/(P-S))+R6*AL OG/(P+S)/(P-S))
	С			3R7*ALOG((S+T)/(S-T))+(A*A/(B*B))*(C*C/(D*D))*(E*E/(E*E))*(C*C/(D*D))
	С	USING CONFORMAL TRANSFORMATION MARRING CONSTANTS THE DUNCTON	1	4))*(0*0/(P*P))*(0*0/(R*R))*(S*0*0/(T*T))
	С	CONSTANTS OF THE LENS SYSTEM IN THE Z-DIANE ARE CALCULATED	0061	SS8=U+R1 *ALOG((8+U)/(8-U))+82*ALOG((0+U))(0
0040		RR1 = ((A + A - B + B))/(2 + B) + (B + B - C + C)/(B + B) + (A + B - B + B)/(2 + B) + (B + B - C + C)/(B + B - C)/(B + C)/(B + B - C)/(B + C		2) 1+R4*AL DG((H+H)/(H+H))+P5*AL DC((D+H)/(D-H))+R3*AL DG((F+H)/(F-H)
		2(18=8=C=C=C)/(8=9=U=U))+(10=0=C+C)/(0=0=0+0))+((8=8=C=C=C)/(8=8=C=C)/(8=8=C)/(8=8=C		387* AL OG((T+U)/(T-U))+ At A(A+A)(D+D)((P+U))+R6* ALOG((R+U)/(R-U))+
		2(()+d=(+C)/(d+b=(++))+((D+0=(+U)/(B*B=P*P))*((B*B=Q*Q)/(B*B=R*R))*		4))*(0+0/(0+0))*(0+0/)*(0+0))*(0+0))*(0+0/)
0041		5((0+0-3+3)/(0+0-1+1))/+((0+0-0+0)/(0+0))	0062	Pp1-pp1+pr
0041		RR2=((AFA-DFD)/(2FD))*((C+C-D+D)/(B+B-D+D))*((D+D-E+E)/(D+D-F+F))*	0063	
		2((D*D-G*G)/(D*D-H*H))*((D*D-O*O)/(D*D-P*P))*((D*D-Q*Q)/(D*D-R*R))*	0066	
		3((D*D-S*S)/(D*D-T*T))*((D*C-U*U)/(D*D))	0046	KKJ =KKJ # PI
0042		RR3=((A*A-F*F)/(2*F))*((C*C-F*F)/(B*B-F*F))*((F*F-F*F)/(D*D-F*F))*	0005	KR 4=RR 4*PI
		2((F*F-G*G)/(F*F-H*H))*((F*F-O*O)/(F*F-P*P))*((F*F-O*O)/(F*F-O*O))*	0000	RR5=RR5*PI
		3((F*F-S*S)/(F*F-T*T))*((F*F-1)*()/(F*F))	0067	RR6=RR6*PI
0043		$RR 4\pi ((A * A - H * H) / (2 * H)) * (/ C * C - H * H) / (0 * C - H * H) / (2 * H)) = 0$	0068	RR7=RR7*PI
		2/(C+C-H+H)/(C+C-H+H))+((C+C-H+H)/(C+C-H+H))+((C+C-H+H)/(D+D-H+H))*	0069	WRITE(6.69)551.552.553.554.555.554.555.554.555.554.555
		2 (1 × 1 - Q × Q) / (H × H - Q × Q) / (H × H - Q × Q) / (H × H - Q × Q) / (H × H - Q × Q) /		2886-887
4400		21111-1-3-3//(TTTT-(F)//TT((HTT)-UTU)/(HTH))	0070	G FORMAT (141 // 1 TRAJECTORY CALLEND
0044		KKD={{A*A-P*P}/{Z*P}}*{{C*C-P*P}/{B*B-P*P}}*{{E*E-P*P}/{D*D-P*P}}*		253 CONTRACT LITTING TO TRAJECTURY CALCULATION ON A LENS SYSTEM WITH ST.
		2((G*G-P*P)/(F*F-P*P))*((O*O-P*P)/(H*H-P*P))*((P*P-O*O)/(P*P-R*R))*		232, 33, 54, 55, 56, 57, 58*,/,* D1, D2, D3, D4, D5, D6, D7 RESPECT
1		3((P*P-S*S)/(P*P-T*T))*((P*P-U*U)/(P*P))	0071	SIVELY,15(/,5X,F7.4))
0045		RR6=((A*A-R*R)/(2*R))*((C*C-R*R)/(B*B-R*R))*((F*F-R*R)/(D*D-R*R))*	0011	RI=RRI/PI
		2((G*G-R*R)/(F*F-R*R))*((D*D-R*R)/(H*H-R*R))*((D*D-R*R)/(D*D-R*R))*(D*D-R*R))*((D*D-R*R)	0072	R2=RR2/PI
			0073	R3=RR3/PI

0074		R4=RR4/PI
0075		R5=RR5/PI
0076		86=886 / BI
0077		
0077		RI-RRIPPI
0078		Q2=0.0 B 00
0079		Q3=7.440D 03
0080		04=03
0081		05=03
0002		
0082		uo≖us solution in the solution of the solutio
0083		97=92
0084		TOL=1.E-14
0085		XLNGTH=XD1+XD2+XD3+XD5+XD5+XD5+XD7
0086		
0087		
0001		
0088		AMU=39,948
0089		CHARGE=1.6021917D-19
0090		DT=+75D-09
0091		NUM=5
0002		NUM 2 - E
0072		
0093		XKE=7.280D 03
C094		XMASS=AMU*(1.66043E-24)
0095		STAR T= XL NG TH
	C	
	ř	THE NUMBER OF ADDITIONAL TON KINETIC ENCOURSE STATTING AT ANY ST
000/	C	THE NOMBER OF ADDITIONAL ION KINETIC ENERGIES STARTING AT "XKE"
0098		DU 40 1*1,NUM
0097		XX=•01
	С	
	С	THE NUMBER OF PARAXIAL TRAJECTORIES IN ADDITION TO THE INITIAL AVAIL
0098	-	DO 10 TET. NUM2
0000		
0099		V=SURT ((2+CHARGE*ARE*1.0D 07)7XMASS)
0100		V=-V
0101		N=O
0102		Y=START
01 03		X=XX
0104		
0104		VA-VJIN(ALTRA)
0105		VI=V+CUS (ALPHA)
01 C6		WRITE(6,17)X,VX,VY,XKE
0107		17 FORMAT(1H0,//, INITIAL VALUES OF X. VX. VY. & XKF./.FR.4.
	•	23(2X, F14,6))
	c	
	č	START OF STER ON STER DAY TRUCK LOOP
	C.	START OF STEP-BT-STEP RAT TRACE LUUP
0108		13 CALL FIND(Y,TOL,ROOT,BOMB)
0109		IF(BOMB-EQ.1) GO TO 50
0110		CALL FSTPOT(ROOT)
0111		CALL SNDPOT (BOOT)
0112		
0112		
0115		CALL FRHPUTCRUUT
0114		FORCEX=-X*T0TAL2+X*X*X*T0TAL4/6
0115		FORCEY=TOTAL1-X*X*TOTAL3/2
0116		N=N+1
0117		21 VY==CHARGESECREEXEDT +1 OD OT/YHASSAWY
0119		
0110		VI=-CHARGE+FURCEI+UI+I.OU U// XMASS+VY
0114		
0120		X=X+AX ≠D⊥
0121		IF(VY)11,10,10
0122		11 [E(Y-X07)]5-15-13
01 23		15 WDITE(6.36)N
0124		24 ENEMATING & DESITION OF CLOTICLE AT CUMPE STREAMED -
0124		SO FORMALLINU, POSITION OF PARTICLE AT GUARD ELECTRODE AFTER ,18,2X,

2'ITERATIONS') WRITE(6,99)X,VX,Y,VY 99 FORMAT(5X,'X-POSITION *',F8.4,10X,'X-VELOCITY *',E14.6,/,5X,'Y-POS 2TITION *',F8.4,10X,'Y-VELOCITY *'E14.6) 10 XX=XX-.002 01 50 STOR END

ł

0125 0126

C	SUBROUTINE FUNC(X,Y,VAL)	0001	SUBROUTINE FIND (Y,TOL,ROOT,BOMB)	
	SUBROUTINE 'FUNC' IS USED TO EVALUATE THE 'INVERSE FUNCTION' AND RETURN A NUMERICAL VALUE ("VAL") OF THIS FUNCTION FOR ANY X AND Y. Y = Y-COORDINATE OF THE ION IN THE LENS, Z-PLANE. (CM) X = VARIABLE NAME NOT THE COORDINATE IN THE Z-PLANE		C SUBROUTINE "FIND" IS RESPONSIBLE FOR FINDING ROOTS FOR THE "INVERSE FUNCTION". STARTING AT AN ARBITRARY POINT OF "X" AND PROCEED- ING IN ORDER OF MACHITUDE STEPS SUBROUTINE FUNC IS CALLED TO RETURN VALUES FOR THE 'INVERSE FUNCTION'. THE RANGE OF SEARCH IS DICTATED BY THE SIZE OF 'DO 1 1=1, #2 THE SEARCH RUNS THEREFORE FROM X TO X X4(10)*(#41). A PORT IS TREPORT	
C	IMPLICIT REAL+8 (A-H,O-Z) COMMON PIA18.C,D,E,F,G,H-O,P,Q,R,S,T,U,XS1,XS2,XS3,XS4,XS5,XS6, 2XS7,XS8,R1,R2,R3,R4,R5,R6,R7,XMESS,02,03,04,05,06,07,DVDR2,DVDR3, 3UVDR4,DVDR5,DVDR6,DVDR7,SVR22,SVR23,SVR24,SVR25,SVR26,XVR27,IVR32,		A FLAG, MONE SIGN. IF NO POSITIVE ROOT IS FOUND THE PROGRAM RETURNS A FLAG, MONNEY INDICATING TO THE MAIN PROGRAM THAT THE RANGE OF SEARCH WAS NOT LARGE ENDUGH.	
	4TVR33, TVR34, TVR35, TVR36, TVR37, DVDV2, DVDV3, DVDV3, DVDV5, DVDV5, DVDV5, DVDV7, SVV23, SVV23, SVV24, SVV25, SVV26, SVV27, TVV35, TVV35, TVV35, TVV35, TVV35, 6TVY37, DVDR, SVR2, TVR3, SVR4, DR0Y, SRV2, TRV3, FVR42, FVR43, FVR44, FVR45, FVR46, FVR47, FVV42, FVV3, FVV44, FVV45, FVV46, FVV46, FVV47, FYR4, FR74, TOTALV, 8TOTAL1, TOTAL2, TOTAL3, TOTAL4, Z8, Z0, ZF, ZH, ZP, ZR, ZT ATAN(X) = DATAN(X) VAL = X+2*R1*ATAN(X/B) +2*R2*ATAN(X/D) +2*R3*ATAN(X/F) + 2*R4*ATAN(X/H) + 2*R5*ATAN(X/F) +2*R6*ATAN(X/R) +2*R7*ATAN(X/T) - XHESS /X - Y RETURN	0002	IMPLICIT REAL*8 (A-H,O-Z) COMMON P1 A, B C, DE, F, G, G, H, Q, P, Q, R, S, T, U, XS1, XS2, XS3, XS4, XS5, XS6, 2XS7, XS8, PL, PZ R3, PC, R5, R8, R7, XHES5, QZ, Q3, Q4, Q5, Q6, Q7, DV DR2, DVDR3, 30VDR4, DV DR5, DVDR6, DVDR7, SVR22, SVR23, SVR24, SVR25, SVR26, SVR27, TVR32, 4VR33, TVR34, TVR35, TVR35, TVR37, DVDV27, DVDV35, DVDV56, DVDV76, DVDV7, 5SV722, SVY23, SVY25, SVY26, SVY27, TV Y32, TVY33, TVY34, TVY35, TVY36, 6TVY37, DVDR5, TVR32, SVR37, SVR24, SVR27, TVY32, TVY34, TVY34, TVY35, TVY36, 7TVR46, FVR47, FVY42, FVY43, FVY44, FVY45, FYY46, FVY44, FVR44, FFVR46, FFVR4, TOTAL V, 8TOTAL, TOTAL, TOTAL3, TOTAL4, Z0, Z0, ZF, ZH, Z9, R2, ZT	
	END	0004 0005	SIGN(X,Y)=DSIGN(X,Y) ABS(X)=DABS(X)	
		C 0006 0007 0008 0009	STARTING POINT IN SEARCH OF RODT X=1.E-20 X1=X IFLAG=0 BOMB=0.	
		0010 0011 0012 0013 0014	2 CALL FUNC(X,Y,TRY1) DO 1 [x=1,40 X=X*10 X2=X CALL FUNC(X,Y,TRY2)	
		0015 0016 9017 0018 0019	CHANGE=SIGNITRY],TRY2) IF[CHANGE=NE=TRY1) GO TO 10 X1=X2 1 Try1=Try2 IF(IIFLAG=NE=O) GO TO 3	
		C C 0020 0021 0022 0023 0024	THESE STATEMENTS EXECUTED ONLY IF NO POSITIVE ROOT IS FOUND X=-1.E-20 IFLAG=1 GO TO 2 3 X1=-1.E-9	
		0024 0025 0026 0027 0028 0029	X=-1.E-9 CALL FUNC(X,Y,TRY1) X2=1.5E-9 X=1.5E-9 CALL FUNC(X,Y,TRY2) CHANGESICA(TRY INV INV)	
		003 0 0031 0032 0033	IFICHANGE.NE.TRYII GO TO 10 BOHB=1. WRITEC6.BJY 8 FORMAT(IHO, ROOT CANNOT BE BRACKETED USING THE LIMITS IN SUBROUTIN	

0003

0005

0007

		2E FIND FOR Y= '.E14.6)
0034		RETURN
	C	
	с	RODT IS BRACKETED BISECTION BEGINS
0035	10	IF(ABS((X1-X2)/X1)) F. TO() GO TC 25
0036		X = (X1 + X2)/2
0037		CALL FUNC(X.Y.TRY)
0038		CHANGE=SIGN(TRY.TRY1)
0039		IF (CHANGE-NE-TRY) GO TO 15
0040		X1 = X
0041		TRY1=TRY
0042		GO TO 10
0043	15	X2 = X
0044		TR Y2=TRY
0045		GO TO 10
0046	25	ROOT=X1
0047		RETURN
0048		END

.

c	SUBROUTINE FSTPOT (ROOT)
č	
с с	SUBROUTINE FSTPOT CALCULATES THE FIRST DERIVATIVE OF THE POTENTIAL WITH RESPECT TO THE Y-COORDINATE (7-0) AND J
C C	
C -	INPLICIT REALES (A-U.O.7)
	2X57, X58, R1, R2, R3, R4, R5, R6, R7, XMFSS, 02, 03, 04, 05, 07, 07, 03, 04, 05, 07, 07, 08, 08, 08, 08, 08, 08, 08, 08, 08, 08
	30VDR4, 0VDR5, 0VDR6, 0VDR7, SVR22, SVR23, SVR24, SVR24, SVR25, S
	4TVR33, TVR34, TVR35, TVR36, TVR37, DVDY2, DVDY3, DVDY4, DVDY5, DVDY5, DVDY7
	55VY22, SVY23, SVY24, SVY25, SVY26, SVY27, TV Y32, TVY33, TVY34, TVY34
	6TV Y37, DYDR, SYR2, TYR3, SYRY, DRDY, SRY2, TRY3, FVR42, FVR43, FVR44, EVP44
	7F VR46 + FVR47 + FVY42 + FVY43 + FVY44 + FVY45 + FVY46 + FVY47 + FYR4 - FR V4 - TOTAL V
	BIOTAL1.TOTAL2.TOTAL3.TOTAL4.ZB.ZD.ZF.ZH.ZP.ZR.ZT
	ZB=B+B+RCOT +ROOT
C	
c	FIRST DERIVATIVE OF THE DOTENTIAL WITH PROPERTY AND
c	FOR THE ELECTRODE DATES 42-47
	DVDR2 = Q2 + (2/P1) + (T/T) - (R/T0)
	PVDR3 = Q3 + (2/PL) + ((R/7R) - (P/7P))
	DVDR4 = Q4 + (2/PI) + ((P/ZP) - (H/ZH))
	0VDR5 = 45+(2/PI)+((H/ZH)-(F/ZF))
	DVDR6 = Q6*(2/PI)*((F/ZF)-(D/ZD))
	DVDR7 =Q7*(2/PI)*((D/ZD)-(B/ZB))
5	
L	FIRST DERIVATIVE OF THE Y-COORDINATE WITH RESPECT TO THE ROOT R
	07DR =1+2*R1 *B/ZB+2*R2*D/ZD+2*R3*F/ZF+2*R4*H/ZH+2*R5*P/ZP+2*R6*R
r	272R+2+R (*172 I+ XME SS/ (ROOT*ROOT)
č	FIRST DED THATTUS OF SUB CONTINUES
Č.	THE ST DERIVATIVE OF THE POTENTIAL WITH RESPECT TO THE Y-COORDINATE
	DVDY2 ELCERUDE PAIKS #2-#/.
	DVDY5 ≭BVDR5 /DYDR
	DVDY6 ≠DVDR6 /DYDR
	DVDY7 =DVDR7 /DVDR
c	
C	FIRST DERIVATIVE OF THE ROOT, R. WITH RESPECT TO THE V-CORPORATE
_	DRDY =1/DYDR
C	
C ·	TOTAL CONTRIBUTION OF THE ELECTRODE PAIRS #2-#7 TO THE FIRST
C	DERIVATIVE OF THE POTENTIAL WITH RESPECT TO THE Y-COORDINATE.
	101AL1=0VDY2+0VDY3+0VDY4+0VDY5+0VDY6+0VDY7
	END
	טטט טטט טטט טעט טעט טעט טעט טעט טעט טעט

0001	SUBROUTINE SNOPOT (RODT)	0001	SUBROUTINE TROPOT (ROOT)
	SUBROUTINE 'SNOPOT' CALCULATES THE SECOND DERIVATIVE OF THE POTENTIAL WITH RESPECT TO THE Y-COORDINATE (Z-PLANE).		C C SUBROUTINE 'TROPOT' CALCULATES THE THIRD QERIVATIVE OF THE POTENTIAL C with respect to the Y-coordinate (Z-plane). C
C C C	IMPLICIT REAL*8 (A-H, O-Z) COMMON PI, A, B, C, D, E, F, G, H, O, P, Q, R, S, T, U, XS1, XS2, XS3, XS4, XS5, XS6, 2XS7, XS8, R1, R2, R3, R4, R5, R6, R7, XMESS, Q2, Q3, Q4, Q5, Q6, Q7, DVQR2, DVQR3, 30VQR4, DVQR5, DVDR7, SVR22, SVR23, SVR24, SVR25, SVR25, SVR26, SVR27, TVR32, 4TVR33, TVR34, TVR35, TVR36, TVR37, DV072, DVDY3, DVDY4, DVDY5, DVDY6, DVDY7, 5SV722, SVY23, SVY24, SVY25, SVY26, SVY27, TV33, TVY34, TVY35, TVY36, 6TVY37, DVQR5, SVR2, TYR3, SVR4, DVA5, FVY46, FVY47, FVR43, FVR46, FVR45, 7FVR66, FVR47, FVY43, FVY43, FVY44, FVY45, FVY46, FVY47, FVR4, FRY4, TOTAL*, 8TOTAL1, TOTAL2, TOTAL2, TOTAL4, ZB, ZD, ZF, ZH, ZF, RA, ZT	0002 0003	C IHPLIC IT REAL+8 (A-H,O-Z) COMMON PI,A,B,C,D,E,F,G,H,O,P,Q,R,S,T,U,XSI,XS2,XS3,XS4,XS5,XS6, ZX57,XS8,R1,R2,R3,R4,R5,R6,R7,XMESS,Q2,Q3,44,SW25,SW26,ZW0R2,DV0R3, 30VDR4,DV0R5,DV0R6,DW0R7,SVR23,SVR23,SVR24,SVR25,SVR26,SVR27,TVR32, 4TVR33,TVR34,TVR35,TVR36,TVR35,JV072,DV072,DV073,DV074,DV075,DV074,DV075, 5VY23,SV723,SV724,SV725,SV726,SV727,TVY32,TV733,TV734,TVY35,TVY36, 4TVR34,GFVR47,FV782,FV73,FV745,FV745,FV746,FV747,FVR43,FVR45,FV746,FV747,FVR45,FV746,FV747,FVR45,FV746,FV747,FVR45,FV746,FV747,FVR44,FV75,TV734,TV734,TV734,TV734,TV734,TV734,TV734,TV734,TV734,TV734,TV734,FV745,FV746,FV747,FVR45,FV745,FV746,FV747,FVR45,FV745,FV746,FV747,FVR45,FV7477,FV7477,FV7477,FV7477,FV747777777777
0004 0005 0006 0007 0008 0009 C	SECOND DERIVATIVE OF THE POTENTIAL WITH RESPECT TO THE ROOT,R, SQUARED FOR ELECTRODE PAIRS #2-#7. SVR22 = Q28(-(14/PI)*R*ROOT)/(ZP4ZT)+((4/PI)*R*ROOT)/(ZP4ZP)) SVR23 = Q38(-(14/PI)*R*ROOT)/(ZP4ZP)+((4/PI)*R*ROOT)/(ZP4ZP)) SVR24 = Q46(-(14/PI)*R*ROOT)/(ZP4ZP)+((4/PI)*R*ROOT)/(ZP4ZP)) SVR25 = Q55(-(14/PI)*R*ROOT)/(ZP4ZP)+((4/PI)*R*ROOT)/(ZP4ZP)) SVR25 = Q56(-(14/PI)*R*ROOT)/(ZP4ZP)+((4/PI)*R*ROOT)/(ZP4ZP)) SVR26 = Q66(-(14/PI)*R*ROOT)/(ZP4ZP)+((4/PI)*R*ROOT)/(ZP4ZP)) SVR27 = Q74(-(14/PI)*D*ROOT)/(ZP4ZD)+((4/PI)*B*ROOT)/(ZB4ZB))	00.04 00.05 00.06 00.07	<pre>THIRD DERIVATIVE OF THE POTENTIAL WITH RESPECT TO THE ROOT,R, CUBED FOR ELECTRIDE PAIRS #2-#7. TVR32 = 022 (-(+/P)1+X7/(2T*2T)+((16/P1)+T*ROOT*ROOT)/(2T*2T*2T+2T)+((24/P1)*R1/(2R*2R)-(16/P1)*R*ROOT*ROOT)/(2R*2R*2R)) TVR33 = 034(-(+/P)1*R*ROOT*ROOT)/(2R*2R*2R)) TVR34 = 044(-(+/P1)*R*(2R*2R)*(16/P1)*P*ROOT*ROOT)/(2R*2R*2R)+((24/P1)*P1/(2P*2P)-(16/P1)*P*ROOT*ROOT)/(2**2**2P)) TVR34 = 044(-(4/P1)*P*ROOT*ROOT)/(2**2**2P)) TVR35 = 056(-(4/P1)*P*ROOT*ROOT)/(2**2**2P)) TVR55 = 056(-(4/P1)*U(7**2*)) TVR55 = 056(-(4/P1)*U(7**2*))</pre>
0010 C	SECOND DERIVATIVE OF THE Y-C CORDINATE WITH RESPECT TO THE RODTR, SQUARED. SYR2 =-(4*R149*RODT)/(20+28)-(4*R2*0*RODT)/(20+28)-(4*R3*F*RDOT) 2/(2F*2F)-(4*R4#H*RODT)/(21*27)-(4*R5*P*RODT)/(2P*2P)-(4*R6*R*RODT) 3/(2R*2R)-(4*R7*T*RODT)/(2T*2T)-2*XMESS/(RODT**3)	0008 0009	24/P1)+2)/(ZF+ZF)-(L16/P1)+F+R00T+R00T)/(ZF+ZF+ZF)+1(TVR36 = 264(-(4/P1)+F/(ZF+ZF)+(116/P1)+F+R00T+(ZF+ZF+ZF)+((24/P1)+0)/(Z0+Z0)-((16/P1)+D+R00T+R00T)/(Z0+Z0+Z0)) TVR37 = 27+(-(4/P1)+0/(Z0+Z0+Z))+(16/P1)+0 R00T+R00T)/(Z0+ZD+Z0)+((24/P1)+B)/(ZB+ZB)-((16/P1)+B)R00T+R00T)/(Z0+ZD+ZD))
0011 C C C C 0012	SECOND DERIVATIVE OF THE Y-CCORDINATE WITH RESPECT TO THE ROOT,R, AND Y- Syry =Syr2 *DRDY Second derivative of the root,r, with respect to the y-coordinate Souared. Sry2=-Syry/(Dydr#dydr)	001 0	<pre>C THIRD DERIVATIVE OF THE Y-COORDINATE WITH RESPECT TO THE ROOT,R, CUBED. TYR3 =-(4*R1*B)/(2B*2B)+(16*R1*0*ROOT)/(2B*3)-(4*R3*F)/(2D 2*20)+(10*R2*D*ROOT*ROOT)/(2D*3)-(4*R3*F)/(2F*2)+(16*R3*F*ROOT)/(2D 3ROOT)/(2f**3)-(4*R4*H)/(2H*2H)+(16*R4*H*ROOT*ROOT)/(2H*3)-(4*R5*F) 3ROOT)/(2f**3)-(4*R4*H)/(2H*2H)+(16*R4*H*ROOT*ROOT)/(2H*3)-(4*R5*F) 5ROOT)/(2f*2P)+(16*R5*P*ROOT*ROOT)/(2f*3)-(4*R4*F)/(2F*2F)+(16*R5*F*R6*F*F 5ROOT)/(2f*2F)+(10*R5*F)/(ROOT*ROOT)/(2f*2T)+(16*R5*F)/(2f*2F)+(16*R5*F)/(2f*2F))+ 6ROOT/2f*+(10*R5*F)/(ROOT*ROOT))/(2f*2T)+(10*R5*F*ROOT)/(2f*2F))+</pre>
C C 0013 0014 0015 0016 0017 0018 C C C 0019	SECOND DERIVATIVE OF THE POTENTIAL WITH RESPECT TO THE Y-COORDINATE SQUARED FOR ELECTRODE PAIRS #2-#7. SV22=DVDR2*SV2*SV2*DRDOW*DRDY SVY23=DVDR2*SV2*SV2*DRDO*DRDY SVY25=DVDR4*SV2*SV2*DRDY*DRDY SVY25=DVDR5*SV2*SV2*DRDY*DRDY SVY25=DVDR5*SV2*SV25*DRDY*DRDY SVY25=DVDR5*SV2*SV25*DRDY*DRDY SVY25=DVDR7*SV25*SV25*DRDY*DRDY TOTAL CONTRIBUTION OF ELECTRODE PAIRS #2-#7 TO THE SECOND DERIVATIVE OF THE POTENTIAL WITH RESPECT TO THE Y-COORDINATE SQUARED. IOTAL=SVY25*SV25*V25*SV26*SV72	0011 0012 0013 0014 0015 0016 0017	C THIRD DERIVATIVE OF THE ROOT, R, WITH RESPECT TO THE Y-COORDINATE CUBED. TRY3 =-TYR3 /(DYDR **4)+3*SRY2 *SYR2 /(DYDR **5) C THIRD DERIVATIVE OF THE POTENTIAL WITH RESPECT TO THE Y-COORDINATE C GUEDE FOR ELECTRODE PAIRS #2-#7. TVY32=DVDR2*TRY3+3*SRY2*SVR2*ADRY*TVR33*(DRDY**3) TVY32=DVDR3*TRY3+3*SRY2*SVR2*ADRY*TVR33*(DRDY**3) TVY35=DVDR5*TRY3+3*SRY2*SVR2*ADRY*TVR35*(DRDY**3) TVY35=DVDR5*TRY3+3*SRY2*SVR2*ADRY*TVR35*(DRDY**3) TVY35=DVDR5*TRY3+3*SRY2*SVR2*ADRY*TVR35*(DRDY**3) TVY35=DVDR5*TRY3+3*SRY2*SVR2*ADRY*TVR35*(DRDY**3) TVY35=DVDR5*TRY3+3*SRY2*SVR2*ADRY*TVR35*(DRDY**3) TVY35=DVDR5*TRY3+3*SRY2*SVR2*ADRY*TVR35*(DRDY**3) TVY35=DVDR5*TRY3+3*SRY2*SVR2*ADRY*TVR35*(DRDY**3)
0020 0021	KETUKN END	00 18 0019 0020	C 10TAL CONTRIBUTION OF ELECTRODE PAIRS #2-#7 TO THE THIRD DERIVATIVE C DF THE POTENTIAL WITH RESPECT TO THE Y-CODRDINATE CUBED. TJTAL3=TVY32+TVY33+TVY34+TVY35+TVY36+TVY37 RETURN END

c	SUBROUTINE FRHPOT (ROOT)
č	
С С С	SUBROUTINE 'FRHPOT' CALCULATES THE FOURTH DERIVATIVE OF THE POTENTIAL WITH RESPECT TO THE Y-COORDINATE (Z-PLANE).
č	
. с	THDI 1017 DEALTO /A 11 0 4
	COMMON OF A P C D C P C P C P C P C P C P C P C P C
	2X57, VCA D1 D2 D1 D1C, D1C, P1G, H, O, P1Q, R, S, T, U1XS1, XS2, XS3, XS4, XS5, XS6,
	20V046 0V025 0V025 0V025 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	4TV9 33 TV9 24 TV9 25 TV9 27 SVR22, SVR23, SVR24, SVR25, SVR26, SVR27, TVR32.
	554733 5W34, 14835, 14836, 14837, DVDY2, DVDY3, DVDY4, DVDY5, DVDY6, DVDY7.
	54122, 54125, 54124, 54125, 5426, 54427, TVY32, TVY33, TVY34, TVY35, TVY36,
	TEVELS FURATE FURATE STR2, TTR3, SYRY, DRDY, SRY2, TRY3, FVR42, FVR43, FVR44, FVR45.
	TT THE FURT 1. FUT 42, FUY 43, FUY 44, FUY 45, FUY 46, FUY 47, FY R4, FR Y4, TOTAL V.
r	STOTALI, TOTALZ, TOTAL3, TOTAL4, ZB, ZD, ZF, ZH, ZP, ZR, ZT
ž	
č	FOURTH POWER FOR ELECTRODE DATES AN ATT RESPECT TO THE ROOT, R, TO THE
	FVR42 = 02* (48/PI)*R00T* ((T/(2T*3))*(1-2*P00T*P00T*2T) - (0.017)*P00T* (2T) - (0.017)*(0.0
	2]]+(1-2+R00T+R00T/ZR)]
	FVR43 = 23+(48/PI)+ROOT+((R/(ZR++3))+(1-2+ROOT+POOT+/2R)-(D/(ZR++2))
	2))*(1-2*ROOT*ROOT/ZP))
	FVR46 =Q4+(48/PI)+ROOT+((P/(ZP++3))+(1-2+ROOT+ROOT/70)-(4//74++3
	2)]*(1-2*ROOT*ROOT/2H))
	FVR45 =Q5+(48/PI)+ROOT+((H/(ZH++3))+(1-2+ROOT+ROOT/ZH)-(5//ZE++3)
	2)]+(1-2+R00T+R00T/ZF))
	FVR46 = = g6# (48/PI) # ROOT# ((F/ (ZF##3)) # (1-2#ROOT#ROOT / 7F)= (0// 20##3
	2))+(1-2+R00T+R00T/Z0))
	FVR47 = 97*(48/PI)*R00T*((D/(ZD**3))*(1-2*R00T*R00T/20)-(*//20++2
	2) I + (1-2+ ROOT+ROOT/ZB))
C	
	FOURTH DERIVATIVE OF THE Y-COORDINATE WITH RESPECT TO THE POOT. P. TO
ι	THE FOURTH POWER.
	FYR4 =-48*ROOT*((R1*8/(Z6**3))*(-1+2*ROOT*ROOT/Z6)+(R2*0/(Z0**3)
	2) = (-1+2*ROOT*ROOT/ZD) + (R3*F/(ZF**3)) + (-1+2*ROOT*ROOT/ZF) + (R4+4//ZH
•	3##3]]*(-1+2*ROOT*RODT/ZH)+(R5*P/(ZP*+3))*(-1+2*ROOT*ROOT/ZP)+/P4+P
	4/(ZR*+3))*(-1+2*ROOT*ROOT/ZR)+ ((R7*T/(ZT*ZT))*(1/7T))*(-1+2*ROOT*
	5ROOT/ZT})-((24*XMESS/(ROOT**3))*(1/(ROOT**2)))
č	
- ř -	TO THE DERIVATIVE OF THE ROOT, R, WITH RESPECT TO THE Y-COORDINATE
	EQVATE / FUNCTION PUNCKS
	20Y09++21 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
c	2010R++3/J-13#((STK2/DYDR)##3)#(1/(DYDR##4))
č	EDUPTH DEPTHATING OF THE OFFENDER
Ē.	TO THE EQUAL PROPERTY AND A POTENTIAL WITH RESPECT TO THE Y-COORDINATE
	EVY2=DVD2=EEVX4444TDV2=EVECEVECEVECEVECEVECEVECEVECEVECEVECEVE
	2 DP DV #TVD 32 5 CV 62 + (N Y 3 * S V R 22 * D R DY + 3 * S RY 2 * S RY 2 * S V R 22 + 6 * S R Y 2 * D R D Y *
	2DR DY=TW 33FFV9454105541000+461
	20R0Y#T VR3454FV0444 # 1000Y#44 \
	2080Y2+TV2354EV96541070+41073+34823+DRDY+3+5RY2+SRY2+SVR25+6+SRY2+DRDY+
	208 D ¥#T V9 34 5 V84 5 V 0 20 ¥ 0 20 ¥ 0 8 D R D ¥ +3 *5 R ¥ 2 *5 R ¥ 2 *5 V R 26 + 6 * S R ¥ 2 * D R D ¥ *
	AND TATION TRADICULUITERS

FVY47=DVDR7+FRY4+4+TRY3+SVR27+DRDY+3+SRY2+SRY2+SVR27+6+SRY2+DRDY+ 2DRDy+TVR37+FVR47+(DRDy++4)

TOTAL CONTRIBUTION OF ELECTRODE PAIRS \$2-\$7 TO THE FOURTH DERIVATIVE OF THE POTENTIAL WITH RESPECT TO THE Y-COORDINATE TO THE FOURTH PONEMA TOTALLS=FVY42+FVY43+FVY44+FVY45+FVY46+FVY47 RETURN END

0019 0020

0003

Robert Joseph Ryba

Candidate for the Degree of

Doctor of Philosophy

Thesis: MODIFICATION OF A MATTAUCH-HERZOG GEOMETRY MASS SPECTROMETER FOR IMPROVED RESOLUTION ION KINETIC ENERGY SPECTROMETRY

Major Field: Chemistry

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Biographical:

- Personal Data: Born in Detroit, Michigan, on November 19, 1945, the son of Mr. and Mrs. Joseph Ryba.
- Education: Graduated from Edwin Denby High School, Detroit, Michigan in June, 1963; received the Bachelor of Science in Chemistry degree from Wayne State University, Detroit, Michigan, August, 1967; completed requirements for the Doctor of Philosophy degree at Oklahoma State University, May, 1976.
- Professional Experience: Graduate Teaching Assistant, Oklahoma State University, 1971-1975; Research Award, Oklahoma State University, summers 1972 and 1974; Continental Oil Company Fellow, Summer, 1973, June 1 - December 31, 1974; Phillips Oil Company Fellow, Summer 1975.

Membership in Honorary and Professional Societies: Phi Lambda Upsilon, Honorary Chemical Society; American Chemical Society.

VITA