

Letter of Transmittal

To: Senior Management

From: Engineering Department

Subject: Modular Distributed Ammonia Synthesis

To Whom It May Concern,

The enclosed report is our design team's response to senior management's proposal for an anhydrous ammonia plant located in the Minnesota River Valley. The design also includes the upstream production of hydrogen and nitrogen. We are pleased to deliver this requested process design as it is technically feasible, economically attractive, and safe. This report entails a thorough discussion of all aspects that went into the design, including but not limited to optimization of the system, economics, risk analyses, and safety considerations. If additional information is desired, the team would be happy to provide such details. We thank you for taking the time to consider this report.

Regards,

Team 9

CHE 4224
Spring 2020

AIChE National Student Design
Competition

Modular Distributed Ammonia Synthesis

April 2, 2020

Group Number 9

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Abstract

The preliminary design of an anhydrous ammonia plant was performed. In the United States, the Corn Belt is the largest consumer of anhydrous ammonia fertilizer, yet the Corn Belt obtains most of its fertilizer from the Gulf Coast. The transportation of ammonia fertilizer from the Gulf Coast to the Corn Belt is both costly and hazardous. To mitigate the additional safety and cost burdens associated with transportation of anhydrous ammonia, it is the objective of this project to produce the preliminary design of a plant located in the Minnesota River Valley. The project memo states this location to be especially suited for ammonia production due to its high demand in agricultural use within this region of the United States.

The plant is designed to produce 50 metric tons per day of anhydrous ammonia with a product purity of 99.5% by mass. The reactants utilized to produce anhydrous ammonia can be expensive and hazardous to transport, so it is the objective of this preliminary design to also design onsite production of both hydrogen and nitrogen. The desired purity is 99.9% by mole for both hydrogen and nitrogen.

The design selected to meet these requirements includes a pressure swing adsorption system for nitrogen production, which includes two adsorption towers, three double pipe heat exchangers, and three reciprocating compressors. The steam methane reforming for hydrogen production includes: one packed bed reactor, one membrane reactor, two shell and tube heat exchangers, one reciprocating compressor, one fired heater and two adsorption towers. The Haber-Bosch process was utilized for ammonia production, and includes one packed bed reactor, two shell and tube heat exchangers, three reciprocating compressors, one flash drum, one air cooled heat exchanger, and three storage tanks. Aspen HYSYS was utilized to simulate the process and evaluate methods for optimization.

A safety analysis was performed by examining mistakes that have occurred over the last 50 years in ammonia production that have led to safety issues. By discovering what could go wrong and what has gone wrong in the past, accommodations were made to produce an inherently safer design. Loss of containment was the biggest concern associated with the project resulting in focus throughout the process of mitigating this risk through inherent safety.

An economic analysis has been completed on the design with an expected project life of 20 years. The economic analysis yielded the net present value to be \$15,000,000 in 2020 US dollars, and the DCFROR to be 13%. This displays the economic feasibility of the project as the minimum rate of return is 8%. The payback period was found to be approximately 8.3 years, and the breakeven product price was found to be \$460. The design team has determined from this analysis that the project is both technically and economically feasible.

A sensitivity analysis was performed to determine the risk associated with the project. The impact of variation of the capital investment, raw material cost, operating cost, and revenue on the net present value and DCFROR were analyzed. Each variable was analyzed at a $\pm 10\%$, $\pm 20\%$, and $\pm 30\%$ variation. The variation of revenue had the greatest impact on the project. Through this analysis the team has deemed the risks associated with the project low. This supports the recommendation to move forward to the detailed design phase of the project.

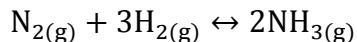
Introduction

The objective of this project is to perform a preliminary design, evaluate the economics, and mitigate potential safety hazards of an anhydrous ammonia plant. Compared to other commercial fertilizers, anhydrous ammonia fertilizer has the highest nitrogen content (1). Nitrogen is a crucial component for crop growth (2). Through years of producing crops the soil can become depleted of nitrogen, making ammonia popular among farmers for crop production (1). Additionally, ammonia production is crucial to the world population, as it is reported to be at least two to three billion larger in size due to the crop yield created by ammonia-based fertilizers and other chemicals (3).

In the United States, corn production has historically been the largest consumer of ammonia (4). Currently, most of the ammonia used in the Corn Belt is produced on the Gulf Coast; yet, this shipment is costly and hazardous (5). Implementation of an ammonia plant within the Corn Belt has the potential to not only alleviate these issues, but also be quite profitable. To meet these demands and alleviate these issues, the designed plant's location will be in the region of the Minnesota River Valley. Additionally, the project memo states this to be the chosen location for this ammonia production facility due to the high ammonia demand for agricultural use. This region also offers the availability of sweet natural gas from neighboring states that can be sent directly to the plant via distribution lines (6).

The plant is designed to produce 50 metric tons per day, 110,231 lbs. per day, of commercial-grade anhydrous ammonia, of 99.5% by mass. This ammonia can be sold as is for fertilization, through injecting the liquid ammonia into the ground (7). This results in no additional downstream processing of ammonia being necessary in the plant.

In this process ammonia is produced through the reaction of nitrogen and hydrogen over a ruthenium-cesium catalyst via the following reaction:



To lower production costs and mitigate safety concerns of large onsite storage, the design contains the upstream production of hydrogen and nitrogen needed for this reaction. The team designed different options for both hydrogen and nitrogen production. The team analyzed pressure swing adsorption and membranes for nitrogen production. Steam methane reforming and electrolysis were analyzed for hydrogen production. The process description includes only the selected options; however, in the section of "important considerations" information on how these selections were made is provided. After production, the anhydrous ammonia is stored onsite in tanks that conform to the requirements of 29CFR1910.111 (8).

The project is set to purchase equipment in mid-2020, but for construction to not begin until mid-2021. Beginning construction in 2021 allows time to obtain a construction permit, which can take at least 6 months to obtain from time of submission. The permit request includes the completed design basis, site characteristics, and all expected environmental discharge. The purchase of equipment takes place prior to permit issuance to provide a schedule advantage. Due to the design of this project production is set to begin in mid-2024.

The plant was analyzed with an expected lifespan of 20 years. Depreciation, write-offs, inflation, and taxes were also considered. The net present value, rate of return, and risks were all considered to determine the economic feasibility of the plant. In deciding the optimal process, the team prioritized a mitigated carbon footprint of the plant, lowered economic losses, and increased inherent safety. An overview of the process is shown below in Figure 1. Throughout this report information regarding the steam methane reforming unit will be referred to as hydrogen production, information regarding the pressure swing adsorption unit will be referred to as nitrogen production, and information referring to the Haber-Bosch process unit will be referred to as ammonia production.

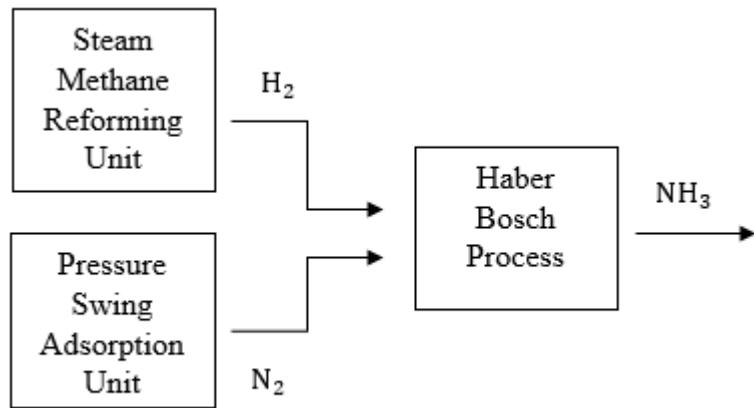


Figure 1: Block Flow Diagram of Process

Process Flow Diagram and Material Balances

The process flow diagram for the preliminary design of the nitrogen production section of the plant is shown in Figure 2, along with the stream summary table, Table 1. The process flow diagram for the preliminary design of the hydrogen production section of the plant is displayed in Figure 3, with the stream summary table in Table 2. The preliminary design of the ammonia production section of the plant is displayed in Figure 4, and the stream summary table for this section is in Table 3.

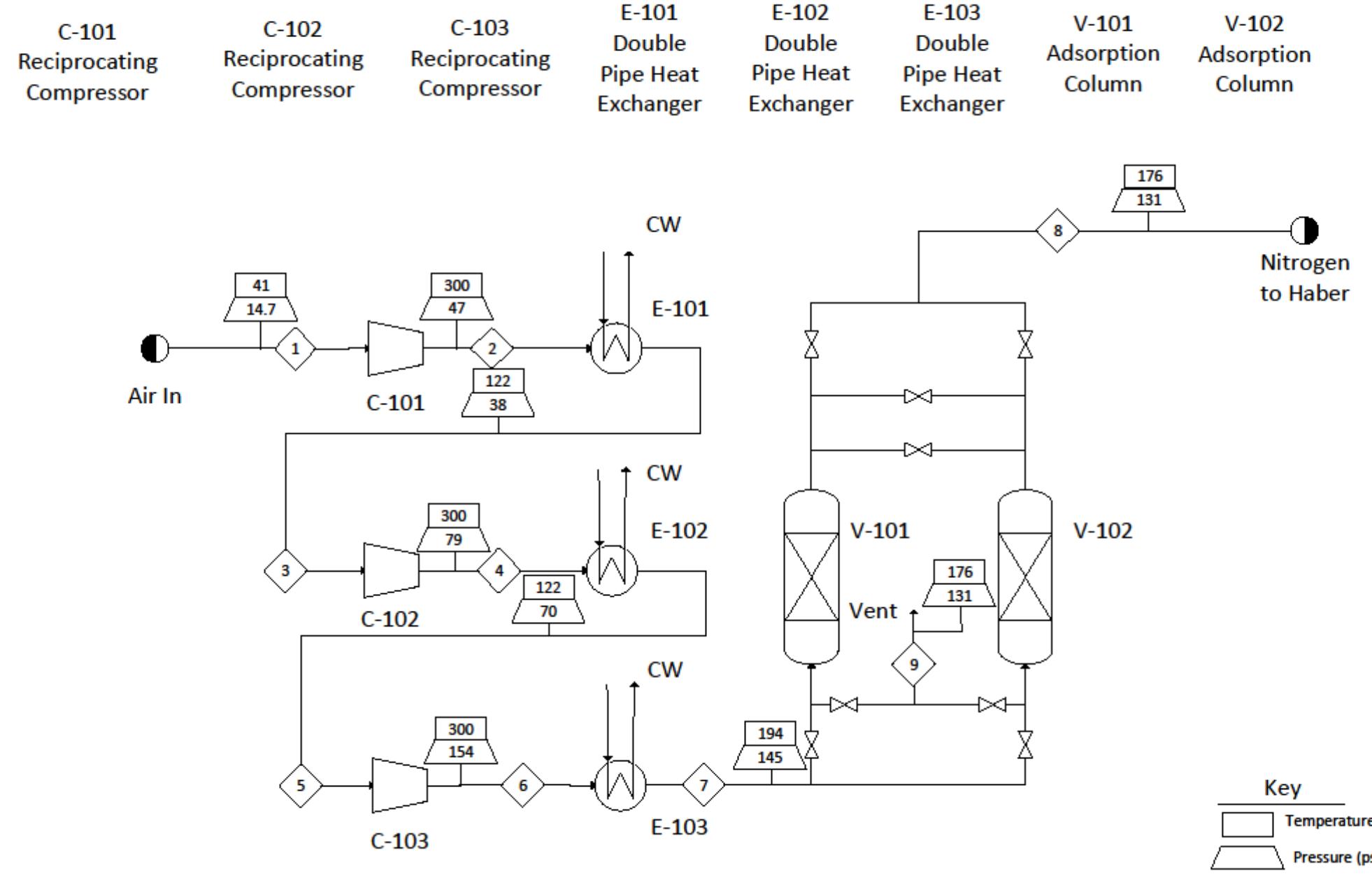


Figure 2: Process Flow Diagram of Nitrogen Production

Table 1: Nitrogen Stream Summary Table

Stream ID #	Unit	Nitrogen Production								
		1	2	3	4	5	6	7	8	9
Vapour Fraction		1	1	1	1	1	1	1	1	1
Temperature	F	41	300	122	300	122	300	194	176	176
Pressure	psia	15	47	38	79	70	154	145	131	131
Molar Enthalpy	Btu/lbmole	-931	891	-371	887	-378	879	120	-835	658
Molar Flow	lbmole/hr	250	250	250	250	250	250	250	136	114
Master Comp Molar Flow (Argon)	lbmole/hr	2	2	2	2	2	2	2	2	0
Master Comp Molar Flow (CO)	lbmole/hr	0	0	0	0	0	0	0	0	0
Master Comp Molar Flow (CO2)	lbmole/hr	1	1	1	1	1	1	1	1	0
Master Comp Molar Flow (H2O)	lbmole/hr	0	0	0	0	0	0	0	0	0
Master Comp Molar Flow (Nitrogen)	lbmole/hr	195	195	195	195	195	195	195	59	137
Master Comp Molar Flow (Oxygen)	lbmole/hr	53	53	53	53	53	53	53	53	0
Mass Flow	lb/hr	7,259	7,259	7,259	7,259	7,259	7,259	7,259	3,936	3,323
Actual Volume Flow	barrel/day	391,071	186,226	176,201	110,511	95,266	56,744	51,746	183,915	221,169
Molar Density	lbmole/ft3	0.00	0.01	0.01	0.01	0.01	0.02	0.02	0.02	0.02

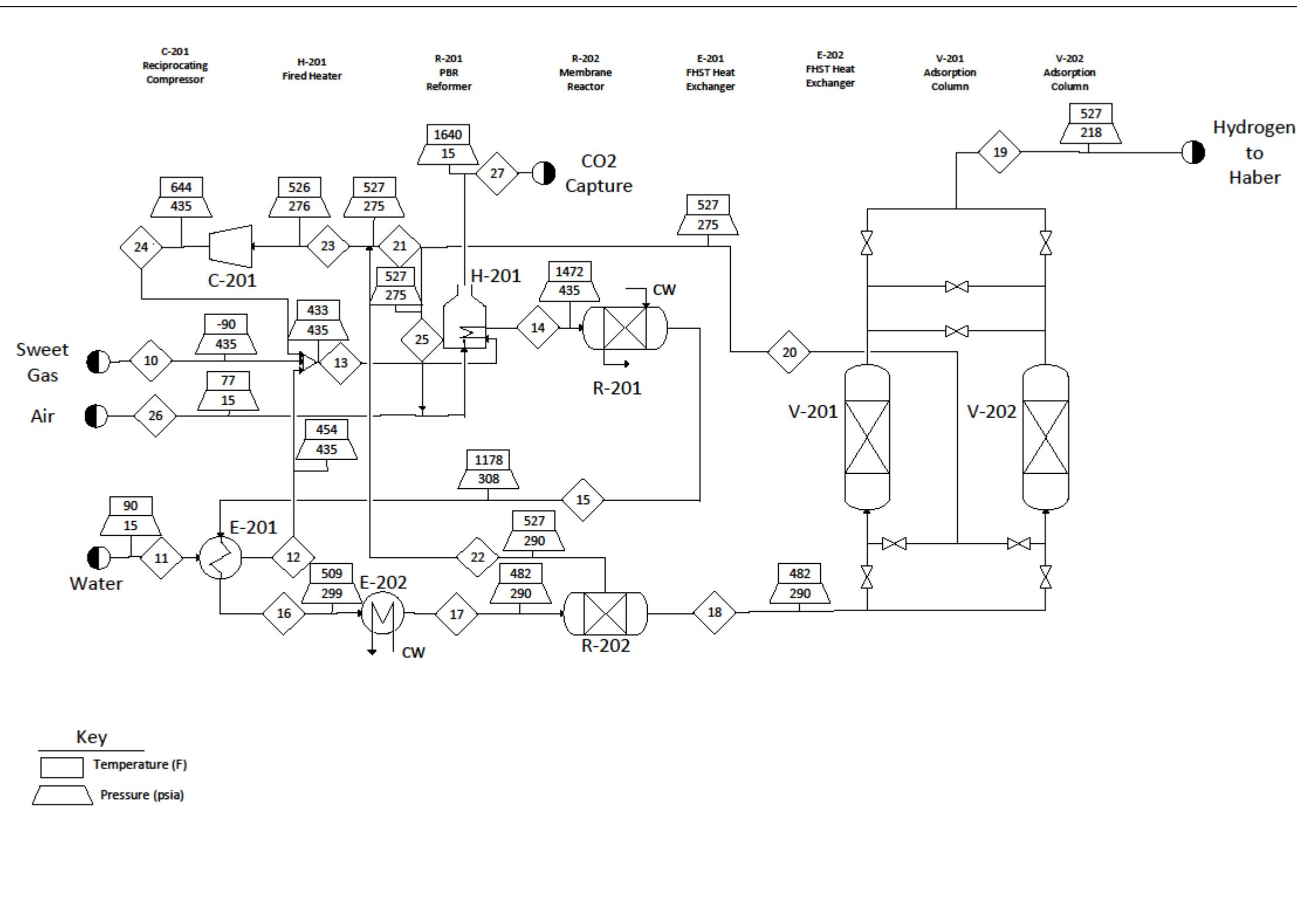


Figure 3: Process Flow Diagram of Hydrogen Production

Table 2: Hydrogen Stream Summary Table

	Unit	Hydrogen Production													
Stream ID #		10	11	12	13	14	15	16	17	18	19	20	21	22	23
Vapour Fraction		1	0	1	1	1	1	1	1	1	1	1	1	1	1
Temperature	F	-90	90	454	433	1472	1178	509	482	482	527	527	527	527	526
Pressure	psia	435	15	435	435	435	308	299	290	290	218	276	276	290	276
Molar Enthalpy	Btu/lbmole	-34638	-122811	-101492	-86121	-73798	-68417	-75671	-75932	-25141	5268	-97959	-97959	-94614	-95818
Molar Flow	lbmole/hr	179	357	357	973	973	1050	1050	1050	798	408	390	157	279	436
Molar Flow (CO)	lbmole/hr	0	0	0	4	4	41	41	41	0	0	10	4	0	4
Molar Flow (CO2)	lbmole/hr	0	0	0	187	187	189	189	189	4	0	120	48	139	187
Molar Flow (Ethane)	lbmole/hr	18	0	0	53	53	53	53	53	0	0	20	8	27	36
Molar Flow (H2O)	lbmole/hr	0	357	357	444	444	404	404	404	208	1	159	64	23	87
Molar Flow (Hydrogen)	lbmole/hr	0	0	0	76	76	193	193	193	583	407	27	11	65	76
Molar Flow (Methane)	lbmole/hr	161	0	0	208	208	170	170	170	4	0	54	22	25	47
Molar Flow (Nitrogen)	lbmole/hr	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Molar Flow (Oxygen)	lbmole/hr	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Mass Flow	lb/hr	3115	6434	6434	21453	21453	21453	21453	21453	5153	842	9967	4009	7861	11870
Liquid Volume Flow	barrel/day	693	441	441	2465	2465	2600	2600	2600	1437	805	1029	414	913	1327
Actual Volume Flow	barrel/day	5047	440	30298	87876	198765	256389	153666	153832	118560	115650	62995	25340	43366	71007
Molar Density	lbmole/ft3	0.15	3.47	0.05	0.05	0.02	0.02	0.03	0.03	0.03	0.02	0.03	0.03	0.03	0.03

	Unit	Hydrogen Production			
Stream ID #		24	25	26	27
Vapour Fraction		1	1	1	1
Temperature	F	644	527	77	1640
Pressure	psia	435	276	15	15
Molar Enthalpy	Btu/lbmole	-94581	-97959	-4	-103956
Molar Flow	lbmole/hr	436	233	130	341
Molar Flow (CO)	lbmole/hr	4	6	0	0
Molar Flow (CO2)	lbmole/hr	187	72	0	147
Molar Flow (Ethane)	lbmole/hr	36	12	0	0
Molar Flow (H2O)	lbmole/hr	87	95	0	154
Molar Flow (Hydrogen)	lbmole/hr	76	16	0	0
Molar Flow (Methane)	lbmole/hr	47	32	0	0
Molar Flow (Nitrogen)	lbmole/hr	0	0	27	27
Molar Flow (Oxygen)	lbmole/hr	0	0	103	13
Mass Flow	lb/hr	11870	5958	4063	10414
Liquid Volume Flow	barrel/day	1327	615	263	816
Actual Volume Flow	barrel/day	50444	37654	218259	2236146
Molar Density	lbmole/ft3	0.04	0.03	0.00	0.00

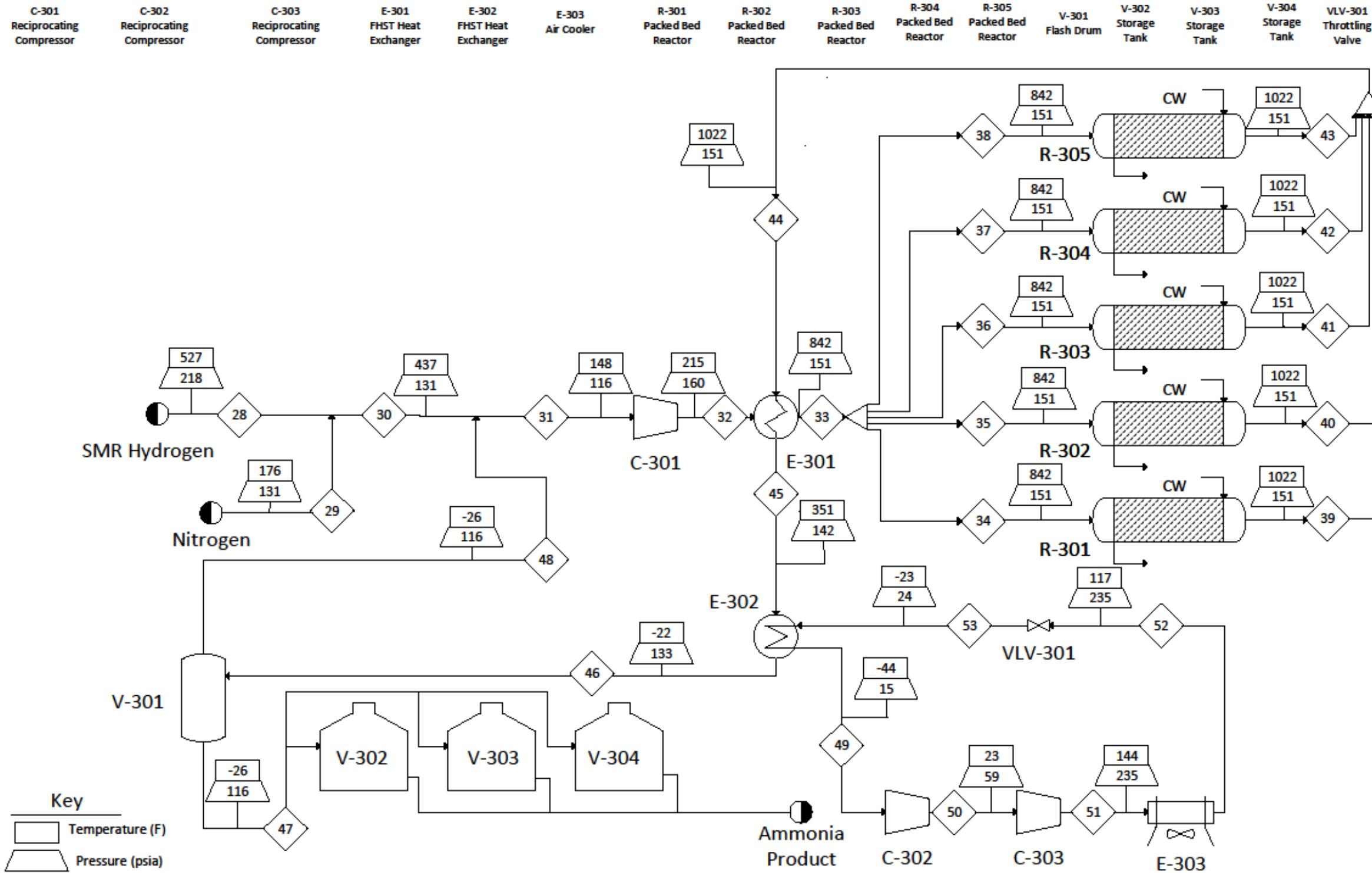


Figure 4: Process Flow Diagram of Ammonia Production

Table 3: Ammonia Stream Summary Table

	Unit	Ammonia Production														
Stream ID #		28	29	30	31	32	33	34	35	36	37	38	39	40	41	42
Vapour Fraction		1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
Temperature	F	527	176	437	148	215	842	842	842	842	842	842	1022	1022	1022	1022
Pressure	psia	218	131	131	116	160	151	151	151	151	151	151	151	151	151	151
Molar Enthalpy	Btu/lbmole	2783	675	2254	-1292	-819	3787	3787	3787	3787	3787	3787	968	968	968	968
Molar Flow	lbmole/hr	408	137	545	1425	1425	1425	285	285	285	285	285	231	231	231	231
Master Comp Molar Flow (Ammonia)	lbmole/hr	0	0	0	123	123	123	25	25	25	25	25	78	78	78	78
Master Comp Molar Flow (H ₂ O)	lbmole/hr	1	0	1	1	1	1	0	0	0	0	0	0	0	0	0
Master Comp Molar Flow (Hydrogen)	lbmole/hr	407	0	407	904	904	904	181	181	181	181	181	100	100	100	100
Master Comp Molar Flow (Nitrogen)	lbmole/hr	0	137	137	387	387	387	77	77	77	77	77	51	51	51	51
Master Comp Molar Flow (Oxygen)	lbmole/hr	0	0	0	10	10	10	2	2	2	2	2	2	2	2	2
Master Comp Molar Flow (Propane)	lbmole/hr	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Mass Flow	lb/hr	842	3830	4671	15109	15109	15109	3022	3022	3022	3022	3022	3022	3022	3022	3022
Std Ideal Liq Vol Flow	barrel/day	805	325	1130	2960	2960	2960	592	592	592	592	592	470	470	470	470
Actual Volume Flow	barrel/day	85192	30546	172029	342492	276908	566605	113321	113321	113321	113321	113321	104565	104565	104565	104565
Molar Density	lbmole/ft ³	0.02	0.02	0.01	0.02	0.02	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01

	Unit	Ammonia Production											
Stream ID #		42	43	44	45	46	47	48	49	50	51	52	53
Vapour Fraction		1	1	1	1	1	0	1	1	1	1	0	1
Temperature	F	1022	1022	1022	351	-22	-26	-26	-44	23	144	117	-23
Pressure	psia	151	151	151	142	133	116	116	15	59	235	235	24
Molar Enthalpy	Btu/lbmole	968	968	968	-4710	-9942	-31149	-3486	-46711	-45835	-44201	-50337	-50337
Molar Flow	lbmole/hr	231	231	1156	1156	1156	270	886	1668	1668	1668	1668	1668
Comp Molar Flow (Ammonia)	lbmole/hr	78	78	392	392	392	268	123	0	0	0	0	0
Comp Molar Flow (H ₂ O)	lbmole/hr	0	0	1	1	1	1	0	0	0	0	0	0
Comp Molar Flow (Hydrogen)	lbmole/hr	100	100	500	500	500	0	500	0	0	0	0	0
Comp Molar Flow (Nitrogen)	lbmole/hr	51	51	253	253	253	0	252	0	0	0	0	0
Comp Molar Flow (Oxygen)	lbmole/hr	2	2	10	10	10	0	10	0	0	0	0	0
Comp Molar Flow (Propane)	lbmole/hr	0	0	0	0	0	0	0	1668	1668	1668	1668	1668
Mass Flow	lb/hr	3022	3022	15108	15108	15108	4594	10514	73544	73544	73544	73544	73544
Std Ideal Liq Vol Flow	barrel/day	470	470	2351	2351	2351	510	1842	9939	9939	9939	9939	9939
Actual Volume Flow	barrel/day	104565	104565	522825	303007	133100	467	150975	2092544	568751	152594	11082	678184
Molar Density	lbmole/ft ³	0.01	0.01	0.01	0.02	0.04	2.47	0.03	0.00	0.01	0.05	0.64	0.01

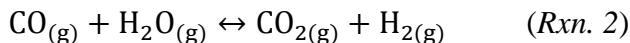
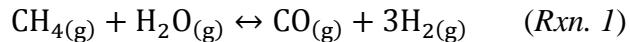
Process Description

Nitrogen Production

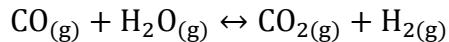
For 50 metric tons of ammonia to be produced per day, 41.7 metric tons of nitrogen must be produced per day. The group employed pressure swing adsorption to meet this demand. Before entering the pressure swing adsorption column, the feed stream of air, stream 1, is compressed to the desired operating pressure of 145 psia by C-101, C-102, and C-103. E-101 and E-102 serve as interstage coolers between C-101, C-102, and C-103. The stream exits C-103, and is cooled to 195 °F, by E-103. This cooled stream, stream 7, then enters the pressure swing adsorption system, V-101 and V-102. The stream enters V-101 where pressurization and adsorption will occur, while depressurization and desorption occur in V-102. Each bed will operate with a time shift of 65 seconds from the other bed's current operation (9). Stream 8 is then sent to the downstream process of ammonia production.

Hydrogen Production

The mechanism employed to produce 50 metric tons per day of ammonia requires 9.2 metric tons per day of hydrogen to be available. The onsite production of hydrogen utilizes steam methane reforming. Natural gas and water must be purchased for this process. Natural gas is obtained from the distribution line system (6). The sweet natural gas is sent to mix with stream 12, which is water that has been heated by E-204 to steam. The natural gas and steam mixture, stream 13, is then heated prior to entering the reactor by H-201, to ensure it is at the desired reaction temperature of 1470 °F. The natural gas and steam mixture exiting H-201 then enters R-201, and is reacted over a Ni-Al₂O₃ catalyst via the following reactions:



The unreacted material and products are then cooled by E-205 to reach the desired reaction temperature of the following reactor, R-202 of 480 °F. This reactor serves to produce hydrogen via the water gas shift mechanism over a copper membrane catalyst, shown below:

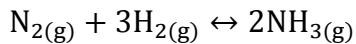


R-202 has two streams that exit it, with one containing most of the undesired byproduct and unreacted material, stream 22. Stream 18 also exits R-202 and enters the pressure swing adsorption system, V-201 and V-202. Stream 18 enters V-201, the first adsorption column, where pressurization and adsorption occur, and depressurization and desorption occur in V-201.

The columns operate off a time shift, 65 s (9). The purified hydrogen in stream 19, then goes to the downstream process. The adsorbed material is purged and sent to a t-splitter in stream 20. Part of the stream, stream 25, is sent to the fired heater, H-201, and is utilized as a fuel. H-201 also serves to convert the unreacted carbon monoxide in stream 25, to carbon dioxide. Exiting the t-splitter is also stream 21, which is combined with stream 22, and recycled back to the process by stream 23. Stream 23 must be compressed by C-201 to achieve the desired operating pressure of R-201, which is 435 psia.

Ammonia Production

The Haber-Bosch process was utilized to produce 50 metric tons per day of ammonia. The process begins with stream 28, carrying hydrogen, and stream 29, carrying nitrogen combining with the recycle stream, 48. C-301 serves to compress the feed to the desired pressure of the reaction, 145 psia. This compressed feed then enters E-301 to be heated to the reaction temperature of 840 °F, utilizing heat integration. The reaction takes place in R-301, R-302, R-303, R-304, and R-305 over a ruthenium-cesium catalyst, via the following reaction chemistry:



The streams exiting R-301, R-302, R-303, R-304, and R-305 combine to form stream 44 to then be utilized for heat integration in E-302. This stream, now labeled stream 45, then enters E-303 to be further cooled for separation of the desired ammonia product and unreacted nitrogen and hydrogen. The separation takes place in V-301. The unreacted hydrogen and nitrogen are recycled back in stream 46, and the ammonia is sent to storage tanks V-302, V-303, and V-304 in stream 47.

Energy Balance and Utility Requirements

Below in Table 4, an energy balance has been provided; additionally, in Table 5 the utility requirements are displayed.

Energy Balance

Below is the energy summary for the given process.

Table 4: Energy Balance

Stream	Molar Enthalpy (Btu/lbm)	Stream	Molar Enthalpy (Btu/lbm)
1	-931.196	27	-103956
2	890.5461	28	2783.371
3	-370.993	29	675.0804
4	887.0348	30	2254.165
5	-377.523	31	-1292.32
6	879.2921	32	-818.817
7	120.1409	33	3786.759
8	-834.6526335	34	3786.759
9	657.5421603	35	3786.759
10	-34638.3	36	3786.759
11	-122811	37	3786.759
12	-101492	38	3786.759
13	-86120.5	39	968.2813
14	-73798.3	40	968.2813
15	-68417.2	41	968.2813
16	-75671.2	42	968.2813
17	-75931.7	43	968.2813
18	-25140.8	44	968.2813
19	5268.37602	45	-4709.93
20	-97959.4	46	-9941.57
21	-97959.4	47	-31149.4
22	-94614.3	48	-3485.82
23	-95818.4	49	-46711.3
24	-94581.1	50	-45835.4
25	-97959.4	51	-44201.1
26	-3.95859	52	-50336.8
27	-103956	53	-50336.8

Utility Requirements

This process requires electricity and cooling water for operation. The utility requirements are broken up by hydrogen production, nitrogen production, and ammonia production in Table 5. The ammonia production utilizing the Haber-Bosch process, requires the most electricity and cooling water.

Table 5: Utility Requirements

	Electricity (BTU/hr)	Cooling Water (lb/hr)
Nitrogen Production		
C-101	457208	-
C-102	313904	-
C-103	313904	-
E-101	-	9995
E-102	-	10019
E-103	-	6015
Hydrogen Production		
C-201	539096	-
E-201	-	8930
Ammonia Production		
C-301	675576	-
C-302	1460336	-
C-303	2726188	-
R-301	-	25709
R-302	-	25709
R-303	-	25709
R-304	-	25709
R-305	-	25709
Total	1624112	34959

Equipment List and Unit Descriptions

For an overview of the equipment within each unit Table 6 is provided. More detail sizing information is provided in Tables 7-20.

Table 6: Overall Process Equipment Summary

Nitrogen Production			
Unit	Sizing	MAWP	MOC
C-101	457208 Btu/hr	47 psia	CS
C-102	313904 Btu/hr	79 psia	CS
C-103	313904 Btu/hr	154 psia	CS
E-101	16 ft ²	210 psia	SS
E-102	23 ft ²	100 psia	SS
E-103	43 ft ²	130 psia	SS
V-101	207 ft ³	195 psia	CS
V-102	207 ft ³	195 psia	CS
Hydrogen Production			
Unit	Sizing	MAWP	MOC
C-201	741 hp	435 psia	SS
E-201	354 ft ²	485 psia	SS
E-202	146 ft ²	276 psia	SS
H-201	17930000 Btu/hr	435 psia	SS
R-201	27 ft ³	485 psia	SS
R-202	386 ft ³	340 psia	SS
V-201	848 ft ³	340 psia	SS
V-202	848 ft ³	340 psia	SS
Ammonia Production			
Unit	Sizing	MAWP	MOC
C-301	921 hp	160 psia	SS
C-302	1964 hp	59 psia	SS
C-303	3636 hp	235 psia	SS
E-301	1840 ft ²	210 psia	SS
E-302	7770 ft ²	195 psia	SS
E-303	311 ft ²	285 psia	CS
R-301	151 ft ³	200 psia	SS
R-302	151 ft ³	200 psia	SS
R-303	151 ft ³	200 psia	SS
R-304	151 ft ³	200 psia	SS
R-305	151 ft ³	200 psia	SS
V-301	12.75 ft ³	166 psia	SS
V-302	28894 ft ³	250 psia	CS
V-303	28894 ft ³	250 psia	CS
V-304	28894 ft ³	250 psia	CS

Reactors

Reactors were utilized in this process for hydrogen production in the steam methane reforming unit and ammonia synthesis in the Haber-Bosch process, shown in Tables 6 and 7, respectively. The design pressure for all reactors is 50 psi larger than the operating pressure, for safety purposes (22). All reactors used in this process are suggested to be made of stainless steel, due to its ability to withstand temperatures well above the operating temperatures of each reactor (10). Stainless steel is also resistant to hydrogen embrittlement, and all the reactors encounter hydrogen (28).

The reactors were simulated in Aspen HYSYS. The kinetic data obtained from literature for each reaction occurring at the desired operating conditions over the catalyst used was utilized to set the reactions occurring within the reactors in Aspen HYSYS. For each reaction the weight of catalyst per feed flow rate at the given conversion was obtained from literature. This was then used to determine the weight of catalyst needed using Equation 1 in Appendix A. Once the weight of the catalyst was found the volume of the reactor was determined using Equation 2 in Appendix A.

Hydrogen Production

Table 7: Hydrogen Production Reactor Specifications

Parameters	R-201	R-202
Type	PBR	Membrane
MOC	SS	SS
Temperature (°F)	900	482
Design Pressure (psia)	485	340
Orientation	Horizontal	Horizontal
Capacity (ft ³)	27	386
Length (ft)	6.75	16.25
Diameter (ft)	2.25	5.5
Internals	Ni-Al ₂ O ₃	Cu

In this process two reactors were used to produce hydrogen. R-201 serves to produce hydrogen and carbon monoxide from water and methane, this reaction is known as steam reforming. This reaction takes place at a pressure of 435 psia and a temperature of 1184 °F. It is important to note that the water gas shift reaction, which produces carbon dioxide and hydrogen

from carbon monoxide and water, also takes place in this reactor in small quantities. R-201 is designed as a packed bed reactor, PBR, due to their effectiveness at high temperatures and pressures, and low operating, maintenance, and capital costs (11). Ni-Al₂O₃ is the catalyst selected to be used in this reactor because it is highly active and durable (12). For simulation in Aspen HYSYS the kinetic data was obtained from (13). R-201 has a cooling jacket to maintain the temperature below the autoignition of the components.

The second reactor, R-202, produces carbon dioxide and hydrogen from the carbon monoxide and unreacted water exiting R-201. R-202 is a membrane reactor. Membrane reactors contain, as the name implies, a catalytic membrane within the pressurized vessel. Through combining separation with the reaction, as the product is removed the reaction conversion is increased due to Le Châtelier's principle (14). It was found in the literature that the conversion rate for the water gas shift reaction taking place in R-202, could be increased by 10% when utilizing a membrane reactor instead of a packed bed reactor (15). This increase in conversion was utilized to reduce the cost of the following pressure swing adsorption, an in-depth analysis of this can be found in "other important considerations". The reaction occurring in R-202 was simulated in Aspen HYSYS as done with the other reactors to determine the incoming and exiting flow rates at the given conversion. The kinetics and weight of catalyst per reactant flow rate was obtained from (15). Equation 3 in Appendix A was utilized to determine the amount of membrane required for the desired reaction. The reactor is operated at a pressure of 290 psia and a temperature of 482 °F.

Ammonia Production

Table 8: Ammonia Production Reactor Specifications

Parameters	R-301	R-302	R-303	R-304	R-305
Type	PBR	PBR	PBR	PBR	PBR
MOC	SS	SS	SS	SS	SS
Temperature (°F)	842	842	842	842	842
Design Pressure (psia)	200	200	200	200	200
Orientation	Horizontal	Horizontal	Horizontal	Horizontal	Horizontal
Capacity (ft ³)	151	151	151	151	151
Length (ft)	12	12	12	12	12
Diameter (ft)	4	4	4	4	4
Internals	Ru-Cs	Ru-Cs	Ru-Cs	Ru-Cs	Ru-Cs

R-301, R-302, R-303, R-304, and R-305 serve to produce anhydrous ammonia. These reactors utilize a Ru-Cs catalyst to convert hydrogen and nitrogen to ammonia. This reaction takes place at 150 psia and a temperature of 842 °F. Packed bed reactors were utilized for this reaction, due to the high pressure and temperature associated with the reaction and for the lower capital cost. This reaction at the above specified temperature and pressure was simulated in Aspen HYSYS using kinetic data at the specified temperature, pressure, and catalyst obtained from (16), and the weight of catalyst per flow of reactants was obtained from (17) to determine the amount of catalyst needed and volume of reactor. Modular manufacturing was utilized to produce these reactors to lower the capital investment and reduce safety concerns associated with the production of ammonia. R-301, R-302, R-303, R-304, and R-305 all have a cooling jacket to maintain a temperature below the component's autoignition temperatures, for safety purposes.

Pressure Swing Adsorption Columns

Pressure swing adsorption technology was employed to provide nitrogen for the downstream reaction and in the steam methane reforming unit to separate hydrogen. For nitrogen and hydrogen, values for each vessel are shown in Tables 8 and 9, respectively. To appropriately size the volume of the pressurized vessels it was necessary to determine the volume of adsorbent needed to create the desired output of product. It is important to note that some of the desired product will be adsorbed in both pressure swing adsorption systems. To account for this, Equation 4 located in Appendix A was used to determine the necessary flow rate into the systems to combat this loss, and experimental product recovery values obtained from (18) and (19) were utilized.

The volume of the pressurized vessel was calculated using Equation 5 in Appendix A, obtained from (9). The system does not operate with 100% efficiency either, as some of the voidage spaces will be empty each cycle (9). To account for this a bed voidage factor was used to determine the actual adsorbent and pressurized vessel size that should be purchased (9). These calculations are in Appendix B.2. For the bed voidage variable, the more conservative value obtained from (18, 20), is used to account for uncertainty. These smaller bed voidage values result in larger total vessel volumes, which provides a more conservative estimate for capital costs.

As the operating pressure of a pressure swing adsorption system increases the amount adsorbed has logarithmic growth, which results in higher purity at higher pressures (21). For both systems, information from literature was obtained to determine which operating pressure would be best suited for this process. For safety purposes, the adsorption towers are designed to withstand operation at a pressure that is 50 psi higher than the actual operating pressure (22).

Nitrogen Production

Table 9: Nitrogen Production Pressure Swing Adsorption Specifications

Parameters	V-101	V-102
MOC	CS	CS
Temperature (°F)	194	194
Design Pressure (psia)	195	195
Orientation	Vertical	Vertical
Capacity (ft ³)	207	207
Height (ft)	18.75	18.75
Diameter (ft)	3.75	3.75
Internals	CMS (3A)	CMS (3A)
Internals	CMS (5A)	CMS (5A)

The nitrogen pressure swing adsorption system, V-101 and V-102, utilizes carbon molecular sieve (CMS 5A) within the column first and then carbon molecular sieve (CMS 3A). This stacking allows for the removal of water vapor by CMS 5A, so that it does not excessively absorb on the CMS 3A preventing oxygen removal and in turn increasing the necessary adsorbent (19). The 3-angstrom pore size of CMS 3A allows oxygen, carbon monoxide, carbon dioxide, and other undesirable air particles to be trapped in the void between carbon particles (23). This adsorption column is designed to achieve a nitrogen purity of 99.9% (18). The pressure drop along the adsorption system is 14.5 psia (24). The pressurized vessel's material of construction is suggested to be carbon steel, CS, due to its low cost and the components within the adsorption column are non-acidic (25).

Hydrogen Production

Table 10: Hydrogen Production Pressure Swing Adsorption Specifications

Parameters	V-201	V-202
MOC	SS	SS
Temperature (°F)	542	542
Design Pressure (psia)	340	340
Orientation	Vertical	Vertical
Capacity (ft ³)	848	848
Height (ft)	30	30
Diameter (ft)	6	6
Internals	CMS (5A)	CMS (5A)

To separate hydrogen from the other products and unreacted material of R-202, a pressure swing adsorption column was employed, V-201 and V-202. Carbon molecular sieve 5A (CMS 5A), was used as the adsorbent. This adsorbent was selected based on its ability to absorb methane, carbon dioxide, carbon monoxide, and water, as these components are present in the stream carrying the hydrogen product (19). The pressure swing adsorption system is designed to produce hydrogen at a purity of 99.9% (26). A pressure drop of 14 psia is expected across the vessel (24). The material of construction is suggested to be stainless steel as it can withstand hydrogen embrittlement and is unreactive with the components entering (28).

Flash drum

Ammonia Production

V-301 is utilized as a flash drum in the downstream process to separate liquid ammonia from the unreacted hydrogen and nitrogen. V-301 was simulated in Aspen HYSYS, which provided liquid and vapor flow rates and densities. Equations 6-10 located in Appendix A were obtained from (27), to size the pressurized vessel. The vessel is designed to withstand a pressure 50 psi higher than the operating pressure for safety purposes. The flash drum is recommended to be made of stainless steel, due to the interaction with hydrogen (28). Specifications for V-301 are listed in Table 11.

Table 11: Ammonia Flash Drum Specifications

Parameters	V-301
MOC	SS
Temperature (°F)	-26
Design Pressure (psia)	166
Orientation	Vertical
Capacity (ft ³)	12.75
Height (ft)	5.25
Diameter (ft)	1.75

Compressors

Reciprocating compressors were utilized throughout this project due to their durability, efficiency, affordability, and significant product life (29). The compressors in this process utilize electric motors as the drivers for their simplified and safer operation (30). These motors also typically have lower initial capital cost compared to natural gas motors (30). The compressors for this process were simulated in Aspen HYSYS to determine the gas horsepower (GHP). The brake horsepower (BHP) was then calculated from this value using Equation 12 in Appendix A. Using Equation 13 in Appendix A, the purchased horsepower was then found from using the calculated brake horsepower (BHP) and the more conservative driver efficiency obtained from (31). The equations used to calculate the purchased horsepower were obtained from (32).

Nitrogen Production

The pressure swing adsorption system for nitrogen production, V-101 and V-102, is designed to be operated at a pressure of 145 psia. To achieve this the incoming air stream, 1, is compressed from atmospheric pressure, 14 psia, to 145 psia. This compression takes place in multiple stages, C-101, C-102, and C-103, so that interstage cooling can be employed to maintain the temperature of the stream below 300 °F. It is desirable to keep the stream temperature below 300 °F within the reciprocating compressors to prevent degradation of the lube oil and extend the life of the compressors (33). The material of construction is suggested to be carbon steel, as it is unreactive with air and is low in cost (25). Specifications for C-101, C-102, and C-103 can be found below in Table 12.

Table 12: Nitrogen Production Compressor Specifications

Parameters	C-101	C-102	C-103
Type	Reciprocating	Reciprocating	Reciprocating
Drive	Electric	Electric	Electric
MOC	CS	CS	CS
Operating Pressure (psia)	47	79	154
Purchased (hp)	629	440	440
Driver Efficiency (%)	30	30	30

Hydrogen Production

C-201, shown in Table 13, is employed in the steam methane reforming production of hydrogen, to increase the recycle stream, 23, pressure from 275 psia to 435 psia. This pressure increase takes place to ensure the reaction within R-201 occurs at the desired reaction pressure. Due to the corrosive nature of the components in stream 23 it is recommended for the material of construction to be stainless steel for C-201 (28).

Table 13: Hydrogen Production Compressor Specifications

Parameters	C-201
Type	Reciprocating
Drive	Electric
MOC	SS
Operating Pressure (psia)	435
Purchased (hp)	741
Driver Efficiency (%)	30

Ammonia Production

C-301 is in the downstream production of ammonia to increase the incoming reactant mixture stream, 31, to the desired pressure of 145 psia for R-301, R-302, R-303, R-304, and R-305. It is suggested that C-301 be made of stainless steel, to prevent hydrogen embrittlement or reaction with any of the components (28). A vapor compression refrigeration cycle is used to

cool stream 49, so ammonia can be separated from the unreacted material. This cycle requires the compression of the refrigerant (34). C-302 and C-303 are used to increase the pressure of stream 49 from 15 to 235 psia. The material of construction is suggested to be stainless steel due to the hydrogen present in stream 49 (28). Specifications for C-301, C-302, and C-303 can be found below in Table 14.

Table 14: Ammonia Production Compressor Specifications

Parameters	C-301	C-302	C-303
Type	Reciprocating	Reciprocating	Reciprocating
Drive	Electric	Electric	Electric
MOC	SS	SS	SS
Operating Pressure (psia)	160	59	235
Purchased (hp)	921	1,964	3,636
Driver Efficiency (%)	30	30	30

Heat Exchangers

The equations obtained from (35) was used to calculate the heat transfer coefficients for all the employed heat exchangers, using Equations 14 and 15 in Appendix A. The heat transfer area was then calculated using Equation 16 in Appendix A, with the calculations located in Appendix B.5. The duties, inlet, and outlet temperatures were obtained from simulation of each heat exchanger in Aspen HYSYS. The more conservative film heat transfer and fouling resistance values were used to account for the uncertainty of the heat exchanger duty. This will result in smaller overall heat transfer coefficients, which will result in larger heat transfer surface areas. These larger areas provide a more moderate capital cost estimate. All heat exchangers were designed to withstand a pressure 50 psi above the operating pressure.

Nitrogen Production

E-101 and E-102, shown in Table 15, are interstage coolers used after C-101 and C-102, respectively. As stated previously these heat exchangers are employed to maintain the temperature within the compressors below 300 °F, and to extend the product life of the compressors (32). A double pipe heat exchanger design was selected for E-101 and E-102, because of industrial typical practices and the low surface area requirement for the needed heat transfer (36). Cooling water flows on the tube-side of E-101 and E-102, so the tubes are suggested to be made of stainless steel to prevent corrosion (28). The shell-side is suggested to be made of carbon steel, due to its nonreactivity with air and low cost (25).

E-103, shown in Table 15, serves to lower the temperature of the incoming air stream to V-101 and V-102, because the amount of adsorbate adsorbed decreases with increasing temperature (21). E-103 is designed as a double pipe heat exchanger due to the low surface area requirement, for the given heat transfer. Air flows through the shell-side and is suggested to be made of carbon steel due to its low cost (25). The tube-side is suggested to be made of stainless steel, due to the corrosiveness of cooling water (37).

Table 15: Nitrogen Production Heat Exchanger Specifications

Parameters	E-101	E-102	E-103
Type	Double Pipe	Double Pipe	Double Pipe
Area (ft ²)	16	23	43
Heat Duty (BTU/hr)	103,120	171,365	171,745
Design Pressure (psia)	210	100	130
Tube			
Max Operating Temp (°F)	120	120	120
MOC	SS	SS	SS
Shell			
Max Operating Temp (°F)	300	300	300
MOC	CS	CS	CS

Hydrogen Production

E-201, shown in Table 16, utilizes heat integration of stream 15, to heat the incoming water, stream 11, to steam for reaction in R-201. E-201 is designed as a shell and tube heat exchanger, which serves the advantage of being able to withstand high pressures, small pressure drop, and flexibility in design (38). The shell and tube side are both recommended to be made of stainless steel, due to the corrosiveness of the incoming water and stream 15.

E-202, shown in Table 16, cools the material exiting R-201 to the desired reaction temperature of R-202. This is a shell-and-tube heat exchanger with cooling water on the tube-side and stream 16 on the shell-side. It is suggested that the material of construction for both the tube-side and-shell side be stainless steel to prevent corrosion.

Table 16: Hydrogen Production Heat Exchanger Specifications

Parameters	E-201	E-202
TEMA Type	BEP	BEP
Area (ft ²)	354	146
Heat Duty (BTU/hr)	7,609,075	3,160,020
Design Pressure (psia)	485	276
Tube		
Max Operating Temp (°F)	454	120
MOC	SS	SS
Shell		
Max Operating Temp (°F)	1178	509
MOC	SS	SS

Ammonia Production

E-301 utilizes heat integration of stream 44, to heat stream 32 to the desired reaction temperature of R-301, R-302, R-303, R-304, and R-305.. The shell-side contains the products and unreacted material of the ammonia reactors and the tube -ide contains the reactants flowing into the ammonia reactors. It is suggested that both the shell-and-tube side be made of stainless steel.

After utilization in E-301 stream 44 now labeled stream 45 then enters E-302 and is cooled to -22 °F. This cooling takes place so that stream 46 can then be flashed in V-301, to separate the desired ammonia product from the unreacted material. To achieve the desired temperature of -22 °F a vapor compression refrigeration cycle was utilized, where E-302 serves as the condenser. E-302 is designed as a shell-and-tube heat exchanger, with stream 45 on the shell-side and the refrigerant on the tube-side. The material of construction is suggested to be stainless steel on both the tube-side and shell-side, to extend the lifetime of E-302. Specifications for E-301 and E-302 are shown below in Table 17.

Table 17: Ammonia Production Heat Exchanger Specifications

Parameters	E-301	E-302
TEMA Type	BEP	BEP
Area (ft ²)	1840	7770
Heat Duty (BTU/hr)	5,696,380	6,912,430
Design Pressure (psia)	210	195
Tube		
Max Operating Temp (°F)	1022	351
MOC	SS	SS
Shell		
Max Operating Temp (F)	842	-22
MOC	SS	SS

Heaters

Hydrogen Production

A fired heater, H-201, was utilized to heat stream 13 to the desired reaction temperature of R-201. A fired heater was selected due to its ability to utilize the waste from the pressure swing adsorption system, V-201 and V-202, as fuel (39). Within the heater the waste is combusted to carbon dioxide and water. This combustion releases heat to increase the temperature of stream 13 to 1470 °F prior to entering R-201. The thermal efficiency was found from literature to be 75% (40). H-201 was simulated in Aspen HYSYS to obtain the duty required. The material of construction is suggested to be stainless steel, due to corrosiveness of the material within it and extreme heat transfer (28). H-201 specifications can be found below in Table 18.

Table 18: Hydrogen Production Heater Specifications

Parameters	H-201
Type	Fired Heater
MOC	SS
Heat Duty (BTU/hr)	17,930,000
Max Operating Temperature (°F)	1640
Design Pressure (psia)	435
Thermal Efficiency (%)	75

Air Cooled Heat Exchanger

Ammonia Production

E-303, shown in Table 19, is an air cooler used in the vapor compression refrigeration cycle that is present in the ammonia production process to cool stream 45 to -27 °F. E-303 is modeled in Aspen HYSYS to obtain the heat duty, mass flow rate, and density of air needed to condense the refrigerant propane to a saturated liquid at 117 °F, prior to it being flashed across a Joule Thomson valve to substantially drop the temperature of propane. The surface area was calculated using Equation 17 in Appendix A, utilizing the values obtained from Aspen HYSYS. These equations were obtained from (41).

Table 19: Ammonia Production Air Cooler Specifications

Parameters	E-303
Type	Air Cooler
MOC	CS
Heat Duty (BTU/hr)	11,700,000
Design Pressure (psia)	285
Area (ft ²)	311

Storage Tanks

Ammonia Production

The anhydrous ammonia produced by the process must be stored on site until shipment can remove it. V-302, V-303, and V-304 store the ammonia and the specifications for the vessels are shown in Table 20 below. The storage of anhydrous ammonia is regulated by the U.S. Department of Labor. The anhydrous ammonia will be stored at 200 psia. For safety purposes, the tanks are designed for storage at 250 psia and with 85% occupancy of the tank, following the ASME Boiler and Pressure Vessel Code listed in the project memo. The vessels are stored under pressure at atmospheric temperature. The vessels are designed to hold 10 days of production each, that is 750 metric tons of ammonia at the above specifications. The volume of the required vessel was obtained from Equation 18 in Appendix A. The material of construction is suggested to be stainless steel for this vessel.

Table 20: Ammonia Production Storage Vessel Specifications

Parameters	V-302	V-303	V-304
MOC	SS	SS	SS
Temperature (F)	90	90	90
Design Pressure (psia)	250	250	250
Orientation	Vertical	Vertical	Vertical
Capacity (ft ³)	28,894	28,894	28,894
Height (ft)	96.75	96.75	96.75
Diameter (ft)	19.5	19.5	19.5

Equipment Cost Summary

To determine the economic feasibility of the project, the estimated bare module cost of each piece of equipment was calculated. This cost is influenced by the material of construction, design pressure, cost of installation, and size. These prices were optimized throughout the process to reduce expenses, while also maintaining safe margins of error. The capital costs listed in Table 21, were found using Equations 19-22 located in Appendix A. The project is projected to begin construction in mid-2021, to allow time to obtain a construction permit. However, the equipment is expected to be purchased in 2020. The estimates for the bare module costs for all pieces of equipment were not in 2020 USD but were in 2001 USD. Thus, these prices had to be scaled to 2020 USD to account for the escalation of equipment costs and are presented at this escalated value in Table 21 below.

Table 21: Equipment Cost Summary

Equipment	Capital Cost
Adsorbers	
V-101	\$217,800
V-102	\$217,800
V-201	\$916,200
V-202	\$916,200
Storage Tanks	
V-302	\$129,000
V-303	\$129,000
V-304	\$129,000
Air cooler	
E-303	\$241,500
Heat Exchangers	
E-101	\$21,500
E-102	\$24,400
E-103	\$19,900
E-201	\$210,200
E-202	\$190,700
E-301	\$364,300
E-302	\$1,034,100
Heaters	
H-201	\$1,660,200
Flash drum	
V-301	\$46,700
Compressors	
K-101	\$597,200
K-102	\$525,300
K-103	\$525,100
K-201	\$636,900
K-301	\$698,100
K-302	\$1,009,000
K-303	\$1,429,900
Reactors	
R-201	\$143,500
R-202	\$407,000
R-301	\$141,400
R-302	\$113,100
R-303	\$99,200
R-304	\$90,500
R-305	\$84,200
Total	\$12,968,900

For comparison purposes, the bare module capital cost breakdown between the three processes is shown in Figure 5. This figure displays that the equipment for ammonia production resulted in the highest capital cost investment. Whereas nitrogen production resulted in the lowest capital cost investment.

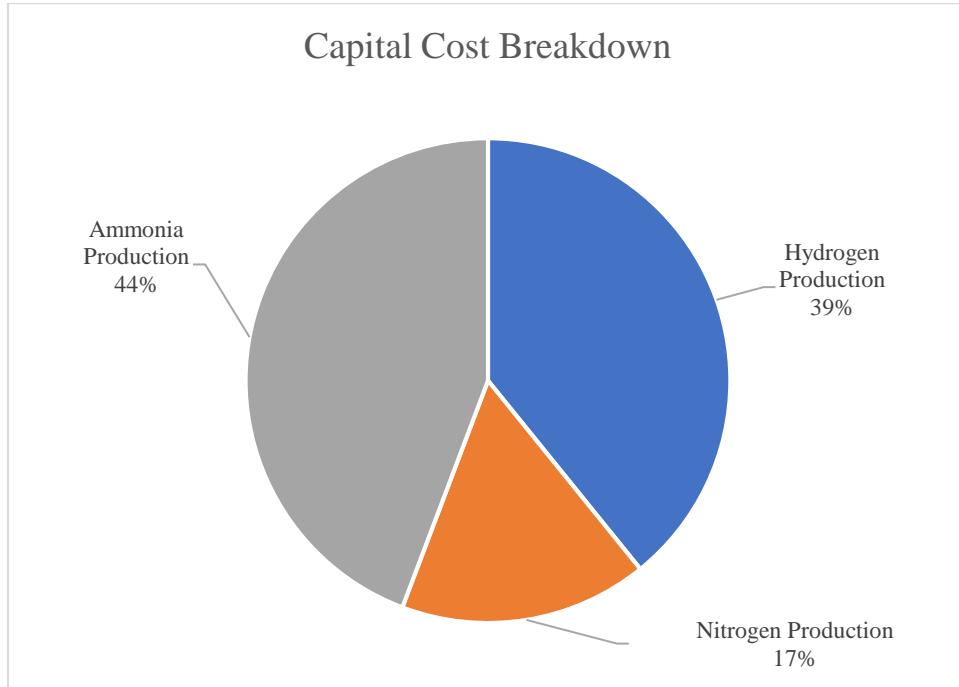


Figure 5: Capital Cost Breakdown by Unit

Fixed Capital Investment Summary

The bare module capital cost shown in Table 22, was then multiplied by a contingency factor to cover any unforeseen circumstances, as shown in Equation 23 in Appendix A (25). The grassroots cost in 2020 USD was then calculated using Equation 24 in Appendix A, to account for auxiliary facility costs, using the factor and equation obtained from Turton et al. (25). The grassroots cost was the value utilized in the cash flow table to determine the economic feasibility of the project. Table 22 below displays the bare module cost, the total module cost, and the grassroots cost.

Table 22: Total Installation Capital Cost Investment

	Capital Investment
Bare Module Cost	\$13,000,000
Total Module Cost	\$15,300,000
Grassroots Costs	\$21,800,000

Safety, Health, and Environmental Considerations

Introduction

In the process, there are several materials to consider when discussing safety, health, and environmental concerns. Material properties of ammonia, hydrogen, nitrogen, methane, air, carbon dioxide, and water are shown and compared in Table 23. The material that stands out in the process, in terms of quantity and safety, is ammonia. Two things that stand out about ammonia are its strong reactivity with water and its high toxicity limits, 100 ppm (42). Ammonia, under normal conditions, is very stable and has flammability limits of 15% to 28% by volume of ammonia in air (43). For hydrogen, the most concerning property is the flammability of the gas. Hydrogen's flammability limits are 4%-75%, so hydrogen burns over wide concentrations in air (45). While not as flammable as hydrogen, methane's risk is the same. Methane's flammability limits are 5%-15% by volume in air (46). The other materials present no or minimal risk (45-49).

Table 23: Material Properties

Material	Ammonia	Hydrogen	Nitrogen	Methane	Air	Carbon Dioxide	Water
Molecular Weight (g/mol)	17.03	2.02	28.01	16.04	28.96	44.01	18.02
Boiling Point (°F)	-28.03	-423.2	-320.4	-258.7	-317.8	-109.2	212
Flammability Limits	15-28	4-75	-	5-15	-	-	-
Flash Point (°F)	-	-	-	-306	-	-	-
Auto Ignition Temperature (°F)	1204	1058	-	999	-	-	-
Liquid Density (lbm/ft ³)	42.57	4.43	50.47	26.38	0.07	48.25	62.4
Reactivity of Water	strong	poor	poor	poor	poor	poor	-
Toxicity Limits (ppm)	100	41,000	900,000	1,000	-	5,000	-

The materials listed above were placed in an interaction matrix generator, with the results being shown in Table 24 (51). The table outlines if a material is compatible with another, shown in green, or if there is caution between the two materials, shown in yellow. Four material combinations came back with a note of caution. For ammonia interacting with water, the caution is that heat is generated. For carbon dioxide and water interacting, the caution is that heat is generated, and it becomes corrosive. For ammonia and carbon dioxide interacting, the caution is that heat is generated. For hydrogen and air interacting, there is the caution of heat being

generated along with the mixture being unstable when heated and possibly resulting in an intense or explosive reaction.

Table 24: Interaction Matrix

	Water					
Ammonia	Caution	Ammonia				
Hydrogen	Compatible	Compatible	Hydrogen			
Nitrogen	Compatible	Compatible	Compatible	Nitrogen		
Methane	Compatible	Compatible	Compatible	Compatible	Methane	
Air	Compatible	Compatible	Caution	Compatible	Compatible	Air
Carbon Dioxide	Caution	Caution	Compatible	Compatible	Compatible	Compatible

On the site of the process, ammonia is the only hazardous material that is being stored. Specific hazards of ammonia can be viewed above in Table 23. The team has planned for three storage tanks to be available, instead of one, to minimize the risk. This safer alternative has been put in place to limit the amount of ammonia that would be released in the chance of a loss of containment.

For ammonia, hydrogen, and methane, a more in-depth hazard identification was constructed. Along with material properties and the interaction matrix, the inventory estimates, process technology, equipment, and operating condition hazards were listed. The most common hazard is the high temperature and high pressure the process is operating at. These can be found in Table 25 below.

Table 25: Hazard Identification Summary

Material	Source	Hazards
Ammonia	Material Properties	Ammonia is highly toxic to humans and animals if exposed.
	Interaction Matrix	Ammonia can generate heat when exposed to water or carbon dioxide. Ammonia is corrosive when exposed to carbon dioxide.
	Inventory Estimates	There is a risk of leaking ammonia out of storage tanks if there is a loss of containment.
	Process Technology, Equipment and Operating Conditions	There are three storage tanks on ammonia. When ammonia is present in tank, there should be no welding or heat source nearby. Due to the high level of pressure when stored, this could lead to an explosion if heated or over pressurized.
Hydrogen	Material Properties	Hydrogen gas is a highly flammable gas that can combust at low concentrations.
	Interaction Matrix	Hydrogen, when mixed with air, is unstable when heated. The two can also generate heat and lead to an intense or explosive reaction.
	Inventory Estimates	-
	Process Technology, Equipment, and Operating Conditions	Hydrogen is used in the process which operates at high temperatures and high pressures.
Methane	Material Properties	Methane is highly flammable.
	Interaction Matrix	Methane does not react with any of the materials listed.
	Inventory Estimates	-
	Process Technology, Equipment, and Operating Conditions	Methane is used in the process which operates at high temperatures and high pressures.

Several hazards are mentioned in Table 26 along with a rating for different potential consequences if that hazard were to happen. Specifically, equipment damage, environmental compliance, loss of life, disruption of other business units, legal and PR, and the community impact are discussed and if the hazard will have no, low, medium, or a high impact.

Table 26: Potential Consequence Summary

Number	Hazard	Equipment Damage	Environmental Compliance	Loss of Life	Disruption of Other Business Units	Legal/PR	Community Impact
1	Toxicity (AA)	-	-	high	medium	high	low
2	VCE (AA)	high	-	high	high	high	medium
3	Flammability (H)	medium	-	medium	low	low	low
4	VCE (H)	high	-	high	high	high	medium
5	Toxicity (M)	-	-	low	low	low	low
6	Water and CO ₂ reactivity	medium	-	low	low	low	low
7	Water and Ammonia reactivity	medium	-	medium	low	low	low
8	Ammonia and CO ₂ reactivity	medium	-	low	low	low	low

The team's preliminary design includes several safeguards that are incorporated.

Whenever working with chemicals, personal protective equipment (PPE) should be worn to minimize the exposure to chemicals and hazards that can cause illness or injury. Employees who regularly work with anhydrous ammonia and are subject to overexposure should be provided with the necessary PPE. Specific PPE for working with the process and anhydrous ammonia are safety goggles, impervious gloves and clothes, boots, and gas masks (51). In addition, during clean up procedures, shoe covers should be worn to minimize the possibility of a slip. It is advised to keep water on hand in case of leak or exposure (51). All storage containers should be completely cleaned and ventilated, and never welded on unless it is an open container. These containers should be kept away from flames and hot surfaces. Another safeguard set in place is utilizing modular manufacturing in the ammonia reactors to alleviate the amount that would be released if an incident were to occur. The ammonia storage tanks on site are set to be spaced so that if one leaked, it would not affect the other two tanks. The team also added 50 psi to all of the vessels' operating pressure so they would be designed to withstand a higher pressure. The last safeguard set in place is the use of stainless steel in areas where corrosion could be a possibility. In the detailed design, additional safeguards need to be set in place such as fire protection, training procedures and alarms, for example high level alarms on storage tanks.

For the process, reasons for the project to be terminated would be if the plant site was determined to be inadequate for the process. If a catastrophe were to occur onsite, the project could possibly be terminated. Detailed design needs to be concerned with making sure the proper alarms are placed correctly to mitigate an accident occurring. PSM and RMP have no special concerns that have not already been stated. Overall, the process is hazardous, but has steps in place to minimize the risks associated with those hazards.

Listed below in Table 27 is a list of hazards that could be a problem to the process. Alongside the hazards are the inherently safer design concepts the team has set in place to lessen the risks if any of the hazards happened. The team has utilized minimization, substitution, and moderation.

Table 27: Inherently Safer Design Application Summary

Hazard	Inherently Safer Concept	How Incorporated in Prelim Design
Ammonia toxicity	Minimization	Due to modular manufacturing and multiple storage tanks in the process, if ammonia's containment was lost, the amount of ammonia lost would be reduced and less toxic material leaked.
Ammonia VCE	Minimization	Due to modular manufacturing and multiple storage tanks in the process, if ammonia's containment was lost, the amount of ammonia lost, and the size of vapor clouds would be reduced.
Hydrogen flammability	Minimization	The process is producing hydrogen onsite instead of buying it in order to make a continuous process instead of onsite storage.
Hydrogen VCE	Minimization	The process is producing hydrogen onsite instead of buying it in order to make a continuous process instead of onsite storage.
Methane toxicity	Substitution	For methane, the membrane reactor was selected resulting in less throughout the process which lessens what would get released.
Water and CO ₂ reactivity	Substitution	Any equipment that would encounter water reacting with CO ₂ , stainless steel has been used to prevent corrosion.
Water and Ammonia reactivity	Moderation	Utilizing refrigeration in the process, the magnitude of the consequences if ammonia was to react with water would be reduced.
Ammonia and CO ₂ reactivity	Moderation	Utilizing refrigeration in the process, the magnitude of the consequences if ammonia was to react with CO ₂ would be reduced.

Process Safety Considerations

Minimizing Environmental Impacts

In the group's design of producing ammonia, there is no liquid or solid waste generated by the process, but there is gaseous waste. The plant is producing 6,448 lbs. of carbon dioxide per hour. Given that roughly 1400 lbs. of carbon dioxide emission is allowed, the remaining amount of carbon dioxide being released is 5,046 lbs. per hour (53). On an annual basis, the plant is producing 21,219 tons of carbon dioxide waste. The best available control technology the group is putting into place to manage these emissions is capturing the carbon dioxide (54). To capture, the carbon dioxide will be trapped at its source of emission. Per ton of carbon dioxide, there is an allowance cost of \$40 (55). On an annual basis, the cost of capturing the carbon dioxide would be roughly \$850,000.

Assessing and Mitigating Potential Health Impacts

For the process, health risks were looked at for ammonia, hydrogen, nitrogen, methane, carbon dioxide, and water. These risks are outlined in Table 28 below. To mitigate these health risks, plant workers will be utilizing PPE to limit exposure to these materials in case loss of containment does occur. As mentioned in picking the best available control technology, carbon dioxide waste is managed to limit the amount exposed to the environment and therefore mitigating the health risks.

Table 28: Key Health Risks

Material	Health Hazard
Ammonia	Ammonia causes severe burns and eye damage, very toxic to aquatic life, and may displace oxygen and cause rapid suffocation.
Hydrogen	Hydrogen may displace oxygen and cause rapid suffocation.
Nitrogen	Nitrogen may displace oxygen and cause rapid suffocation.
Methane	Methane may displace oxygen and cause rapid suffocation.
Carbon Dioxide	Carbon Dioxide may increase respiration and heart rate and may displace oxygen and cause rapid suffocation.
Water	Water in the form of steam can cause extensive burns and eye damage.

Safety - Learning from Experience

When creating the preliminary design, precautions were taken by looking at a paper that documented 50 years of history in the manufacturing of ammonia (56). By discovering what could go wrong and what has gone wrong in the past, accommodations were made to produce an inherently safer design. This is to reduce and possibly avoid hazards.

In item 48, an incident involving a tank of ammonia overflowing occurred. The root cause for this incident was the failure of high-level alarms and a shutdown system, and the action taken was to install reliable additional high-level alarms and trip systems. In the detailed design, when working with ammonia storage tanks, multiple high-level alarms and trip systems are to be set in place along with conforming to the requirements of 29CFR1910.111 put in place by OSHA (57).

In item 85, due to improper welding during construction there was an ammonia tank floor and foundation failure. In item 217, there were defects in the manufacturing causing weld zone cracks in the ammonia converter. To mitigate these risks, simplification was set in place by using modular manufacturing in the design instead of stick built. Using modular manufacturing, there is better control over the manufacturing process, which in turn, can lessen the risks and hazards.

Other Important Considerations

Nitrogen Production

As mentioned previously membrane technology was also considered to produce nitrogen. The membrane technology was sized using Equations 25 and 26, located in Appendix A. A perovskite membrane was selected to pursue. The incoming stream to the membrane would need to be compressed to 29 psia and heated to 932 F, for the perovskite membrane that was selected (58). The team hoped that the need for a smaller compressor may offset the more expensive membrane required. However, as shown in Table 29 the project is so sensitive to capital cost, the net present value was much lower using pressure swing adsorption technology.

Table 29: Comparison of Pressure Swing Adsorption to Pervoskite Membrane

	Pressure Swing Adsorption	Membrane
Total Capital Cost of Nitrogen Production Unit	\$2,149,000	\$19,482,700
Operating Cost/yr	\$356,300	\$33,871
NPV	\$15,000,000	\$7,000,000

Information on how all operating costs were calculated are available in the following section “Manufacturing/Utility Costs”, along with calculation information in Appendix B. The net present value calculations are further discussed in the “Economic Analyses” section. The cash flow table for membrane technology is in Appendix C. With this information of the greater economic burden associated with membrane technology the team moved forward with pressure swing adsorption.

Hydrogen Production Steam Methane Reforming versus Electrolysis

For hydrogen production, electrolysis was considered as a greener production pathway due to the possibility of zero greenhouse emissions from this process (59). Electrolysis does provide high purity hydrogen with only water needed, which is relatively safer compared to steam methane reforming (60). The electrolysis was sized by determining the molar flow of hydrogen needed from the Haber process simulation, thermodynamics was then utilized for solving for the electrical energy requirement and checked against literature values (61). The equations utilized for solving for both electrolysis capital cost and operating cost can be found in 27-29, located in Appendix A.

For determining the capital cost and type of electrolyzer the design team used data provided by Sayed M. Saba et al. (62). An alkal-system electrolyzer was determined best suitable for the specified needs of the amount of hydrogen produced. The costing was based on a kW input basis. Table 30, shown below, compares the capital and operating cost of the electrolysis unit to the selected steam methane reforming unit.

Table 30: Comparison of Steam Methane Reforming and Electrolysis

	Steam Methane Reforming	Electrolysis
Capital Investment in Hydrogen Production Unit	\$5,265,700	\$6,039,500
Operating Cost/yr	\$163,400	\$10,972,600
Raw Material Cost/yr	\$16,300	\$18,100

The price of operating cost outweighed the environmental and safety benefits of electrolysis. The team moved forward with steam methane reforming, as the project was economically feasible with the given operating and raw material cost. As mentioned before an in-depth explanation of how operating and raw material cost are calculated will be provided in the following “Manufacturing/Operating Cost” Section.

Hydrogen Production- Water gas shift Reactor – Packed Bed versus Membrane Reactor

As mentioned previously a membrane reactor was utilized for the water gas shift reaction taking place in R-202 instead of a packed bed reactor. This resulted in an increase in capital investment in R-202, but a decrease in capital investment in V-201 and V-202. Table 31 compares the total bare module capital investment in 2020 USD, when utilizing a packed bed reactor versus a membrane reactor. The table also displays a comparison of the reactor's capital investment, the fired heater's capital investment, and the pressure swing adsorption system (PSA)'s capital investment, utilizing both of the reactors.

Table 31: Comparison of Packed Bed Reactor to Membrane Reactor

	Packed Bed Reactor	Membrane Reactor
Total Bare Module Cost	\$25,800,000	\$13,000,000
Reactor Capital Investment	\$20,000	\$400,000
PSA Capital Investment	\$14,000,000	\$1,800,000
Heater Capital Investment	\$2,900,000	\$1,700,000
Operating and Raw Material Cost of SMR	\$1,500,000	\$750,000

Through utilizing a membrane reactor, the conversion rate was higher which in turn lowered the amount of material that needed to be removed by the pressure swing adsorption system, V-201 and V-202. This decreased the cost of the pressure swing adsorption system from approximately \$14 million dollars to \$2 million dollars. This increase in conversion resulted in a decrease in methane, carbon monoxide, carbon dioxide, and water, which decreased the amount of material recycled back. This decreased the flow rate of the material being heated by H-201, the fired heater, which in turn decreased the size of the fired heater.

The other equipment pieces involved in the steam methane reforming, had minute changes in capital investment that are within the uncertainty of costing. That is why the only capital investment displayed is the pieces of equipment with substantial changes from the utilization of a different reactor. To display the overall impact on the project the total bare module cost has been displayed, which is the sum of the capital investment of each piece equipment.

Hydrogen Production – Optimization

The team noted the expensive capital cost associated with hydrogen production. To combat this, the team hoped to optimize the reactors. The team began by optimizing the reformer reactor, R-201. The team simulated reactor pressures of 435 psia, 508 psia, and 580 psia in Aspen HYSYS utilizing the reaction data found in (13). It should be noted that for 435 psia only

one compressor was needed to achieve these pressures; however, for both the 508 psia and 580 psia an additional compressor was utilized. This resulted in a sharp increase in the cost of operation of R-201 at pressures 508 psia and 580 psia. The team found the pressure of 435 psia to be the best option to move forward with, as the capital investment was the lowest.

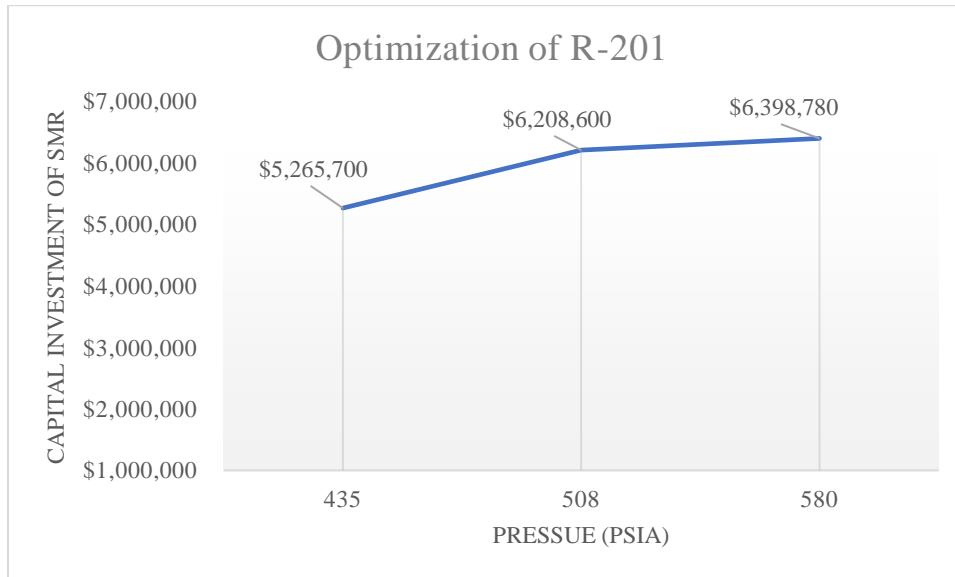


Figure 6: Capital investment of the steam methane reforming at various pressures

For the water gas shift reaction taking place in R-202, the kinetic data utilized was available at pressures from 145 psia to 290 psia (15). The team sought to determine if a lower reaction pressure would in turn lower the capital investment associated with hydrogen production. The team simulated the process with a reaction pressure at 290 psia, 218 psia, and 145 psia. Figure 7 displays the impact of different pressures on the steam methane reforming capital investment. The decrease in pressure of steam methane reforming not only increases the capital investment of steam methane reforming but also C-301 located in the ammonia production unit of the plant, as the incoming stream from the hydrogen unit will need to be compressed further. For the purpose of this analysis only the capital investment of Steam Methane Reforming has been included.

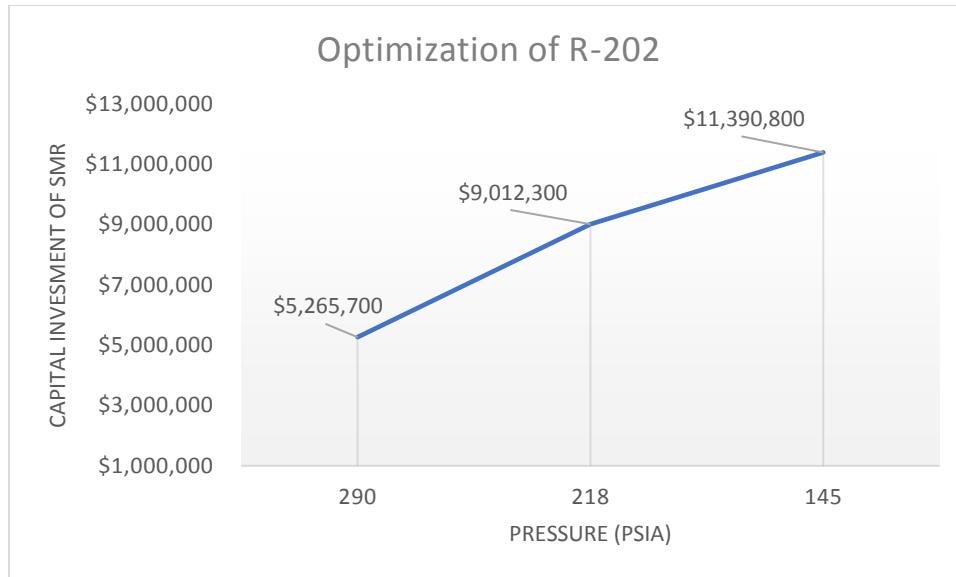


Figure 7: Capital Investment of Steam Methane Reforming at various pressures.

The lower pressure did lower the capital investment in R-202, but it increased the capital investment in the other associated equipment enough to offset this reduction in price. The increase in other equipment at a lower pressure was a result of the pressure swing adsorption system being most efficient at higher pressures (21). By lowering the pressure of the stream exiting R-202, V-201 and V-202 increased in size and price. The lower reaction pressure also yielded a lower conversion rate, which increased other equipment such as the fired heater, H-201 and the recycle compressor, C-201. The fired heater's cost and size increased due to the need to heat a larger stream entering R-201, as more material was being recycled back. The compressor also increased in size due to the larger recycle stream.

Ammonia Production – Modular versus Stick Built

Modular manufacturing of the ammonia reactor served to both lower the capital investment and create a more inherently safe design. The cost of modular manufacturing decreases for each additional unit produced. The cost of each additional module was calculated using equations 30 and 31 in Appendix A, and Table 32 displays the capital cost associated with modular manufacturing versus a stick-built reactor.

Table 32: Comparison of Stick-Built to Modular Manufactured

Equipment	Stick-Built	Modular
R-301	\$ 545,400	\$ 141,400
R-302	-	\$ 113,100
R-303	-	\$ 99,200
R-304	-	\$ 90,500
R-305	-	\$ 84,200
Total	\$ 545,400	\$ 528,400

Parallel operation was selected for these reactors. This allows the reactors to, at a lower production rate, continue producing ammonia if one reactor is out for maintenance. The unit scale selected to design the modular manufactured reactors is 10 metric tons per day each, as this is the maximum size that can be transported. Only the reactors were modular manufactured for the sake of simplicity within the plant, through reducing the connections and equipment required the process is inherently simpler.

Manufacturing/Operating Costs (exclusive of Capital Requirements)

Revenue

To determine the sales price, the team looked to online resources to find common sale prices of anhydrous ammonia fertilizer within the corn belt. The team found prices ranging from \$595 to \$622 per ton in 2019 dollars (63,64). With the expectation that the project would be most sensitive to revenue, the more conservative value of \$595 obtained from (63) was used for the economic analysis.

It was assumed that the 50 metric tons per day scale is right sized for continuous, year-round operation and seasonal variation in fertilizer demand, and will be leveled out through sales to other facilities that convert ammonia to other forms. The revenue was multiplied by a service factor of 0.98. This service factor accounts for down time in the plant associated with maintenance and other factors.

As mentioned previously this sales price is given in 2019 USD, so an escalation rate of 2% was used. This 2% escalation rate was selected, based on typical industry best practices, to try and create the most accurate economic analyses (65). The results of this escalation are displayed in Table 33. The washout assumption was applied meaning the profit margin between operating cost and revenue was assumed to remain constant during the project life, so the revenue was escalated to the year of 2020. This is the year that operating costs were found at.

The first year of production 2024, is only a half year of production. The revenue in this year has been modified accordingly.

Table 33: Revenue Escalation

Year	Sales Price \$/2000 lbs. (65)
2019	\$ 595.00
2020	\$ 606.90

Cost of Labor

Utilizing Equation 32 in Appendix A, the number of operators for the process was determined. Excluding pumps and vessels, the number of pieces of equipment along with a P value with an assumption of zero were used to find the number of operators. There are 8 pieces of equipment from the Haber-Bosch process, 7 from the SMR, and 7 from the PSA for a total of 22 pieces of equipment. To run the plant, it was determined that 15 operators needed to be hired. The annual salary of an operator was found from data provided from the Bureau of Labor Statistics for a chemical plant operator in Minnesota (66). In Table 34, the estimated annual labor cost for the 15 operators is shown.

Table 34: Annual Labor Costs

Factor	Overall
P	0
N _{ol}	3.37
N _{np}	22
Operators Needed	15
Average Salary	\$51,340
Labor Costs/year	\$770,100

Utilities

To produce the desired quantity of ammonia, electricity and cooling water were utilized in the process with electricity being the more expensive of the two. A cost of \$0.10 per kW-hr was used for electricity and a cost of \$2.46 per 1000 gallons was used for the cooling water (67-68). Electricity cost was calculated using the power from compressors and an air cooler from the PSA, SMR, and the Haber-Bosch process. Using Equation 33 which involves the specific heat of cooling water, the change in temperature, and the cooling water duty, the mass flow rate was calculated. Specific heat of water is known to be 1 BTU/lbm-°F and the change in temperature was found to be 30°F. Once the group found the mass flow rate, the yearly cost of cooling water

was calculated. In Tables 35 and 36, the cost breakdown and total annual cost is shown for electricity and cooling water, respectively.

Table 35: Cost for Electricity

Process	Equipment	\$ per kWh	kW	Btu/hr	\$ per year
PSA	C-101	\$0.10	134	456203	\$121,455
PSA	C-102	\$0.10	92	314941	\$83,846
PSA	C-103	\$0.10	92	314599	\$83,756
SMR	C-102	\$0.10	158	539460	\$143,620
Haber	C-105	\$0.10	198	675604	\$179,866
Haber	C-106	\$0.10	428	1460738	\$388,891
Haber	C-107	\$0.10	799	2725619	\$725,640
Haber	E-303	\$0.10	292	997369	\$265,529
				Total	\$1,992,602

Table 36: Cost for Cooling Water

Process	Equipment	\$ per 1000 gal	lb/hr	\$ per year
PSA	E-101	\$2.46	9994.6	\$25,846
PSA	E-102	\$2.46	10,019	\$25,908
PSA	E-103	\$2.46	6,015	\$15,554
SMR	E-202	\$2.46	8,886	\$22,979
SMR	Cooling Jacket	\$2.46	223,874	\$578,928
Haber	Reactor	\$2.46	127,932	\$330,826
				Total
				\$ 1,000,040

Raw Materials

The raw materials that were accounted for were liquid methane and water. Using the cost of \$3.96 per 1000 feet cubed and \$2.46 per 1000 gallons and flow rates, the cost of raw materials was found (68-69). In Table 37, the annual raw material cost is shown.

Table 37: Raw Material Cost

Material	\$	Flow Rate	\$ per year
Water	\$2.46	2918	\$16,591
Methane	\$3.96	1,181	\$40,968
			Total
			\$57,560

Operating costs calculated consist of labor costs, utilities, and raw materials, the most expensive being utilities and the least expensive being raw materials. It is important to note, operating costs are cut in half in the year 2024 due to production not beginning until the middle of year 2024. Starting in 2025, the remainder of the project timeline is assumed to be at full operation. In Table 38, the total annual operating cost is shown.

Table 38: Total Annual Operating Cost

Source	Cost
Labor	\$770,100
Utilities	\$3,026,589
Raw Materials	\$57,560
Total	\$3,854,249

Economic Analysis

Cash Flow Table

To determine the profit obtained from the process, a cash flow table was constructed, shown below in Table 39. For this analysis, a tax rate of 25% and Minimum Acceptable Rate of Return of 8% were assumed. The analysis is for a 20-year useful plant life, with depreciation being accounted for with Modified Accelerated Cost Recovery System (MACRS). It has also been assumed that construction will last three years beginning in mid-2021, and production beginning in mid-2024. A 5-year depreciation system was utilized due to this plant's role in chemical production (70). This depreciation rate was obtained from Stermole et al. (71).

Table 39: Cash Flow Table

End of Year	2020	21	22	23	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043
Production, tons					8943	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885
Sales Price, \$/tons					607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607
Sales Revenue					5427203	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407
+Salvage																								
-Royalties																								
Net Revenue					5427203	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407
-Raw Material Costs					28204	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409
-Operating Costs					1843744	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487
Waste Removal					424382	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764
-Depreciation					4357550	6972081	4183248	2509949	2509949	1254975														
- Amortization																								
- Depletion																								
- Loss Forward						1226677	1937011																	
- Writeoff																								
Taxable Income					(1226677)	(1937011)	141487	3751798	3751798	5006772	6261747	6261747	6261747	6261747	6261747	6261747	6261747	6261747	6261747	6261747	6261747	6261747	6261747	
-Tax @ 25%							35372	937949	937949	1251693	1565437	1565437	1565437	1565437	1565437	1565437	1565437	1565437	1565437	1565437	1565437	1565437	1565437	
Net Income					(1226677)	(1937011)	106115	2813848	2813848	3755079	4696310	4696310	4696310	4696310	4696310	4696310	4696310	4696310	4696310	4696310	4696310	4696310	4696310	
+Depreciation					4357550	6972081	4183248	2509949	2509949	1254975	0	0	0	0	0	0	0	0	0	0	0	0	0	
+ Depletion																								
+ Loss Forward						1226677	1937011																	
+ Writeoff																								2178775
working capital					(2178775)																			
- Fixed Capital					(21787752)																			
Cash Flow	(23966527)	0	0	0	3130873	6261747	6226375	5323797	5323797	5010054	4696310	4696310	4696310	4696310	4696310	4696310	4696310	4696310	4696310	4696310	4696310	4696310	4696310	4696310
Discount Factor (P/Fi*,n)	1.0	0.9	0.9	0.8	0.7	0.7	0.6	0.6	0.5	0.5	0.5	0.4	0.4	0.4	0.3	0.3	0.3	0.3	0.3	0.2	0.2	0.2	0.2	0.2
Discounted Cash Flow	(23966527)	0	0	0	2301285	4261639	3923672	3106385	2876282	2506274	2175300	2014167	1864969	1726823	1598911	1480473	1370808	1269267	1175247	1088192	1007585	932949	863842	1170932
NPV @ i* =	14748474																							
DCFROR =	0																							
B/C =	2																							
GROR =	12																							
PVR	1																							
Discounted Payback Period (yrs)	8																							
Break even feed price	\$460																							

Working capital is typically estimated by taking 5-30% of the total fixed capital cost for chemical plants (72). For the purposes of this analysis, it was estimated to be 10% of the fixed capital cost due to the single final product. The net present value (NPV) was calculated from summing the discounted cash flow obtained from the cash flow table. The net present value considers the fixed capital cost, operating cost, revenue and depreciation for the project over the project life. The NPV for this project was found to be \$15,000,000.

To ensure that the upstream production of nitrogen and hydrogen are more economically attractive than purchasing these two reactants, two additional net present values were calculated. These cash flow tables are in Appendix C. The capital cost, operating cost, and raw material costs were adjusted to consider production versus buying the reactants. The price of hydrogen and nitrogen were found from literature to be \$3.53/kg and \$1.52/kg in 2019\$, respectively (73,74). Through purchasing nitrogen and hydrogen, the project also incurs delivery fees, fuel surcharges, and environmental fees, that total over \$500 per month (74). The escalation rate of 2% was used to produce what these values would be in the future corresponding years. In Table 40, these NPV values are displayed for comparison. The economic analysis displays that for the given minimum rate of return, project lifespan, and rate of production it is more economically attractive to produce nitrogen and hydrogen onsite instead of buying either reactant.

Table 40: NPV Values

	H2 bought & N2 produce	H2 produce & N2 bought	H2 & N2 produce
NPV	-\$36,000,000	\$13,000,000	\$15,000,000

The Discounted Cash Flow Rate of Return (DCFROR) was also calculated. For the project to be economically attractive the DCFROR needs to be greater than the Minimum Acceptable Rate of Return of 8%. The DCFROR was calculated to be 13%. The discounted payback period was found to be 8.3 years. The team also found the breakeven product price to be \$460. At this sales price the net present value of the project becomes zero.

Sensitivity Analyses

A sensitivity analysis was performed to determine how sensitive the economic attractiveness is to the capital cost, operating cost, revenues, and raw material costs. These variables were selected due to the uncertainty associated with each variable. The revenue and raw material prices may fluctuate with market prices. The capital cost is a function of the CEPCI, and there is resultant uncertainty due to this.

The impact of these variables on the NPV and DCFROR were analyzed, by varying the parameters by 10%, 20% and 30%. This analysis was performed through holding constant all

other variables, but the variable being analyzed. The outcome of variation of 10%, 20%, and 30% is shown in Tables 41-44.

Table 41: Impact of Variation of Capital Cost on Economic Attractiveness of Project

Capital Cost					
Capital Cost	Variance (%)	NPV	Change in NPV	DCFROR	Change DCFROR
\$15,251,426	-30	\$20,815,778	\$6,067,304	17%	32%
\$17,430,202	-20	\$18,807,047	-\$4,058,572	15%	20%
\$19,608,977	-10	\$16,798,316	-\$2,049,841	14%	9%
\$21,787,752	0	\$14,748,474	\$0	13%	0%
\$23,801,870	10	\$12,780,853	-\$1,967,621	12%	-8%
\$25,965,677	20	\$10,656,036	-\$4,092,439	11%	-15%
\$28,129,483	30	\$9,319,881	-\$5,428,593	10%	-20%

Table 42: Impact of Variation of Raw Material Cost on Economic Attractiveness of Project

Raw Material					
Raw Material Cost	Variance (%)	NPV	Change in NPV	DCFROR (%)	Change DCFROR
\$39,486.30	-30	\$14,883,84 1	\$135,366	13%	0%
\$45,127.20	-20	\$14,852,42 2	\$103,948	13%	0%
\$50,768.10	-10	\$14,821,00 3	\$72,529	13%	0%
\$56,409.00	0	\$14,748,47 4	\$0	13%	0%
\$62,049.90	10	\$14,758,16 6	\$9,691	13%	0%
\$67,690.80	20	\$14,685,34 7	-\$63,128	13%	0%
\$73,331.70	30	\$14,653,78 3	-\$94,691	13%	0%

Table 43: Impact of Variation of Operating Cost on Economic Attractiveness of Project

Operating Cost					
Operating Cost	Variance (%)	NPV	Change in NPV	DCFROR (%)	Change DCFROR
2185050	-30	\$20,951,193	\$6,202,719	15%	14%
2497200	-20	\$18,897,324	\$4,148,849	14%	10%
2809350	-10	\$16,843,454	\$2,094,980	13%	0%
3121500	0	\$14,748,474	\$0	13%	0%
3433650	10	\$12,735,715	-\$2,012,760	12%	-5%
3745800	20	\$10,681,845	-\$4,066,629	11%	-10%
4057950	30	\$8,627,976	-\$6,120,499	11%	-16%

Table 44: Impact of Variation of Revenue on Economic Attractiveness of Project

Revenue					
Revenue	Variance (%)	NPV	Change in NPV	DCFROR	Change DCFROR
\$7,598,085	-30	-\$3,347,592	-\$18,096,067	6%	-55%
\$8,683,526	-20	\$2,698,133	-\$12,050,341	9%	-33%
\$9,768,966	-10	\$8,743,859	-\$6,004,616	11%	-15%
\$10,854,407	0	\$14,748,474	\$0	13%	0%
\$11,939,848	10	\$20,835,310	\$6,086,836	15%	14%
\$13,025,288	20	\$22,519,761	\$7,771,286	16%	26%
\$14,110,729	30	\$32,926,761	\$18,178,287	18%	38%

The sensitivity analysis, shown in Figure 8 below, displays that at the worst-case scenario variation of 30% for raw materials, operating cost and capital cost analyzed, the project is still economically attractive. The analysis showed that the attractiveness of the project is most sensitive to a variation in revenue, as shown below in Figure 8. It should be noted as mentioned before the lower sales price value in the range found was used for the economic analysis, with the hopes to provide a more conservative economic analysis. The project is secondly most sensitive to capital cost. This risk should be mitigated through the precautions taken throughout the design to provide the most conservative estimate on capital cost. From the tornado chart displays that variations in raw material cost have minute effects on the net present value of the project.

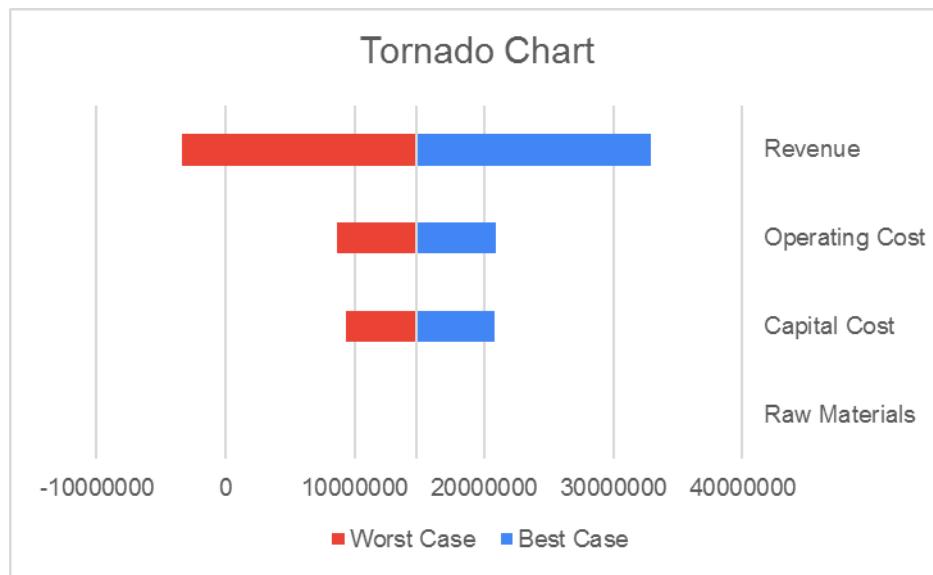


Figure 8: 30% Variation Sensitivity Analysis

Conclusions and Recommendations

The design process carried out indicates that an anhydrous ammonia plant with onsite production of hydrogen and nitrogen is not only technically feasible, but also economically attractive. The plant's specifications of 50 metric tons per day, with a 99.5% mass purity were met, along with environmental and safety requirements. The plant is economically attractive due to its net present value of \$15,000,000 which is larger than \$0, and a rate of return of 13% which is larger than the 8% minimum rate of return.

As shown in the sensitivity analysis, the project is most sensitive to revenue. It is worth stating again that the lowest selling price of anhydrous ammonia per ton that was obtained was utilized for this economic analysis. Though at a -30% variation the project does become unattractive, the team still suggests moving forward with the project. This is due to the initial sales price used for all calculations of \$606.90, being at the lower end of sales price range found. The risks that have been considered are not of great concern at this time, so it is recommended to move forward with the project.

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Appendices

Appendix A

Reactor Equations

$$\frac{W}{F} = \frac{\text{Catalyst Weight (g)}}{\text{Reactor Flow } (\frac{\text{mol}}{\text{s}})} \quad (1)$$

$$\rho_{cat} \left(\frac{\text{kg}}{\text{m}^3} \right) = \frac{\text{Catalyst Mass (kg)}}{\text{Catalyst Volume (m}^3\text{)}} \quad (2)$$

$$SA_{\text{Membrane}}(\text{m}^2) = 2\pi R_{\text{Reactor}}(m)L_{\text{Reactor}}(m) \quad (3)$$

Pressure Swing Adsorption Equations

$$\dot{m}_{in} = \frac{\dot{m}_{out}}{PR_A * x_A} \quad (4)$$

\dot{m}_{in} = molar flow rate of into pressure swing adsorption system

PR_A = product recovery

x_A = mole fraction of product A present in \dot{m}_{in}

\dot{m}_{out} = desired molar flow rate of product out of pressure swing adsorption system

$$V_{ads} = \frac{x_B \cdot \dot{m}_{in} \cdot R \cdot T_{in} \cdot D}{\varepsilon_p \cdot P \cdot \varepsilon_b} \quad (5)$$

V_{ads} = volume of adsorbent needed

x_B = mole fraction of material adsorbed

\dot{m}_{in} = molar flow rate of into pressure swing adsorption system

R = gas constant $0.082060 \frac{\text{L-atm}}{\text{K-mol}}$

T_{in} = Temperature of \dot{m}_{in} (K)

P = Pressure of \dot{m}_{in} (atm)

$$D = \frac{\text{time total}}{\text{bed}} (s)$$

ε_p = particle voidage

ε_b = bed voidage

Flash Drum Equations

$$F_{lv} = \frac{w_l}{w_v} \sqrt{\frac{\rho_v}{\rho_l}} \quad (6)$$

$$K_{drum} = \exp (A + Bln(F_{lv}) + Cln(F_{lv})^2 + Dln(F_{lv})^3 + Eln(F_{lv})^4) \quad (7)$$

$$A = -1.877478097$$

$$B = -0.8145804597$$

$$C = -0.1870744085$$

$$D = -0.0145228667$$

$$E = -0.0010148518$$

$$U_{Perm} = K_{Drum} \sqrt{\frac{\rho_l - \rho_v}{\rho_v}} \quad (8)$$

$$A_c = \frac{V \cdot MW_v}{3600 \cdot U_{Perm} \cdot \rho_v} \quad (9)$$

$$D = \sqrt{\frac{4A_c}{\pi}} \quad (10)$$

Compressor Equations

$$GHP(kW) = \frac{GHP(\frac{kJ}{hr})}{3600} \quad (11)$$

$$BHP = GHP + GHP^{0.4} \quad (12)$$

$$\dot{W}_{Driver}(kW) = \frac{BHP}{\eta_{Driver}} \quad (13)$$

Heat Exchanger Equations

$$U_o = \frac{1}{\frac{d_o}{h_i d_i} + R_{fi} \frac{d_o}{d_i} + \frac{d_o \ln(\frac{d_o}{d_i})}{2k_w} + R_{fo} + \frac{1}{h_o}} \quad (14)$$

U_o = Overall Heat Transfer Coefficient (BTU/h·ft²·°F)

d_o = outer diameter (ft)

d_i = inner diameter (ft)

R_{fi} = inner Fouling Resistance (h·ft²·°F/BTU)

R_{fo} = Fouling Resistance (h·ft²·°F/BTU)

K_w = Conductive Heat Transfer Coefficient (BTU/h·ft·°F)

h = Convective Heat Transfer Coefficient (BTU/h·ft²·°F)

$$LMTD = LMTD_{countercurrent} = \frac{(T_{h,i} - T_{c,o}) - (T_{h,o} - T_{c,i})}{\ln(\frac{T_{h,i} - T_{c,o}}{T_{h,o} - T_{c,i}})} \quad (15)$$

$T_{h,i}$ = Hot in stream Temperature (°F)

$T_{h,o}$ = Hot out stream Temperature ($^{\circ}\text{F}$)

$T_{c,i}$ = Cold in stream Temperature ($^{\circ}\text{F}$)

$T_{c,o}$ = Cold out stream Temperature ($^{\circ}\text{F}$)

$$A = \frac{Q}{U * LMTD} \quad (16)$$

A= Transfer Area

Q = Total Heat Transfer (Btu/hr)

U_o = Overall Heat Transfer Coefficient (BTU/h·ft²· $^{\circ}\text{F}$)

Fans Equations

$$A_{Face} = \dot{m}_{air} \rho_{air} V_{Face} \quad (17)$$

Storage Tank Equations

$$D = \sqrt[3]{\frac{4*V}{3*\pi}} \quad (18)$$

Capital Cost Equations (25)

$$\log_{10} C_p^0 = K_1 + K_2 \log_{10} A + K_3 [\log_{10} A]^2 \quad (19)$$

C_p^0 = Base Purchase Cost 2001 US\$

K = Table A.1 Coefficients (25)

A = Sizing Unit

$$\log_{10} F_p = C_1 + C_2 \log_{10} P + C_3 (\log_{10} P)^2 \quad (20)$$

F_p = Pressure Factor

C = Table A.2 Coefficients (25)

P = Pressure (Barg)

$$C_{BM} = C_p^0 [B_1 + B_2 F_p F_M] \quad (21)$$

C_{BM} = Bare Module Cost US 2001\$

C_p^0 = Base Purchase Cost (\$)

F_m = Material of Construction Factor (25)

F_p = Pressure Factor

B = Table A.4 Constants (25)

$$C_{bm}(2020) = CEPCI(2019\$)(C_{bm2001\$})(\text{escalation factor}) \quad (22)$$

CEPCI 2019\$ obtained from (75)

Escalation factor 1.02 obtained from (65)

Fixed Capital Investment Summary (25)

$$C_{TM} = 1.18 \sum_{i=1}^n C_{Bm,i} \quad (23)$$

C_{TM} = Total Module Cost in 2020 US\$

$$C_{GR} = C_{TM} + 0.50 \sum_{i=1}^n C_{BM,i} \quad (24)$$

C_{GR} = Grassroots Costs in 2020 US\$

Membrane Equations

$$\text{Surface Area} = \frac{\text{Transfer Rate}}{\frac{P_{O_2}}{ST} * (\Delta P)} \quad (25)$$

Transfer Rate = $O\%$ * V

$O\%$ = volumetric percent of Oxygen in Air

V = volumetric flow rate of Air ($\frac{\text{cm}^3}{\text{hr}}$)

P_{O_2} = permeability of O_2 through membrane ($\frac{\text{cm}^3 \text{cm}}{\text{cm}^2 * \text{sec} * \text{cm Hg}}$)

ST = Separation Thickness (cm)

$$\Delta P = P_s - P_t \text{ (cm Hg)} \quad (26)$$

P_t = Partial pressure of Oxygen on Tube Side (cm Hg)

P_s = Partial Pressure of Oxygen on Shell Side (cm Hg)

Electrolysis Equations

$$\text{Energy Required (kW)} = \frac{m_{H_2O} \Delta G}{3600} \quad (27)$$

m_{H_2O} = molar flow rate of water in mole/hour

ΔG = change in Gibbs Free energy (76)

$$\text{Capital Investment \$} = \text{Energy Requirement} * \$500 \text{ obtained from (62)} \quad (28)$$

$$\text{Electrolysis Operating Cost \$} = \text{\$price of electricity} * \text{energy requirement} \quad (29)$$

Modular Manufacturing Equation

$$k_n = k_1 n^{\log_2 p} \quad (30)$$

k_n = the cost of the nth unit

k_1 = the cost of the first of a kind unit

$p = 0.8$

$$K(N) = \sum_1^N k_n \quad (31)$$

$K(N)$ = total cost of a modular unit

Operating cost

$$N_{OL} = (6.29 + 31.7P^2 + 0.23N_{NP})^{0.5} \quad (32)$$

$$Q = \dot{m} * C_{PCW} * \Delta T_{CW} \quad (33)$$

Appendix B

Below is the calculations performed to determine the size and cost of the reformer for steam methane reforming R-201 on the left and costing and sizing of the water gas shift reactor for R-202 on the right.

reformer		Water gas shift with membrane reactor		total flow rate out of R-202	476	
Hydrogen Reactor Costing		For 93% conversion, W/F = 500 gmcat/hr/molCO				
Flow of Methane =	441396.7 mol/h	W/F =	500 gm cat hr/mol CO			
Total Flow =		mol CO/hr	18.44082538 kmol/hr			
Wcat = 1.5F			18440.82538 mol/hr			
Cat =	662095.05 g	W =	9220412.691 gm cat			
	662.09505 kg		9220.412691 kg cat			
	0.66209505 metric tons of catalyst	Catalyst density :	0.9 g/cm3			
Bulk Density =	0.9 kg/L	Density =	0.9 kg/L			
Reactor Volume =	735.6611667	Density =	900 kg/m3			
	0.7356611667 m3	Reactor Volume :	10.24490299 m3			
L/D Ratio	3	L/D Ratio	3			
Reactor Diameter	0.6784047788 m	Reactor Diamete	1.632170678			
Reactor Height	2.035214336 m	Reactor Height	4.896512033			
A =	0.7356611667	A =	10.24490299			
K1 =	3.5565	K1 =	3.5565			
K2 =	0.3776	K2 =	0.3776			
K3 =	0.0905	K3 =	0.0905			
log10Cp =	3.507766169	log10Cp =	4.030479678			
Cpo =	3219.334981	Cpo =	\$10,727.03			
P =	33.45 bar	P =	23.45			
Fp =	2.670066346	Fp =	4.133858079			
B1 =	1.49	B1 =	1.49			
B2 =	1.52	B2 =	1.52			
Fm =	3.5	Fm =	3.5			
Cbm =	50526.66723	Cbm =	\$251,893.56	Reactor Radius:	0.8160853389 m	
Catalyst Cost =	66209.505			Reactor Circumference:	5.127615411 m	
Total Cost (Vessel+Catalyst)=	\$ 116,736.17	Membrane Cost	21620.30975	Reactor Outer SA:	25.10743056 m2	
2020	143515.3059	Total Cost (Vesse	\$ 273,513.87			
Conditions:						
T =	640 °C					
P =	1 atm					
X =	0.8					
		2019	\$407,017.46	Membrane cost:	21620.30975	

Below is the Calculations to size and cost the packed bed reactor, R-301, for ammonia production.

	10 bar ruthenium	425 C		10 \$/kg
Space Time (Mass Activ)	0.379	kgNH3/hkgcat	$\log_{10}C_p = K_1 + K_2 \log_{10}(A) + K_3 (\log_{10}(A))^2$	
Molec Weight NH3	17.03	kg/kmol	A =	20.6595215
Flow NH3	122.3	kmolNH3/hr	K1 =	3.5565
Mass Flow NH3	2082.769	kg/hr	K2 =	0.3776
Mass Catalyst:	5495.432718	kg	K3 =	0.0905
Density Catalyst:	0.7	g/cm3	$\log_{10}C_p =$	4.209612897
	700	kg/m3	Cpo =	16203.6516
Catalyst Volume	7.850618168	m3	P =	13.45
Void Fraction:	0.38		Fp =	3.114440697
Reactor Volume:	20.6595215	m3	B1 =	1.49
Reactor Volume =	20.6595215	m^3	B2 =	1.52
L/D Ratio	3		Fm =	3.1
Reactor Diameter	2.062068276	m	Cbm =	\$ 261,935.99
Reactor Height	6.186204827	m	Catalyst Cost =	\$ 144,616.65
Catalyst Density =	0.7	g/cm3	Total Cost (Vessel+Cata)	\$ 545,378.72
	700	kg/m3		
Catalyst Mass =	14461.66505	kg		

Costing and Sizing for the Pressure swing adsorption tower within nitrogen production, V-101 and V-102.

Temp (K)	363	Type	10 bar
Voidage	0.33	Total cost in 2020	217841.357
R (L *atm/(K-mol))	0.08206	for two bed	
O2 mole fraction	0.21	Cost in 2019 dollar of one bed	145862.357
molar flow rate in (kmole/day)	2725	Cbm	95334.87387
D = time total/bed (s/bed)	64.7	d (m) need to find rounding increments	3.75
adsorbent used	0.71	I (m)	18.75
density (lb/ft)	47.4	P barg	13.44738
h2O mole fraction	0.005	CMS Price	70039.2
L/D	5	Ib	9240
V=pi(D^2/4)I		CMS price for water removal	1939.8
D=		Ib	323.3
density of zeolite (kg/m^3)	1126	$C_p = 10^{(K_1 + K_2 \log(A) + K_3 (\log(A))^2)}$	8071.33893
amount of nitrogen removed	0.3	K1 pg 1251	3.4974
		K2	0.4485
		K3	0.1074
		V (m^3)	5.9
		Fp, vessel	5.253588726
		B1	2.25
		B2	1.82

Pressure (Bar)	Pressure (atm)	V bed (m^3/bed)	V ads (L/bed)	Adsorbent (lb/bed)	D (m)	L (m)
10	9.86923	5.65	131.4	326.3	1.12903	5.64516

Costing and Sizing for the Pressure swing adsorption tower within hydrogen production, V-201 and V-202.

Temp (K)	556	Type	zeolite
Voidage	0.503	Total cost in 2020	916199.4621
R (L *atm/(K-mol))	0.08206	for one bed	738365.7321
removal amount	0.489	Cost in 2020 dollar of one bed	738365.7321
molar flow rate in (kmole/day)	8688	Cbm	482591.9818
D = time total/bed (s/bed)	64.7	d (m)	1.83
adsorbent used	0.609	I (m)	
denisty (kg/m^3)	1126	P barg	23.45
hydrogen removed	0.2	CMS Price	- 177833.73
		Ib	58691
		Cp0	20942.08528
		K1	3.4974
		K2	0.4485
		K3	0.1074
		V (m^3)	24
		Fp_vessel	4.574304467
		B1	1.49
		B2	1.52
		Fm (SS)	3.1

Pressure (atm)	V bed (m^3/bed)	V ads (L/bed)	dsorbent (kg/bed)	D (m)	L (m)
20.00000	23.69246	23692.46460	26677.71514	1.82047	9.10235

Below are the calculations for costing and sizing the flash drum V-301.

Separator Costing	
Formulas and Heuristics taken from "Separation Process Engineering" by Wankat	
Uperm = Kdrum*SQRT((pl - pv)/pv)	
Kdrum = exp(A + B(LN(FLV)) + C(LN(FLV))^2 + D(LN(FLV))^3 + E(LN(FLV))^4)	
FLV = (WL/WV)*SQRT(pv/pl)	
Ac = (V*MWv)/(Uperm*3600*pv)	
D = SQRT((4*Ac)/PI())	
A =	-1.877478097
B =	-0.8145804597
C =	-0.1870744085
D =	-0.0145228667
E =	-0.0010148518
pv =	0.52172618 lb/ft ³
pl =	42.51488771 lb/ft ³
WL =	4594.683169 lb/hr
WV =	10570.90753 lb/hr
V =	695.9265985 lbmol/hr
MWv =	15.18968746 lb/lbmol
V =	0.1794188297 m ³
A =	0.1794188297
K1 =	3.4974
K2 =	0.4485
K3 =	0.1074
log10Cp =	3.222550776
Cpo =	1669.36297
P =	23 barg
Fp =	1.498052414
B1 =	1.49
B2 =	1.52
Fm =	3.5 Stainless
Cbm =	\$ 15,791.57
	2020 24161.10331
D Rounded=	1.5 ft
H/D =	3 ft/ft
H =	4.5 ft
V =	6.336116175 ft ³

Costing and sizing calculations for C-101, C-102, and C-103.

P = 10 bar	K-101			K-103		
Stage 1 Compressor Energy =	481365.5973	kJ/h		Stage 3 Compressor Energy =	332092.8645	kJ/h
	133.7126659	kW			92.24801791	kW
GHP =	133.7126659		Stage 2 Compressor Energy =	332413.3279	kJ/h	
BHP =	140.7997734			92.33703552	kW	
Driver Efficiency =	0.3		GHP =	92.33703552		
Driver Power =	469.332578	kW	BHP =	98.44857147		
Ce = a + b*(S^n)			Driver Efficiency =	0.3		
S =	469.332578	kW	Driver Power =	328.1619049	kW	
a =	260000		Ce = a + b*(S^n)			
b =	2700		S =	328.1619049	kW	
n =	0.75		a =	260000		
Ce =	\$ 532,254.01		b =	2700		
Purchased Horsepower	629.3843737	hp	n =	0.75		
			Ce =	\$ 468,175.63		
					\$ 468,030.70	
					439.6632253	hp

Compressor C-201 and C-301 calculations

Stage 1 Compressor Energy =	569274.7327	kJ/h	Stage 1 Compressor Energy =	711870.2799	kJ/h
	158.1318702	kW		197.7417444	kW
GHP =	158.1318702		GHP =	197.7417444	
BHP =	165.7107979		BHP =	206.029546	
Driver Efficiency =	0.3		Driver Efficiency =	0.3	
Driver Power =	552.3693263	kW	Driver Power =	686.7651533	kW
Ce = a + b*(S^n)			Ce = a + b*(S^n)		
S =	552.3693263	kW	S =	686.7651533	kW
a =	260000		a =	260000	
b =	2700		b =	2700	
n =	0.75		n =	0.75	
Ce =	\$ 567,635.13		Ce =	\$ 622,217.94	
Purchased Horsepower:	740.7383139	hp	Purchased Horsepower:	920.9658059	hp

Calculations for K-302 and K-303.

Stage 1 Compressor Energy =	1541221.851	kJ/h	Stage 2 Compressor Energy =	2875831.777	kJ/h
	428.1171807	kW		798.8421603	kW
GHP =	428.1171807		GHP =	798.8421603	
BHP =	439.4053903		BHP =	813.3293581	
Driver Efficiency =	0.3		Driver Efficiency =	0.3	
Driver Power =	1464.684634	kW	Driver Power =	2711.09786	kW
Ce = a + b*(S^n)			Ce = a + b*(S^n)		
S =	1464.684634	kW	S =	2711.09786	kW
a =	260000		a =	260000	
b =	2700		b =	2700	
n =	0.75		n =	0.75	
Ce =	\$ 899,251.65		Ce =	\$ 1,274,431.34	
Purchased Horsepower:	1964.171388	hp	Purchased Horsepower:	3635.636453	hp

Heat exchanger costing and sizing for E-101, E-102 and E-103, involved in nitrogen production.

	E-103	E-101	E-102		interstage	interstage	pre psa
Q kj/hr	200600	333300	334100	Heat Exchanger	E-101	E-102	E-103
A m^2	2.775168797	3.961833561	7.385473764	Type	double pipe	double pipe	double pipe
Rfi m^2 k/w	0.0001	0.0001	0.0001	2020	21497.86124	24435.32355	19850.58145
Rfo m^2k/w	0.0001	0.0001	0.0001	Cbm	14050.8897	15970.79971	12974.23625
d1 m	0.02	0.02	0.02	P (barg)	6.44	8.88	13.44
d2 m	0.02	0.02	0.02	k1 (tabel A.1)	3.3444	3.3444	3.3444
w/m^2-k (20000 k)	5000	5000	5000	k2	0.2745	0.2745	0.2745
w/m^2-k (20,000 k)	1500	1500	1500	k3	-0.0472	-0.0472	-0.0472
Tin shell C	149	149	149	B1 (table A.4)	1.74	1.74	1.74
T out shell (C)	90	50	50	B2	1.55	1.55	1.55
Tin tube	32	32	32	Fm (figure A.18)	1.8	1.8	1.8
Tout tube	49	49	49	identification nun	1.8		
kw w/m^2-k	21	21	21	Fp (eq A.3 pg 12)	1	1	1
U0	937.5	937.5	937.5	Cp0	3101.741655	3525.56285	2864.069811
Tlm	77.10281751	89.73622806	48.25327998	A(m^2)	3.96	7.39	2.78
F	1	1	1	C1 (0 if below 40 barg)			
changeT1	100	100	100	C2			
ChangeT2	58	18	18	C3			

Costing and Sizing of E-201 and E-202 involved in the SMR production of Hydrogen.

	E-201	E-202	Heat Exchanger	E-201	E-202
Q kj/hr	8033000	288400	Type	shell and tube	shell and tube
A m^2	46.08870722	5.3161666665	2020	210181.2379	190683.6992
Rfi m^2 k/w	0.0001	0.0001	Cbm	137373.3581	124629.8688
Rfo m^2k/w	0.0001	0.0001	P (barg)	33.44	18
d1 m	0.02	0.02	k1 (tabel A.1)	4.8306	4.8306
d2 m	0.02	0.02	k2	-0.8509	-0.8509
hi w/m^2-k (20000 kpa)	5000	5000	k3	0.3187	0.3187
ho w/m^2-k (20,000 kpa)	1500	500	B1 (table A.4)	1.63	1.63
Tin shell C	637	265	B2	1.66	1.66
T out shell (C)	265	250	FBm	2.8	2.8
Tin tube	32	32	identification nun	5	5
Tout tube	235	49	Fp (eq A.3 pg 12)	1.140558376	1.062321462
kw w/m^2-k	21	21	Cp0	19819.23365	18976.26796
U0	937.5	416.6666667	A(kw or m^2)	46.1	13
Tlm	309.8565733	216.9984639	C1 (0 if below 5 t)	0.03881	0.03881
F	0.6	0.6	C2	-0.11272	-0.11272
changeT1	402	216	C3	0.08183	0.08183
ChangeT2	233	218			

Costing and sizing of E-301 and E-302 involved in the production of Ammonia.

Haber Heat Exchangers	E-107	E-108		pre reactor	refrigeration
Q kj/hr	6924000	6379000	Heat Exchanger	E-301	E-302
A m^2	203.6175351	752.8831038	Type	shell and tube	shell and tube
Rfi m^2 k/w	0.0001	0.0001	2020	364263.3316	1034077.027
Rfo m^2k/w	0.0001	0.0001	Cbm	238080.6089	675867.3381
d1 m	0.02	0.02	P (barg)	14.44	13.44
d2 m	0.02	0.02	k1 (tabel A.1)	4.8306	4.8306
hi w/m^2-k (20000 kpa)	1500	500	k2	-0.8509	-0.8509
ho w/m^2-k (20,000 kpa)	1500	1500	k3	0.3187	0.3187
Tin shell C	102	-31	B1 (table A.4)	1.63	1.63
T out shell (C)	450	-42.19	B2	1.66	1.66
Tin tube	550	177	Fm (figure A.18)	2.8	2.8
Tout tube	177	-30	identification number (ss tubes and cs shell)	4	4
kw w/m^2-k	21	21	Fp (eq A.3 pg 1264)	1.042634	1.037073981
U0	652.173913	348.8372093	Cp0	36762.60389	104780.4376
Tlm	86.90148742	40.48097811	A(m^2)	204	753
F	0.6	0.6	C1 (0 if below 5 barg)	0.03881	0.03881
changeT1	100	219.19	C2	-0.11272	-0.11272
ChangeT2	75	1	C3	0.08183	0.08183

H-201 costing and sizing

Fired Heater Costing	
Duty	18914880.61 kJ/h
A =	5254.133504 kW
K1 =	7.3488
K2 =	-1.1666
K3 =	0.2028
log10Cp =	5.815647065
Cpo =	\$ 654,104.39
P =	29 barg
C1 =	0.1347
C2 =	-0.2368
C3 =	0.1021
Fp =	1.015677943
Fm =	2.8
Cbm =	\$ 1,860,206.33

E-303 costing and sizing

AFaceT = mair * pair * V face	
mair =	406674.6337 kg/hr
p air=	1.275 kg/m³
V face =	10972.8 m³/h
Aface=	29.06828677 m²
A =	29.06828677
K1 =	4.0336
K2 =	0.2341
K3 =	0.0497
log10Cp =	4.482623833
Cpo =	30382.52286
P =	1.6
Fp =	1
B1 =	0.96 barg
B2 =	1.21
Fm =	3.5
Cbm =	\$ 157,837.21

Storage tanks V-301, V-302, and V-303 costing and sizing

Tank for Ammonia	
using ss	129053.4992
	129053.4992
Cp0	84348.69228
K1	4.8506
K2	-0.3973
K3	0.1445
A = volume (m³)	847
B1	2.25
B2	1.82
Fm	3.1
D (m)	7.110346383
P (bar)	17.2369
Fp	12.08449262
overall volume	2541
flow rate (30 days)	1547469

Costing and sizing of Membrane, fired heater, and compressor for membrane option.

Membrane Type	hollow fiber	Fired Heater Costing	Compressor Cost
Flux	transfer rate/ area		
mass flow rate air (kg/day)	4110	Duty = 756914.672 kJ/h	2 bar
molar flow rate	45359.2	A = 210.2540756 kW	Stage 1 Compressor Energy = 136681.6115 kJ/h
kg/hr	1712.916667	K1 = 7.3488	37.96711431 kW
m³/h	21049.65666	K2 = -1.1666	GHP = 37.96711431
perovskite BaCoxFeyZr1-x-yO3-δ (BCFZ) at 500 C	0.45	K3 = 0.2028	BHP = 42.25026186
volumetric fraction of O2	0.1769	log10Cp = 5.733221084	Driver Efficiency = 0.3
transfer rate (m³/h)	3723.684259	Cpo = \$ 541,029.67	Driver Power = 140.8342062 kW
nitrogen out flow m³/min	284.696606	P = 29 barg	Ce = a + b*(S/n)
0.45*60*(10^-2)	0.27	C1 = 0.1347	S = 140.8342062 kW
area for temp of 500	13791.42318	C2 = -0.2368	a = 260000
4.8*(1*10^-2)*(60)	2.88	C3 = 0.1021	b = 2700
		Fp = 1.015677943	n = 0.75
		Fm = 2.8	Ce = 370381.1405
		Cbm = \$ 1,538,633.33	Purchased Horsepower = 188.8614872 hp
		2020 Dollars = \$ 2,354,109.00	

Costing and Sizing of Electrolysis option for hydrogen production.

H2O	Molar Flow	183.4	kgmole/hr
	Mass Flow	3304.868	kg/hr
	ΔG	237.1	KJ/mole
Energy required (Calculation)		12078.92778	
	Costing	500	\$/kW
	Capital Investment	\$6,039,464	
cell operating temp	60-80C		
Minnnesota electricity price		10.37	cents/kWh
		0.1037	\$/kWh
energy requirement yearly		105811407.3	kWh
Electricity cost (per year)		\$10,972,643	

Costing and sizing for the water gas shift reactor R-202, using a packed bed reactor.

Water Gas Shift Packed Bed Reactor	P =	15
For 10% conversion of CO ₂ ,	W/FCO ₂ = 0.5 gcat/molCO ₂	F _p = 1.091329147
FCO ₂	309.17 kmol/h	B ₁ = 1.49
	309170 mol/h	B ₂ = 1.52
W=	154.585 g	F _m = 3.5
Catalyst Mass=	154.585 kg	C _{bm} = 11227.32822
Catalyst density =	0.9 g/cm ³	Catalyst Cost = 2318.775
Density =	0.9 kg/L	Total Cost (Vessel+Catalyst)= \$13,546.10
Density =	900 kg/m ³	2019 19496.58717
Reactor Volume =	0.171761111 m ³	Conditions:
L/D Ratio	3	T = 453 K
Reactor Diameter	0.417738562	P = 15 atm
Reactor Height	1.253215688	X = 0.7
A =	0.171761111	
K ₁ =	3.4974	
K ₂ =	0.4485	
K ₃ =	0.1074	
log ₁₀ C _p =	3.217129307	

Appendix C

Cash flow table for membrane.

End of Year	2020	21	22	23	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043	
Production, tons					8943	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	
Sales Price, \$/tons					607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	
Sales Revenue					5427203	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407
+Salvage																									
-Royalties																									
Net Revenue					5427203	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407
-Raw Material Costs					28204	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409	56409
-Operating Costs					1430948	2861896	2861896	2861896	2861896	2861896	2861896	2861896	2861896	2861896	2861896	2861896	2861896	2861896	2861896	2861896	2861896	2861896	2861896	2861896	2861896
Waste Removal					424400	848800	848800	848800	848800	848800	848800	848800	848800	848800	848800	848800	848800	848800	848800	848800	848800	848800	848800	848800	848800
-Depreciation					7794353	12470964	7482579	4489547	4489547	2244774															
- Amortization																									
- Depletion																									
- Loss Forward						4250702	9634365																		
- Writeoff																									
Taxable Income					(4250702)	(9634365)	(10029642)																		
-Tax @ 25%																									
Net Income					(4250702)	(9634365)	(7522231)																		
+Depreciation					7794353	12470964	7482579	4489547	4489547	2244774	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
+ Depletion																									
+ Loss Forward																									
+ Writeoff																									3897176
working capital					(3897176)																				
- Fixed Capital					(38971764)																				
Cash Flow					(42868940)			0	0	3543651	7087302	9594712	6437863	6437863	5876670	5315476	5315476	5315476	5315476	5315476	5315476	5315476	5315476	5315476	9212653
Discount Factor (P/Fi*,n)	1.00	0.93	0.86		0.79	0.74	0.68	0.63	0.58	0.54	0.50	0.46	0.43	0.40	0.37	0.34	0.32	0.29	0.27	0.25	0.23	0.21	0.20	0.18	
Discounted Cash Flow		(42868940)		0	0	2813064	5209378	6530000	4056946	3756431	3174982	2659062	2462094	2279717	2110849	1954490	1809713	1675660	1551537	1436608	1330193	1231660	1140426	1055950	1694580
NPV @ i* =	7064398																								

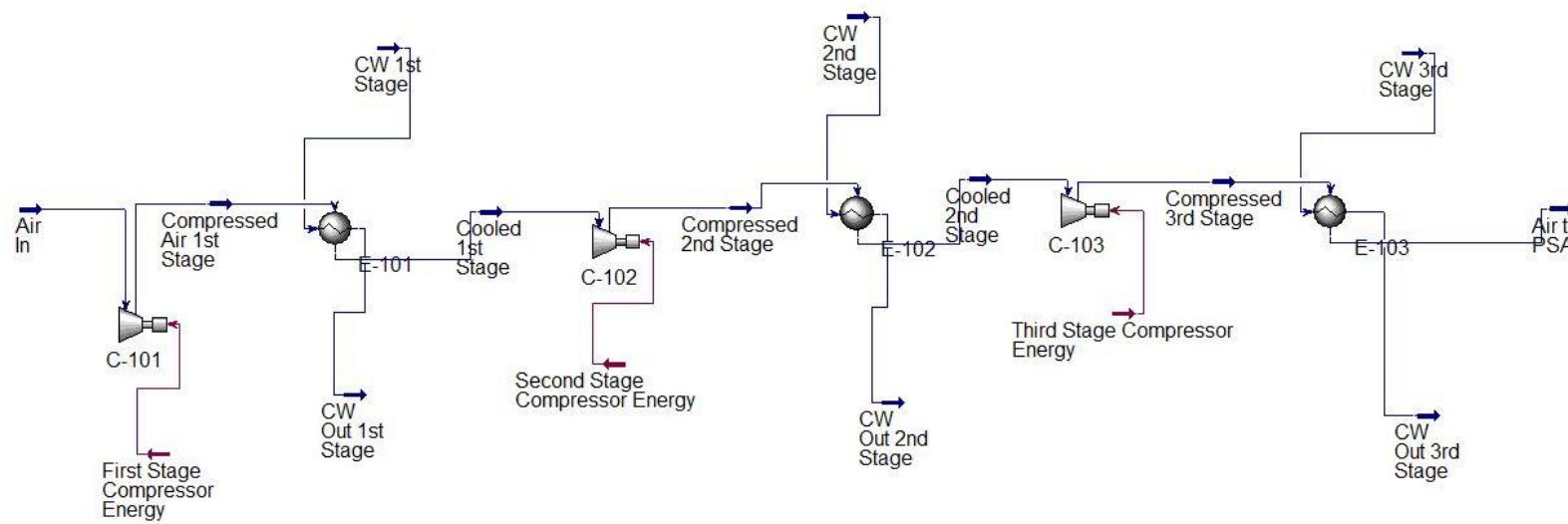
Cash flow Table for buying hydrogen and producing nitrogen.

End of Year	2020	21	22	23	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043					
Production, tons					8943	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885					
Sales Price, \$/tons					607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607					
Sales Revenue					5427203	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407					
+Salvage																													
-Royalties																													
Net Revenue					5427203	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407					
-Raw Material Costs					5788130	11576259	11576259	11576259	11576259	11576259	11576259	11576259	11576259	11576259	11576259	11576259	11576259	11576259	11576259	11576259	11576259	11576259	11576259	11576259					
-Operating Costs					1101754	2203508	2203508	2203508	2203508	2203508	2203508	2203508	2203508	2203508	2203508	2203508	2203508	2203508	2203508	2203508	2203508	2203508	2203508						
waste removal																													
-Depreciation					2650368	4240589	2544353	1526612	1526612	763306																			
- Amortization																													
- Depletion																													
- Loss Forward																													
- Writeoff																													
Taxable Income					(4113049)	(7165950)	(5469715)	(4451973)	(4451973)	(3688667)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)					
-Tax @ 25%																													
Net Income					(4113049)	(7165950)	(5469715)	(4451973)	(4451973)	(3688667)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)					
+Depreciation					2650368	4240589	2544353	1526612	1526612	763306	0	0	0	0	0	0	0	0	0	0	0	0	0	0					
+ Depletion																													
+ Loss Forward																													
+ Writeoff																									1325184				
working capital					(1325184)																								
- Fixed Capital					(13251840)																								
Cash Flow					(14577024)	0	0	0	(1462681)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(2925361)	(1600177)					
Discount Factor (P/Fi*,n)					1.00	0.	0.	0.	0.74	0.68	0.63	0.58	0.54	0.50	0.46	0.43	0.40	0.37	0.34	0.32	0.29	0.27	0.25	0.23	0.21	0.20	0.18	0.17	
Discounted Cash Flow					(14577024)	0	0	0	(1075114)	(1990952)	(1843474)	(1706920)	(1580482)	(1463409)	(1355008)	(1254637)	(1161701)	(1075649)	(995972)	(922196)	(853885)	(790634)	(732069)	(677842)	(627631)	(581140)	(538092)	(272535)	
NPV @ i* =					(36076366)																								

Cash flow table for buying nitrogen and producing hydrogen.

End of Year	2020	21	22	23	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043				
Production, tons					8943	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885	17885				
Sales Price, \$/tons					607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607	607				
Sales Revenue					5427203	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407			
+Salvage																												
-Royalties																												
Net Revenue					5427203	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407	10854407			
-Raw Material Costs					373083	401287	401287	401287	401287	401287	401287	401287	401287	401287	401287	401287	401287	401287	401287	401287	401287	401287	401287	401287	401287			
-Operating Costs					1843744	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487	3687487			
Waste Removal	0	0	0		424382	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764	848764			
-Depreciation					4357550	6972081	4183248	2509949	2509949	1254975																		
- Amortization																												
- Depletion																												
- Loss Forward					1571556	2626768	893148																					
- Writeoff																												
Taxable Income					(1571556)	(2626768)	(893148)	2513771	3406919	4661894	5916868	5916868	5916868	5916868	5916868	5916868	5916868	5916868	5916868	5916868	5916868	5916868	5916868	5916868	5916868			
-Tax @ 25%								628443	851730	1165473	1479217	1479217	1479217	1479217	1479217	1479217	1479217	1479217	1479217	1479217	1479217	1479217	1479217	1479217				
Net Income					(1571556)	(2626768)	(893148)	1885328	2555189	3496420	4437651	4437651	4437651	4437651	4437651	4437651	4437651	4437651	4437651	4437651	4437651	4437651	4437651	4437651	4437651			
+Depreciation					4357550	6972081	4183248	2509949	2509949	1254975	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
+ Depletion																												
+ Loss Forward								1571556	2626768	893148																		
+ Writeoff																									2178775			
working capital					(2178775)																							
- Fixed Capital					(21787752)																							
Cash Flow					(23966527)	0	0	0	2785995	5916868	5916868	5288425	5065138	4751395	4437651	4437651	4437651	4437651	4437651	4437651	4437651	4437651	4437651	4437651	4437651	6616426		
Discount Factor (P/Fi*,n)	1.00	0.93	0.86	0.79	0.74	0.68	0.63	0.58	0.54	0.50	0.46	0.43	0.40	0.37	0.34	0.32	0.29	0.27	0.25	0.23	0.21	0.20	0.18	0.17				
Discounted Cash Flow					(23966527)	0	0	0	2047789	4026921	3728631	3085745	2736537	2376880	2055491	1903232	1762252	1631715	1510847	1398933	1295308	1199359	1110518	1028257	952090	881565	816264	1126879
NPV @ i* =					12708687																							

Appendix D



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INPUT SUMMARY

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FLUID PACKAGE: Basis-1(Peng-Robinson)

Property Package Type: PengRob
Component List - 1: Nitrogen /Oxygen /CO2 /Argon /H2O /CO /Methane /

FLOWSHEET: Main

Fluid Package: Basis-1

STREAM: Air In (Material Stream)

Temperature = 5 C
Pressure = 101.324997 kPa
Molar Flow = 113.6 kgmole/h
Composition Basis (In Mole Flows):Nitrogen = 88.608/ Oxygen = 23.856/ CO2 = 0.4544/ Argon = 0.6816/ H2O = 0/ CO = 0/ Methane = 0/

STREAM: First Stage Compressor Energy (Energy Stream)
STREAM: Compressed Air 1st Stage (Material Stream)

Temperature = 148.9 C

UNIT OPERATION: C-102 (Compressor)

Feed Stream = Cooled 1st Stage
Product Stream = Compressed 2nd Stage
Energy Stream = Second Stage Compressor Energy
AdiabaticEfficiency = 75
CurveCollectionName = CC-0
SelectedCurveCollection = True
NumberOfCurves = 0
NumberOfCurves = 0
NumberOfCurves = 0
EffCurveType = 0
NumberOfCurves = 0

STREAM: Cooled 1st Stage (Material Stream)
Temperature = 50 C

STREAM: Compressed 2nd Stage (Material Stream)
Temperature = 148.888889 C

STREAM: Second Stage Compressor Energy (Energy Stream)

UNIT OPERATION: E-103 (Heat Exchanger)

TubeInletStream = CW 3rd Stage
TubeOutletStream = CW Out 3rd Stage
ShellInletStream = Compressed 3rd Stage
ShellOutletStream = Air to PSA
TubeOuterDiameter = 20 mm
TubeInnerDiameter = 16 mm
TubeThickness = FEMPTY mm
HCurveName = CW 3rd Stage-CW Out 3rd Stage
HCurveName = Compressed 3rd Stage-Air to PSA
ShellPressureDrop = 62 kPa
TubePressureDrop = 0 kPa

STREAM: Air to PSA (Material Stream)

Temperature = 90 C

STREAM: CW 3rd Stage (Material Stream)

Temperature = 32 C
Pressure = 101.3 kPa
Composition Basis (In Mole Fractions):Nitrogen = 0/ Oxygen = 0/ CO2 = 0/
Argon = 0/ H2O = 1/ CO = 0/ Methane = 0/

STREAM: CW Out 3rd Stage (Material Stream)

Temperature = 49 C

UNIT OPERATION: E-101 (Heat Exchanger)

TubeInletStream = CW 1st Stage
TubeOutletStream = CW Out 1st Stage
ShellInletStream = Compressed Air 1st Stage
ShellOutletStream = Cooled 1st Stage
TubeOuterDiameter = 20 mm
TubeInnerDiameter = 16 mm
TubeThickness = FEMPTY mm
HCurveName = CW 1st Stage-CW Out 1st Stage
HCurveName = Compressed Air 1st Stage-Cooled 1st Stage
ShellPressureDrop = 62 kPa

UNIT OPERATION: C-103 (Compressor)

Feed Stream = Cooled 2nd Stage
Product Stream = Compressed 3rd Stage
Energy Stream = Third Stage Compressor Energy
AdiabaticEfficiency = FEMPTY
CurveCollectionName = CC-0
SelectedCurveCollection = True
NumberOfCurves = 0

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NumberOfCurves = 0
NumberOfCurves = 0
EffCurveType = 0
NumberOfCurves = 0
STREAM: Compressed 3rd Stage (Material Stream)
Temperature = 148.888889 C
Pressure = 1062 kPa
STREAM: Third Stage Compressor Energy (Energy Stream)
STREAM: CW 1st Stage (Material Stream)
Temperature = 32 C
Pressure = 101.3 kPa
Composition Basis (In Mole Fractions ):Nitrogen = 0/ Oxygen = 0/ CO2 = 0/
Argon = 0/ H2O = 1/ CO = 0/ Methane = 0/
STREAM: CW 2nd Stage (Material Stream)
Temperature = 32 C
Pressure = 101.3 kPa
Composition Basis (In Mole Fractions ):Nitrogen = 0/ Oxygen = 0/ CO2 = 0/
Argon = 0/ H2O = 1/ CO = 0/ Methane = 0/
STREAM: Cooled 2nd Stage (Material Stream)
Temperature = 50 C
UNIT OPERATION: E-102 (Heat Exchanger)
TubeInletStream = CW 2nd Stage
TubeOutletStream = CW Out 2nd Stage
ShellInletStream = Compressed 2nd Stage
ShellOutletStream = Cooled 2nd Stage
TubeOuterDiameter = 20 mm
TubeInnerDiameter = 16 mm
TubeThickness = FEMPTY mm
HCurveName = CW 2nd Stage-CW Out 2nd Stage
HCurveName = Compressed 2nd Stage-Cooled 2nd Stage
ShellPressureDrop = 62 kPa
STREAM: CW Out 1st Stage (Material Stream)
Temperature = 49 C
Pressure = 101.3 kPa
STREAM: CW Out 2nd Stage (Material Stream)
Temperature = 49 C
Pressure = 101.3 kPa
#####
##### OUTPUT SUMMARY #####
#####
OKLAHOMA STATE UNIVERSIT Case Name: Nitrogen Final.hsc
Bedford, MA
USA          Unit Set: SI

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Date/Time: Wed Apr 01 18:48:17 2020

Basis-1 (Fluid Package): Component List

Fluid Package: Basis-1

COMPONENT LIST

Component List - 1 [HYSYS Databanks]

COMPONENT	TYPE	MOLECULAR	BOILING PT	IDEAL LIQ	CRITICAL
	WEIGHT	(C)	DENSITY (kg/m3)	TEMP (C)	
Nitrogen	Pure	28.01	-195.8	806.4	-147.0
Oxygen	Pure	32.00	-183.0	1138	-118.4
CO2	Pure	44.01	-78.55	825.3	30.95
Argon	Pure	39.95	-185.9	1370	-122.4
H2O	Pure	18.02	100.0	998.0	374.1
CO	Pure	28.01	-191.5	799.4	-140.2
Methane	Pure	16.04	-161.5	299.4	-82.45

(Continued..) Component List - 1 [HYSYS Databanks]

COMPONENT	CRITICAL PRES	CRITICAL VOL	ACENTRICITY	HEAT OF FORM
	(kPa)	(m3/kgmole)	(kJ/kgmole)	
Nitrogen	3394	9.000e-002	4.000e-002	0.0000
Oxygen	5080	7.320e-002	1.900e-002	0.0000
CO2	7370	9.390e-002	0.2389	-3.938e+005
Argon	4864	7.490e-002	-4.000e-003	0.0000
H2O	2.212e+004	5.710e-002	0.3440	-2.418e+005
CO	3499	8.930e-002	9.300e-002	-1.106e+005
Methane	4641	9.900e-002	1.150e-002	-7.490e+004

Case (Simulation Case): Mass and Energy Balance, Utility Balance, Process CO2 Emissions

Simulation Case: Case

OVERALL MASS BALANCE

In Stream	Count	Mass Flow	Out Stream	Count	Mass Flow
	(kg/h)			(kg/h)	
Air In	Yes	3293	CW Out 3rd Stage	Yes	2734
CW 3rd Stage	Yes	2734	Air to PSA	Yes	3293
CW 1st Stage	Yes	4543	CW Out 1st Stage	Yes	4543
CW 2nd Stage	Yes	4554	CW Out 2nd Stage	Yes	4554
Total In MassFlow (kg/h)	1.512e+004	Total Out MassFlow (kg/h)	1.512e+004		
Mass Imbalance (kg/h)	0.0000	Rel Mass Imbalance Pct (%)	0.00		

OVERALL ENERGY BALANCE

InStream	Count	Energy Flow	OutStream	Count	Energy Flow
	(kJ/h)			(kJ/h)	
Air In	Yes	-2.461e+05	CW Out 3rd Stage	Yes	-4.315e+07
First Stage Compressor Energy	Yes	4.814e+05	Air to PSA	Yes	3.175e+04
Second Stage Compressor Energy	Yes	3.324e+05	CW Out 1st Stage	Yes	-7.170e+07
CW 3rd Stage	Yes	-4.335e+07	CW Out 2nd Stage	Yes	-7.188e+07
CW 1st Stage	Yes	-7.204e+07			
Third Stage Compressor Energy	Yes	3.321e+05			
CW 2nd Stage	Yes	-7.221e+07			
Total In EnergyFlow (kJ/h)	-1.867e+008	Total Out EnergyFlow (kJ/h)	-1.867e+008		
Energy Imbalance (kJ/h)	-2.619e-008	Rel Energy Imbalance Pct (%)	0.00		

OVERALL UTILITY BALANCE

Utility Name	Usage	Info	Energy Flow	Mass Flow	Cost
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Hot Utility Summary Cold Utility Summary

Utility Flow ---	Utility Flow ---
Utility Cost ---	Utility Cost ---
Carbon Emiss. ---	Carbon Emiss. ---
Carbon Fees ---	Carbon Fees ---

PROCESS CO2 EMISSIONS

Inlet Stream	Count	IFPP (1995)	IFPP (2007)	EPA (2009)
	(kg/h)	(kg/h)	(kg/h)	
Air In	Yes	2.000e+01	2.000e+01	2.000e+01
CW 3rd Stage	Yes	0.000e-01	0.000e-01	0.000e-01
CW 1st Stage	Yes	0.000e-01	0.000e-01	0.000e-01
CW 2nd Stage	Yes	0.000e-01	0.000e-01	0.000e-01
Total from Inlets		2.000e+01	2.000e+01	2.000e+01
Total Carbon Fees		0.000e-01	0.000e-01	0.000e-01
from Inlets (Cost/hr)				
Outlet Stream	Count	IFPP (1995)	IFPP (2007)	EPA (2009)
	(kg/h)	(kg/h)	(kg/h)	
CW Out 3rd Stage	Yes	0.000e-01	0.000e-01	0.000e-01
Air to PSA	Yes	2.000e+01	2.000e+01	2.000e+01
CW Out 1st Stage	Yes	0.000e-01	0.000e-01	0.000e-01
CW Out 2nd Stage	Yes	0.000e-01	0.000e-01	0.000e-01
Total from Outlets		2.000e+01	2.000e+01	2.000e+01
Total Carbon Fees		0.000e-01	0.000e-01	0.000e-01
from Outlets (Cost/hr)				

Air In (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Air In Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction	1.0000	1.0000
Temperature: (C)	5.000	5.000
Pressure: (kPa)	101.3	101.3
Molar Flow (kgmole/h)	113.6	113.6
Mass Flow (kg/h)	3293	3293
Std Ideal Liq VolFlow (m ³ /h)	3.793	3.793
Molar Enthalpy (kJ/kgmole)	-2.166e+03	-2.166e+03
Molar Entropy (kJ/kgmole-C)	1.501e+02	1.501e+02
Heat Flow (kJ/h)	-2.461e+05	-2.461e+05
Liq VolFlow @Std Cond (m ³ /h)	2684	2684

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
(kgmole/h) (kg/h) (m³/h)

Nitrogen	88.61	0.7800	2482	0.7538	3.078	0.8115
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Oxygen	23.86	0.2100	763.4	0.2318	0.6710	0.1769
CO2	0.4544	0.0040	20.00	0.0061	2.423e-002	0.0064
Argon	0.6816	0.0060	27.23	0.0083	1.987e-002	0.0052
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	113.6	1.0000	3293	1.0000	3.793	1.0000
Vapour Phase				Phase Fraction	1.000	

COMPONENTS	MOLE FLOW (kgmole/h)	MOLE FRAC (kg/h)	MASS FLOW (m ³ /h)	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
Nitrogen	88.61	0.7800	2482	0.7538	3.078	0.8115
Oxygen	23.86	0.2100	763.4	0.2318	0.6710	0.1769
CO2	0.4544	0.0040	20.00	0.0061	2.423e-002	0.0064
Argon	0.6816	0.0060	27.23	0.0083	1.987e-002	0.0052
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	113.6	1.0000	3293	1.0000	3.793	1.0000

Compressed Air 1st Stage (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Compressed Air 1st Stage Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction	1.0000	1.0000
Temperature: (C)	148.9	148.9
Pressure: (kPa)	323.3	323.3
Molar Flow (kgmole/h)	113.6	113.6
Mass Flow (kg/h)	3293	3293
Std Ideal Liq VolFlow (m ³ /h)	3.793	3.793
Molar Enthalpy (kJ/kgmole)	2.071e+03	2.071e+03
Molar Entropy (kJ/kgmole-C)	1.527e+02	1.527e+02
Heat Flow (kJ/h)	2.353e+05	2.353e+05
Liq VolFlow @Std Cond (m ³ /h)	2684	2684

COMPOSITION

Overall Phase	Vapour Fraction	1.0000
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COMPONENTS	MOLE FLOW (kgmole/h)	MOLE FRAC (kg/h)	MASS FLOW (m ³ /h)	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
Nitrogen	88.61	0.7800	2482	0.7538	3.078	0.8115
Oxygen	23.86	0.2100	763.4	0.2318	0.6710	0.1769
CO2	0.4544	0.0040	20.00	0.0061	2.423e-002	0.0064
Argon	0.6816	0.0060	27.23	0.0083	1.987e-002	0.0052
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	113.6	1.0000	3293	1.0000	3.793	1.0000
Vapour Phase				Phase Fraction	1.000	

COMPONENTS	MOLE FLOW (kgmole/h)	MOLE FRAC (kg/h)	MASS FLOW (m ³ /h)	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
Nitrogen	88.61	0.7800	2482	0.7538	3.078	0.8115
Oxygen	23.86	0.2100	763.4	0.2318	0.6710	0.1769
CO2	0.4544	0.0040	20.00	0.0061	2.423e-002	0.0064
Argon	0.6816	0.0060	27.23	0.0083	1.987e-002	0.0052
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	113.6	1.0000	3293	1.0000	3.793	1.0000

Cooled 1st Stage (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Cooled 1st Stage Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction	1.0000	1.0000
Temperature: (C)	50.00	50.00
Pressure: (kPa)	261.3	261.3
Molar Flow (kgmole/h)	113.6	113.6
Mass Flow (kg/h)	3293	3293
Std Ideal Liq VolFlow (m ³ /h)	3.793	3.793
Molar Enthalpy (kJ/kgmole)	-8.629e+02	-8.629e+02

Molar Entropy (kJ/kgmole-C) 1.466e+02 1.466e+02

Heat Flow (kJ/h) -9.803e+04 -9.803e+04

Liq VolFlow @Std Cond (m3/h) 2684 2684

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
(kgmole/h) (kg/h) (m3/h)

Nitrogen	88.61	0.7800	2482	0.7538	3.078	0.8115
Oxygen	23.86	0.2100	763.4	0.2318	0.6710	0.1769
CO2	0.4544	0.0040	20.00	0.0061	2.423e-002	0.0064
Argon	0.6816	0.0060	27.23	0.0083	1.987e-002	0.0052
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	113.6	1.0000	3293	1.0000	3.793	1.0000

Vapour Phase Phase Fraction 1.000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
(kgmole/h) (kg/h) (m3/h)

Nitrogen	88.61	0.7800	2482	0.7538	3.078	0.8115
Oxygen	23.86	0.2100	763.4	0.2318	0.6710	0.1769
CO2	0.4544	0.0040	20.00	0.0061	2.423e-002	0.0064
Argon	0.6816	0.0060	27.23	0.0083	1.987e-002	0.0052
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	113.6	1.0000	3293	1.0000	3.793	1.0000

K VALUE

Compressed 2nd Stage (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Compressed 2nd Stage Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction 1.0000 1.0000

Temperature: (C) 148.9 148.9

Pressure: (kPa) 544.9 544.9

Molar Flow (kgmole/h) 113.6 113.6

Mass Flow (kg/h) 3293 3293

Std Ideal Liq VolFlow (m3/h) 3.793 3.793

Molar Enthalpy (kJ/kgmole) 2.063e+03 2.063e+03

Molar Entropy (kJ/kgmole-C) 1.484e+02 1.484e+02

Heat Flow (kJ/h) 2.344e+05 2.344e+05

Liq VolFlow @Std Cond (m3/h) 2684 2684

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
(kgmole/h) (kg/h) (m3/h)

Nitrogen	88.61	0.7800	2482	0.7538	3.078	0.8115
Oxygen	23.86	0.2100	763.4	0.2318	0.6710	0.1769
CO2	0.4544	0.0040	20.00	0.0061	2.423e-002	0.0064
Argon	0.6816	0.0060	27.23	0.0083	1.987e-002	0.0052
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	113.6	1.0000	3293	1.0000	3.793	1.0000

Vapour Phase Phase Fraction 1.000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
(kgmole/h) (kg/h) (m3/h)

Nitrogen	88.61	0.7800	2482	0.7538	3.078	0.8115
Oxygen	23.86	0.2100	763.4	0.2318	0.6710	0.1769
CO2	0.4544	0.0040	20.00	0.0061	2.423e-002	0.0064
Argon	0.6816	0.0060	27.23	0.0083	1.987e-002	0.0052
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	113.6	1.0000	3293	1.0000	3.793	1.0000

K VALUE

Air to PSA (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Air to PSA

Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction 1.0000 1.0000
Temperature: (C) 90.00 90.00
Pressure: (kPa) 1000 1000
Molar Flow (kgmole/h) 113.6 113.6
Mass Flow (kg/h) 3293 3293
Std Ideal Liq VolFlow (m³/h) 3.793 3.793
Molar Enthalpy (kJ/kgmole) 2.794e+02 2.794e+02
Molar Entropy (kJ/kgmole-C) 1.388e+02 1.388e+02
Heat Flow (kJ/h) 3.175e+04 3.175e+04
Liq VolFlow @Std Cond (m³/h) 2684 2684

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

	(kgmole/h)	(kg/h)	(m ³ /h)			
Nitrogen	88.61	0.7800	2482	0.7538	3.078	0.8115
Oxygen	23.86	0.2100	763.4	0.2318	0.6710	0.1769
CO ₂	0.4544	0.0040	20.00	0.0061	2.423e-002	0.0064
Argon	0.6816	0.0060	27.23	0.0083	1.987e-002	0.0052
H ₂ O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	113.6	1.0000	3293	1.0000	3.793	1.0000
Vapour Phase				Phase Fraction	1.000	

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

	(kgmole/h)	(kg/h)	(m ³ /h)			
Nitrogen	88.61	0.7800	2482	0.7538	3.078	0.8115
Oxygen	23.86	0.2100	763.4	0.2318	0.6710	0.1769
CO ₂	0.4544	0.0040	20.00	0.0061	2.423e-002	0.0064
Argon	0.6816	0.0060	27.23	0.0083	1.987e-002	0.0052
H ₂ O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	113.6	1.0000	3293	1.0000	3.793	1.0000

CW 3rd Stage (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: CW 3rd Stage

Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL AQUEOUS PH.

Vapour / Phase Fraction 0.0000 1.0000
Temperature: (C) 32.00 32.00
Pressure: (kPa) 101.3 101.3
Molar Flow (kgmole/h) 151.7 151.7
Mass Flow (kg/h) 2734 2734
Std Ideal Liq VolFlow (m³/h) 2.739 2.739
Molar Enthalpy (kJ/kgmole) -2.857e+05 -2.857e+05
Molar Entropy (kJ/kgmole-C) 5.551e+01 5.551e+01
Heat Flow (kJ/h) -4.335e+07 -4.335e+07
Liq VolFlow @Std Cond (m³/h) 2.694 2.694

COMPOSITION

Overall Phase Vapour Fraction 0.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

	(kgmole/h)	(kg/h)	(m ³ /h)			
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO ₂	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Argon	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ O	151.7	1.0000	2734	1.0000	2.739	1.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	151.7	1.0000	2734	1.0000	2.739	1.0000
Aqueous Phase				Phase Fraction	1.000	

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

	(kgmole/h)	(kg/h)	(m ³ /h)			
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Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO2	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Argon	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2O	151.7	1.0000	2734	1.0000	2.739	1.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	151.7	1.0000	2734	1.0000	2.739	1.0000

CW Out 3rd Stage (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: CW Out 3rd Stage Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL AQUEOUS PH.

Vapour / Phase Fraction	0.0000	1.0000
Temperature: (C)	49.00	49.00
Pressure: (kPa)	101.3	101.3
Molar Flow (kgmole/h)	151.7	151.7
Mass Flow (kg/h)	2734	2734
Std Ideal Liq VolFlow (m ³ /h)	2.739	2.739
Molar Enthalpy (kJ/kgmole)	-2.844e+05	-2.844e+05
Molar Entropy (kJ/kgmole-C)	5.972e+01	5.972e+01
Heat Flow (kJ/h)	-4.315e+07	-4.315e+07
Liq VolFlow @Std Cond (m ³ /h)	2.694	2.694

COMPOSITION

Overall Phase Vapour Fraction 0.0000

COMPONENTS	MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
(kgmole/h)	(kg/h)		(m ³ /h)			
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO2	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Argon	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2O	151.7	1.0000	2734	1.0000	2.739	1.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	151.7	1.0000	2734	1.0000	2.739	1.0000
Aqueous Phase				Phase Fraction 1.000		

COMPONENTS	MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
(kgmole/h)	(kg/h)		(m ³ /h)			
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO2	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Argon	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2O	151.7	1.0000	2734	1.0000	2.739	1.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	151.7	1.0000	2734	1.0000	2.739	1.0000

Compressed 3rd Stage (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Compressed 3rd Stage Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction	1.0000	1.0000
Temperature: (C)	148.9	148.9
Pressure: (kPa)	1062	1062
Molar Flow (kgmole/h)	113.6	113.6
Mass Flow (kg/h)	3293	3293
Std Ideal Liq VolFlow (m ³ /h)	3.793	3.793
Molar Enthalpy (kJ/kgmole)	2.045e+03	2.045e+03
Molar Entropy (kJ/kgmole-C)	1.428e+02	1.428e+02
Heat Flow (kJ/h)	2.323e+05	2.323e+05
Liq VolFlow @Std Cond (m ³ /h)	2684	2684

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS	MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
(kgmole/h)	(kg/h)		(m ³ /h)			
Nitrogen	88.61	0.7800	2482	0.7538	3.078	0.8115

Oxygen	23.86	0.2100	763.4	0.2318	0.6710	0.1769
CO2	0.4544	0.0040	20.00	0.0061	2.423e-002	0.0064
Argon	0.6816	0.0060	27.23	0.0083	1.987e-002	0.0052
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	113.6	1.0000	3293	1.0000	3.793	1.0000
Vapour Phase					Phase Fraction	1.000

COMPONENTS	MOLE FLOW (kgmole/h)	MOLE FRAC (kg/h)	MASS FLOW (m3/h)	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
Nitrogen	88.61	0.7800	2482	0.7538	3.078	0.8115
Oxygen	23.86	0.2100	763.4	0.2318	0.6710	0.1769
CO2	0.4544	0.0040	20.00	0.0061	2.423e-002	0.0064
Argon	0.6816	0.0060	27.23	0.0083	1.987e-002	0.0052
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	113.6	1.0000	3293	1.0000	3.793	1.0000

CW 1st Stage (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: CW 1st Stage Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL AQUEOUS PH.

Vapour / Phase Fraction	0.0000	1.0000
Temperature: (C)	32.00	32.00
Pressure: (kPa)	101.3	101.3
Molar Flow (kgmole/h)	252.2	252.2
Mass Flow (kg/h)	4543	4543
Std Ideal Liq VolFlow (m3/h)	4.552	4.552
Molar Enthalpy (kJ/kgmole)	-2.857e+05	-2.857e+05
Molar Entropy (kJ/kgmole-C)	5.551e+01	5.551e+01
Heat Flow (kJ/h)	-7.204e+07	-7.204e+07
Liq VolFlow @Std Cond (m3/h)	4.477	4.477

COMPOSITION

Overall Phase	Vapour Fraction	0.0000
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COMPONENTS	MOLE FLOW (kgmole/h)	MOLE FRAC (kg/h)	MASS FLOW (m3/h)	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO2	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Argon	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2O	252.2	1.0000	4543	1.0000	4.552	1.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	252.2	1.0000	4543	1.0000	4.552	1.0000
Aqueous Phase					Phase Fraction	1.000

COMPONENTS	MOLE FLOW (kgmole/h)	MOLE FRAC (kg/h)	MASS FLOW (m3/h)	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO2	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Argon	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2O	252.2	1.0000	4543	1.0000	4.552	1.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	252.2	1.0000	4543	1.0000	4.552	1.0000

CW 2nd Stage (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: CW 2nd Stage Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL AQUEOUS PH.

Vapour / Phase Fraction	0.0000	1.0000
Temperature: (C)	32.00	32.00
Pressure: (kPa)	101.3	101.3
Molar Flow (kgmole/h)	252.8	252.8
Mass Flow (kg/h)	4554	4554
Std Ideal Liq VolFlow (m3/h)	4.563	4.563
Molar Enthalpy (kJ/kgmole)	-2.857e+05	-2.857e+05

Molar Entropy (kJ/kgmole-C) 5.551e+01 5.551e+01

Heat Flow (kJ/h) -7.221e+07 -7.221e+07

Liq VolFlow @Std Cond (m3/h) 4.487 4.487

COMPOSITION

Overall Phase Vapour Fraction 0.0000

COMPONENTS	MOLE FLOW (kgmole/h)	MOLE FRAC (kg/h)	MASS FLOW (m3/h)	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO2	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Argon	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2O	252.8	1.0000	4554	1.0000	4.563	1.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	252.8	1.0000	4554	1.0000	4.563	1.0000
Aqueous Phase				Phase Fraction	1.000	

COMPONENTS	MOLE FLOW (kgmole/h)	MOLE FRAC (kg/h)	MASS FLOW (m3/h)	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO2	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Argon	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2O	252.8	1.0000	4554	1.0000	4.563	1.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	252.8	1.0000	4554	1.0000	4.563	1.0000

Cooled 2nd Stage (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Cooled 2nd Stage Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction 1.0000 1.0000

Temperature: (C) 50.00 50.00

Pressure: (kPa) 482.9 482.9

Molar Flow (kgmole/h) 113.6 113.6

Mass Flow (kg/h) 3293 3293

Std Ideal Liq VolFlow (m3/h) 3.793 3.793

Molar Enthalpy (kJ/kgmole) -8.781e+02 -8.781e+02

Molar Entropy (kJ/kgmole-C) 1.414e+02 1.414e+02

Heat Flow (kJ/h) -9.975e+04 -9.975e+04

Liq VolFlow @Std Cond (m3/h) 2684 2684

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS	MOLE FLOW (kgmole/h)	MOLE FRAC (kg/h)	MASS FLOW (m3/h)	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
Nitrogen	88.61	0.7800	2482	0.7538	3.078	0.8115
Oxygen	23.86	0.2100	763.4	0.2318	0.6710	0.1769
CO2	0.4544	0.0040	20.00	0.0061	2.423e-002	0.0064
Argon	0.6816	0.0060	27.23	0.0083	1.987e-002	0.0052
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	113.6	1.0000	3293	1.0000	3.793	1.0000
Vapour Phase				Phase Fraction	1.000	

COMPONENTS	MOLE FLOW (kgmole/h)	MOLE FRAC (kg/h)	MASS FLOW (m3/h)	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
Nitrogen	88.61	0.7800	2482	0.7538	3.078	0.8115
Oxygen	23.86	0.2100	763.4	0.2318	0.6710	0.1769
CO2	0.4544	0.0040	20.00	0.0061	2.423e-002	0.0064
Argon	0.6816	0.0060	27.23	0.0083	1.987e-002	0.0052
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	113.6	1.0000	3293	1.0000	3.793	1.0000

CW Out 1st Stage (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: CW Out 1st Stage Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL AQUEOUS PH.
 Vapour / Phase Fraction 0.0000 1.0000
 Temperature: (C) 49.00 49.00
 Pressure: (kPa) 101.3 101.3
 Molar Flow (kgmole/h) 252.2 252.2
 Mass Flow (kg/h) 4543 4543
 Std Ideal Liq VolFlow (m³/h) 4.552 4.552
 Molar Enthalpy (kJ/kgmole) -2.844e+05 -2.844e+05
 Molar Entropy (kJ/kgmole-C) 5.972e+01 5.972e+01
 Heat Flow (kJ/h) -7.170e+07 -7.170e+07
 Liq VolFlow @Std Cond (m³/h) 4.477 4.477
 COMPOSITION

Overall Phase Vapour Fraction 0.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (kgmole/h) (kg/h) (m³/h)
 Nitrogen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Oxygen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 CO₂ 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Argon 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 H₂O 252.2 1.0000 4543 1.0000 4.552 1.0000
 CO 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Methane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Total 252.2 1.0000 4543 1.0000 4.552 1.0000
 Aqueous Phase Phase Fraction 1.000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (kgmole/h) (kg/h) (m³/h)
 Nitrogen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Oxygen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 CO₂ 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Argon 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 H₂O 252.2 1.0000 4543 1.0000 4.552 1.0000
 CO 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Methane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Total 252.2 1.0000 4543 1.0000 4.552 1.0000

CW Out 2nd Stage (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: CW Out 2nd Stage Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL AQUEOUS PH.
 Vapour / Phase Fraction 0.0000 1.0000
 Temperature: (C) 49.00 49.00
 Pressure: (kPa) 101.3 101.3
 Molar Flow (kgmole/h) 252.8 252.8
 Mass Flow (kg/h) 4554 4554
 Std Ideal Liq VolFlow (m³/h) 4.563 4.563
 Molar Enthalpy (kJ/kgmole) -2.844e+05 -2.844e+05
 Molar Entropy (kJ/kgmole-C) 5.972e+01 5.972e+01
 Heat Flow (kJ/h) -7.188e+07 -7.188e+07
 Liq VolFlow @Std Cond (m³/h) 4.487 4.487
 COMPOSITION

Overall Phase Vapour Fraction 0.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (kgmole/h) (kg/h) (m³/h)
 Nitrogen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Oxygen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 CO₂ 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Argon 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 H₂O 252.8 1.0000 4554 1.0000 4.563 1.0000
 CO 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Methane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Total 252.8 1.0000 4554 1.0000 4.563 1.0000
 Aqueous Phase Phase Fraction 1.000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (kgmole/h) (kg/h) (m³/h)
 Nitrogen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Oxygen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 CO₂ 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Argon 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

H2O	252.8	1.0000	4554	1.0000	4.563	1.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	252.8	1.0000	4554	1.0000	4.563	1.0000

C-101 (Compressor): Design, Rating, Performance

Compressor: C-101

DESIGN

Connections

Inlet Stream

STREAM NAME	FROM UNIT OPERATION
Air In	
Outlet Stream	

STREAM NAME	TO UNIT OPERATION
Compressed Air 1st Stage	E-101 Heat Exchanger
Energy Stream	

STREAM NAME	FROM UNIT OPERATION
First Stage Compressor Energy	
Parameters	

Speed: ---	Duty: 1.3371e+02 kW
Adiabatic Eff.: 75.00	PolyTropic Eff.: 78.59
Adiabatic Head: 1.118e+004 m	Polytropic Head: 1.172e+004 m
Adiabatic Fluid Head: 109.6 kJ/kg	Polytropic Fluid Head: 114.9 kJ/kg
Polytropic Exp. 1.564	Isentropic Exp. 1.398
User Variables	Poly Head Factor 1.001

RATING

Curves

Compressor Speed: ---	Efficiency: Adiabatic	Curves Enabled: Yes
Head Offset: 0.0000 m	Efficiency Offset: 0.00 %	
Speed:		

Flow	Head	Efficiency (%)
Flow Limits		

Surge Curve: Inactive

Speed Flow

Stone Wall Curve: Inactive

Speed Flow

Surge Flow Rate --- Field Flow Rate 2591 ACT_m3/h Stone Wall Flow --- Compressor Volume 0.0000 m³

Nozzle Parameters

Base Elevation Relative to Ground Level 0.0000 m		
Air In	Compressed Air 1st Stage	
Diameter (m)	5.000e-002	5.000e-002
Elevation (Base) (m)	0.0000	0.0000
Elevation (Ground) (m)	0.0000	0.0000
Inertia		

Rotational inertia (kg-m ²) 6.000	Radius of gyration (m) 0.2000
Mass (kg) 150.0	Friction loss factor (rad/min) (kg-m ² /s) 6.000e-003

PERFORMANCE

Results

Adiabatic Head (m)	1.118e+004	Power Consumed (kW)	133.7
Polytropic Head (m)	1.172e+004	Polytropic Head Factor	1.001
Adiabatic Fluid Head (kJ/kg)	109.6	Polytropic Exponent	1.564
Polytropic Fluid Head (kJ/kg)	114.9	Isentropic Exponent	1.398
Adiabatic Efficiency	75	Speed (rpm)	---
Polytropic Efficiency	79		
Power/Torque			

Total Rotor Power (kW) 133.7	Total Rotor Torque (N-m) ---
Transient Rotor Power (kW) 0.0000	Transient Rotor Torque (N-m) ---
Friction Power Loss (kW) 0.0000	Friction Torque Loss (N-m) ---
Fluid Power (kW)	133.7
	Fluid Torque (N-m) ---

C-102 (Compressor): Design, Rating, Performance

Compressor: C-102

DESIGN

Connections

Inlet Stream

STREAM NAME FROM UNIT OPERATION
Cooled 1st Stage E-101 Heat Exchanger
Outlet Stream

STREAM NAME TO UNIT OPERATION
Compressed 2nd Stage E-102 Heat Exchanger
Energy Stream

STREAM NAME FROM UNIT OPERATION
Second Stage Compressor Energy
Parameters

Speed: --- Duty: 9.2337e+01 kW
Adiabatic Eff.: 75.00 PolyTropic Eff.: 77.37
Adiabatic Head: 7721 m Polytropic Head: 7965 m
Adiabatic Fluid Head: 75.71 kJ/kg Polytropic Fluid Head: 78.11 kJ/kg
Polytropic Exp. 1.576 Isentropic Exp. 1.396 Poly Head Factor 1.000
User Variables

RATING

Curves

Compressor Speed: --- Efficiency: Adiabatic Curves Enabled: Yes
Head Offset: 0.0000 m Efficiency Offset: 0.00 %
Speed:

Flow Head Efficiency (%)
Flow Limits

Surge Curve: Inactive

Speed Flow

Stone Wall Curve: Inactive

Speed Flow

Surge Flow Rate --- Field Flow Rate 1167 ACT_m3/h Stone Wall Flow --- Compressor Volume 0.0000 m3
Nozzle Parameters

Base Elevation Relative to Ground Level 0.0000 m

Cooled 1st Stage Compressed 2nd Stage

Diameter (m) 5.000e-002 5.000e-002

Elevation (Base) (m) 0.0000 0.0000

Elevation (Ground) (m) 0.0000 0.0000

Inertia

Rotational inertia (kg-m2) 6.000 Radius of gyration (m) 0.2000
Mass (kg) 150.0 Friction loss factor (rad/min) (kg-m2/s) 6.000e-003
PERFORMANCE

Results

Adiabatic Head (m) 7721 Power Consumed (kW) 92.34
Polytropic Head (m) 7965 Polytropic Head Factor 1.000
Adiabatic Fluid Head (kJ/kg) 75.71 Polytropic Exponent 1.576
Polytropic Fluid Head (kJ/kg) 78.11 Isentropic Exponent 1.396
Adiabatic Efficiency 75 Speed (rpm) ---
Polytropic Efficiency 77 ---
Power/Torque

Total Rotor Power (kW) 92.34 Total Rotor Torque (N-m) ---
Transient Rotor Power (kW) 0.0000 Transient Rotor Torque (N-m) ---
Friction Power Loss (kW) 0.0000 Friction Torque Loss (N-m) ---
Fluid Power (kW) 92.34 Fluid Torque (N-m) ---

C-103 (Compressor): Design, Rating, Performance

Compressor: C-103

DESIGN

Connections

Inlet Stream

STREAM NAME FROM UNIT OPERATION
Cooled 2nd Stage E-102 Heat Exchanger
Outlet Stream

STREAM NAME TO UNIT OPERATION
Compressed 3rd Stage E-103 Heat Exchanger
Energy Stream

STREAM NAME FROM UNIT OPERATION
Third Stage Compressor Energy
Parameters

Speed: --- Duty: 9.2248e+01 kW
Adiabatic Eff.: 81.12 PolyTropic Eff.: 83.04
Adiabatic Head: 8343 m Polytropic Head: 8540 m
Adiabatic Fluid Head: 81.81 kJ/kg Polytropic Fluid Head: 83.75 kJ/kg
Polytropic Exp. 1.521 Isentropic Exp. 1.400 Poly Head Factor 1.000
User Variables

RATING

Curves

Compressor Speed: --- Efficiency: Adiabatic Curves Enabled: Yes

Head Offset: 0.0000 m Efficiency Offset: 0.00 %

Speed:
Flow Head Efficiency (%)
Flow Limits

Surge Curve: Inactive

Speed Flow

Stone Wall Curve: Inactive

Speed Flow

Surge Flow Rate --- Field Flow Rate 631.1 ACT_m3/h Stone Wall Flow --- Compressor Volume 0.0000 m3

Nozzle Parameters

Base Elevation Relative to Ground Level 0.0000 m
Cooled 2nd Stage Compressed 3rd Stage

Diameter (m) 5.000e-002 5.000e-002
Elevation (Base) (m) 0.0000 0.0000
Elevation (Ground) (m) 0.0000 0.0000
Inertia

Rotational inertia (kg-m²) 6.000 Radius of gyration (m) 0.2000
Mass (kg) 150.0 Friction loss factor (rad/min) (kg-m²/s) 6.000e-003
PERFORMANCE

Results

Adiabatic Head (m) 8343 Power Consumed (kW) 92.25
Polytropic Head (m) 8540 Polytropic Head Factor 1.000
Adiabatic Fluid Head (kJ/kg) 81.81 Polytropic Exponent 1.521
Polytropic Fluid Head (kJ/kg) 83.75 Isentropic Exponent 1.400
Adiabatic Efficiency 81 Speed (rpm) ---
Polytropic Efficiency 83 ---
Power/Torque

Total Rotor Power (kW) 92.25 Total Rotor Torque (N-m) ---
Transient Rotor Power (kW) 0.0000 Transient Rotor Torque (N-m) ---
Friction Power Loss (kW) 0.0000 Friction Torque Loss (N-m) ---
Fluid Power (kW) 92.25 Fluid Torque (N-m) ---

E-103 (Heat Exchanger): Design, Rating, Details, Tables, HTFS Results, Exchanger Design and Rating

Heat Exchanger: E-103

CONNECTIONS

Tube Side Shell Side
Inlet Outlet Inlet Outlet

Name CW 3rd Stage Name CW Out 3rd Stage Name Compressed 3rd Stage Name Air to PSA
 From Op. To Op. From Op. C-103 To Op.
 Op. Type Op. Type Op. Type Compressor Op. Type
 Temp 32.00 C Temp 49.00 C Temp 148.89 C Temp 90.00 C
PARAMETERS

Heat Exchanger Model: Simple End Point

Tube Side DeltaP: 0.0000 kPa Shell Side DeltaP: 62.00 kPa Passes: ---
 UA: 2682 kJ/C-h Tolerance: 1.0000e-04
 Tube Side Data Shell Side Data
 Heat Transfer Coeff --- Heat Transfer Coeff ---
 Tube Pressure Drop 0.00 kPa Shell Pressure Drop 62.00 kPa
 Fouling 0.00000 C-h-m2/kJ Fouling 0.00000 C-h-m2/kJ
 Tube Length 6.00 m Shell Passes 1
 Tube O.D. 20.00 mm Shell Series 1
 Tube Thickness 2.0000 mm Shell Parallel 1
 Tube Pitch 50.0000 mm Baffle Type Single
 Orientation Horizontal Baffle Cut(%Area) 20.00
 Passes Per Shell 2 Baffle Orientation Horizontal
 Tubes Per Shell 160 Spacing 800.0000 mm
 Layout Angle Triangular (30 degrees) Diameter 739.0488 mm
 TEMA Type A E L Area 60.32 m2
SPECS

Spec Value	Curr Value	Rel Error	Active Estimate	
E-101 Heat Balance 0.0000 kJ/h	8.851e-009 kJ/h	4.412e-014	On	Off
E-101 UA ---	2682 kJ/C-h	---	On	Off

Detailed Specifications

E-101 Heat Balance
 Type: Duty Pass: Error Spec Value: 0.0000 kJ/h
 E-101 UA
 Type: UA Pass: Overall Spec Value: ---
 User Variables

RATING

Sizing

Overall Data
 Configuration
 # of Shells in Series 1 Tube Passes per Shell 2 Elevation (Base) 0.0000 m
 # of Shells in Parallel 1 Exchange Orientation Horizontal First Tube Pass Flow Direction Counter
 TEMA Type: A E L
 Calculated Information
 Shell HT Coeff --- Tube HT Coeff ---
 Overall U 44.46 kJ/h-m2-C Overall UA 2682 kJ/C-h
 Shell DP 62.00 kPa Tube DP 0.0000 kPa
 Shell Vol per Shell 2.272 m3 Tube Vol per Shell 0.1930 m3
 HT Area per Shell 60.32 m2
 Shell Data
 Shell and Tube Bundle
 Shell Diameter 739.0 Tube Pitch 50.00 Shell Fouling 0.0000
 (mm) (mm) (C-h-m2/kJ)
 # of Tubes per Shell 160 Tube Layout Angle Triangular (30 degrees)
 Shell Baffles
 Shell Baffle Type Single Shell Baffle Orientation Horizontal
 Baffle Cut (%Area) 20.00 Baffle Spacing 800.0 mm
 Tube Data
 Dimensions
 OD 20.00 ID 16.00 Tube Thickness 2.000 Tube Length 6.000
 (mm) (mm) (mm) (m)
 Tube Properties
 Tube Fouling 0.0000 Thermal Cond. 45.00 Wall Cp --- Wall Density ---
 (C-h-m2/kJ) (W/m-K) (kJ/kg-C) (kg/m3)
 Nozzle Parameters

Base Elevation Relative to Ground Level 0.0000 m
 CW 3rd Stage Compressed 3rd Stage CW Out 3rd Stage
 Diameter (m) 5.000e-002 5.000e-002 5.000e-002
 Elevation (Base) (m) 0.0000 0.0000 0.0000
 Elevation (Ground) (m) 0.0000 0.0000 0.0000
 Elevation (% of Height) (%) 0.00 0.00 0.00
 Air to PSA
 Diameter (m) 5.000e-002
 Elevation (Base) (m) 0.0000
 Elevation (Ground) (m) 0.0000
 Elevation (% of Height) (%) 0.00
DETAILS

Overall/Detailed Performance

Duty: 2.006e+05 kJ/h UA Curv. Error: 0.00e-01 kJ/C-h
 Heat Leak: 0.000e-01 kJ/h Hot Pinch Temp: 90.00 C
 Heat Loss: 0.000e-01 kJ/h Cold Pinch Temp: 32.00 C
 UA: 2.682e+03 kJ/C-h Ft Factor: ---
 Min. Approach: 58.00 C Uncorrected Lmtd: 77.06 C
 Lmtd: 74.81 C

TABLES

Shell Side - Overall Phase

Temperature (C)	Pressure (kPa)	Heat Flow (kJ/h)	Enthalpy (kJ/kgmole)
90.00	1000.00	0.00	279.45
148.89	1062.00	200593.27	2045.23
UA (kJ/C-h)	Molar Vap Frac	Mass Vap Frac	Heat of Vap. (kJ/kgmole)
0.00	1.0000	1.0000	---
0.00	1.0000	1.0000	---

Shell Side - Vapour Phase

Mass Flow (kg/h)	Molecular Wt (kg/m3)	Density (kg/m3)	Mass Sp (kJ/kg-C)	Heat Viscosity (cP)	Thermal Cond (W/m-K)	Cond (W/m-K)
3292.79	28.99	9.61	1.03	0.02	0.03	0.03
3292.79	28.99	8.76	1.04	0.02	0.03	0.03
Std Gas Flow (m3/h)	Z Factor	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega	
2686.01	1.00	3773.07	-140.10	0.29	0.04	
2686.01	1.00	3773.07	-140.10	0.29	0.04	

Shell Side - Light Liquid Phase

Tube Side - Overall Phase

Temperature (C)	Pressure (kPa)	Heat Flow (kJ/h)	Enthalpy (kJ/kgmole)
32.00	101.30	0.00	-285676.72
49.00	101.30	200593.27	-284354.80
UA (kJ/C-h)	Molar Vap Frac	Mass Vap Frac	Heat of Vap. (kJ/kgmole)
0.00	0.0000	0.0000	---
0.00	0.0000	0.0000	---

Tube Side - Vapour Phase

Tube Side - Heavy Liquid Phase

Mass Flow (kg/h)	Density (kg/m3)	Mass Sp (kg/m3)	Heat Viscosity (kJ/kg-C)	Thermal Cond (W/m-K)	Surface Tens (dyne/cm)
2733.70	1002.05	4.31	0.76	0.62	70.89
2733.70	989.02	4.32	0.55	0.64	67.91
Molecular Wt (kg/m3)	Sp Gravity (C)	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega
18.02	1.00	22120.00	374.15	0.26	0.34
18.02	0.99	22120.00	374.15	0.26	0.34

Tube Side - Mixed Liquid

Mass Flow (kg/h)	Density (kg/m3)	Mass Sp (kg/m3)	Heat Viscosity (kJ/kg-C)	Thermal Cond (W/m-K)	Surface Tens (dyne/cm)
2733.70	1002.05	4.31	0.76	0.62	---
2733.70	989.02	4.32	0.55	0.64	---
Molecular Wt (kg/m3)	Sp Gravity (C)	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega
18.02	1.00	22120.00	374.15	0.26	0.34
18.02	0.99	22120.00	374.15	0.26	0.34

HTFS

Exchanger Design and Rating

E-101 (Heat Exchanger): Design, Rating, Details, Tables, HTFS Results, Exchanger Design and Rating

Heat Exchanger: E-101

CONNECTIONS

Tube Side	Shell Side		
Inlet	Outlet	Inlet	Outlet
Name CW 1st Stage Name	CW Out 1st Stage Name	Compressed Air 1st Stage Name	Cooled 1st Stage
From Op.	To Op.	From Op. C-101	To Op. C-102
Op. Type	Op. Type	Op. Type Compressor	Op. Type Compressor
Temp 32.00 C	Temp 49.00 C	Temp 148.90 C	Temp 50.00 C
PARAMETERS			

Heat Exchanger Model: Simple End Point

```

Tube Side DeltaP: 0.0000 kPa Shell Side DeltaP: 62.00 kPa Passes: ---
UA: 8368 kJ/C-h Tolerance: 1.0000e-04
Tube Side Data Shell Side Data
Heat Transfer Coeff --- Heat Transfer Coeff ---
Tube Pressure Drop 0.00 kPa Shell Pressure Drop 62.00 kPa
Fouling 0.00000 C-h-m2/kJ Fouling 0.00000 C-h-m2/kJ
Tube Length 6.00 m Shell Passes 1
Tube O.D. 20.00 mm Shell Series 1
Tube Thickness 2.0000 mm Shell Parallel 1
Tube Pitch 50.0000 mm Baffle Type Single
Orientation Horizontal Baffle Cut(%Area) 20.00
Passes Per Shell 2 Baffle Orientation Horizontal
Tubes Per Shell 160 Spacing 800.0000 mm
Layout Angle Triangular (30 degrees) Diameter 739.0488 mm
TEMA Type A E L Area 60.32 m2
SPECS

```

	Spec	Value	Curr	Value	Rel Error	Active	Estimate	
E-100 Heat Balance	0.0000	kJ/h	-2.599e-008	kJ/h	-7.796e-014	On		Off
E-100 UA	---		8368	kJ/C-h	---	On	Off	

Detailed Specifications

E-100 Heat Balance
Type: Duty Pass: Error Spec Value: 0.0000 kJ/h
E-100 UA
Type: UA Pass: Overall Spec Value: ---
User Variables

RATING

Sizing

Overall Data Configuration
of Shells in Series 1 Tube Passes per Shell 2 Elevation (Base) 0.0000 m
of Shells in Parallel 1 Exchange Orientation Horizontal First Tube Pass Flow Direction Counter
TEMA Type: A E L

TEMAT Type: Calculated Information

Shell HT Coeff ---
 Overall U 138.7 kJ/h-m²-C
 Shell DP 62.00 kPa
 Shell Vol per Shell 2.272 m³
 HT Area per Shell 60.32 m²

Tube HT Coeff ---
 Overall UA 8368 kJ/C-h
 Tube DP 0.0000 kPa
 Tube Vol per Shell 0.1930 m³

HFI Alca p
Shell Data

Shell Data
Shell and Tube Bundle
Shell Diameter 739.0 Tube Pitch 50.00 Shell Fouling 0.00
(mm) (mm) (C. b. m²/kW)

(mm) # of Tubers =

of Tubes per Shell 160 Tube Layout Angle Triangular (30 degrees)
Shell Baffles
Shell Ruffle Type Single Shell Ruffle Orientation Horizontal

Shell Ball Baffle Cut

Baffle Cut (%Area) 20.00 Baffle Spacing 800.0 mm
Tube Data
Dimensions

Dimensions

OD 20.00 ID 16.00 Tube Thickness 2.000 Tube Length 6.000
 (mm) (mm) (mm) (m)

Tube Fouling 0.

(C-h-m2/kJ) (W/m-K) (kJ/kg-C) (kg/m3)
Nozzle Parameters

Base Elevation Relative to Ground Level 0.0000 m
CW 1st Stage Compressed Air 1st Stage CW Out 1st Stage

Diameter (m)	5.000e-002	5.000e-002	5.000e-002
Elevation (Base) (m)	0.0000	0.0000	0.0000
Elevation (Ground) (m)	0.0000	0.0000	0.0000

Elevation (% of Height) (%) 0.00

Cooled 1st Stage

Elevation (Base) (m) 0.0000
Elevation (Ground) (m) 0.0000
Elevation (% of Height) (%) 0.00
DETAILS

Overall/Detailed Performance

Duty: 3.333e+05 kJ/h UA Curv. Error: 0.00e-01 kJ/C-h
Heat Leak: 0.000e-01 kJ/h Hot Pinch Temp: 50.00 C
Heat Loss: 0.000e-01 kJ/h Cold Pinch Temp: 32.00 C
UA: 8.368e+03 kJ/C-h Ft Factor: ---
Min. Approach: 18.00 C Uncorrected Lmtd: 47.82 C
Lmtd: 39.84 C

TABLES

Shell Side - Overall Phase

Temperature (C)	Pressure (kPa)	Heat Flow (kJ/h)	Enthalpy (kJ/kgmole)
50.00	261.27	0.00	-862.93
148.90	323.27	333341.13	2071.41
UA (kJ/C-h)	Molar Vap Frac	Mass Vap Frac	Heat of Vap. (kJ/kgmole)
0.00	1.0000	1.0000	---
0.00	1.0000	1.0000	---

Shell Side - Vapour Phase

Mass Flow (kg/h)	Molecular Wt	Density (kg/m3)	Mass Sp Heat (kJ/kg-C)	Viscosity (cP)	Thermal Cond (W/m-K)
3292.79	28.99	2.82	1.01	0.02	0.03
3292.79	28.99	2.67	1.03	0.02	0.03
Std Gas Flow (m3/h)	Z Factor	Pseudo Pc (kPa)	Pseudo Tc (C)	Pseudo Zc	Pseudo Omega
2686.01	1.00	3773.07	-140.10	0.29	0.04
2686.01	1.00	3773.07	-140.10	0.29	0.04

Tube Side - Overall Phase

Temperature (C)	Pressure (kPa)	Heat Flow (kJ/h)	Enthalpy (kJ/kgmole)
32.00	101.30	0.00	-285676.72
49.00	101.30	333341.13	-284354.80
UA (kJ/C-h)	Molar Vap Frac	Mass Vap Frac	Heat of Vap. (kJ/kgmole)
0.00	0.0000	0.0000	---
0.00	0.0000	0.0000	---

Tube Side - Heavy Liquid Phase

Mass Flow (kg/h)	Density (kg/m3)	Mass Sp Heat (kJ/kg-C)	Viscosity (cP)	Thermal Cond (W/m-K)	Surface Tens (dyne/cm)
4542.79	1002.05	4.31	0.76	0.62	70.89
4542.79	989.02	4.32	0.55	0.64	67.91
Molecular Wt	Sp Gravity	Pseudo Pc (kPa)	Pseudo Tc (C)	Pseudo Zc	Pseudo Omega
18.02	1.00	22120.00	374.15	0.26	0.34
18.02	0.99	22120.00	374.15	0.26	0.34

Tube Side - Mixed Liquid

Mass Flow (kg/h)	Density (kg/m3)	Mass Sp Heat (kJ/kg-C)	Viscosity (cP)	Thermal Cond (W/m-K)	Surface Tens (dyne/cm)
4542.79	1002.05	4.31	0.76	0.62	---
4542.79	989.02	4.32	0.55	0.64	---
Molecular Wt	Sp Gravity	Pseudo Pc (kPa)	Pseudo Tc (C)	Pseudo Zc	Pseudo Omega
18.02	1.00	22120.00	374.15	0.26	0.34
18.02	0.99	22120.00	374.15	0.26	0.34

HTFS

Exchanger Design and Rating

E-102 (Heat Exchanger): Design, Rating, Details, Tables, HTFS Results, Exchanger Design and Rating

Heat Exchanger: E-102

CONNECTIONS

Tube Side	Shell Side		
Inlet	Outlet	Inlet	Outlet
Name CW 2nd Stage Name	CW Out 2nd Stage Name	Compressed 2nd Stage Name	Cooled 2nd Stage
From Op.	To Op.	From Op. C-102	To Op. C-103
Op. Type	Op. Type	Op. Type Compressor	Op. Type Compressor
Temp 32.00 C	Temp 49.00 C	Temp 148.89 C	Temp 50.00 C
PARAMETERS			

Heat Exchanger Model: Simple End Point

Tube Side DeltaP: 0.0000 kPa Shell Side DeltaP: 62.00 kPa Passes: ---

 UA: 8388 kJ/C-h Tolerance: 1.0000e-04

Tube Side Data	Shell Side Data
Heat Transfer Coeff ---	Heat Transfer Coeff ---
Tube Pressure Drop 0.00 kPa	Shell Pressure Drop 62.00 kPa
Fouling 0.00000 C-h-m ² /kJ	Fouling 0.00000 C-h-m ² /kJ
Tube Length 6.00 m	Shell Passes 1
Tube O.D. 20.00 mm	Shell Series 1
Tube Thickness 2.0000 mm	Shell Parallel 1
Tube Pitch 50.0000 mm	Baffle Type Single
Orientation Horizontal	Baffle Cut(% Area) 20.00
Passes Per Shell 2	Baffle Orientation Horizontal
Tubes Per Shell 160	Spacing 800.0000 mm
Layout Angle Triangular (30 degrees)	Diameter 739.0488 mm
TEMA Type A E L	Area 60.32 m ²
SPECs	

	Spec	Value	Curr	Value	Rel Error	Active	Estimate	
E-102	Heat Balance	0.0000	kJ/h	-2.604e-008	kJ/h	-7.793e-014	On	Off
E-102	UA	---		8388	kJ/C-h	---	On	Off
Detailed Specifications								

E-102 Heat Balance
Type: Duty Pass: Error Spec Value: 0.0000 kJ/h
E-102 UA
Type: UA Pass: Overall Spec Value: ---
User Variables

RATING

Sizing

Overall Data Configuration
of Shells in Series 1 Tube Passes per Shell 2 Elevation (Base) 0.0000 m
of Shells in Parallel 1 Exchange Orientation Horizontal First Tube Pass Flow Direction Counter
TEMA Type: A E L

Calculated Information
 Shell HT Coeff ---
 Overall U 139.1 kJ/h-m²-C
 Shell DP 62.000 kPa
 Shell Vol per Shell 2.272 m³
 HT A = 1.000000
 Shl 60.000000

of Tubes per Shell 160 Tube Layout Angle Triangular (30 degrees)

Shell Baffles
Shell Baffle Type Single Shell Baffle Oriented

Baffle Cut (% Area) 20.00 Baffle Spacing 800.0 mm
Tube Data
Dimensions

Dimensions OD 20.00 ID 16.00 Tube Thickness 2.000 Tube Length 6.000
(mm) (mm) (mm) (m)

Tube Properties

Tube Fouling 0.0000 Thermal Cond. 45.00 Wall Cp --- Wall D

(C-h-m2/kJ) (W/m-K) (kJ/kg-C) (kg/m3)
 - - - - -
 - - - - -

Nozzle Parameters

Base Elevation Relative to Ground Level 0.0000 m

CW 2nd Stage Compressed 2nd Stage CW Out 2nd Stage

Diameter (m) 5.000e-002 5.000e-002 5.000e-002

Elevation (Base) (m) 0.0000 0.0000 0.0000

Elevation (Ground) (m) 0.0000 0.0000 0.0000

Elevation (% of Height) (%) 0.00
Cooled 2nd Stage

Diameter (m) Cooled 2nd Stage 5.000e-002

Diameter (in) 3.0000002

Elevation (Base) (m) 0.0000
Elevation (Ground) (m) 0.0000
Elevation (% of Height) (%) 0.00

DETAILS

Overall/Detailed Performance

Duty: 3.341e+05 kJ/h	UA Curv. Error: 0.00e-01 kJ/C-h
Heat Leak: 0.000e-01 kJ/h	Hot Pinch Temp: 50.00 C
Heat Loss: 0.000e-01 kJ/h	Cold Pinch Temp: 32.00 C
UA: 8.388e+03 kJ/C-h	Ft Factor: ---
Min. Approach: 18.00 C	Uncorrected Lmtd: 47.81 C
Lmtd: 39.83 C	

TABLES

Shell Side - Overall Phase

Temperature (C)	Pressure (kPa)	Heat Flow (kJ/h)	Enthalpy (kJ/kgmole)
50.00	482.90	0.00	-878.12
148.89	544.90	334138.74	2063.24
UA (kJ/C-h)	Molar Vap Frac	Mass Vap Frac	Heat of Vap. (kJ/kgmole)
0.00	1.0000	1.0000	---
0.00	1.0000	1.0000	---

Shell Side - Vapour Phase

Mass Flow (kg/h)	Molecular Wt	Density (kg/m3)	Mass Sp Heat (kJ/kg-C)	Viscosity (cP)	Thermal Cond (W/m-K)
3292.79	28.99	5.22	1.02	0.02	0.03
3292.79	28.99	4.50	1.04	0.02	0.03
Std Gas Flow (STD_m3/h)	Z Factor	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega
2686.01	1.00	3773.07	-140.10	0.29	0.04
2686.01	1.00	3773.07	-140.10	0.29	0.04

Tube Side - Overall Phase

Temperature (C)	Pressure (kPa)	Heat Flow (kJ/h)	Enthalpy (kJ/kgmole)
32.00	101.30	0.00	-285676.72
49.00	101.30	334138.74	-284354.80
UA (kJ/C-h)	Molar Vap Frac	Mass Vap Frac	Heat of Vap. (kJ/kgmole)
0.00	0.0000	0.0000	---
0.00	0.0000	0.0000	---

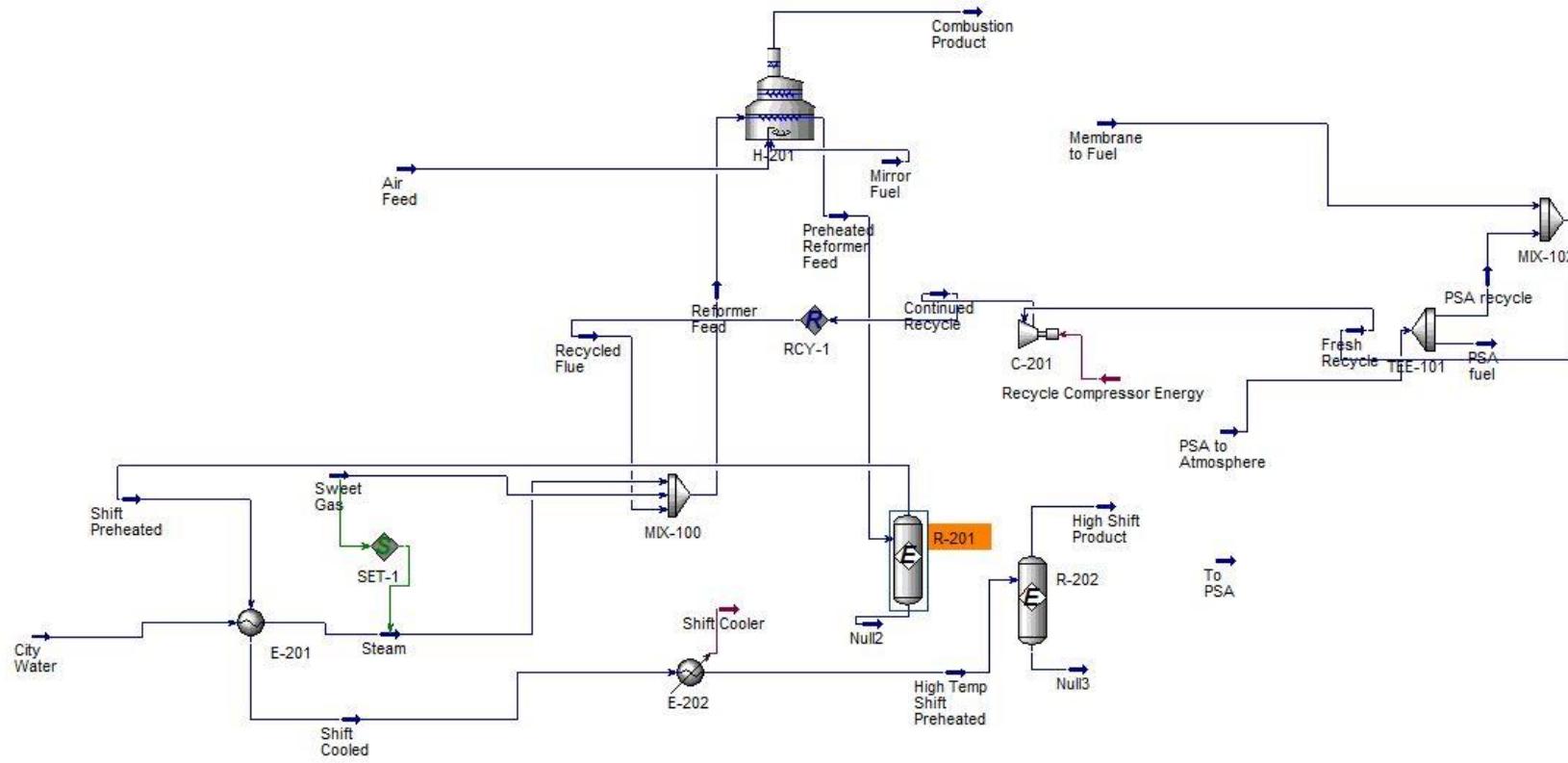
Tube Side - Heavy Liquid Phase

Mass Flow (kg/h)	Density (kg/m3)	Mass Sp Heat (kJ/kg-C)	Viscosity (cP)	Thermal Cond (W/m-K)	Surface Tens (dyne/cm)
4553.66	1002.05	4.31	0.76	0.62	70.89
4553.66	989.02	4.32	0.55	0.64	67.91
Molecular Wt Sp (kPa)	Gravity (C)	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega
18.02	1.00	22120.00	374.15	0.26	0.34
18.02	0.99	22120.00	374.15	0.26	0.34

Tube Side - Mixed Liquid

Mass Flow (kg/h)	Density (kg/m3)	Mass Sp Heat (kJ/kg-C)	Viscosity (cP)	Thermal Cond (W/m-K)	Surface Tens (dyne/cm)
4553.66	1002.05	4.31	0.76	0.62	---
4553.66	989.02	4.32	0.55	0.64	---
Molecular Wt Sp (kPa)	Gravity (C)	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega
18.02	1.00	22120.00	374.15	0.26	0.34
18.02	0.99	22120.00	374.15	0.26	0.34

HTFS



```
*****
***** INPUT SUMMARY *****
*****
```

FLUID PACKAGE: Basis-1(Peng-Robinson)

Property Package Type: PengRob

Component List - 1: Methane /Hydrogen /H2O /CO2 /CO /S_Rhombic /H2S /Propane /Ethane /Oxygen /Nitrogen /

Reaction Set: Reforming Set

Reaction 'Methane to Hydrogen':

Reactants: Methane, Stoich Coeff -1 / H2O, Stoich Coeff -1 / CO, Stoich Coeff 1 / Hydrogen, Stoich Coeff 3 /

Basis Data: Basis = Activity / Phase = VapourPhase /

Reaction 'Water Gas Shift':

Reactants: CO, Stoich Coeff -1 / H2O, Stoich Coeff -1 / CO2, Stoich Coeff 1 / Hydrogen, Stoich Coeff 1 /

Basis Data: Basis = Activity / Phase = VapourPhase /

Reaction Set: Water Gas Shift Set

Reaction 'Rxn-1':

Reactants: CO, Stoich Coeff -1 / H2O, Stoich Coeff -1 / CO2, Stoich Coeff 1 / Hydrogen, Stoich Coeff 1 /

Basis Data: Basis = Activity / Phase = VapourPhase /

Reaction Set: Hydrodesulfurization Set

Reaction 'S to H2S':

Reactants: Hydrogen, Stoich Coeff -1 / S_Rhombic, Stoich Coeff -1 / H2S, Stoich Coeff 1 /

Basis Data: Component = Hydrogen / Phase = Overall /

FLOWSCHEET: Main

Fluid Package: Basis-1

STREAM: Sweet Gas (Material Stream)

Vapour Fraction = 1
Pressure = 435.1131 psia
Molar Flow = 178.5726 lbmole/hr
Composition Basis (In Mole Fractions):Methane = 0.9/ Hydrogen = 0/ H2O = 0/
CO2 = 0/ CO = 0/ S_Rhombic = 0/ H2S = 0/ Propane = 0/ Ethane = 0.1/ Oxygen = 0/ Nitrogen = 0/

UNIT OPERATION: R-201 (Equilibrium Reactor)

Feed Stream = Preheated Reformer Feed
Vapour Product = Shift Preheated
Liquid Product = Null2
Reaction Set=Reforming Set
Delta P = 127.053025 psi

UNIT OPERATION: R-202 (Equilibrium Reactor)

Feed Stream = High Temp Shift Preheated
Vapour Product = High Shift Product
Liquid Product = Null3
Reaction Set=Water Gas Shift Set

STREAM: City Water (Material Stream)

Temperature = 90 F
Pressure = 14.692319 psia
Composition Basis (In Mole Fractions):Methane = 0/ Hydrogen = 0/ H2O = 1/ CO2 = 0/ CO = 0/ S_Rhombic = 0/ H2S = 0/ Propane = 0/ Ethane = 0/ Oxygen = 0/ Nitrogen = 0/

STREAM: Steam (Material Stream)

Vapour Fraction = 1
Pressure = 435.1131 psia

UNIT OPERATION: SET-1 (Set)

Target Object = Steam
Source Object = Sweet Gas
Target Variable = Molar Flow
Multiplier = 2

STREAM: Null2 (Material Stream)

STREAM: Null3 (Material Stream)

UNIT OPERATION: RCY-1 (Recycle)

Inlet Stream = Continued Recycle
Output Stream = Recycled Flue

STREAM: Recycled Flue (Material Stream)

Temperature = 643.613778 F
Pressure = 435.1131 psia
Molar Flow = 437.385365 lbmole/hr
Composition Basis (In Mole Fractions):Methane = 0.107687957/ Hydrogen =

0.174322542/ H2O = 0.199147419/ CO2 = 0.428045573/ CO = 0.00936779342/ S_Rhombic = 0/ H2S = 0/ Propane = 0/ Ethane = 0.0814287157/ Oxygen = 0/ Nitrogen = 0/
 STREAM: High Shift Product (Material Stream)
 STREAM: High Temp Shift Preheated (Material Stream)
 Temperature = 482 F
 STREAM: Continued Recycle (Material Stream)
 Pressure = 435.1131 psia
 UNIT OPERATION: MIX-100 (Mixer)
 Feed Stream = Steam
 Feed Stream = Sweet Gas
 Feed Stream = Recycled Flue
 Product Stream = Reformer Feed
 UseTrivialSolution = True
 STREAM: Reformer Feed (Material Stream)
 STREAM: Preheated Reformer Feed (Material Stream)
 Temperature = 1472 F
 STREAM: Shift Preheated (Material Stream)
 UNIT OPERATION: E-201 (Heat Exchanger)
 TubeInletStream = City Water
 TubeOutletStream = Steam
 ShellInletStream = Shift Preheated
 ShellOutletStream = Shift Cooled
 TubeOuterDiameter = 0.787401575 in
 TubeInnerDiameter = 0.62992126 in
 TubeThickness = FEMPTY in
 HCurveName = City Water-Steam
 HCurveName = Shift Preheated-Shift Cooled
 ShellPressureDrop = 8.9923374 psi
 STREAM: Shift Cooled (Material Stream)
 UNIT OPERATION: H-201 (Fired Heater)
 Radiant Zone Inlet = Reformer Feed
 Radiant Zone Outlet = Preheated Reformer Feed
 Fuel Feed = Mirror Fuel
 Air Feed = Air Feed
 Combustion Product = Combustion Product
 CombustionEfficiency = 75 %
 ExcessAirPercent = 15 %
 ConvZoneNumberOfExternalPasses = 0
 EconZoneNumberOfExternalPasses = 0
 SSModel = Simple fired heater
 STREAM: Air Feed (Material Stream)
 Temperature = 77 F
 Pressure = 14.692319 psia
 Composition Basis (In Mole Fractions):Methane = 0/ Hydrogen = 0/ H2O = 0/ CO2 = 0/ CO = 0/ S_Rhombic = 0/ H2S = 0/ Propane = 0/ Ethane = 0/ Oxygen = 0.79/
 Nitrogen = 0.21/
 STREAM: Combustion Product (Material Stream)
 UNIT OPERATION: E-202 (Cooler)
 Feed Stream = Shift Cooled
 Product Stream = High Temp Shift Preheated
 Energy Stream = Shift Cooler
 Pressure Drop = 8.9923374 psi
 STREAM: Shift Cooler (Energy Stream)
 STREAM: PSA to Atmosphere (Material Stream)
 Temperature = 527 F
 Pressure = 275.57163 psia
 Molar Flow = 390.2142 lbmole/hr
 Composition Basis (In Mole Fractions):Methane = 0.1387874/ Hydrogen = 0.06803645/ H2O = 0.40710572/ CO2 = 0.30769957/ CO = 0.0258849485/ S_Rhombic = 0/ H2S = 0/ Propane = 0/ Ethane = 0.0524859119/ Oxygen = 0/ Nitrogen = 0/
 UNIT OPERATION: C-201 (Compressor)
 Feed Stream = Fresh Recycle
 Product Stream = Continued Recycle
 Energy Stream = Recycle Compressor Energy
 CurveCollectionName = CC-0
 SelectedCurveCollection = True
 NumberOfCurves = 0
 NumberOfCurves = 0
 NumberOfCurves = 0
 EffCurveType = 0
 NumberOfCurves = 0
 STREAM: Fresh Recycle (Material Stream)

STREAM: Recycle Compressor Energy (Energy Stream)
Vapour Fraction = 1
Temperature = 527 F
Pressure = 290.0754 psia
Molar Flow = 279.095085 lbmole/hr
Composition Basis (In Mole Flows):Methane = 25.13244/ Hydrogen = 65.47662/ H2O = 22.663288/ CO2 = 138.515018/ CO = 0/ S_Rhombic = 0/ H2S = 0/ Propane = 0/
Ethane = 27.3077188/ Oxygen = 0/ Nitrogen = 0/
STREAM: To PSA (Material Stream)
Temperature = 543.5 F
Pressure = 290.0754 psia
Molar Flow = 798.17543 lbmole/hr
Composition Basis (In Mole Flows):Methane = 3.990326/ Hydrogen = 582.67578/ H2O = 207.518998/ CO2 = 3.990326/ CO = 0/ S_Rhombic = 0/ H2S = 0/ Propane = 0/
Ethane = 0/ Oxygen = 0/ Nitrogen = 0/
STREAM: Mirror Fuel (Material Stream)
Temperature = 527 F
Pressure = 275.57163 psia
Composition Basis (In Mole Flows):Methane = 26.0667734/ Hydrogen = 46.9046709/ H2O = 43.4934221/ CO2 = 111.149856/ CO = 1.83354623/ S_Rhombic = 0/ H2S = 0/
Propane = 0/ Ethane = 3.72963201/ Oxygen = 0/ Nitrogen = 0/
UNIT OPERATION: MIX-102 (Mixer)
Feed Stream = Membrane to Fuel
Feed Stream = PSA recycle
Product Stream = Fresh Recycle
UseTrivialSolution = True
UNIT OPERATION: TEE-101 (Tee)
Feed Stream = PSA to Atmosphere
Product Stream = PSA recycleProduct Stream = PSA fuel
STREAM: PSA recycle (Material Stream)
STREAM: PSA fuel (Material Stream)
Molar Flow = 233.24668 lbmole/hr

OUTPUT SUMMARY

OKLAHOMA STATE UNIVERSIT Case Name: Hydrogen Production Final.hsc
Bedford, MA
USA Unit Set: Field

Date/Time: Wed Apr 01 17:55:20 2020

Basis-1 (Fluid Package): Component List

Fluid Package: Basis-1						
COMPONENT LIST						
COMPONENT	TYPE	MOLECULAR	BOILING PT	IDEAL LIQ	CRITICAL	
	WEIGHT	(F)	DENSITY	(lb/ft ³)	TEMP (F)	
Methane	Pure	16.04	-258.7	18.69	-116.4	
Hydrogen	Pure	2.016	-422.7	4.361	-399.5	
H2O	Pure	18.02	212.0	62.30	705.5	
CO2	Pure	44.01	-109.4	51.52	87.71	
CO	Pure	28.01	-312.6	49.90	-220.4	
S_Rhombic	Pure	32.07	---	129.2	---	
H2S	Pure	34.08	-75.37	49.22	212.8	
Propane	Pure	44.10	-43.78	31.63	206.1	
Ethane	Pure	30.07	-127.5	22.20	90.10	
Oxygen	Pure	32.00	-297.3	71.02	-181.1	
Nitrogen	Pure	28.01	-320.4	50.34	-232.5	

(Continued..) Component List - 1 [HYSYS Databanks]

COMPONENT	CRITICAL PRES	CRITICAL VOL	ACENTRICITY	HEAT OF FORM
	(psia)	(ft ³ /lbmole)	(Btu/lbmole)	
Methane	673.1	1.586	1.150e-002	-3.220e+004
Hydrogen	190.8	0.8250	-0.1201	0.0000
H2O	3208	0.9147	0.3440	-1.040e+005
CO2	1069	1.504	0.2389	-1.693e+005
CO	507.5	1.430	9.300e-002	-4.755e+004
S_Rhombic	---	---	---	1.192e+005
H2S	1306	1.570	8.100e-002	-8675
Propane	617.4	3.204	0.1524	-4.466e+004
Ethane	708.3	2.371	9.860e-002	-3.643e+004
Oxygen	736.8	1.173	1.900e-002	0.0000
Nitrogen	492.3	1.442	4.000e-002	0.0000

Case (Simulation Case): Mass and Energy Balance, Utility Balance, Process CO2 Emissions

Simulation Case: Case

OVERALL MASS BALANCE

In Stream	Count	Mass Flow (lb/hr)	Out Stream	Count	Mass Flow (lb/hr)
Sweet Gas	Yes	3115	Null2	Yes	0.0000
City Water	Yes	6434	Null3	Yes	0.0000
Air Feed	Yes	4063	High Shift Product	Yes	2.145e+004
Mirror Fuel	Yes	6351	Combustion Product	Yes	1.041e+004
Membrane to Fuel	Yes	7861	PSA fuel	Yes	5958
PSA to Atmosphere	Yes	9967			
Total In MassFlow (lb/hr)		3.779e+004	Total Out MassFlow (lb/hr)		3.782e+004
Mass Imbalance (lb/hr)		33.81	Rel Mass Imbalance Pct (%)		0.09

OVERALL ENERGY BALANCE

InStream	Count	Energy Flow (Btu/hr)	OutStream	Count	Energy Flow (Btu/hr)
Sweet Gas	Yes	-6.186e+06	Null2	Yes	0.000e-01
City Water	Yes	-4.386e+07	Null3	Yes	0.000e-01
Air Feed	Yes	-5.161e+02	High Shift Product	Yes	-7.970e+07
Mirror Fuel	Yes	-2.346e+07	Combustion Product	Yes	-3.545e+07
Recycle Compressor Energy	Yes	5.396e+05	Shift Cooler	Yes	2.734e+05
Membrane to Fuel	Yes	-2.641e+07	PSA fuel	Yes	-2.285e+07
PSA to Atmosphere	Yes	-3.823e+07			
Total In EnergyFlow (Btu/hr)		-1.376e+008	Total Out EnergyFlow (Btu/hr)		-1.377e+008
Energy Imbalance (Btu/hr)		-1.274e+005	Rel Energy Imbalance Pct (%)		0.09

OVERALL UTILITY BALANCE

PROCESS CO2 EMISSIONS

Inlet Stream	Count	IFPP (1995) (lb/hr)	IFPP (2007) (lb/hr)	EPA (2009) (lb/hr)
Sweet Gas	Yes	5.415e+04	6.446e+04	5.415e+04
City Water	Yes	0.000e-01	0.000e-01	0.000e-01
Air Feed	Yes	0.000e-01	0.000e-01	0.000e-01
Mirror Fuel	Yes	1.367e+04	1.535e+04	1.367e+04
Membrane to Fuel	Yes	1.456e+04	1.618e+04	1.456e+04
PSA to Atmosphere	Yes	2.353e+04	2.700e+04	2.353e+04
Total from Inlets		1.059e+05	1.230e+05	1.059e+05
Total Carbon Fees from Inlets (Cost/hr)		0.000e-01	0.000e-01	0.000e-01
Outlet Stream	Count	IFPP (1995) (lb/hr)	IFPP (2007) (lb/hr)	EPA (2009) (lb/hr)
Null2	Yes	0.000e-01	0.000e-01	0.000e-01
Null3	Yes	0.000e-01	0.000e-01	0.000e-01
High Shift Product	Yes	6.711e+04	7.799e+04	6.711e+04
Combustion Product	Yes	6.448e+03	6.448e+03	6.448e+03
PSA fuel	Yes	1.406e+04	1.614e+04	1.406e+04
Total from Outlets		8.762e+04	1.006e+05	8.762e+04
Total Carbon Fees from Outlets (Cost/hr)		0.000e-01	0.000e-01	0.000e-01

Sweet Gas (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Sweet Gas Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH. LIQUID PH.

Vapour / Phase Fraction	1.0000	1.0000	0.0000
Temperature: (F)	-90.05	-90.05	-90.05
Pressure: (psia)	435.1	435.1	435.1
Molar Flow (lbmole/hr)	178.6	178.6	0.0000
Mass Flow (lb/hr)	3115	3115	0.0000
Std Ideal Liq VolFlow (barrel/day)	693.1	693.1	0.0000
Molar Enthalpy (Btu/lbmole)	-3.464e+04	-3.464e+04	-4.016e+04
Molar Entropy (Btu/lbmole-F)	3.377e+01	3.377e+01	2.674e+01
Heat Flow (Btu/hr)	-6.186e+06	-6.186e+06	0.000e-01
Liq VolFlow @Std Cond (barrel/day)	2.882e+005	2.882e+005	0.0000

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS	MOLE FLOW (lbmole/hr)	MOLE FRAC (lb/hr)	MASS FLOW (barrel/day)	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
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Methane	160.7	0.9000	2578	0.8276	589.7	0.8508
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO2	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	17.86	0.1000	537.0	0.1724	103.4	0.1492
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	178.6	1.0000	3115	1.0000	693.1	1.0000
Vapour Phase					Phase Fraction	1.000
COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	160.7	0.9000	2578	0.8276	589.7	0.8508
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO2	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	17.86	0.1000	537.0	0.1724	103.4	0.1492
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	178.6	1.0000	3115	1.0000	693.1	1.0000
Liquid Phase					Phase Fraction	0.0000
COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	0.0000	0.5001	0.0000	0.3480	0.0000	0.3881
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO2	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	0.0000	0.4999	0.0000	0.6520	0.0000	0.6119
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000

City Water (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: City Water Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL AQUEOUS PH.

Vapour / Phase Fraction 0.0000 1.0000

Temperature: (F) 90.00 90.00

Pressure: (psia) 14.69 14.69

Molar Flow (lbmole/hr) 357.1 357.1

Mass Flow (lb/hr) 6434 6434

Std Ideal Liq VolFlow (barrel/day) 441.4 441.4

Molar Enthalpy (Btu/lbmole) -1.228e+05 -1.228e+05

Molar Entropy (Btu/lbmole-F) 1.327e+01 1.327e+01

Heat Flow (Btu/hr) -4.386e+07 -4.386e+07

Liq VolFlow @Std Cond (barrel/day) 434.1 434.1

COMPOSITION

Overall Phase Vapour Fraction 0.0000

COMPONENTS MOLE FLOW

MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

(lbmole/hr) (lb/hr) (barrel/day)

Methane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

Hydrogen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

H2O 357.1 1.0000 6434 1.0000 441.4 1.0000

CO2 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

CO 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

S_Rhombic 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

H2S 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

Propane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

Ethane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	357.1	1.0000	6434	1.0000	441.4	1.0000
Aqueous Phase					Phase Fraction	1.000
COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ O	357.1	1.0000	6434	1.0000	441.4	1.0000
CO ₂	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	357.1	1.0000	6434	1.0000	441.4	1.0000

Steam (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Steam Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH. AQUEOUS PH.

Vapour / Phase Fraction	1.0000	1.0000	0.0000
Temperature: (F)	454.2	454.2	454.2
Pressure: (psia)	435.1	435.1	435.1
Molar Flow (lbmole/hr)	357.1	357.1	0.0000
Mass Flow (lb/hr)	6434	6434	0.0000
Std Ideal Liq VolFlow (barrel/day)	441.4	441.4	0.0000
Molar Enthalpy (Btu/lbmole)	-1.015e+05	-1.015e+05	-1.156e+05
Molar Entropy (Btu/lbmole-F)	3.866e+01	3.866e+01	2.321e+01
Heat Flow (Btu/hr)	-3.625e+07	-3.625e+07	0.000e-01
Liq VolFlow @Std Cond (barrel/day)	434.1	434.1	0.0000

COMPOSITION

Overall Phase	Vapour Fraction	1.0000
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COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	
H ₂ O	357.1	1.0000	6434	1.0000	441.4	1.0000
CO ₂	0.0000	0.0000	0.0000	0.0000	0.0000	
CO	0.0000	0.0000	0.0000	0.0000	0.0000	
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	
H ₂ S	0.0000	0.0000	0.0000	0.0000	0.0000	
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	
Ethane	0.0000	0.0000	0.0000	0.0000	0.0000	
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	
Total	357.1	1.0000	6434	1.0000	441.4	1.0000

Vapour Phase	Phase Fraction	1.000
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COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	
H ₂ O	357.1	1.0000	6434	1.0000	441.4	1.0000
CO ₂	0.0000	0.0000	0.0000	0.0000	0.0000	
CO	0.0000	0.0000	0.0000	0.0000	0.0000	
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	
H ₂ S	0.0000	0.0000	0.0000	0.0000	0.0000	
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	
Ethane	0.0000	0.0000	0.0000	0.0000	0.0000	
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	
Total	357.1	1.0000	6434	1.0000	441.4	1.0000

Aqueous Phase	Phase Fraction	0.0000
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COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
(lbmole/hr)	(lb/hr)	(barrel/day)			
Methane	0.0000	0.0000	0.0000	0.0000	0.0000
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ O	0.0000	1.0000	0.0000	1.0000	0.0000

CO2	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000

Null2 (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Null2		Fluid Package: Basis-1				
		Property Package: Peng-Robinson				
CONDITIONS						
OVERALL VAPOUR PH. AQUEOUS PH.						
Vapour / Phase Fraction	0.0000	0.0000	1.0000			
Temperature: (F)	1178	1178	1178			
Pressure: (psia)	308.1	308.1	308.1			
Molar Flow (lbmole/hr)	0.0000	0.0000	0.0000			
Mass Flow (lb/hr)	0.0000	0.0000	0.0000			
Std Ideal Liq VolFlow (barrel/day)	0.0000	0.0000	0.0000			
Molar Enthalpy (Btu/lbmole)	-6.842e+04	-6.842e+04	-6.842e+04			
Molar Entropy (Btu/lbmole-F)	4.757e+01	4.757e+01	4.757e+01			
Heat Flow (Btu/hr)	0.000e-01	0.000e-01	0.000e-01			
Liq VolFlow @Std Cond (barrel/day)	0.0000	0.0000	0.0000			
COMPOSITION						
Overall Phase	Vapour Fraction 0.0000					
COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	0.0000	0.1615	0.0000	0.1268	0.0000	0.2393
Hydrogen	0.0000	0.1836	0.0000	0.0181	0.0000	0.1465
H2O	0.0000	0.3851	0.0000	0.3395	0.0000	0.1922
CO2	0.0000	0.1800	0.0000	0.3876	0.0000	0.2654
CO	0.0000	0.0387	0.0000	0.0531	0.0000	0.0375
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	0.0000	0.0509	0.0000	0.0750	0.0000	0.1191
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000
Vapour Phase	Phase Fraction 0.0000					
COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	0.0000	0.1615	0.0000	0.1268	0.0000	0.2393
Hydrogen	0.0000	0.1836	0.0000	0.0181	0.0000	0.1465
H2O	0.0000	0.3852	0.0000	0.3395	0.0000	0.1922
CO2	0.0000	0.1800	0.0000	0.3876	0.0000	0.2654
CO	0.0000	0.0387	0.0000	0.0531	0.0000	0.0375
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	0.0000	0.0509	0.0000	0.0750	0.0000	0.1191
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000
Aqueous Phase	Phase Fraction 1.000					
COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	0.0000	0.1615	0.0000	0.1268	0.0000	0.2393
Hydrogen	0.0000	0.1836	0.0000	0.0181	0.0000	0.1465
H2O	0.0000	0.3851	0.0000	0.3395	0.0000	0.1922
CO2	0.0000	0.1800	0.0000	0.3876	0.0000	0.2654
CO	0.0000	0.0387	0.0000	0.0531	0.0000	0.0375
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	0.0000	0.0509	0.0000	0.0750	0.0000	0.1191
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000

Null3 (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Null3 Fluid Package: Basis-1
 Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH. AQUEOUS PH.

Vapour / Phase Fraction	0.0000	0.0000	1.0000
Temperature: (F)	543.5	543.5	543.5
Pressure: (psia)	290.1	290.1	290.1
Molar Flow (lbmole/hr)	0.0000	0.0000	0.0000
Mass Flow (lb/hr)	0.0000	0.0000	0.0000
Std Ideal Liq VolFlow (barrel/day)	0.0000	0.0000	0.0000
Molar Enthalpy (Btu/lbmole)	-1.132e+05	-7.593e+04	-1.132e+05
Molar Entropy (Btu/lbmole-F)	2.584e+01	4.197e+01	2.584e+01
Heat Flow (Btu/hr)	0.000e-01	0.000e-01	0.000e-01
Liq VolFlow @Std Cond (barrel/day)	0.0000	0.0000	0.0000

COMPOSITION

Overall Phase	Vapour Fraction 0.0000					
COMPONENTS	MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	
(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	0.0000	0.0012	0.0000	0.0010	0.0000	0.0034
Hydrogen	0.0000	0.0043	0.0000	0.0005	0.0000	0.0067
H ₂ O	0.0000	0.9839	0.0000	0.9729	0.0000	0.9590
CO ₂	0.0000	0.0104	0.0000	0.0252	0.0000	0.0300
CO	0.0000	0.0000	0.0000	0.0001	0.0000	0.0001
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	0.0000	0.0002	0.0000	0.0003	0.0000	0.0009
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000

Vapour Phase Phase Fraction 0.0000 COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW

LIQVOL FRAC

(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	0.0000	0.1615	0.0000	0.1268	0.0000	0.2325
Hydrogen	0.0000	0.2198	0.0000	0.0217	0.0000	0.1704
H ₂ O	0.0000	0.3490	0.0000	0.3076	0.0000	0.1693
CO ₂	0.0000	0.2162	0.0000	0.4654	0.0000	0.3097
CO	0.0000	0.0026	0.0000	0.0035	0.0000	0.0024
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	0.0000	0.0509	0.0000	0.0750	0.0000	0.1157
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000

Aqueous Phase Phase Fraction 1.0000

COMPONENTS	MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	0.0000	0.0012	0.0000	0.0010	0.0000	0.0034
Hydrogen	0.0000	0.0043	0.0000	0.0005	0.0000	0.0067
H ₂ O	0.0000	0.9839	0.0000	0.9729	0.0000	0.9590
CO ₂	0.0000	0.0104	0.0000	0.0252	0.0000	0.0300
CO	0.0000	0.0000	0.0000	0.0001	0.0000	0.0001
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	0.0000	0.0509	0.0000	0.0750	0.0000	0.1157
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000

Recycled Flue (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Recycled Flue Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction	1.0000	1.0000
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Temperature: (F)	643.6	643.6
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Pressure: (psia)	435.1	435.1
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Molar Flow (lbmole/hr)	437.4	437.4
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Mass Flow (lb/hr)	1.190e+004	1.190e+004
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Std Ideal Liq VolFlow (barrel/day)	1331	1331
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Molar Enthalpy (Btu/lbmole) -9.459e+04 -9.459e+04
 Molar Entropy (Btu/lbmole-F) 4.300e+01 4.300e+01
 Heat Flow (Btu/hr) -4.137e+07 -4.137e+07
 Liq VolFlow @Std Cond (barrel/day) 7.044e+005 7.044e+005
COMPOSITION
 Overall Phase Vapour Fraction 1.0000
 COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (lbmole/hr) (lb/hr) (barrel/day)
 Methane 47.10 0.1077 755.6 0.0635 172.8 0.1299
 Hydrogen 76.25 0.1743 153.7 0.0129 150.7 0.1132
 H₂O 87.10 0.1991 1569 0.1318 107.7 0.0809
 CO₂ 187.2 0.4280 8240 0.6922 683.6 0.5137
 CO 4.097 0.0094 114.8 0.0096 9.831 0.0074
 S_Rhombic 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 H₂S 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Propane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Ethane 35.62 0.0814 1071 0.0900 206.2 0.1549
 Oxygen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Nitrogen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Total 437.4 1.0000 1.190e+004 1.0000 1331 1.0000
 Vapour Phase Phase Fraction 1.000
 COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (lbmole/hr) (lb/hr) (barrel/day)
 Methane 47.10 0.1077 755.6 0.0635 172.8 0.1299
 Hydrogen 76.25 0.1743 153.7 0.0129 150.7 0.1132
 H₂O 87.10 0.1991 1569 0.1318 107.7 0.0809
 CO₂ 187.2 0.4280 8240 0.6922 683.6 0.5137
 CO 4.097 0.0094 114.8 0.0096 9.831 0.0074
 S_Rhombic 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 H₂S 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Propane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Ethane 35.62 0.0814 1071 0.0900 206.2 0.1549
 Oxygen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Nitrogen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Total 437.4 1.0000 1.190e+004 1.0000 1331 1.0000

High Shift Product (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: High Shift Product Fluid Package: Basis-1
Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH. AQUEOUS PH.

Vapour / Phase Fraction 1.0000 1.0000 0.0000
 Temperature: (F) 543.5 543.5 543.5
 Pressure: (psia) 290.1 290.1 290.1
 Molar Flow (lbmole/hr) 1050 1050 0.0000
 Mass Flow (lb/hr) 2.145e+004 2.145e+004 0.0000
 Std Ideal Liq VolFlow (barrel/day) 2675 2675 0.0000
 Molar Enthalpy (Btu/lbmole) -7.593e+04 -7.593e+04 -1.132e+05
 Molar Entropy (Btu/lbmole-F) 4.197e+01 4.197e+01 2.584e+01
 Heat Flow (Btu/hr) -7.970e+07 -7.970e+07 0.0000e-01
 Liq VolFlow @Std Cond (barrel/day) 3289 3289 0.0000

COMPOSITION

Overall Phase Vapour Fraction 1.0000
 COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (lbmole/hr) (lb/hr) (barrel/day)
 Methane 169.6 0.1615 2720 0.1268 622.1 0.2325
 Hydrogen 230.7 0.2198 465.1 0.0217 455.9 0.1704
 H₂O 366.3 0.3490 6599 0.3076 452.8 0.1693
 CO₂ 226.9 0.2162 9985 0.4654 828.4 0.3097
 CO 2.693 0.0026 75.44 0.0035 6.462 0.0024
 S_Rhombic 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 H₂S 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Propane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Ethane 53.47 0.0509 1608 0.0750 309.5 0.1157
 Oxygen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Nitrogen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Total 1050 1.0000 2.145e+004 1.0000 2675 1.0000
 Vapour Phase Phase Fraction 1.000
 COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (lbmole/hr) (lb/hr) (barrel/day)
 Methane 169.6 0.1615 2720 0.1268 622.1 0.2325
 Hydrogen 230.7 0.2198 465.1 0.0217 455.9 0.1704
 H₂O 366.3 0.3490 6599 0.3076 452.8 0.1693

CO2	226.9	0.2162	9985	0.4654	828.4	0.3097
CO	2.693	0.0026	75.44	0.0035	6.462	0.0024
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	53.47	0.0509	1608	0.0750	309.5	0.1157
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	1050	1.0000	2.145e+004	1.0000	2675	1.0000
Aqueous Phase			Phase Fraction	0.0000		
COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	0.0000	0.0012	0.0000	0.0010	0.0000	0.0034
Hydrogen	0.0000	0.0043	0.0000	0.0005	0.0000	0.0067
H2O	0.0000	0.9839	0.0000	0.9729	0.0000	0.9590
CO2	0.0000	0.0104	0.0000	0.0252	0.0000	0.0300
CO	0.0000	0.0000	0.0000	0.0001	0.0000	0.0001
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	0.0000	0.0002	0.0000	0.0003	0.0000	0.0009
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000

High Temp Shift Preheated (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: High Temp Shift Preheated Fluid Package: Basis-1
Property Package: Peng-Robinson

OVERALL VAPOUR PH.

Vapour / Phase Fraction	1.0000	1.0000				
Temperature: (F)	482.0	482.0				
Pressure: (psia)	290.1	290.1				
Molar Flow (lbmole/hr)	1050	1050				
Mass Flow (lb/hr)	2.145e+004	2.145e+004				
Std Ideal Liq VolFlow (barrel/day)	2600	2600				
Molar Enthalpy (Btu/lbmole)	-7.593e+04	-7.593e+04				
Molar Entropy (Btu/lbmole-F)	4.176e+01	4.176e+01				
Heat Flow (Btu/hr)	-7.970e+07	-7.970e+07				
Liq VolFlow @Std Cond (barrel/day)	2821	2821				
COMPOSITION						
Overall Phase	Vapour Fraction	1.0000				
COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	169.6	0.1615	2720	0.1268	622.1	0.2393
Hydrogen	192.7	0.1836	388.6	0.0181	380.9	0.1465
H2O	404.3	0.3852	7283	0.3395	499.7	0.1922
CO2	188.9	0.1800	8315	0.3876	689.8	0.2654
CO	40.65	0.0387	1139	0.0531	97.54	0.0375
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	53.47	0.0509	1608	0.0750	309.5	0.1191
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	1050	1.0000	2.145e+004	1.0000	2600	1.0000
Vapour Phase	Phase Fraction	1.000				

COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	169.6	0.1615	2720	0.1268	622.1	0.2393
Hydrogen	192.7	0.1836	388.6	0.0181	380.9	0.1465
H2O	404.3	0.3852	7283	0.3395	499.7	0.1922
CO2	188.9	0.1800	8315	0.3876	689.8	0.2654
CO	40.65	0.0387	1139	0.0531	97.54	0.0375
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	53.47	0.0509	1608	0.0750	309.5	0.1191
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	1050	1.0000	2.145e+004	1.0000	2600	1.0000

Continued Recycle (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Continued Recycle **Fluid Package: Basis-1**
Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction 1.0000 1.0000

Vapour Phase Fraction 1.0000 1.0000

Temperature: (F) 643.6 643.6

Pressure: (psia) 435.1 435.1

Molar Flow (lbmole/hr) 436.1 436.1

Mass Flow (lb/hr) 1.187e+004 1.187e+004

Std Ideal Liq VolFlow (barrel/day) 1327 1327

Molar Enthalpy (Btu/lbmole) -9.458e+04 -9.458e+04

Molar Entropy (Btu/lbmole-F) 4.300e+01 4.300e+01

Heat Flow (Btu/hr) -4.124e+07 -4.124e+07

Liq VolFlow @Std Cond (barrel/day) 7.023e+005 7.023e+005

COMPOSITION

Overall Phase		Vapour Fraction 1.0000					
COMPONENTS MOLE FLOW		MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL	Frac
(lbmole/hr)	(lb/hr)	(barrel/day)					
Methane	46.92	0.1076	752.7	0.0634	172.1	0.1297	
Hydrogen	76.16	0.1746	153.5	0.0129	150.5	0.1134	
H ₂ O	86.57	0.1985	1559	0.1314	107.0	0.0806	
CO ₂	186.8	0.4284	8222	0.6926	682.1	0.5139	
CO	4.063	0.0093	113.8	0.0096	9.749	0.0073	
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
H ₂ S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
Ethane	35.55	0.0815	1069	0.0900	205.8	0.1550	
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
Total	436.1	1.0000	1.187e+004	1.0000	1327	1.0000	
Vapour Phase			Phase Fraction	1.0000			

	COMPONENTS	MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
	(lbmole/hr)	(lb/hr)		(barrel/day)			
Methane	46.92	0.1076	752.7	0.0634	172.1	0.1297	
Hydrogen	76.16	0.1746	153.5	0.0129	150.5	0.1134	
H2O	86.57	0.1985	1559	0.1314	107.0	0.0806	
CO2	186.8	0.4284	8222	0.6926	682.1	0.5139	
CO	4.063	0.0093	113.8	0.0096	9.749	0.0073	
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
Ethane	35.55	0.0815	1069	0.0900	205.8	0.1550	
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
Total	436.1	1.0000	1.187e+004	1.0000	1327	1.0000	

Reformer Feed (Material Stream); Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Reformer Feed Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH

Vapour / Phase Fraction 1.0000 1.0000

Vapour Phase Fraction 1.0000
 Temperature: (F) 432.9 432.9
 Pressure: (psia) 435.1 435.1
 Molar Flow (lbmole/hr) 973.1 973.1
 Mass Flow (lb/hr) 2.145e+004 2.145e+004
 Std Ideal Liq VolFlow (barrel/day) 2465 2465
 Molar Enthalpy (Btu/lbmole) -8.612e+04 -8.612e+04
 Molar Entropy (Btu/lbmole-F) 4.169e+01 4.169e+01
 Heat Flow (Btu/hr) -8.380e+07 -8.380e+07
 Liq VolFlow @Std Cond (barrel/day) 2416 2416
COMPOSITION
 Overall Phase Vapour Fraction 1.0000
COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (lbmole/hr) (lb/hr) (barrel/day)
 Methane 207.8 0.2136 3334 0.1554 762.5 0.3093
 Hydrogen 76.25 0.0784 153.7 0.0072 150.7 0.0611
 H₂O 444.2 0.4565 8003 0.3731 549.1 0.2227
 CO₂ 187.2 0.1924 8240 0.3841 683.6 0.2773
 CO 4.097 0.0042 114.8 0.0053 9.831 0.0040
 S_Rhombic 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 H₂S 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	53.47	0.0550	1608	0.0750	309.5	0.1256
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	973.1	1.0000	2.145e+004	1.0000	2465	1.0000
Vapour Phase					Phase Fraction	1.000
COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	207.8	0.2136	3334	0.1554	762.5	0.3093
Hydrogen	76.25	0.0784	153.7	0.0072	150.7	0.0611
H ₂ O	444.2	0.4565	8003	0.3731	549.1	0.2227
CO ₂	187.2	0.1924	8240	0.3841	683.6	0.2773
CO	4.097	0.0042	114.8	0.0053	9.831	0.0040
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	53.47	0.0550	1608	0.0750	309.5	0.1256
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	973.1	1.0000	2.145e+004	1.0000	2465	1.0000

Preheated Reformer Feed (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Preheated Reformer Feed Fluid Package: Basis-1
Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction 1.0000 1.0000

Temperature: (F) 1472 1472

Pressure: (psia) 435.1 435.1

Molar Flow (lbmole/hr) 973.1 973.1

Mass Flow (lb/hr) 2.145e+004 2.145e+004

Std Ideal Liq VolFlow (barrel/day) 2465 2465

Molar Enthalpy (Btu/lbmole) -7.380e+04 -7.380e+04

Molar Entropy (Btu/lbmole-F) 5.069e+01 5.069e+01

Heat Flow (Btu/hr) -7.181e+07 -7.181e+07

Liq VolFlow @Std Cond (barrel/day) 2416 2416

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS MOLE FLOW

MOLE FRAC

MASS FLOW

MASS FRAC

LIQVOL FLOW

LIQVOL FRAC

(lbmole/hr) (lb/hr) (barrel/day)

Methane 207.8 0.2136 3334

Hydrogen 76.25 0.0784 153.7

H₂O 444.2 0.4565 8003

CO₂ 187.2 0.1924 8240

CO 4.097 0.0042 114.8

S_Rhombic 0.0000 0.0000 0.0000

H₂S 0.0000 0.0000 0.0000

Propane 0.0000 0.0000 0.0000

Ethane 53.47 0.0550 1608

Oxygen 0.0000 0.0000 0.0000

Nitrogen 0.0000 0.0000 0.0000

Total 973.1 1.0000 2.145e+004

1.0000 2465 1.0000

Vapour Phase Phase Fraction 1.000

COMPONENTS MOLE FLOW

MOLE FRAC

MASS FLOW

MASS FRAC

LIQVOL FLOW

LIQVOL FRAC

(lbmole/hr) (lb/hr) (barrel/day)

Methane 207.8 0.2136 3334

Hydrogen 76.25 0.0784 153.7

H₂O 444.2 0.4565 8003

CO₂ 187.2 0.1924 8240

CO 4.097 0.0042 114.8

S_Rhombic 0.0000 0.0000 0.0000

H₂S 0.0000 0.0000 0.0000

Propane 0.0000 0.0000 0.0000

Ethane 53.47 0.0550 1608

Oxygen 0.0000 0.0000 0.0000

Nitrogen 0.0000 0.0000 0.0000

Total 973.1 1.0000 2.145e+004

1.0000 2465 1.0000

Shift Preheated (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Shift Preheated Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH. AQUEOUS PH.

Vapour / Phase Fraction 1.0000 1.0000 0.0000
 Temperature: (F) 1178 1178 1178
 Pressure: (psia) 308.1 308.1 308.1
 Molar Flow (lbmole/hr) 1050 1050 0.0000
 Mass Flow (lb/hr) 2.145e+004 2.145e+004 0.0000
 Std Ideal Liq VolFlow (barrel/day) 2600 2600 0.0000
 Molar Enthalpy (Btu/lbmole) -6.842e+04 -6.842e+04 -6.842e+04
 Molar Entropy (Btu/lbmole-F) 4.757e+01 4.757e+01 4.757e+01
 Heat Flow (Btu/hr) -7.181e+07 -7.181e+07 0.000e-01
 Liq VolFlow @Std Cond (barrel/day) 2821 2821 0.0000

COMPOSITION

Overall Phase Vapour Fraction 1.0000
 COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

	(lbmole/hr)	(lb/hr)	(barrel/day)			
Methane	169.6	0.1615	2720	0.1268	622.1	0.2393
Hydrogen	192.7	0.1836	388.6	0.0181	380.9	0.1465
H2O	404.3	0.3852	7283	0.3395	499.7	0.1922
CO2	188.9	0.1800	8315	0.3876	689.8	0.2654
CO	40.65	0.0387	1139	0.0531	97.54	0.0375
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	53.47	0.0509	1608	0.0750	309.5	0.1191
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	1050	1.0000	2.145e+004	1.0000	2600	1.0000

Vapour Phase Phase Fraction 1.000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

	(lbmole/hr)	(lb/hr)	(barrel/day)			
Methane	169.6	0.1615	2720	0.1268	622.1	0.2393
Hydrogen	192.7	0.1836	388.6	0.0181	380.9	0.1465
H2O	404.3	0.3852	7283	0.3395	499.7	0.1922
CO2	188.9	0.1800	8315	0.3876	689.8	0.2654
CO	40.65	0.0387	1139	0.0531	97.54	0.0375
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	53.47	0.0509	1608	0.0750	309.5	0.1191
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	1050	1.0000	2.145e+004	1.0000	2600	1.0000

Aqueous Phase Phase Fraction 0.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

	(lbmole/hr)	(lb/hr)	(barrel/day)			
Methane	0.0000	0.1615	0.0000	0.1268	0.0000	0.2393
Hydrogen	0.0000	0.1836	0.0000	0.0181	0.0000	0.1465
H2O	0.0000	0.3851	0.0000	0.3395	0.0000	0.1922
CO2	0.0000	0.1800	0.0000	0.3876	0.0000	0.2654
CO	0.0000	0.0387	0.0000	0.0531	0.0000	0.0375
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	0.0000	0.0509	0.0000	0.0750	0.0000	0.1191
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000

Shift Cooled (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Shift Cooled Fluid Package: Basis-1
Property Package: Peng-Robinson**CONDITIONS**

OVERALL VAPOUR PH.

Vapour / Phase Fraction 1.0000 1.0000
 Temperature: (F) 508.8 508.8
 Pressure: (psia) 299.1 299.1
 Molar Flow (lbmole/hr) 1050 1050
 Mass Flow (lb/hr) 2.145e+004 2.145e+004
 Std Ideal Liq VolFlow (barrel/day) 2600 2600
 Molar Enthalpy (Btu/lbmole) -7.567e+04 -7.567e+04
 Molar Entropy (Btu/lbmole-F) 4.198e+01 4.198e+01
 Heat Flow (Btu/hr) -7.943e+07 -7.943e+07

Liq VolFlow @Std Cond (barrel/day) 2821 2821

COMPOSITION

Overall Phase Vapour Fraction 1.0000
COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

	(lbmole/hr)	(lb/hr)	(barrel/day)			
Methane	169.6	0.1615	2720	0.1268	622.1	0.2393
Hydrogen	192.7	0.1836	388.6	0.0181	380.9	0.1465
H2O	404.3	0.3852	7283	0.3395	499.7	0.1922
CO2	188.9	0.1800	8315	0.3876	689.8	0.2654
CO	40.65	0.0387	1139	0.0531	97.54	0.0375
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	53.47	0.0509	1608	0.0750	309.5	0.1191
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	1050	1.0000	2.145e+004	1.0000	2600	1.0000

Vapour Phase Phase Fraction 1.000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

	(lbmole/hr)	(lb/hr)	(barrel/day)			
Methane	169.6	0.1615	2720	0.1268	622.1	0.2393
Hydrogen	192.7	0.1836	388.6	0.0181	380.9	0.1465
H2O	404.3	0.3852	7283	0.3395	499.7	0.1922
CO2	188.9	0.1800	8315	0.3876	689.8	0.2654
CO	40.65	0.0387	1139	0.0531	97.54	0.0375
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	53.47	0.0509	1608	0.0750	309.5	0.1191
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	1050	1.0000	2.145e+004	1.0000	2600	1.0000

Air Feed (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Air Feed Fluid Package: Basis-1
Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction 1.0000 1.0000

Temperature: (F) 77.00 77.00

Pressure: (psia) 14.69 14.69

Molar Flow (lbmole/hr) 130.4 130.4

Mass Flow (lb/hr) 4063 4063

Std Ideal Liq VolFlow (barrel/day) 263.5 263.5

Molar Enthalpy (Btu/lbmole) -3.959e+00 -3.959e+00

Molar Entropy (Btu/lbmole-F) 3.581e+01 3.581e+01

Heat Flow (Btu/hr) -5.161e+02 -5.161e+02

Liq VolFlow @Std Cond (barrel/day) 2.109e+005 2.109e+005

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

	(lbmole/hr)	(lb/hr)	(barrel/day)			
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO2	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	103.0	0.7900	3296	0.8112	198.4	0.7528
Nitrogen	27.38	0.2100	766.9	0.1888	65.12	0.2472
Total	130.4	1.0000	4063	1.0000	263.5	1.0000

Vapour Phase Phase Fraction 1.000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

	(lbmole/hr)	(lb/hr)	(barrel/day)			
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO2	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	103.0	0.7900	3296	0.8112	198.4	0.7528
Nitrogen	27.38	0.2100	766.9	0.1888	65.12	0.2472
Total	130.4	1.0000	4063	1.0000	263.5	1.0000

Combustion Product (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Combustion Product Fluid Package: Basis-1
Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction	1.0000	1.0000
Temperature: (F)	1640	1640
Pressure: (psia)	14.69	14.69
Molar Flow (lbmole/hr)	341.0	341.0
Mass Flow (lb/hr)	1.041e+004	1.041e+004
Std Ideal Liq VolFlow (barrel/day)	815.9	815.9
Molar Enthalpy (Btu/lbmole)	-1.040e+05	-1.040e+05
Molar Entropy (Btu/lbmole-F)	5.587e+01	5.587e+01
Heat Flow (Btu/hr)	-3.545e+07	-3.545e+07
Liq VolFlow @Std Cond (barrel/day)	731.3	731.3

COMPOSITION

Overall Phase	Vapour Fraction 1.0000					
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COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC						
(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2O	153.7	0.4507	2769	0.2659	190.0	0.2329
CO2	146.5	0.4296	6448	0.6192	534.9	0.6556
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	13.43	0.0394	429.9	0.0413	25.87	0.0317
Nitrogen	27.38	0.0803	766.9	0.0736	65.12	0.0798
Total	341.0	1.0000	1.041e+004	1.0000	815.9	1.0000

Vapour Phase	Phase Fraction 1.000					
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COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC						
(lbmole/hr)	(lb/hr)	(barrel/day)				
Methane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2O	153.7	0.4507	2769	0.2659	190.0	0.2329
CO2	146.5	0.4296	6448	0.6192	534.9	0.6556
CO	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	13.43	0.0394	429.9	0.0413	25.87	0.0317
Nitrogen	27.38	0.0803	766.9	0.0736	65.12	0.0798
Total	341.0	1.0000	1.041e+004	1.0000	815.9	1.0000

PSA to Atmosphere (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: PSA to Atmosphere Fluid Package: Basis-1
Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction	1.0000	1.0000
Temperature: (F)	527.0	527.0
Pressure: (psia)	275.6	275.6
Molar Flow (lbmole/hr)	390.2	390.2
Mass Flow (lb/hr)	9967	9967
Std Ideal Liq VolFlow (barrel/day)	1029	1029
Molar Enthalpy (Btu/lbmole)	-9.796e+04	-9.796e+04
Molar Entropy (Btu/lbmole-F)	4.365e+01	4.365e+01
Heat Flow (Btu/hr)	-3.823e+07	-3.823e+07
Liq VolFlow @Std Cond (barrel/day)	993.2	993.2

COMPOSITION

Overall Phase	Vapour Fraction 1.0000					
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COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
(lbmole/hr) (lb/hr) (barrel/day)

Methane	54.16	0.1388	868.8	0.0872	198.7	0.1932
Hydrogen	26.55	0.0680	53.52	0.0054	52.46	0.0510
H2O	158.9	0.4071	2862	0.2871	196.4	0.1909
CO2	120.1	0.3077	5284	0.5302	438.4	0.4262
CO	10.10	0.0259	282.9	0.0284	24.23	0.0236
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	20.48	0.0525	615.9	0.0618	118.6	0.1152
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	390.2	1.0000	9967	1.0000	1029	1.0000
Vapour Phase				Phase Fraction	1.000	

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
(lbmole/hr) (lb/hr) (barrel/day)

Methane	54.16	0.1388	868.8	0.0872	198.7	0.1932
Hydrogen	26.55	0.0680	53.52	0.0054	52.46	0.0510
H2O	158.9	0.4071	2862	0.2871	196.4	0.1909
CO2	120.1	0.3077	5284	0.5302	438.4	0.4262
CO	10.10	0.0259	282.9	0.0284	24.23	0.0236
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	20.48	0.0525	615.9	0.0618	118.6	0.1152
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	390.2	1.0000	9967	1.0000	1029	1.0000

Fresh Recycle (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Fresh Recycle Fluid Package: Basis-1
Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction	1.0000	1.0000
Temperature: (F)	526.5	526.5
Pressure: (psia)	275.6	275.6
Molar Flow (lbmole/hr)	436.1	436.1
Mass Flow (lb/hr)	1.187e+004	1.187e+004
Std Ideal Liq VolFlow (barrel/day)	1327	1327
Molar Enthalpy (Btu/lbmole)	-9.582e+04	-9.582e+04
Molar Entropy (Btu/lbmole-F)	4.271e+01	4.271e+01
Heat Flow (Btu/hr)	-4.178e+07	-4.178e+07
Liq VolFlow @Std Cond (barrel/day)	7.023e+005	7.023e+005

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
(lbmole/hr) (lb/hr) (barrel/day)

Methane	46.92	0.1076	752.7	0.0634	172.1	0.1297
Hydrogen	76.16	0.1746	153.5	0.0129	150.5	0.1134
H2O	86.57	0.1985	1559	0.1314	107.0	0.0806
CO2	186.8	0.4284	8222	0.6926	682.1	0.5139
CO	4.063	0.0093	113.8	0.0096	9.749	0.0073
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	35.55	0.0815	1069	0.0900	205.8	0.1550
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	436.1	1.0000	1.187e+004	1.0000	1327	1.0000
Vapour Phase				Phase Fraction	1.000	

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

Methane	46.92	0.1076	752.7	0.0634	172.1	0.1297
Hydrogen	76.16	0.1746	153.5	0.0129	150.5	0.1134
H2O	86.57	0.1985	1559	0.1314	107.0	0.0806
CO2	186.8	0.4284	8222	0.6926	682.1	0.5139
CO	4.063	0.0093	113.8	0.0096	9.749	0.0073
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

Material Stream: PSA recycle Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction 1.0000 1.0000

Temperature: (F) 527.0 527.0

Pressure: (psia) 275.6 275.6

Molar Flow (lbmole/hr) 157.0 157.0

Mass Flow (lb/hr) 4009 4009

Std Ideal Liq VolFlow (barrel/day) 413.8 413.8

Molar Enthalpy (Btu/lbmole) -9.796e+04 -9.796e+04

Molar Entropy (Btu/lbmole-F) 4.365e+01 4.365e+01

Heat Flow (Btu/hr) -1.538e+07 -1.538e+07

Liq VolFlow @Std Cond (barrel/day) 399.5 399.5

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

(lbmole/hr) (lb/hr) (barrel/day)

Methane 21.79 0.1388 349.5 0.0872 79.93 0.1932

Hydrogen 10.68 0.0680 21.53 0.0054 21.10 0.0510

H₂O 63.90 0.4071 1151 0.2871 78.99 0.1909

CO₂ 48.30 0.3077 2126 0.5302 176.3 0.4262

CO 4.063 0.0259 113.8 0.0284 9.749 0.0236

S_Rhombic 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

H₂S 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

Propane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

Ethane 8.239 0.0525 247.7 0.0618 47.69 0.1152

Oxygen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

Nitrogen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

Total 157.0 1.0000 4009 1.0000 413.8 1.0000

Vapour Phase Phase Fraction 1.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

(lbmole/hr) (lb/hr) (barrel/day)

Methane 21.79 0.1388 349.5 0.0872 79.93 0.1932

Hydrogen 10.68 0.0680 21.53 0.0054 21.10 0.0510

H₂O 63.90 0.4071 1151 0.2871 78.99 0.1909

CO₂ 48.30 0.3077 2126 0.5302 176.3 0.4262

CO 4.063 0.0259 113.8 0.0284 9.749 0.0236

S_Rhombic 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

H₂S 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

Propane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

Ethane 8.239 0.0525 247.7 0.0618 47.69 0.1152

Oxygen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

Nitrogen 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

Total 157.0 1.0000 4009 1.0000 413.8 1.0000

PSA fuel (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: PSA fuel Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction 1.0000 1.0000

Temperature: (F) 527.0 527.0

Pressure: (psia) 275.6 275.6

Molar Flow (lbmole/hr) 233.2 233.2

Mass Flow (lb/hr) 5958 5958

Std Ideal Liq VolFlow (barrel/day) 614.9 614.9

Molar Enthalpy (Btu/lbmole) -9.796e+04 -9.796e+04

Molar Entropy (Btu/lbmole-F) 4.365e+01 4.365e+01

Heat Flow (Btu/hr) -2.285e+07 -2.285e+07

Liq VolFlow @Std Cond (barrel/day) 593.7 593.7

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

(lbmole/hr) (lb/hr) (barrel/day)

Methane 32.37 0.1388 519.3 0.0872 118.8 0.1932

Hydrogen 15.87 0.0680 31.99 0.0054 31.36 0.0510

H₂O 94.96 0.4071 1711 0.2871 117.4 0.1909

CO₂ 71.77 0.3077 3159 0.5302 262.0 0.4262

CO 6.038 0.0259 169.1 0.0284 14.49 0.0236

S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	12.24	0.0525	368.1	0.0618	70.87	0.1152
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	233.2	1.0000	5958	1.0000	614.9	1.0000
Vapour Phase	Phase Fraction 1.000					
COMPONENTS	MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
(lbmole/hr)	(lb/hr)		(barrel/day)			
Methane	32.37	0.1388	519.3	0.0872	118.8	0.1932
Hydrogen	15.87	0.0680	31.99	0.0054	31.36	0.0510
H2O	94.96	0.4071	1711	0.2871	117.4	0.1909
CO2	71.77	0.3077	3159	0.5302	262.0	0.4262
CO	6.038	0.0259	169.1	0.0284	14.49	0.0236
S_Rhombic	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethane	12.24	0.0525	368.1	0.0618	70.87	0.1152
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	233.2	1.0000	5958	1.0000	614.9	1.0000

R-201 (Equilibrium Reactor): Design, Reactions, Rating

Equilibrium Reactor: R-201

CONNECTIONS

Inlet Stream Connections

Stream Name From Unit Operation
Preheated Reformer Feed H-201 Fired Heater

Outlet Stream Connections

Stream Name To Unit Operation
Shift Preheated Heat Exchanger: E-201
Null2

Energy Stream Connections

Stream Name From Unit Operation

PARAMETERS

Physical Parameters Optional Heat Transfer
Delta P Vessel Volume Duty Energy Stream
127.1 psi --- 0.0000 Btu/hr

User Variables

REACTION DETAILS

Component	Molecular Weight	Stoichiometric Coefficient
Methane	16.04	-1
H2O	18.02	-1
CO	28.01	1
Hydrogen	2.016	3

Component	Molecular Weight	Stoichiometric Coefficient
CO	28.01	-1
H2O	18.02	-1
CO2	44.01	1
Hydrogen	2.016	1

REACTION RESULTS FOR : Reforming Set

Extents

Act. % Conv.	Base Comp.	Eqm Constant	Rxn Extent
Methane to Hydrogen 18.41	Methane	1.742	4.821e-003
Water Gas Shift 41.66	CO	2.234	2.151e-004

Balance

	Total Inflow	Total Rxn	Total Outflow
Methane	2.618e-002	-4.821e-003	2.136e-002
Hydrogen	9.607e-003	1.468e-002	2.429e-002
H2O	5.598e-002	-5.036e-003	5.094e-002
CO2	2.359e-002	2.151e-004	2.380e-002
CO	5.163e-004	4.606e-003	5.122e-003
S_Rhombic	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000
Ethane	6.738e-003	8.674e-019	6.738e-003
Oxygen	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000

RATING

R-202 (Equilibrium Reactor): Design, Reactions, Rating

Equilibrium Reactor: R-202

CONNECTIONS

Inlet Stream Connections

Stream Name From Unit Operation
 High Temp Shift Preheated E-202 Cooler

Outlet Stream Connections

Stream Name To Unit Operation
 High Shift Product
 Null3

Energy Stream Connections

Stream Name From Unit Operation

PARAMETERS

Physical Parameters Optional Heat Transfer
 Delta P Vessel Volume Duty Energy Stream
 0.0000 psi --- 0.0000 Btu/hr

User Variables

REACTION DETAILS

Component	Molecular Weight	Stoichiometric Coefficient
CO	28.01	-1
H2O	18.02	-1
CO2	44.01	1
Hydrogen	2.016	1

REACTION RESULTS FOR : Water Gas Shift Set

Extents

	Act. % Conv.	Base Comp.	Eqn Constant	Rxn Extent
Rxn-1	93.38	CO	55.07	4.783e-003
Balance		Total Inflow	Total Rxn	Total Outflow

Methane	2.136e-002	0.0000	2.136e-002
Hydrogen	2.429e-002	4.783e-003	2.907e-002
H2O	5.094e-002	-4.783e-003	4.616e-002
CO2	2.380e-002	4.783e-003	2.859e-002
CO	5.122e-003	-4.783e-003	3.393e-004
S_Rhombic	0.0000	0.0000	0.0000
H2S	0.0000	0.0000	0.0000
Propane	0.0000	0.0000	0.0000
Ethane	6.738e-003	0.0000	6.738e-003
Oxygen	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000

RATING

SET-1 (Set): Design

Set: SET-1

	OBJECT	VARIABLE
Target		
Steam	Molar Flow	
Source		
Sweet Gas	Molar Flow	
Equation Parameters		
MULTIPLIER	OFFSET	
2.000	0.0000 lbmole/hr	

User Variables

RCY-1 (Recycle): Design

Recycle: RCY-1

CONNECTIONS

Inlet Stream

Stream Name From Unit Operation
 Continued Recycle C-201 Compressor

Outlet Stream

Stream Name To Unit Operation
 Recycled Flue MIX-100 Mixer

TOLEURANCE

Vapour Fraction: 10.00 Temperature: 10.00 Pressure: 10.00
 Flow: 10.00 Enthalpy: 10.00 Composition: 10.00

NUMERICAL

Acceleration Type: Wegstein Iteration Type: Nested
 Maximum Iterations: 10 Iteration Count: 0
 Wegstein Count: 3 Q Minimum: -20.00 Q Maximum: 0.0000
 Iteration History

Iteration Variable Outlet Value Inlet Value

0 Converged --- ---
 User Variables
 MIX-100 (Mixer): Design, Rating

Mixer: MIX-100
 CONNECTIONS
 Inlet Stream
 STREAM NAME FROM UNIT OPERATION
 Steam E-201 Heat Exchanger
 Sweet Gas
 Recycled Flue RCY-1 Recycle
 Outlet Stream
 STREAM NAME TO UNIT OPERATION
 Reformer Feed H-201 Fired Heater

PARAMETERS

MIX-102 (Mixer): Design, Rating

Mixer: MIX-102
 CONNECTIONS
 Inlet Stream
 STREAM NAME FROM UNIT OPERATION
 Membrane to Fuel
 PSA recycle TEE-101 Tee
 Outlet Stream
 STREAM NAME TO UNIT OPERATION
 Fresh Recycle C-201 Compressor

PARAMETERS
 User Variables

E-201 (Heat Exchanger): Design, Rating, Details, Tables, HTFS Results, Exchanger Design and Rating

Heat Exchanger: E-201
 CONNECTIONS
 Tube Side Shell Side
 Inlet Outlet Inlet Outlet
 Name City Water Name Steam Name Shift Preheated Name Shift Cooled
 From Op. To Op. MIX-100 From Op. R-201 To Op. E-202
 Op. Type Op. Type Mixer Op. Type Equilibrium Reactor Op. Type Cooler
 Temp 90.00 F Temp 454.24 F Temp 1178.25 F Temp 508.81 F

PARAMETERS
 Heat Exchanger Model: Simple End Point
 Tube Side DeltaP: -420.4 psi Shell Side DeltaP: 8.992 psi Passes: ---
 UA: 1.609e+004 Btu/F-hr Tolerance: 1.0000e-04
 Tube Side Data Shell Side Data
 Heat Transfer Coeff --- Heat Transfer Coeff ---
 Tube Pressure Drop -420.42 psi Shell Pressure Drop 8.99 psi
 Fouling 0.00000 F-hr-ft²/Btu Fouling 0.00000 F-hr-ft²/Btu
 Tube Length 19.69 ft Shell Passes 1
 Tube O.D. 0.79 in Shell Series 1
 Tube Thickness 0.0787 in Shell Parallel 1
 Tube Pitch 1.9685 in Baffle Type Single
 Orientation Horizontal Baffle Cut(%Area) 20.00
 Passes Per Shell 2 Baffle Orientation Horizontal
 Tubes Per Shell 160 Spacing 31.4961 in
 Layout Angle Triangular (30 degrees) Diameter 29.0964 in
 TEMA Type A E L Area 649.26 ft²
 SPECS
 Spec Value Curr Value Rel Error Active Estimate
 E-103 Heat Balance 0.0000 Btu/hr -3.103e-009 Btu/hr -4.076e-016 On Off
 E-103 UA --- 1.609e+004 Btu/F-hr --- On Off

Detailed Specifications
 E-103 Heat Balance
 Type: Duty Pass: Error Spec Value: 0.0000 Btu/hr
 E-103 UA

Type: UA Pass: Overall Spec Value: ---
 User Variables
 RATING
 Sizing
 Overall Data
 Configuration
 # of Shells in Series 1 Tube Passes per Shell 2 Elevation (Base) 0.0000 ft
 # of Shells in Parallel 1 Exchange Orientation Horizontal First Tube Pass Flow Direction Counter
 TEMA Type: A E L

Calculated Information

Shell HT Coeff --- Tube HT Coeff ---
 Overall U 24.78 Btu/hr-ft²-F Overall UA 1.609e+004 Btu/F-hr
 Shell DP 8.992 psi Tube DP -420.4 psi
 Shell Vol per Shell 80.24 ft³ Tube Vol per Shell 6.816 ft³
 HT Area per Shell 649.3 ft²

Shell Data

Shell and Tube Bundle

Shell Diameter 29.10 Tube Pitch 1.969 Shell Fouling 0.0000
 (in) (in) (F-hr-ft²/Btu)
 # of Tubes per Shell 160 Tube Layout Angle Triangular (30 degrees)

Shell Baffles

Shell Baffle Type Single Shell Baffle Orientation Horizontal
 Baffle Cut (%Area) 20.00 Baffle Spacing 31.50 in

Tube Data

Dimensions

OD 0.7874 ID 0.6299 Tube Thickness 7.874e-002 Tube Length 19.69
 (in) (in) (in) (ft)

Tube Properties

Tube Fouling 0.0000 Thermal Cond. 26.00 Wall Cp --- Wall Density ---
 (F-hr-ft²/Btu) (Btu/hr-ft-F) (Btu/lb-F) (lb/ft³)

Nozzle Parameters

Overall/Detailed Performance

Duty: 7.614e+06 Btu/hr UA Curv. Error: 0.00e-01 Btu/F-hr
 Heat Leak: 0.000e-01 Btu/hr Hot Pinch Temp: 508.8 F
 Heat Loss: 0.000e-01 Btu/hr Cold Pinch Temp: 90.00 F
 UA: 1.609e+04 Btu/F-hr Ft Factor: ---
 Min. Approach: 418.8 F Uncorrected Lmtd: 557.6 F
 Lmtd: 473.3 F

TABLES

Shell Side - Overall Phase

Temperature (F)	Pressure (psia)	Heat Flow (Btu/hr)	Enthalpy (Btu/lbmole)
508.81	299.07	0.00	-75671.24
1178.25	308.06	7614173.82	-68417.17
UA	Molar Vap Frac	Mass Vap Frac	Heat of Vap.
(Btu/F-hr)			(Btu/lbmole)
0.00	1.0000	1.0000	---
0.00	1.0000	1.0000	---

Shell Side - Vapour Phase

Mass Flow (lb/hr)	Molecular Wt (lb/ft ³)	Density (Btu/lb-F)	Mass Sp (cP)	Heat Viscosity (Btu/hr-ft-F)	Thermal Cond (Btu/hr-ft ² -F)
21453.15	20.44	0.60	0.48	0.02	0.04
21453.15	20.44	0.36	0.57	0.03	0.07
Std Gas Flow (MMSCFD)	Z Factor (psia)	Pseudo Pc (F)	Pseudo Tc	Pseudo Zc	Pseudo Omega
9.54	0.99	1627.59	191.40	0.28	0.16
9.54	1.00	1627.59	191.40	0.28	0.16

Shell Side - Light Liquid Phase

Mass Flow (lb/hr)	Density (lb/ft ³)	Mass Sp (Btu/lb-F)	Heat Viscosity (cP)	Thermal Cond (Btu/hr-ft-F)	Surface Tens (dyne/cm)
---	---	---	---	---	---
0.00	0.36	0.57	0.00	0.08	0.00
0.00	---	---	---	---	---
Molecular Wt (psia)	Sp Gravity (F)	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega
---	---	---	---	---	---
20.44	0.01	1627.54	191.38	0.28	0.16

Shell Side - Mixed Liquid

Mass Flow (lb/hr)	Density (lb/ft ³)	Mass Sp (Btu/lb-F)	Heat Viscosity (cP)	Thermal Cond (Btu/hr-ft-F)	Surface Tens (dyne/cm)
---	---	---	---	---	---
0.00	0.36	0.57	0.00	0.08	---
0.00	---	---	---	---	---
Molecular Wt (psia)	Sp Gravity (F)	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega
---	---	---	---	---	---
20.44	0.01	1627.54	191.38	0.28	0.16

Tube Side - Overall Phase

Temperature (F)	Pressure (psia)	Heat Flow (Btu/hr)	Enthalpy (Btu/lbmole)
90.00	14.69	0.00	-122811.45
331.92	105.60	1646365.88	-118201.70
454.24	435.11	7614173.82	-101492.12

UA	Molar Vap Frac	Mass Vap Frac	Heat of Vap.		
(Btu/F-hr)			(Btu/lbmole)		
0.00	0.0000	0.0000	---		
0.00	0.0000	0.0000	---		
0.00	1.0000	1.0000	---		
Tube Side - Vapour Phase					
Mass Flow	Molecular Wt	Density	Mass Sp Heat	Viscosity	Thermal Cond
(lb/hr)	(lb/ft ³)	(Btu/lb-F)	(cP)	(Btu/hr-ft-F)	
---	---	---	---	---	---
0.00	18.02	0.23	0.48	0.01	0.02
6434.01	18.02	0.91	0.54	0.02	0.03
Std Gas Flow	Z Factor	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega
(MMSCFD)		(psia)	(F)		
---	---	---	---	---	---
0.00	0.96	3208.23	705.47	0.26	0.34
3.25	0.88	3208.23	705.47	0.26	0.34
Tube Side - Light Liquid Phase					
Mass Flow	Density	Mass Sp Heat	Viscosity	Thermal Cond	Surface Tens
(lb/hr)	(lb/ft ³)	(Btu/lb-F)	(cP)	(Btu/hr-ft-F)	(dyne/cm)
6434.01	62.55	1.03	0.76	0.36	70.85
6434.01	55.43	1.11	0.16	0.39	45.17
0.00	50.85	1.26	0.11	0.37	29.80
Molecular Wt	Sp Gravity	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega
(psia)	(F)				
18.02	1.00	3208.23	705.47	0.26	0.34
18.02	0.89	3208.23	705.47	0.26	0.34
18.02	0.81	3208.23	705.47	0.26	0.34
Tube Side - Mixed Liquid					
Mass Flow	Density	Mass Sp Heat	Viscosity	Thermal Cond	Surface Tens
(lb/hr)	(lb/ft ³)	(Btu/lb-F)	(cP)	(Btu/hr-ft-F)	(dyne/cm)
6434.01	62.55	1.03	0.76	0.36	---
6434.01	55.43	1.11	0.16	0.39	---
0.00	50.85	1.26	0.11	0.37	---
Molecular Wt	Sp Gravity	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega
(psia)	(F)				
18.02	1.00	3208.23	705.47	0.26	0.34
18.02	0.89	3208.23	705.47	0.26	0.34
18.02	0.81	3208.23	705.47	0.26	0.34

HTFS

H-201 (Fired Heater): Design, Rating, Performance

Fired Heater: H-201

CONNECTIONS

Combustion Product Combustion Product Fuel Gas Feed Air Feed

Economizer Zone Connections

Econ Zone Inlet	Econ Zone Outlet	# of Tubes 0
Convective Zone		
Conv Zone Inlet	Conv Zone Outlet	# of Tubes 0
Radiative Zone		
Radiant Zone Inlet	Radiant Zone Outlet	# of Tubes 1
Reformer Feed	Preheated Reformer Feed	

PARAMETERS

Min Air Fuel Ratio --- Flame Temp --- Heater SS Efficiency 75.00
 Air Fuel Ratio --- Lean Factor 1.000 Heater SS Excess Air Percent 15.00

Max Air Fuel Ratio --- Rich Factor 40.00

User Variables

RATING

Sizing

Radiant Tube Inner Diameters (ft) --- Radiant Zone Inner Diameters (ft) 5.577
 Radiant Tube Outer Diameters (ft) --- Radiant Zone Outer Diameters (ft) 6.562

Number of Radiant Tubes --- Radiant Zone Height (ft) 14.04

Radiant Tube Lengths (ft) ---

Tube Inner Area (ft²) --- Tube Outer Area (ft²) --- Wall Inner Area (ft²) 246.0 Wall Outer Area (ft²) 289.5

Convective Zone

Convective Tube Inner Diameters (ft) --- Convective Zone Inner Diameter (ft) 3.714
 Convective Tube Outer Diameters (ft) --- Convective Zone Outer Diameter (ft) 4.698

Number of Convective Tubes --- Convective Zone Height (ft) 5.577

Convective Tube Lengths (ft) ---

Tube Inner Area (ft²) --- Tube Outer Area (ft²) ---

Economizer Zone

Economizer Tube Inner Diameters (ft) --- Economizer Zone Inner Diameter (ft) 1.280
 Economizer Tube Outer Diameters (ft) --- Economizer Zone Outer Diameter (ft) 1.608

Number of Economizer Tubes --- Economizer Zone Height (ft) 38.12

Economizer Tube Lengths (ft) ---

Tube Inner Area (ft²) --- Tube Outer Area (ft²) ---
 Heat Transfer
 Reformer Feed 432.9 1472 --- ---
 Temp Profile
 Top Temp --- --- --- Bottom Temp ---
 Wall Inner Temp --- Wall Outer Temp ---
PERFORMANCE TABLE
 Reformer Feed
 Overall Phase
 Temperature Pressure Heat Flow Enthalpy
 (F) (psia) (Btu/hr) (Btu/lbmole)
 432.91 435.11 0.00 -86120.47
 536.82 435.11 1057955.84 -85033.28
 640.73 435.11 2147781.90 -83913.34
 744.64 435.11 3269987.72 -82760.13
 848.55 435.11 4425476.79 -81572.71
 952.46 435.11 5613800.40 -80351.56
 1056.37 435.11 6833664.23 -79097.99
 1160.27 435.11 8083279.88 -77813.85
 1264.18 435.11 9360639.38 -76501.19
 1368.09 435.11 10663748.74 -75162.08
 1472.00 435.11 11990838.06 -73798.32
 Vapour Phase
 Mass Flow Molecular Wt Density Mass Sp Heat Viscosity Thermal Cond
 (lb/hr) (lb/ft³) (Btu/lb-F) (cP) (Btu/hr-ft-F)
 21453.12 22.05 1.04 0.47 0.02 0.03
 21453.12 22.05 0.92 0.48 0.02 0.03
 21453.12 22.05 0.83 0.50 0.02 0.04
 21453.12 22.05 0.75 0.51 0.02 0.04
 21453.12 22.05 0.69 0.53 0.03 0.05
 21453.12 22.05 0.64 0.54 0.03 0.05
 21453.12 22.05 0.59 0.55 0.03 0.05
 21453.12 22.05 0.55 0.57 0.03 0.06
 21453.12 22.05 0.52 0.58 0.03 0.06
 21453.12 22.05 0.49 0.59 0.03 0.07
 21453.12 22.05 0.46 0.60 0.03 0.07
 Std Gas Flow Z Factor Pseudo Pc Pseudo Tc Pseudo Zc Pseudo Omega
 (MMSCFD) (psia) (F)
 8.85 0.96 1870.06 286.80 0.27 0.20
 8.85 0.97 1870.06 286.80 0.27 0.20
 8.85 0.98 1870.06 286.80 0.27 0.20
 8.85 0.99 1870.06 286.80 0.27 0.20
 8.85 0.99 1870.06 286.80 0.27 0.20
 8.85 1.00 1870.06 286.80 0.27 0.20
 8.85 1.00 1870.06 286.80 0.27 0.20
 8.85 1.00 1870.06 286.80 0.27 0.20
 8.85 1.00 1870.06 286.80 0.27 0.20
 8.85 1.00 1870.06 286.80 0.27 0.20
 8.85 1.00 1870.06 286.80 0.27 0.20
 Light Liquid Phase

E-202 (Cooler): Design, Rating, Profiles, Tables

Cooler: E-202
 CONNECTIONS
 Inlet Stream
 STREAM NAME FROM UNIT OPERATION
 Shift Cooled E-201 Heat Exchanger
 Outlet Stream
 STREAM NAME TO UNIT OPERATION
 High Temp Shift Preheated R-202 Equilibrium Reactor
 Energy Stream
 STREAM NAME TO UNIT OPERATION
 Shift Cooler

PARAMETERS

Pressure Drop: 8.992 psi Duty: 2.734e+005 Btu/hr Volume: 3.531 ft³
 Function: Not Selected Zones: 1

User Variables

Zone	Pressure	Temperature	Vapour Fraction	Enthalpy
	(psia)	(F)		(Btu/lbmole)
Inlet	299.07	508.81	1.0000	-75671.24
0	290.08	482.00	1.0000	-75931.68

PERFORMANCE TABLE

Light Liquid Phase

C-201 (Compressor): Design, Rating, Performance

Compressor: C-201

DESIGN

Connections

Inlet Stream

STREAM NAME

Fresh Recycle MIX-102 Mixer

Outlet Stream

STREAM NAME

Continued Recycle RCY-1 Recycle

Energy Stream

STREAM NAME

Recycle Compr Benzene

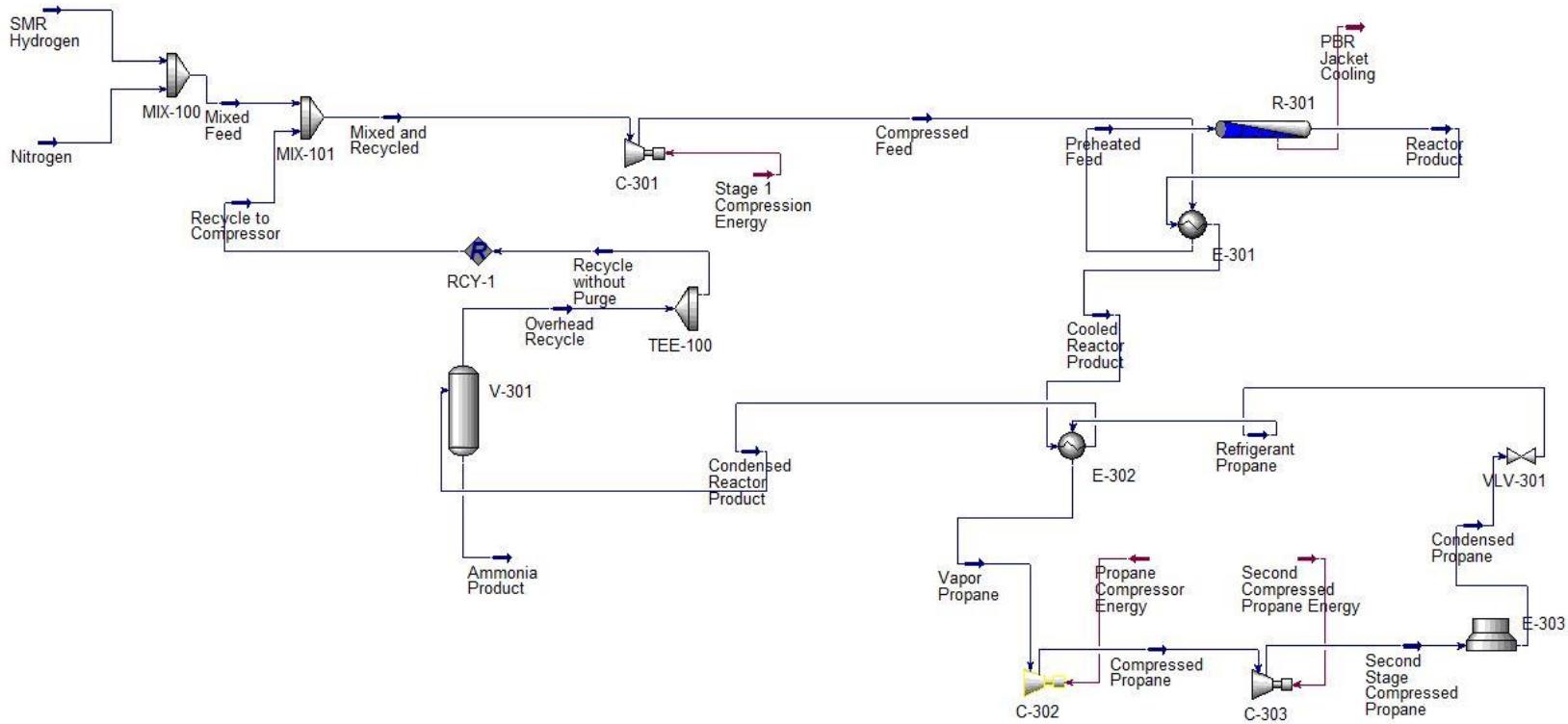
Parameters
Speed: Duty: 2.1206e+02 km

Speed: --- D

Adiabatic Head: 2.653 ± 0.004

Adiabatic Head: 2.653e+004

Adiabatic Fluid Head: 2.653e+004 lbf-ft/lbm Polytropic Fluid Head: 2.689e+004 lbf-ft/lbm
Polytropic Exp. 1.336 Isentropic Exp. 1.239 Poly Head Factor 1.001
User Variables
RATING
Rotational inertia (lb·ft²) 142.4 Radius of gyration (ft) 0.6562
Mass (lb) 330.7 Friction loss factor (rad/min) (lb·ft²/s) 0.1424
PERFORMANCE
Results
Adiabatic Head (ft) 2.653e+004 Power Consumed (hp) 212.1
Polytropic Head (ft) 2.689e+004 Polytropic Head Factor 1.001
Adiabatic Fluid Head (lbf-ft/lbm) 2.653e+004 Polytropic Exponent 1.336
Polytropic Fluid Head (lbf-ft/lbm) 2.689e+004 Isentropic Exponent 1.239
Adiabatic Efficiency 75 Speed (rpm) ---
Polytropic Efficiency 76 ---
Total Rotor Power (hp) 212.1 Total Rotor Torque (lbf-ft) ---
Transient Rotor Power (hp) 0.0000 Transient Rotor Torque (lbf-ft) ---
Friction Power Loss (hp) 0.0000 Friction Torque Loss (lbf-ft) ---
Fluid Power (hp) 212.1 Fluid Torque (lbf-ft) ---



```
*****
***** INPUT SUMMARY *****
*****
```

FLUID PACKAGE: Basis-1(Peng-Robinson)

Property Package Type: PengRob
Component List - 1: Hydrogen /Nitrogen /Ammonia /Oxygen /H2O /Propane /
Reaction Set: Set-1
Reaction 'Rxn-1':
Reactants: Hydrogen, Stoich Coeff -3 / Nitrogen, Stoich Coeff -1 / Ammonia,
Stoich Coeff 2 /
Basis Data: Basis = Partial Pres / Component = Nitrogen / Phase = VapourPhase
/ RateUnits = kgmole/m3-s /
Kinetic Coefficients: Fwd Freq Factor = 1120000 / Fwd Activation Energy =
136000 /

FLOWSHEET: Main

Fluid Package: Basis-1
STREAM: SMR Hydrogen (Material Stream)
Temperature = 275 C
Pressure = 1500 kPa
Molar Flow = 185 kgmole/h
Composition Basis (In Mole Flows):Hydrogen = 184.445/ Nitrogen = 0/ Ammonia =
0/ Oxygen = 0/ H2O = 0.555/ Propane = 0/
STREAM: Nitrogen (Material Stream)
Vapour Fraction = 1
Temperature = 80.2 C
Pressure = 900 kPa
Molar Flow = 62 kgmole/h
Composition Basis (In Mole Fractions):Hydrogen = 0/ Nitrogen = 0.999/ Ammonia
= 0/ Oxygen = 0.001/ H2O = 0/ Propane = 0/
UNIT OPERATION: MIX-100 (Mixer)
Feed Stream = Nitrogen
Feed Stream = SMR Hydrogen
Product Stream = Mixed Feed
UseTrivialSolution = True
UNIT OPERATION: K-100 (Compressor)
Feed Stream = Mixed and Recycled
Product Stream = Compressed Feed
Energy Stream = Stage 1 Compression Energy
AdiabaticEfficiency = 85
CylinderType = Single-acting, Outer End
= 1
CurveCollectionName = CC-0
SelectedCurveCollection = True
NumberOfCurves = 0
NumberOfCurves = 0
NumberOfCurves = 0
EffCurveType = 0
NumberOfCurves = 0
UseDutySpec = 0
UseAdiabaticEfficiencySpec = 1
UsePolytropicEfficiencySpec = 0
UseSpeedSpec = 1
STREAM: Mixed Feed (Material Stream)
STREAM: Compressed Feed (Material Stream)
Pressure = 1100 kPa
STREAM: Preheated Feed (Material Stream)
Temperature = 450 C
STREAM: Reactor Product (Material Stream)
Temperature = 550 C
STREAM: Condensed Reactor Product (Material Stream)
Temperature = -30 C
UNIT OPERATION: V-100 (Separator)
Feed Stream = Condensed Reactor Product
Vapour Product = Overhead Recycle
Liquid Product = Ammonia Product
Delta P = FEMPTY kPa
STREAM: Ammonia Product (Material Stream)
Pressure = 800 kPa

STREAM: Stage 1 Compression Energy (Energy Stream)
 STREAM: Cooled Reactor Product (Material Stream)
 UNIT OPERATION: MIX-101 (Mixer)
 Feed Stream = Mixed Feed
 Feed Stream = Recycle to Compressor
 Product Stream = Mixed and Recycled
 UseTrivialSolution = True
 STREAM: Mixed and Recycled (Material Stream)
 STREAM: Overhead Recycle (Material Stream)
 STREAM: Recycle to Compressor (Material Stream)
 Temperature = -32.0310422 C
 Pressure = 800 kPa
 Molar Flow = 399.351699 kgmole/h
 Composition Basis (In Mole Fractions):Hydrogen = 0.564486814/ Nitrogen = 0.284575368/ Ammonia = 0.139272636/ Oxygen = 0.0116651543/ H₂O = 2.69335854e-008/
 Propane = 0/
 UNIT OPERATION: Named E-106 (Heat Exchanger)
 TubeInletStream = Reactor Product
 TubeOutletStream = Cooled Reactor Product
 ShellInletStream = Compressed Feed
 ShellOutletStream = Preheated Feed
 TubeOuterDiameter = 20 mm
 TubeInnerDiameter = 16 mm
 TubeThickness = FEMPTY mm
 HCurveName = Reactor Product-Cooled Reactor Product
 HCurveName = Compressed Feed-Preheated Feed
 ShellPressureDrop = 62 kPa
 TubePressureDrop = 62 kPa
 calcFTMoniker = False
 UNIT OPERATION: RCY-1 (Recycle)
 Inlet Stream = Recycle without Purge
 Output Stream = Recycle to Compressor
 UNIT OPERATION: PFR-100 (Plug Flow Reactor)
 Feed Stream = Preheated Feed
 Product Stream = Reactor Product
 Energy Stream = PBR Jacket Cooling
 Reaction Set=Set-1
 DeltaPType = 1
 SinglePhase = True
 TubeTotalVolume = 538.4 m³
 TubeDiameter = 6.1 m
 VoidFraction = 0.9
 UNIT OPERATION: TEE-100 (Tee)
 Feed Stream = Overhead Recycle
 Product Stream = Recycle without Purge
 STREAM: Recycle without Purge (Material Stream)
 UNIT OPERATION: K-101 (Compressor)
 Feed Stream = Vapor Propane
 Product Stream = Compressed Propane
 Energy Stream = Propane Compressor Energy
 AdiabaticEfficiency = FEMPTY
 PressureRatio = 4
 CylinderType = Single-acting, Outer End
 = 1
 CurveCollectionName = CC-0
 SelectedCurveCollection = True
 NumberOfCurves = 0
 NumberOfCurves = 0
 NumberOfCurves = 0
 EffCurveType = 0
 NumberOfCurves = 0
 UseDutySpec = 0
 UseAdiabaticEfficiencySpec = 1
 UsePolytropicEfficiencySpec = 0
 UseSpeedSpec = 1
 UNIT OPERATION: VLV-100 (Valve)
 Feed Stream = Condensed Propane
 Product Stream = Refrigerant Propane
 ValveManufacturer = FISHER
 ValveManufacturerType = 0
 C1 = 33.4664011
 RigorousSizingMethod = True
 UseXtTable = False
 RigorousFlowCalc = True

UNIT OPERATION: Named E-107 (Heat Exchanger)
 TubeInletStream = Cooled Reactor Product
 TubeOutletStream = Condensed Reactor Product
 ShellInletStream = Refrigerant Propane
 ShellOutletStream = Vapor Propane
 TubeOuterDiameter = 20 mm
 TubeInnerDiameter = 16 mm
 TubeThickness = FEMPTY mm
 HCurveName = Cooled Reactor Product-Condensed Reactor Product
 HCurveName = Refrigerant Propane-Vapor Propane
 ShellPressureDrop = 62 kPa
 TubePressureDrop = 62 kPa
 STREAM: Refrigerant Propane (Material Stream)
 STREAM: Vapor Propane (Material Stream)
 Vapour Fraction = 1
 Pressure = 101.3 kPa
 STREAM: Compressed Propane (Material Stream)
 Vapour Fraction = 1
 STREAM: Propane Compressor Energy (Energy Stream)
 STREAM: Condensed Propane (Material Stream)
 Vapour Fraction = 0
 Composition Basis (In Mole Fractions):Hydrogen = 0/ Nitrogen = 0/ Ammonia = 0/
 Oxygen = 0/ H₂O = 0/ Propane = 1/
 STREAM: PBR Jacket Cooling (Energy Stream)
 UNIT OPERATION: K-102 (Compressor)
 Feed Stream = Compressed Propane
 Product Stream = Second Stage Compressed Propane
 Energy Stream = Second Compressed Propane Energy
 PressureRatio = 4
 CurveCollectionName = CC-0
 SelectedCurveCollection = True
 NumberOfCurves = 0
 NumberOfCurves = 0
 NumberOfCurves = 0
 EffCurveType = 0
 NumberOfCurves = 0
 STREAM: Second Stage Compressed Propane (Material Stream)
 STREAM: Second Compressed Propane Energy (Energy Stream)
 UNIT OPERATION: AC-100 (Air cooler)
 Feed Stream = Second Stage Compressed Propane
 Product Stream = Condensed Propane
 Pressure Drop = 2 kPa
 UA = 645329.254 kJ/C-h
 NumberOfFans = 1
 Fan_Name = Fan 0
 Tolerance = 1e-005

OUTPUT SUMMARY

OKLAHOMA STATE UNIVERSIT Case Name: Haber Process Final.hsc
 Bedford, MA
 USA Unit Set: SI

Date/Time: Wed Apr 01 18:35:41 2020

Basis-1 (Fluid Package): Component List

Fluid Package: Basis-1

COMPONENT LIST

Component List - 1 [HYSYS Databanks]

COMPONENT	TYPE	MOLECULAR BOILING PT	IDEAL LIQ	CRITICAL
		WEIGHT (C)	DENSITY (kg/m ³)	TEMP (C)
Hydrogen	Pure	2.016	-252.6	69.86
Nitrogen	Pure	28.01	-195.8	806.4
Ammonia	Pure	17.03	-33.45	616.1
Oxygen	Pure	32.00	-183.0	1138
H ₂ O	Pure	18.02	100.0	998.0
Propane	Pure	44.10	-42.10	506.7

(Continued..) Component List - 1 [HYSYS Databanks]

COMPONENT	CRITICAL PRES (kPa)	CRITICAL VOL (m ³ /kgmole)	ACENTRICITY	HEAT OF FORM (kJ/kgmole)
Hydrogen	1316	5.150e-002	-0.1201	0.0000

Nitrogen	3394	9.000e-002	4.000e-002	0.0000
Ammonia	1.128e+004	8.040e-002	0.2550	-4.571e+004
Oxygen	5080	7.320e-002	1.900e-002	0.0000
H2O	2.212e+004	5.710e-002	0.3440	-2.418e+005
Propane	4257	0.2000	0.1524	-1.039e+005

Case (Simulation Case): Mass and Energy Balance, Utility Balance, Process CO2 Emissions

Simulation Case: Case

OVERALL MASS BALANCE

In Stream	Count	Mass Flow	Out Stream	Count	Mass Flow
	(kg/h)			(kg/h)	

Nitrogen	Yes	1737	Ammonia Product	Yes	2084
----------	-----	------	-----------------	-----	------

SMR Hydrogen	Yes	381.8			
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Total In MassFlow (kg/h)	2119	Total Out MassFlow (kg/h)	2084		
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Mass Imbalance (kg/h)	-35.10	Rel Mass Imbalance Pct (%)	-1.66		
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OVERALL ENERGY BALANCE

InStream	Count	Energy Flow	OutStream	Count	Energy Flow
	(kJ/h)			(kJ/h)	

Nitrogen	Yes	9.735e+04	Ammonia Product	Yes	-8.864e+06
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SMR Hydrogen	Yes	1.198e+06	PBR Jacket Cooling	Yes	4.512e+06
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Stage 1 Compression Energy	Yes	7.119e+05			
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Propane Compressor Energy	Yes	1.541e+06			
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Second Compressed Propane Energy	Yes	2.876e+06			
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Total In EnergyFlow (kJ/h)	6.424e+006	Total Out EnergyFlow (kJ/h)	-4.352e+006		
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Energy Imbalance (kJ/h)	-1.078e+007	Rel Energy Imbalance Pct (%)	-167.74		
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OVERALL UTILITY BALANCE

Utility Name	Usage Info	Energy Flow	Mass Flow	Cost
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Hot Utility Summary		Cold Utility Summary		
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Utility Flow ---		Utility Flow ---		
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Utility Cost ---		Utility Cost ---		
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Carbon Emiss. ---		Carbon Emiss. ---		
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Carbon Fees ---		Carbon Fees ---		
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PROCESS CO2 EMISSIONS

Inlet Stream	Count	IFPP (1995)	IFPP (2007)	EPA (2009)
	(kg/h)		(kg/h)	(kg/h)

Nitrogen	Yes	0.000e-01	0.000e-01	0.000e-01
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SMR Hydrogen	Yes	0.000e-01	0.000e-01	0.000e-01
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Total from Inlets	---	---	---	
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Total Carbon Fees	---	---	---	
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from Inlets (Cost/hr)				
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Outlet Stream	Count	IFPP (1995)	IFPP (2007)	EPA (2009)
	(kg/h)		(kg/h)	(kg/h)

Ammonia Product	Yes	0.000e-01	0.000e-01	0.000e-01
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Total from Outlets	---	---	---	
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Total Carbon Fees	---	---	---	
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from Outlets (Cost/hr)				
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SMR Hydrogen (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: SMR Hydrogen		Fluid Package: Basis-1	
		Property Package: Peng-Robinson	

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction	1.0000	1.0000
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Temperature: (C)	275.0	275.0
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Pressure: (kPa)	1500	1500
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Molar Flow (kgmole/h)	185.0	185.0
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Mass Flow (kg/h)	381.8	381.8
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Std Ideal Liq VolFlow (m3/h)	5.333	5.333
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Molar Enthalpy (kJ/kgmole)	6.474e+03	6.474e+03
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Molar Entropy (kJ/kgmole-C)	1.184e+02	1.184e+02
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Heat Flow (kJ/h)	1.198e+06	1.198e+06
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Liq VolFlow @Std Cond (m3/h)	4376	4376
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COMPOSITION

Overall Phase		Vapour Fraction 1.0000
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COMPONENTS	MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
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	(kgmole/h)	(kg/h)	(m3/h)			
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Hydrogen	184.4	0.9970	371.8	0.9738	5.323	0.9981
----------	-------	--------	-------	--------	-------	--------

Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
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Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
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Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
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H2O	0.5550	0.0030	9.998	0.0262	1.002e-002	0.0019
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Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
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Total	185.0	1.0000	381.8	1.0000	5.333	1.0000
Vapour Phase					Phase Fraction	1.000
COMPONENTS	MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
(kgmole/h)	(kg/h)		(m3/h)			
Hydrogen	184.4	0.9970	371.8	0.9738	5.323	0.9981
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ O	0.5550	0.0030	9.998	0.0262	1.002e-002	0.0019
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	185.0	1.0000	381.8	1.0000	5.333	1.0000

Nitrogen (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Nitrogen Fluid Package: Basis-1
Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction 1.0000 1.0000

Temperature: (C) 80.20 80.20

Pressure: (kPa) 900.0 900.0

Molar Flow (kgmole/h) 62.00 62.00

Mass Flow (kg/h) 1737 1737

Std Ideal Liq VolFlow (m³/h) 2.153 2.153

Molar Enthalpy (kJ/kgmole) 1.570e+03 1.570e+03

Molar Entropy (kJ/kgmole-C) 1.348e+02 1.348e+02

Heat Flow (kJ/h) 9.735e+04 9.735e+04

Liq VolFlow @Std Cond (m³/h) 1465 1465

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

(kgmole/h)	(kg/h)		(m ³ /h)			
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Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
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Nitrogen	61.94	0.9990	1735	0.9989	2.152	0.9992
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Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
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Oxygen	6.200e-002	0.0010	1.984	0.0011	1.744e-003	0.0008
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H ₂ O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
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Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
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Total	62.00	1.0000	1737	1.0000	2.153	1.0000
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Vapour Phase Phase Fraction 1.000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

(kgmole/h)	(kg/h)		(m ³ /h)			
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Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
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Nitrogen	61.94	0.9990	1735	0.9989	2.152	0.9992
----------	-------	--------	------	--------	-------	--------

Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
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Oxygen	6.200e-002	0.0010	1.984	0.0011	1.744e-003	0.0008
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H ₂ O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
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Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
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Total	62.00	1.0000	1737	1.0000	2.153	1.0000
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Mixed Feed (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Mixed Feed Fluid Package: Basis-1
Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction 1.0000 1.0000

Temperature: (C) 224.9 224.9

Pressure: (kPa) 900.0 900.0

Molar Flow (kgmole/h) 247.0 247.0

Mass Flow (kg/h) 2119 2119

Std Ideal Liq VolFlow (m³/h) 7.486 7.486

Molar Enthalpy (kJ/kgmole) 5.243e+03 5.243e+03

Molar Entropy (kJ/kgmole-C) 1.309e+02 1.309e+02

Heat Flow (kJ/h) 1.295e+06 1.295e+06

Liq VolFlow @Std Cond (m³/h) 5841 5841

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

(kgmole/h)	(kg/h)		(m ³ /h)			
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Hydrogen	184.4	0.7467	371.8	0.1755	5.323	0.7110
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Nitrogen	61.94	0.2508	1735	0.8189	2.152	0.2874
----------	-------	--------	------	--------	-------	--------

Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
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Oxygen	6.200e-002	0.0003	1.984	0.0009	1.744e-003	0.0002
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H2O	0.5550	0.0022	9.998	0.0047	1.002e-002	0.0013
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	247.0	1.0000	2119	1.0000	7.486	1.0000
Vapour Phase				Phase Fraction	1.000	
COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(kgmole/h)	(kg/h)	(m3/h)				
Hydrogen	184.4	0.7467	371.8	0.1755	5.323	0.7110
Nitrogen	61.94	0.2508	1735	0.8189	2.152	0.2874
Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	6.200e-002	0.0003	1.984	0.0009	1.744e-003	0.0002
H2O	0.5550	0.0022	9.998	0.0047	1.002e-002	0.0013
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	247.0	1.0000	2119	1.0000	7.486	1.0000

Compressed Feed (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Compressed Feed Fluid Package: Basis-1
Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction 1.0000 1.0000

Temperature: (C) 101.7 101.7

Pressure: (kPa) 1100 1100

Molar Flow (kgmole/h) 646.4 646.4

Mass Flow (kg/h) 6853 6853

Std Ideal Liq VolFlow (m3/h) 19.61 19.61

Molar Enthalpy (kJ/kgmole) -1.905e+03 -1.905e+03

Molar Entropy (kJ/kgmole-C) 1.284e+02 1.284e+02

Heat Flow (kJ/h) -1.231e+06 -1.231e+06

Liq VolFlow @Std Cond (m3/h) 1.528e+004 1.528e+004

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS MOLE FLOW

MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

(kgmole/h) (kg/h) (m3/h)

Hydrogen	409.9	0.6341	826.3	0.1206	11.83	0.6032
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Nitrogen	175.6	0.2717	4919	0.7177	6.100	0.3111
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Ammonia	55.62	0.0861	947.2	0.1382	1.537	0.0784
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Oxygen	4.720	0.0073	151.1	0.0220	0.1328	0.0068
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H2O	0.5550	0.0009	9.999	0.0015	1.002e-002	0.0005
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Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
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Total	646.4	1.0000	6853	1.0000	19.61	1.0000
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Vapour Phase Phase Fraction 1.00

COMPONENTS MOLE FLOW

MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

(kgmole/h) (kg/h) (m3/h)

Hydrogen	409.9	0.6341	826.3	0.1206	11.83	0.6032
----------	-------	--------	-------	--------	-------	--------

Nitrogen	175.6	0.2717	4919	0.7177	6.100	0.3111
----------	-------	--------	------	--------	-------	--------

Ammonia	55.62	0.0861	947.2	0.1382	1.537	0.0784
---------	-------	--------	-------	--------	-------	--------

Oxygen	4.720	0.0073	151.1	0.0220	0.1328	0.0068
--------	-------	--------	-------	--------	--------	--------

H2O	0.5550	0.0009	9.999	0.0015	1.002e-002	0.0005
-----	--------	--------	-------	--------	------------	--------

Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
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Total	646.4	1.0000	6853	1.0000	19.61	1.0000
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Preheated Feed (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Preheated Feed Fluid Package: Basis-1
Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction 1.0000 1.0000

Temperature: (C) 450.0 450.0

Pressure: (kPa) 1038 1038

Molar Flow (kgmole/h) 646.4 646.4

Mass Flow (kg/h) 6853 6853

Std Ideal Liq VolFlow (m3/h) 19.61 19.61

Molar Enthalpy (kJ/kgmole) 8.808e+03 8.808e+03

Molar Entropy (kJ/kgmole-C) 1.490e+02 1.490e+02

Heat Flow (kJ/h) 5.693e+06 5.693e+06

Liq VolFlow @Std Cond (m3/h) 1.528e+004 1.528e+004

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS MOLE FLOW

MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC

(kgmole/h) (kg/h) (m3/h)

Hydrogen	409.9	0.6341	826.3	0.1206	11.83	0.6032
----------	-------	--------	-------	--------	-------	--------

Nitrogen	175.6	0.2717	4919	0.7177	6.100	0.3111
----------	-------	--------	------	--------	-------	--------

Ammonia	55.62	0.0861	947.2	0.1382	1.537	0.0784
Oxygen	4.720	0.0073	151.1	0.0220	0.1328	0.0068
H2O	0.5550	0.0009	9.999	0.0015	1.002e-002	0.0005
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	646.4	1.0000	6853	1.0000	19.61	1.0000
Vapour Phase				Phase Fraction	1.000	
COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(kgmole/h)	(kg/h)	(m3/h)				
Hydrogen	409.9	0.6341	826.3	0.1206	11.83	0.6032
Nitrogen	175.6	0.2717	4919	0.7177	6.100	0.3111
Ammonia	55.62	0.0861	947.2	0.1382	1.537	0.0784
Oxygen	4.720	0.0073	151.1	0.0220	0.1328	0.0068
H2O	0.5550	0.0009	9.999	0.0015	1.002e-002	0.0005
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	646.4	1.0000	6853	1.0000	19.61	1.0000

Reactor Product (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Reactor Product Fluid Package: Basis-1
 Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH. LIQUID PH.

Vapour / Phase Fraction	1.0000	1.0000	0.0000
Temperature: (C)	550.0	550.0	550.0
Pressure: (kPa)	1038	1038	1038
Molar Flow (kgmole/h)	524.3	524.3	0.0000
Mass Flow (kg/h)	6853	6853	0.0000
Std Ideal Liq VolFlow (m3/h)	15.58	15.58	0.0000
Molar Enthalpy (kJ/kgmole)	2.252e+03	2.252e+03	2.252e+03
Molar Entropy (kJ/kgmole-C)	1.690e+02	1.690e+02	1.690e+02
Heat Flow (kJ/h)	1.181e+06	1.181e+06	0.000e-01
Liq VolFlow @Std Cond (m3/h)	1.238e+004	1.238e+004	0.0000

COMPOSITION

Overall Phase		Vapour Fraction	1.0000			
COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(kgmole/h)	(kg/h)	(m3/h)				
Hydrogen	226.7	0.4325	457.1	0.0667	6.543	0.4200
Nitrogen	114.5	0.2185	3208	0.4682	3.979	0.2554
Ammonia	177.7	0.3390	3026	0.4416	4.913	0.3154
Oxygen	4.720	0.0090	151.1	0.0220	0.1328	0.0085
H2O	0.5550	0.0011	9.999	0.0015	1.002e-002	0.0006
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	524.3	1.0000	6853	1.0000	15.58	1.0000

Vapour Phase Phase Fraction 1.000

COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(kgmole/h)	(kg/h)	(m3/h)				
Hydrogen	226.7	0.4325	457.1	0.0667	6.543	0.4200
Nitrogen	114.5	0.2185	3208	0.4682	3.979	0.2554
Ammonia	177.7	0.3390	3026	0.4416	4.913	0.3154
Oxygen	4.720	0.0090	151.1	0.0220	0.1328	0.0085
H2O	0.5550	0.0011	9.999	0.0015	1.002e-002	0.0006
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	524.3	1.0000	6853	1.0000	15.58	1.0000

Liquid Phase Phase Fraction 0.0000

COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(kgmole/h)	(kg/h)	(m3/h)				
Hydrogen	0.0000	0.4325	0.0000	0.0667	0.0000	0.4200
Nitrogen	0.0000	0.2185	0.0000	0.4682	0.0000	0.2554
Ammonia	0.0000	0.3390	0.0000	0.4416	0.0000	0.3154
Oxygen	0.0000	0.0090	0.0000	0.0220	0.0000	0.0085
H2O	0.0000	0.0011	0.0000	0.0015	0.0000	0.0006
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000

Condensed Reactor Product (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Condensed Reactor Product Fluid Package: Basis-1
 Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH. LIQUID PH.

Vapour / Phase Fraction	0.7633	0.7633	0.2367
Temperature: (C)	-30.00	-30.00	-30.00
Pressure: (kPa)	914.0	914.0	914.0
Molar Flow (kgmole/h)	524.3	400.2	124.1

Mass Flow (kg/h) 6853 4740 2113
 Std Ideal Liq VolFlow (m³/h) 15.58 12.15 3.425
 Molar Enthalpy (kJ/kgmole) -2.312e+04 -7.884e+03 -7.228e+04
 Molar Entropy (kJ/kgmole-C) 1.076e+02 1.207e+02 6.507e+01
 Heat Flow (kJ/h) -1.212e+07 -3.155e+06 -8.968e+06
 Liq VolFlow @Std Cond (m³/h) 1.238e+004 9459 3.445
COMPOSITION
 Overall Phase Vapour Fraction 0.7633
 COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (kgmole/h) (kg/h) (m³/h)
 Hydrogen 226.7 0.4325 457.1 0.0667 6.543 0.4200
 Nitrogen 114.5 0.2185 3208 0.4682 3.979 0.2554
 Ammonia 177.7 0.3390 3026 0.4416 4.913 0.3154
 Oxygen 4.720 0.0090 151.1 0.0220 0.1328 0.0085
 H₂O 0.5550 0.0011 9.999 0.0015 1.002e-002 0.0006
 Propane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Total 524.3 1.0000 6853 1.0000 15.58 1.0000
 Vapour Phase Phase Fraction 0.7633
 COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (kgmole/h) (kg/h) (m³/h)
 Hydrogen 226.7 0.5665 457.0 0.0964 6.542 0.5383
 Nitrogen 114.5 0.2862 3208 0.6768 3.978 0.3274
 Ammonia 54.25 0.1356 923.9 0.1949 1.500 0.1234
 Oxygen 4.712 0.0118 150.8 0.0318 0.1325 0.0109
 H₂O 1.204e-005 0.0000 2.169e-004 0.0000 2.174e-007 0.0000
 Propane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Total 400.2 1.0000 4740 1.0000 12.15 1.0000
 Liquid Phase Phase Fraction 0.2367
 COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (kgmole/h) (kg/h) (m³/h)
 Hydrogen 3.366e-002 0.0003 6.785e-002 0.0000 9.713e-004 0.0003
 Nitrogen 1.195e-002 0.0001 0.3347 0.0002 4.150e-004 0.0001
 Ammonia 123.5 0.9951 2103 0.9949 3.413 0.9966
 Oxygen 8.756e-003 0.0001 0.2802 0.0001 2.463e-004 0.0001
 H₂O 0.5550 0.0045 9.998 0.0047 1.002e-002 0.0029
 Propane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Total 124.1 1.0000 2113 1.0000 3.425 1.0000

Ammonia Product (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Ammonia Product Fluid Package: Basis-1
Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH. LIQUID PH.

Vapour / Phase Fraction 0.0000 0.0000 1.0000
 Temperature: (C) -32.03 -32.03 -32.03
 Pressure: (kPa) 800.0 800.0 800.0
 Molar Flow (kgmole/h) 122.3 0.0000 122.3
 Mass Flow (kg/h) 2084 0.0000 2084
 Std Ideal Liq VolFlow (m³/h) 3.377 0.0000 3.377
 Molar Enthalpy (kJ/kgmole) -7.245e+04 -8.108e+03 -7.245e+04
 Molar Entropy (kJ/kgmole-C) 6.443e+01 1.218e+02 6.443e+01
 Heat Flow (kJ/h) -8.864e+06 0.000e-01 -8.864e+06
 Liq VolFlow @Std Cond (m³/h) 3.397 0.0000 3.397

COMPOSITION

Overall Phase Vapour Fraction 0.0000
 COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (kgmole/h) (kg/h) (m³/h)
 Hydrogen 2.769e-002 0.0002 5.582e-002 0.0000 7.990e-004 0.0002
 Nitrogen 9.790e-003 0.0001 0.2742 0.0001 3.401e-004 0.0001
 Ammonia 121.7 0.9951 2073 0.9949 3.365 0.9966
 Oxygen 7.500e-003 0.0001 0.2400 0.0001 2.110e-004 0.0001
 H₂O 0.5550 0.0045 9.998 0.0048 1.002e-002 0.0030
 Propane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Total 122.3 1.0000 2084 1.0000 3.377 1.0000
 Vapour Phase Phase Fraction 0.0000
 COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (kgmole/h) (kg/h) (m³/h)
 Hydrogen 0.0000 0.5641 0.0000 0.0958 0.0000 0.5362
 Nitrogen 0.0000 0.2849 0.0000 0.6727 0.0000 0.3261
 Ammonia 0.0000 0.1393 0.0000 0.1999 0.0000 0.1268
 Oxygen 0.0000 0.0117 0.0000 0.0316 0.0000 0.0109
 H₂O 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Propane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

Total	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000
Liquid Phase					Phase Fraction	1.000
COMPONENTS	MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
(kgmole/h)	(kg/h)		(m3/h)			
Hydrogen	2.769e-002	0.0002	5.582e-002	0.0000	7.990e-004	0.0002
Nitrogen	9.790e-003	0.0001	0.2742	0.0001	3.401e-004	0.0001
Ammonia	121.7	0.9951	2073	0.9949	3.365	0.9966
Oxygen	7.500e-003	0.0001	0.2400	0.0001	2.110e-004	0.0001
H2O	0.5550	0.0045	9.998	0.0048	1.002e-002	0.0030
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	122.3	1.0000	2084	1.0000	3.377	1.0000

Cooled Reactor Product (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Cooled Reactor Product Fluid Package: Basis-1
Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction 1.0000 1.0000

Temperature: (C) 177.0 177.0

Pressure: (kPa) 976.0 976.0

Molar Flow (kgmole/h) 524.3 524.3

Mass Flow (kg/h) 6853 6853

Std Ideal Liq VolFlow (m3/h) 15.58 15.58

Molar Enthalpy (kJ/kgmole) -1.096e+04 -1.096e+04

Molar Entropy (kJ/kgmole-C) 1.483e+02 1.483e+02

Heat Flow (kJ/h) -5.743e+06 -5.743e+06

Liq VolFlow @Std Cond (m3/h) 1.238e+004 1.238e+004

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS	MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
(kgmole/h)	(kg/h)		(m3/h)			

Hydrogen	226.7	0.4325	457.1	0.0667	6.543	0.4200
----------	-------	--------	-------	--------	-------	--------

Nitrogen	114.5	0.2185	3208	0.4682	3.979	0.2554
----------	-------	--------	------	--------	-------	--------

Ammonia	177.7	0.3390	3026	0.4416	4.913	0.3154
---------	-------	--------	------	--------	-------	--------

Oxygen	4.720	0.0090	151.1	0.0220	0.1328	0.0085
--------	-------	--------	-------	--------	--------	--------

H2O	0.5550	0.0011	9.999	0.0015	1.002e-002	0.0006
-----	--------	--------	-------	--------	------------	--------

Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
---------	--------	--------	--------	--------	--------	--------

Total	524.3	1.0000	6853	1.0000	15.58	1.0000
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Vapour Phase Phase Fraction 1.000

COMPONENTS	MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
(kgmole/h)	(kg/h)		(m3/h)			

Hydrogen	226.7	0.4325	457.1	0.0667	6.543	0.4200
----------	-------	--------	-------	--------	-------	--------

Nitrogen	114.5	0.2185	3208	0.4682	3.979	0.2554
----------	-------	--------	------	--------	-------	--------

Ammonia	177.7	0.3390	3026	0.4416	4.913	0.3154
---------	-------	--------	------	--------	-------	--------

Oxygen	4.720	0.0090	151.1	0.0220	0.1328	0.0085
--------	-------	--------	-------	--------	--------	--------

H2O	0.5550	0.0011	9.999	0.0015	1.002e-002	0.0006
-----	--------	--------	-------	--------	------------	--------

Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
---------	--------	--------	--------	--------	--------	--------

Total	524.3	1.0000	6853	1.0000	15.58	1.0000
-------	-------	--------	------	--------	-------	--------

Mixed and Recycled (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Mixed and Recycled Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction 1.0000 1.0000

Temperature: (C) 64.37 64.37

Pressure: (kPa) 800.0 800.0

Molar Flow (kgmole/h) 646.4 646.4

Mass Flow (kg/h) 6853 6853

Std Ideal Liq VolFlow (m3/h) 19.61 19.61

Molar Enthalpy (kJ/kgmole) -3.006e+03 -3.006e+03

Molar Entropy (kJ/kgmole-C) 1.280e+02 1.280e+02

Heat Flow (kJ/h) -1.943e+06 -1.943e+06

Liq VolFlow @Std Cond (m3/h) 1.528e+004 1.528e+004

COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS	MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
(kgmole/h)	(kg/h)		(m3/h)			

Hydrogen	409.9	0.6341	826.3	0.1206	11.83	0.6032
----------	-------	--------	-------	--------	-------	--------

Nitrogen	175.6	0.2717	4919	0.7177	6.100	0.3111
----------	-------	--------	------	--------	-------	--------

Ammonia	55.62	0.0861	947.2	0.1382	1.537	0.0784
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Oxygen	4.720	0.0073	151.1	0.0220	0.1328	0.0068
H2O	0.5550	0.0009	9.999	0.0015	1.002e-002	0.0005
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	646.4	1.0000	6853	1.0000	19.61	1.0000
Vapour Phase	Phase Fraction 1.000					
COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(kgmole/h)	(kg/h)	(m3/h)				
Hydrogen	409.9	0.6341	826.3	0.1206	11.83	0.6032
Nitrogen	175.6	0.2717	4919	0.7177	6.100	0.3111
Ammonia	55.62	0.0861	947.2	0.1382	1.537	0.0784
Oxygen	4.720	0.0073	151.1	0.0220	0.1328	0.0068
H2O	0.5550	0.0009	9.999	0.0015	1.002e-002	0.0005
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	646.4	1.0000	6853	1.0000	19.61	1.0000

Overhead Recycle (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Overhead Recycle	Fluid Package: Basis-1					
Property Package: Peng-Robinson						
OVERALL VAPOUR PH. LIQUID PH.						
Vapour / Phase Fraction	1.0000	1.0000	0.0000			
Temperature: (C)	-32.03	-32.03	-32.03			
Pressure: (kPa)	800.0	800.0	800.0			
Molar Flow (kgmole/h)	401.9	401.9	0.0000			
Mass Flow (kg/h)	4769	4769	0.0000			
Std Ideal Liq VolFlow (m3/h)	12.20	12.20	0.0000			
Molar Enthalpy (kJ/kgmole)	-8.108e+03	-8.108e+03	-7.245e+04			
Molar Entropy (kJ/kgmole-C)	1.218e+02	1.218e+02	6.443e+01			
Heat Flow (kJ/h)	-3.259e+06	-3.259e+06	0.0000e-01			
Liq VolFlow @Std Cond (m3/h)	9500	9500	0.0000			
COMPOSITION						
Overall Phase	Vapour Fraction 1.0000					
COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC			
(kgmole/h)	(kg/h)	(m3/h)	LIQVOL FRAC			
Hydrogen	226.7	0.5641	457.0	0.0958	6.542	0.5362
Nitrogen	114.5	0.2849	3208	0.6727	3.979	0.3261
Ammonia	55.98	0.1393	953.3	0.1999	1.547	0.1268
Oxygen	4.713	0.0117	150.8	0.0316	0.1326	0.0109
H2O	1.082e-005	0.0000	1.949e-004	0.0000	1.953e-007	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	401.9	1.0000	4769	1.0000	12.20	1.0000
Vapour Phase	Phase Fraction 1.00					
COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(kgmole/h)	(kg/h)	(m3/h)				
Hydrogen	226.7	0.5641	457.0	0.0958	6.542	0.5362
Nitrogen	114.5	0.2849	3208	0.6727	3.979	0.3261
Ammonia	55.98	0.1393	953.3	0.1999	1.547	0.1268
Oxygen	4.713	0.0117	150.8	0.0316	0.1326	0.0109
H2O	1.082e-005	0.0000	1.949e-004	0.0000	1.953e-007	0.0000
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	401.9	1.0000	4769	1.0000	12.20	1.0000
Liquid Phase	Phase Fraction 0.0000					
COMPONENTS MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC	
(kgmole/h)	(kg/h)	(m3/h)				
Hydrogen	0.0000	0.0002	0.0000	0.0000	0.0000	0.0002
Nitrogen	0.0000	0.0001	0.0000	0.0001	0.0000	0.0001
Ammonia	0.0000	0.9951	0.0000	0.9949	0.0000	0.9966
Oxygen	0.0000	0.0001	0.0000	0.0001	0.0000	0.0001
H2O	0.0000	0.0045	0.0000	0.0048	0.0000	0.0030
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000

Recycle to Compressor (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Recycle to Compressor	Fluid Package: Basis-1	
Property Package: Peng-Robinson		
CONDITIONS	OVERALL VAPOUR PH.	
Vapour / Phase Fraction	1.0000	1.0000
Temperature: (C)	-32.03	-32.03
Pressure: (kPa)	800.0	800.0
Molar Flow (kgmole/h)	399.4	399.4
Mass Flow (kg/h)	4734	4734
Std Ideal Liq VolFlow (m3/h)	12.12	12.12

Molar Enthalpy (kJ/kgmole) -8.108e+03 -8.108e+03
 Molar Entropy (kJ/kgmole-C) 1.218e+02 1.218e+02
 Heat Flow (kJ/h) -3.238e+06 -3.238e+06
 Liq VolFlow @Std Cond (m3/h) 9439 9439
COMPOSITION
 Overall Phase Vapour Fraction 1.0000
 COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (kgmole/h) (kg/h) (m3/h)
 Hydrogen 225.4 0.5645 454.5 0.0960 6.505 0.5367
 Nitrogen 113.6 0.2846 3184 0.6724 3.948 0.3257
 Ammonia 55.62 0.1393 947.2 0.2001 1.537 0.1268
 Oxygen 4.658 0.0117 149.1 0.0315 0.1310 0.0108
 H2O 1.076e-005 0.0000 1.938e-004 0.0000 1.942e-007 0.0000
 Propane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Total 399.4 1.0000 4734 1.0000 12.12 1.0000
 Vapour Phase Phase Fraction 1.000
 COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (kgmole/h) (kg/h) (m3/h)
 Hydrogen 225.4 0.5645 454.5 0.0960 6.505 0.5367
 Nitrogen 113.6 0.2846 3184 0.6724 3.948 0.3257
 Ammonia 55.62 0.1393 947.2 0.2001 1.537 0.1268
 Oxygen 4.658 0.0117 149.1 0.0315 0.1310 0.0108
 H2O 1.076e-005 0.0000 1.938e-004 0.0000 1.942e-007 0.0000
 Propane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Total 399.4 1.0000 4734 1.0000 12.12 1.0000

Recycle without Purge (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Recycle without Purge Fluid Package: Basis-1
Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH. LIQUID PH.

Vapour / Phase Fraction 1.0000 1.0000 0.0000
 Temperature: (C) -32.03 -32.03 -32.03
 Pressure: (kPa) 800.0 800.0 800.0
 Molar Flow (kgmole/h) 401.9 401.9 0.0000
 Mass Flow (kg/h) 4769 4769 0.0000
 Std Ideal Liq VolFlow (m3/h) 12.20 12.20 0.0000
 Molar Enthalpy (kJ/kgmole) -8.108e+03 -8.108e+03 -7.245e+04
 Molar Entropy (kJ/kgmole-C) 1.218e+02 1.218e+02 6.443e+01
 Heat Flow (kJ/h) -3.259e+06 -3.259e+06 0.000e-01
 Liq VolFlow @Std Cond (m3/h) 9500 9500 0.0000

COMPOSITION

Overall Phase Vapour Fraction 1.0000
 COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (kgmole/h) (kg/h) (m3/h)
 Hydrogen 226.7 0.5641 457.0 0.0958 6.542 0.5362
 Nitrogen 114.5 0.2849 3208 0.6727 3.979 0.3261
 Ammonia 55.98 0.1393 953.3 0.1999 1.547 0.1268
 Oxygen 4.713 0.0117 150.8 0.0316 0.1326 0.0109
 H2O 1.082e-005 0.0000 1.949e-004 0.0000 1.953e-007 0.0000
 Propane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Total 401.9 1.0000 4769 1.0000 12.20 1.0000
 Vapour Phase Phase Fraction 1.000
 COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (kgmole/h) (kg/h) (m3/h)
 Hydrogen 226.7 0.5641 457.0 0.0958 6.542 0.5362
 Nitrogen 114.5 0.2849 3208 0.6727 3.979 0.3261
 Ammonia 55.98 0.1393 953.3 0.1999 1.547 0.1268
 Oxygen 4.713 0.0117 150.8 0.0316 0.1326 0.0109
 H2O 1.082e-005 0.0000 1.949e-004 0.0000 1.953e-007 0.0000
 Propane 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
 Total 401.9 1.0000 4769 1.0000 12.20 1.0000

Liquid Phase Phase Fraction 0.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC
 (kgmole/h) (kg/h) (m3/h)

Hydrogen	0.0000	0.0002	0.0000	0.0000	0.0000	0.0002
Nitrogen	0.0000	0.0001	0.0000	0.0001	0.0000	0.0001
Ammonia	0.0000	0.9951	0.0000	0.9949	0.0000	0.9966
Oxygen	0.0000	0.0001	0.0000	0.0001	0.0000	0.0001
H2O	0.0000	0.0045	0.0000	0.0048	0.0000	0.0030
Propane	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Total	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000

Refrigerant Propane (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Refrigerant Propane Fluid Package: Basis-1
Property Package: Peng-Robinson

CONDITIONS

	OVERALL	VAPOUR PH.	LIQUID PH.
Vapour / Phase Fraction	0.5021	0.5021	0.4979
Temperature: (C)	-30.70	-30.70	-30.70
Pressure: (kPa)	163.3	163.3	163.3
Molar Flow (kgmole/h)	756.5	379.8	376.7
Mass Flow (kg/h)	3.336e+004	1.675e+004	1.661e+004
Std Ideal Liq VolFlow (m ³ /h)	65.84	33.05	32.78
Molar Enthalpy (kJ/kgmole)	-1.171e+05	-1.080e+05	-1.262e+05
Molar Entropy (kJ/kgmole-C)	1.055e+02	1.429e+02	6.781e+01
Heat Flow (kJ/h)	-8.857e+07	-4.102e+07	-4.755e+07
Liq VolFlow @ Std Cond (m ³ /h)	65.71	32.99	32.72

Eq. View CB COMPOSITION

Overall Phase		Vapour Fraction 0.5021					
COMPONENTS MOLE FLOW		MOLE FRAC	MASS FLOW		MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
	(kgmole/h)	(kg/h)	(m ³ /h)				
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	756.5	1.0000	3.336e+004	1.0000	65.84	1.0000	
Total	756.5	1.0000	3.336e+004	1.0000	65.84	1.0000	
Vapour Phase			Phase Fraction 0.5021				

	COMPONENTS	MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC
	(kgmole/h)	(kg/h)		(m ³ /h)			
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	379.8	1.0000	1.675e+004	1.0000	33.05	1.0000	
Total	379.8	1.0000	1.675e+004	1.0000	33.05	1.0000	
Liquid Phase				Phase Fraction	0.4979		
	COMPONENTS	MOLE FLOW	MOLE FRAC	MASS FLOW	MASS FRAC	LIQVOL FLOW	LIQVOL FRAC

COMPOSITIONS MOLE FLOW		MOLE FRACTION		MASS FLOW		MASS FRACTION		LIQ VOL FLOW		LIQ VOL FRACTION	
	(kgmole/h)		(kg/h)		(m3/h)						
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H2O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	376.7	1.0000	1.661e+004	1.0000		32.78	1.0000				
Total	376.7	1.0000	1.661e+004	1.0000		32.78	1.0000				

Vapor Propane (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Vapor Propane Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

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OVERALL VAPOUR PH. LIQUID PH.

Vapour / Phase Fraction    1.0000  1.0000  0.0000
Temperature: (C)          -42.19   -42.19   -42.19
Pressure: (kPa)           101.3    101.3    101.3
Molar Flow (kgmole/h)     756.5    756.5    0.0000
Mass Flow (kg/h)          3.336e+004 3.336e+004 0.0000
Std Ideal Liq VolFlow (m3/h) 65.84   65.84   0.0000
Molar Enthalpy (kJ/kgmole) -1.087e+05 -1.087e+05 -1.274e+05
Molar Entropy (kJ/kgmole-C) 1.441e+02  1.441e+02  6.306e+01
Heat Flow (kJ/h)           -8.219e+07 -8.219e+07 0.000e-01
Liq VolFlow @ Std Cond (m3/h) 65.71   65.71   0.0000

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$\Omega = 11 \text{ Pl}$ $V_0 = 1.5 \text{ eV}$ $F_\pi = 1.0000$

Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	756.5	1.0000	3.336e+004	1.0000	65.84	1.0000
Total	756.5	1.0000	3.336e+004	1.0000	65.84	1.0000
Vapour Phase					Phase Fraction	1.000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC						
	(kgmole/h)	(kg/h)	(m ³ /h)			
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	756.5	1.0000	3.336e+004	1.0000	65.84	1.0000
Total	756.5	1.0000	3.336e+004	1.0000	65.84	1.0000
Liquid Phase					Phase Fraction	0.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC						
	(kgmole/h)	(kg/h)	(m ³ /h)			
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000
Total	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000

Compressed Propane (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Compressed Propane Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH. LIQUID PH.

Vapour / Phase Fraction	1.0000	1.0000	0.0000
Temperature: (C)	-4.998	-4.998	-4.998
Pressure: (kPa)	405.2	405.2	405.2
Molar Flow (kgmole/h)	756.5	756.5	0.0000
Mass Flow (kg/h)	3.336e+004	3.336e+004	0.0000
Std Ideal Liq VolFlow (m ³ /h)	65.84	65.84	0.0000
Molar Enthalpy (kJ/kgmole)	-1.066e+05	-1.066e+05	-1.235e+05
Molar Entropy (kJ/kgmole-C)	1.414e+02	1.414e+02	7.828e+01
Heat Flow (kJ/h)	-8.065e+07	-8.065e+07	0.0000e-01
Liq VolFlow @Std Cond (m ³ /h)	65.71	65.71	0.0000

COMPOSITION

Overall Phase	Vapour Fraction	1.0000
---------------	-----------------	--------

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC						
	(kgmole/h)	(kg/h)	(m ³ /h)			
Hydrogen	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000
Nitrogen	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000
Ammonia	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000
Oxygen	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000
H ₂ O	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000
Propane	756.5	1.0000	3.336e+004	1.0000	65.84	1.0000
Total	756.5	1.0000	3.336e+004	1.0000	65.84	1.0000
Vapour Phase					Phase Fraction	1.000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC						
	(kgmole/h)	(kg/h)	(m ³ /h)			
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	756.5	1.0000	3.336e+004	1.0000	65.84	1.0000
Total	756.5	1.0000	3.336e+004	1.0000	65.84	1.0000
Liquid Phase					Phase Fraction	0.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC						
	(kgmole/h)	(kg/h)	(m ³ /h)			

Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ O	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000
Total	0.0000	1.0000	0.0000	1.0000	0.0000	1.0000

Condensed Propane (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Condensed Propane Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL LIQUID PH. VAPOUR PH.

Vapour / Phase Fraction	0.0000	1.0000	0.0000
Temperature: (C)	47.24	47.24	47.24
Pressure: (kPa)	1619	1619	1619
Molar Flow (kgmole/h)	756.5	756.5	0.0000
Mass Flow (kg/h)	3.336e+004	3.336e+004	0.0000
Std Ideal Liq VolFlow (m ³ /h)	65.84	65.84	0.0000
Molar Enthalpy (kJ/kgmole)	-1.171e+05	-1.171e+05	-1.042e+05
Molar Entropy (kJ/kgmole-C)	9.984e+01	9.984e+01	1.400e+02
Heat Flow (kJ/h)	-8.857e+07	-8.857e+07	0.000e-01
Liq VolFlow @Std Cond (m ³ /h)	65.71	65.71	0.0000

COMPOSITION

Overall Phase	Vapour Fraction	0.0000
---------------	-----------------	--------

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC					
(kgmole/h)	(kg/h)	(m ³ /h)			
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000
Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ O	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	756.5	1.0000	3.336e+004	1.0000	65.84
Total	756.5	1.0000	3.336e+004	1.0000	65.84
Liquid Phase					1.0000
			Phase Fraction	1.000	

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC					
(kgmole/h)	(kg/h)	(m ³ /h)			
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000
Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ O	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	756.5	1.0000	3.336e+004	1.0000	65.84
Total	756.5	1.0000	3.336e+004	1.0000	65.84
Vapour Phase			Phase Fraction	0.0000	

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC					
(kgmole/h)	(kg/h)	(m ³ /h)			
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000
Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ O	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	0.0000	1.0000	0.0000	1.0000	0.0000
Total	0.0000	1.0000	0.0000	1.0000	0.0000

PROCESS UTILITY

Second Stage Compressed Propane (Material Stream): Conditions, Composition, K Value, Package Properties, Attachments

Material Stream: Second Stage Compressed Propane Fluid Package: Basis-1

Property Package: Peng-Robinson

CONDITIONS

OVERALL VAPOUR PH.

Vapour / Phase Fraction	1.0000	1.0000
Temperature: (C)	62.07	62.07
Pressure: (kPa)	1621	1621

Molar Flow (kgmole/h) 756.5 756.5
 Mass Flow (kg/h) 3.336e+004 3.336e+004
 Std Ideal Liq VolFlow (m³/h) 65.84 65.84
 Molar Enthalpy (kJ/kgmole-C) -1.028e+05 -1.028e+05
 Molar Entropy (kJ/kgmole-C) 1.443e+02 1.443e+02
 Heat Flow (kJ/h) -7.778e+07 -7.778e+07
 Liq VolFlow @Std Cond (m³/h) 65.71 65.71
 COMPOSITION

Overall Phase Vapour Fraction 1.0000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC					
(kgmole/h)	(kg/h)	(m ³ /h)			
Hydrogen	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000
Nitrogen	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000
Ammonia	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000
Oxygen	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000
H ₂ O	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000
Propane	756.5	1.0000	3.336e+004	1.0000	65.84 1.0000
Total	756.5	1.0000	3.336e+004	1.0000	65.84 1.0000
Vapour Phase					Phase Fraction 1.000

COMPONENTS MOLE FLOW MOLE FRAC MASS FLOW MASS FRAC LIQVOL FLOW LIQVOL FRAC					
(kgmole/h)	(kg/h)	(m ³ /h)			
Hydrogen	0.0000	0.0000	0.0000	0.0000	0.0000
Nitrogen	0.0000	0.0000	0.0000	0.0000	0.0000
Ammonia	0.0000	0.0000	0.0000	0.0000	0.0000
Oxygen	0.0000	0.0000	0.0000	0.0000	0.0000
H ₂ O	0.0000	0.0000	0.0000	0.0000	0.0000
Propane	756.5	1.0000	3.336e+004	1.0000	65.84 1.0000
Total	756.5	1.0000	3.336e+004	1.0000	65.84 1.0000

MIX-100 (Mixer): Design, Rating

Mixer: MIX-100

CONNECTIONS

Inlet Stream STREAM NAME FROM UNIT OPERATION
 Nitrogen
 SMR Hydrogen
 Outlet Stream STREAM NAME TO UNIT OPERATION
 Mixed Feed MIX-101 Mixer

PARAMETERS

User Variables

NOZZLE PARAMETERS

Base Elevation Relative to Ground Level 0.0000 m

	Nitrogen	SMR Hydrogen	Mixed Feed
Diameter (m)	5.000e-002	5.000e-002	5.000e-002
Elevation (Base) (m)	0.0000	0.0000	0.0000
Elevation (Ground) (m)	0.0000	0.0000	0.0000

MIX-101 (Mixer): Design, Rating

Mixer: MIX-101

CONNECTIONS

Inlet Stream STREAM NAME FROM UNIT OPERATION
 Mixed Feed MIX-100 Mixer
 Recycle to Compressor RCY-1 Recycle
 Outlet Stream STREAM NAME TO UNIT OPERATION
 Mixed and Recycled K-100 Compressor

PARAMETERS

User Variables

NOZZLE PARAMETERS

Base Elevation Relative to Ground Level 0.0000 m

	Mixed Feed	Recycle to Compressor	Mixed and Recycled
Diameter (m)	5.000e-002	5.000e-002	5.000e-002
Elevation (Base) (m)	0.0000	0.0000	0.0000
Elevation (Ground) (m)	0.0000	0.0000	0.0000

K-100 (Compressor): Design, Rating, Performance

Compressor: K-100

DESIGN

Connections

Inlet Stream

STREAM NAME FROM UNIT OPERATION
Mixed and Recycled MIX-101 Mixer

Outlet Stream

STREAM NAME TO UNIT OPERATION
Compressed Feed Named E-106 Heat Exchanger

Energy Stream

STREAM NAME FROM UNIT OPERATION
Stage 1 Compression Energy

Parameters

Speed: 1325 rpm Duty: 1.9774e+02 kW
Adiabatic Eff.: 85.00 PolyTropic Eff.: 85.65
Adiabatic Head: 9003 m Polytropic Head: 9072 m
Adiabatic Fluid Head: 88.29 kJ/kg Polytropic Fluid Head: 88.97 kJ/kg
Polytropic Exp. 1.498 Isentropic Exp. 1.399 Poly Head Factor 1.000

RECIPROCATING SETTINGS

Number of Cylinders: 1 Cylinder Type: Single-acting, Outer End
Bore: 0.2000 m Stroke: 1.000 m
Piston Rod Diameter: 2.500e-002 m Const. Vol. Efficiency Loss: 4.00 %
Default Fixed Clearance Vol.: 15.00 % Zero Speed Flow Resistance: 0.0000 kg/hr/sqrt(kPa-kg/m³)
Typical Design Speed: --- Volumetric Efficiency: 90.81 %
Speed: 1325 rpm

1

Fixed Clearance Vol. (m³) 4.712e-003
Variable Clearance Vol. (m³) 0.0000
Variable Volume Enabled Off
Cylinder is unloaded Off

User Variables

RATING

Nozzle Parameters

Base Elevation Relative to Ground Level 0.0000 m

Mixed and Recycled Compressed Feed

Diameter (m) 5.000e-002 5.000e-002
Elevation (Base) (m) 0.0000 0.0000
Elevation (Ground) (m) 0.0000 0.0000

Inertia

Rotational inertia (kg-m²) 6.000 Radius of gyration (m) 0.2000
Mass (kg) 150.0 Friction loss factor (rad/min) (kg-m²/s) 6.000e-003

PERFORMANCE

Results

Adiabatic Head (m) 9003 Power Consumed (kW) 197.7
Polytropic Head (m) 9072 Polytropic Head Factor 1.000
Adiabatic Fluid Head (kJ/kg) 88.29 Polytropic Exponent 1.498
Polytropic Fluid Head (kJ/kg) 88.97 Isentropic Exponent 1.399
Adiabatic Efficiency 85 Speed (rpm) 1325
Polytropic Efficiency 86 ---

Power/Torque

Total Rotor Power (kW) 197.7 Total Rotor Torque (N-m) 1425
Transient Rotor Power (kW) 0.0000 Transient Rotor Torque (N-m) 0.0000
Friction Power Loss (kW) 0.0000 Friction Torque Loss (N-m) 0.0000
Fluid Power (kW) 197.7 Fluid Torque (N-m) 1425

K-101 (Compressor): Design, Rating, Performance

Compressor: K-101

DESIGN

Connections

Inlet Stream

STREAM NAME FROM UNIT OPERATION
Vapor Propane Named E-107 Heat Exchanger

Outlet Stream

STREAM NAME TO UNIT OPERATION
Compressed Propane K-102 Compressor

Energy Stream

STREAM NAME FROM UNIT OPERATION
Propane Compressor Energy

Parameters

Speed: 1.344e+004 rpm Duty: 4.2812e+02 kW
Adiabatic Eff.: 135.69 PolyTropic Eff.: 132.50

Adiabatic Head: --- Polytropic Head: 6242 m
 Adiabatic Fluid Head: --- Polytropic Fluid Head: 61.22 kJ/kg
 Polytropic Exp. 1.064 Isentropic Exp. 1.104 Poly Head Factor 1.006
RECIPROCATING SETTINGS
 Number of Cylinders: 1 Cylinder Type: Single-acting, Outer End
 Bore: 0.2000 m Stroke: 1.000 m
 Piston Rod Diameter: 2.500e-002 m Const. Vol. Efficiency Loss: 4.00 %
 Default Fixed Clearance Vol.: 15.00 % Zero Speed Flow Resistance: 0.0000 kg/hr/sqrt(kPa-kg/m³)
 Typical Design Speed: --- Volumetric Efficiency: 54.72 %
 Speed: 1.344e+004 rpm
 1
 Fixed Clearance Vol. (m³) 4.712e-003
 Variable Clearance Vol. (m³) 0.0000
 Variable Volume Enabled Off
 Cylinder is unloaded Off
 User Variables
RATING
 Nozzle Parameters
 Base Elevation Relative to Ground Level 0.0000 m
 Vapor Propane Compressed Propane
 Diameter (m) 5.000e-002 5.000e-002
 Elevation (Base) (m) 0.0000 0.0000
 Elevation (Ground) (m) 0.0000 0.0000
 Inertia
 Rotational inertia (kg-m²) 6.000 Radius of gyration (m) 0.2000
 Mass (kg) 150.0 Friction loss factor (rad/min) (kg-m²/s) 6.000e-003
PERFORMANCE
 Results
 Adiabatic Head (m) --- Power Consumed (kW) 428.1
 Polytropic Head (m) 6242 Polytropic Head Factor 1.006
 Adiabatic Fluid Head (kJ/kg) --- Polytropic Exponent 1.064
 Polytropic Fluid Head (kJ/kg) 61.22 Isentropic Exponent 1.104
 Adiabatic Efficiency 136 Speed (rpm) 1.344e+004
 Polytropic Efficiency 132 ---
 Power/Torque
 Total Rotor Power (kW) 428.1 Total Rotor Torque (N-m) 304.2
 Transient Rotor Power (kW) 0.0000 Transient Rotor Torque (N-m) 0.0000
 Friction Power Loss (kW) 0.0000 Friction Torque Loss (N-m) 0.0000
 Fluid Power (kW) 428.1 Fluid Torque (N-m) 304.2

K-102 (Compressor): Design, Rating, Performance

Compressor: K-102
DESIGN
 Connections
 Inlet Stream
 STREAM NAME FROM UNIT OPERATION
 Compressed Propane K-101 Compressor
 Outlet Stream
 STREAM NAME TO UNIT OPERATION
 Second Stage Compressed Propane AC-100 Air cooler
 Energy Stream
 STREAM NAME FROM UNIT OPERATION
 Second Compressed Propane Energy
 Parameters
 Speed: --- Duty: 7.9884e+02 kW
 Adiabatic Eff.: 75.00 PolyTropic Eff.: 77.52
 Adiabatic Head: 6593 m Polytropic Head: 6815 m
 Adiabatic Fluid Head: 64.66 kJ/kg Polytropic Fluid Head: 66.83 kJ/kg
 Polytropic Exp. 1.054 Isentropic Exp. 1.004 Poly Head Factor 1.017
 User Variables
RATING
 Curves
 Compressor Speed: --- Efficiency: Adiabatic Curves Enabled: Yes
 Head Offset: 0.0000 m Efficiency Offset: 0.00 %
 Speed:
 Flow Head Efficiency (%) Surge Curve: Inactive
 Flow Limits Surge Curve: Inactive
 Speed Flow
 Stone Wall Curve: Inactive
 Speed Flow
 Surge Flow Rate --- Field Flow Rate 3768 ACT_m³/h Stone Wall Flow --- Compressor Volume 0.0000 m³
 Nozzle Parameters
 Base Elevation Relative to Ground Level 0.0000 m

Compressed Propane Second Stage Compressed Propane

Diameter (m)	5.000e-002	5.000e-002
Elevation (Base) (m)	0.0000	0.0000
Elevation (Ground) (m)	0.0000	0.0000
Inertia		
Rotational inertia (kg-m ²)	6.000	Radius of gyration (m) 0.2000
Mass (kg)	150.0	Friction loss factor (rad/min) (kg-m ² /s) 6.000e-003

PERFORMANCE

Results

Adiabatic Head (m)	6593	Power Consumed (kW) 798.8
Polytropic Head (m)	6815	Polytropic Head Factor 1.017
Adiabatic Fluid Head (kJ/kg)	64.66	Polytropic Exponent 1.054
Polytropic Fluid Head (kJ/kg)	66.83	Isentropic Exponent 1.004
Adiabatic Efficiency	75	Speed (rpm) ---
Polytropic Efficiency	78	---

Power/Torque

Total Rotor Power (kW)	798.8	Total Rotor Torque (N-m) ---
Transient Rotor Power (kW)	0.0000	Transient Rotor Torque (N-m) ---
Friction Power Loss (kW)	0.0000	Friction Torque Loss (N-m) ---
Fluid Power (kW)	798.8	Fluid Torque (N-m) ---

V-100 (Separator): Design, Reactions, Rating, Carry Over

Separator: V-100

CONNECTIONS

Inlet Stream

Stream Name From Unit Operation

Condensed Reactor Product Heat Exchanger: Named E-107

Outlet Stream

Stream Name To Unit Operation

Overhead Recycle Tee: TEE-100

Ammonia Product

Energy Stream

Stream Name From Unit Operation

PARAMETERS

Vessel Volume: --- Level SP: 50.00 % Liquid Volume: ---

Vessel Pressure: 800.0 kPa Pressure Drop: 114.0 kPa Duty: 0.0000 kJ/h Heat Transfer Mode: Heating

User Variables

RATING

Base Elevation Relative to Ground Level 0.0000 m Diameter --- Length ---

Condensed Reactor Product Overhead Recycle Ammonia Product

Diameter (m)	5.000e-002	5.000e-002	5.000e-002
--------------	------------	------------	------------

Elevation (Base) (m)	0.0000	0.0000	0.0000
----------------------	--------	--------	--------

Elevation (Ground) (m)	0.0000	0.0000	0.0000
------------------------	--------	--------	--------

Elevation (% of Height) (%) ---	---	---
---------------------------------	-----	-----

Level Taps: Level Tap Specification

Level Tap PV High PV Low OP High OP Low

Level Taps: Calculated Level Tap Values

Level Tap Liquid Level Aqueous Level

Options

PV Work Term Contribution (%) 100.00

Named E-106 (Heat Exchanger): Design, Rating, Details, Tables, HTFS Results, Exchanger Design and Rating

Heat Exchanger: Named E-106

CONNECTIONS

Tube Side Shell Side

Inlet	Outlet	Inlet	Outlet
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Name Reactor Product Name	Cooled Reactor Product Name	Compressed Feed Name	Preheated Feed
---------------------------	-----------------------------	----------------------	----------------

From Op. PFR-100	To Op. Named E-107	From Op. K-100	To Op. PFR-100
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Op. Type Plug Flow Reactor	Op. Type Heat Exchanger	Op. Type Compressor	Op. Type Plug Flow Reactor
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Temp 550.00 C	Temp 177.02 C	Temp 101.65 C	Temp 450.00 C
---------------	---------------	---------------	---------------

PARAMETERS

Heat Exchanger Model: Simple End Point

Tube Side DeltaP: 62.00 kPa Shell Side DeltaP: 62.00 kPa Passes: ---

UA: 7.949e+004 kJ/C-h Tolerance: 1.0000e-04

Tube Side Data Shell Side Data

Heat Transfer Coeff --- Heat Transfer Coeff ---

Tube Pressure Drop 62.00 kPa	Shell Pressure Drop 62.00 kPa
------------------------------	-------------------------------

Fouling 0.00000 C-h-m ² /kJ	Fouling 0.00000 C-h-m ² /kJ
--	--

Tube Length 6.00 m	Shell Passes 1
--------------------	----------------

Tube O.D. 20.00 mm	Shell Series 1
--------------------	----------------

Tube Thickness 2.0000 mm	Shell Parallel 1
--------------------------	------------------

Tube Pitch 50.0000 mm	Baffle Type Single
-----------------------	--------------------

Orientation Horizontal Baffle Cut(%Area) 20.00
 Passes Per Shell 2 Baffle Orientation Horizontal
 Tubes Per Shell 160 Spacing 800.0000 mm
 Layout Angle Triangular (30 degrees) Diameter 739.0488 mm
 TEMA Type A E L Area 60.32 m²
 SPEC'S

Spec	Value	curr Value	Rel Error	Active	Estimate
E-100 Heat Balance	0.0000 kJ/h	0.0000 kJ/h	0.0000	On	Off
E-100 UA	---	7.949e+004 kJ/C-h	---	On	Off

Detailed Specifications

E-100 Heat Balance

Type: Duty	Pass: Error	Spec Value: 0.0000 kJ/h
E-100 UA		
Type: UA	Pass: Overall	Spec Value: ---

User Variables

RATING

Sizing

Overall Data

Configuration

of Shells in Series 1 Tube Passes per Shell 2 Elevation (Base) 0.0000 m

of Shells in Parallel 1 Exchange Orientation Horizontal First Tube Pass Flow Direction Counter

TEMA Type: A E L

Calculated Information

Shell HT Coeff ---	Tube HT Coeff ---
Overall U 1318 kJ/h-m ² -C	Overall UA 7.949e+004 kJ/C-h
Shell DP 62.00 kPa	Tube DP 62.00 kPa
Shell Vol per Shell 2.272 m ³	Tube Vol per Shell 0.1930 m ³
HT Area per Shell 60.32 m ²	

Shell Data

Shell and Tube Bundle

Shell Diameter 739.0	Tube Pitch 50.00	Shell Fouling 0.0000
(mm)	(mm)	(C-h-m ² /kJ)

of Tubes per Shell 160 Tube Layout Angle Triangular (30 degrees)

Shell Baffles

Shell Baffle Type Single	Shell Baffle Orientation Horizontal
Baffle Cut (%Area) 20.00	Baffle Spacing 800.0 mm

Tube Data

Dimensions

OD 20.00	ID 16.00	Tube Thickness 2.000	Tube Length 6.000
(mm)	(mm)	(mm)	(m)

Tube Properties

Tube Fouling 0.0000 Thermal Cond. 45.00 Wall Cp ---	Wall Density ---		
(C-h-m ² /kJ)	(W/m-K)	(kJ/kg-C)	(kg/m ³)

Nozzle Parameters

Base Elevation Relative to Ground Level 0.0000 m

Reactor Product	Compressed Feed	Cooled Reactor Product
-----------------	-----------------	------------------------

Diameter (m)	5.000e-002	5.000e-002	5.000e-002
Elevation (Base) (m)	0.0000	0.0000	0.0000
Elevation (Ground) (m)	0.0000	0.0000	0.0000
Elevation (% of Height) (%) 0.00	0.00	0.00	0.00

Preheated Feed

Diameter (m)	5.000e-002
Elevation (Base) (m)	0.0000
Elevation (Ground) (m)	0.0000
Elevation (% of Height) (%) 0.00	0.00

DETAILS

Overall/Detailed Performance

Duty: 6.924e+06 kJ/h	UA Curv. Error: 0.00e-01 kJ/C-h
Heat Leak: 0.000e-01 kJ/h	Hot Pinch Temp: 177.0 C
Heat Loss: 0.000e-01 kJ/h	Cold Pinch Temp: 101.7 C
UA: 7.949e+04 kJ/C-h	Ft Factor: ---
Min. Approach: 75.37 C	Uncorrected Lmtd: ---
Lmtd: 87.11 C	

TABLES

Shell Side - Overall Phase

Temperature (C)	Pressure (kPa)	Heat Flow (kJ/h)	Enthalpy (kJ/kgmole)
101.65	1100.00	0.00	-1904.57
450.00	1038.00	6924087.72	8808.00

UA Molar Vap Frac Mass Vap Frac Heat of Vap.
 (kJ/C-h) (kg/mole)
 0.00 1.0000 1.0000 ---
 0.00 1.0000 1.0000 ---
 Shell Side - Vapour Phase

Mass Flow	Molecular Wt	Density	Mass Sp	Heat	Viscosity	Thermal Cond
(kg/h)	(kg/m3)	(kJ/kg-C)	(cP)	(W/m-K)		
6853.17	10.60	3.74	2.81	0.01	0.11	
6853.17	10.60	1.83	2.99	0.02	0.18	
Std Gas Flow Z Factor	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega		
(STD_m3/h)	(kPa)	(C)				
15282.62	1.00	2782.77	-181.08	0.29	-0.04	
15282.62	1.00	2782.77	-181.08	0.29	-0.04	
Shell Side - Light Liquid Phase						
Temperature	Pressure	Heat Flow	Enthalpy			
(C)	(kPa)	(kJ/h)	(kJ/kgmole)			
177.02	975.96	0.00	-10955.12			
550.00	1037.96	6924087.72	2252.37			
UA Molar Vap Frac	Mass Vap Frac	Heat of Vap.				
(kJ/C-h)	(kg/mole)					
0.00	1.0000	1.0000	---			
0.00	1.0000	1.0000	---			
Tube Side - Vapour Phase						
Mass Flow	Molecular Wt	Density	Mass Sp	Heat	Viscosity	Thermal Cond
(kg/h)	(kg/m3)	(kJ/kg-C)	(cP)	(W/m-K)		
6853.11	13.07	3.41	2.53	0.02	0.09	
6853.11	13.07	1.98	2.89	0.02	0.16	
Std Gas Flow Z Factor	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega		
(STD_m3/h)	(kPa)	(C)				
12395.71	1.00	5202.39	-91.56	0.29	0.04	
12395.71	1.00	5202.39	-91.56	0.29	0.04	
Tube Side - Light Liquid Phase						
Mass Flow	Density	Mass Sp	Heat	Viscosity	Thermal Cond	Surface Tens
(kg/h)	(kg/m3)	(kJ/kg-C)	(cP)	(W/m-K)	(dyne/cm)	
---	---	---	---	---	---	
0.00	1.98	2.89	0.00	0.11	0.00	
Molecular Wt Sp Gravity	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega		
(kPa)	(C)					
---	---	---	---	---	---	
13.07	0.00	5202.38	-91.56	0.29	0.04	
Tube Side - Heavy Liquid Phase						
(kg/h)	(kg/m3)	(kJ/kg-C)	(cP)	(W/m-K)	(dyne/cm)	
---	---	---	---	---	---	
0.00	1.98	2.89	0.00	0.11	---	
Molecular Wt Sp Gravity	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega		
(kPa)	(C)					
---	---	---	---	---	---	
13.07	0.00	5202.38	-91.56	0.29	0.04	
HTFS						
Exchanger Design and Rating						
Tube Side	Shell Side					
Inlet	Outlet	Inlet	Outlet			
Name Cooled Reactor Product Name	Condensed Reactor Product Name	Refrigerant Propane Name	Vapor Propane			
From Op. Named E-106 To Op. V-100	From Op. VLV-100	To Op. K-101				
Op. Type Heat Exchanger	Op. Type Separator	Op. Type Valve	Op. Type Compressor			
Temp 177.02 C	Temp -30.00 C	Temp -30.70 C	Temp -42.19 C			

Tube Thickness 2.0000 mm Shell Parallel 1
 Tube Pitch 50.0000 mm Baffle Type Single
 Orientation Horizontal Baffle Cut(%Area) 20.00
 Passes Per Shell 2 Baffle Orientation Horizontal
 Tubes Per Shell 160 Spacing 800.0000 mm
 Layout Angle Triangular (30 degrees) Diameter 739.0488 mm
 TEMA Type A E L Area 60.32 m²
 SPECS

Spec	Value	Curr Value	Rel Error	Active	Estimate
E-104 Heat Balance	0.0000 kJ/h	-2.774e-005 kJ/h	-4.348e-012	On	Off
E-104 UA	---	1.609e+005 kJ/C-h	---	On	Off

Detailed Specifications

E-104 Heat Balance
 Type: Duty Pass: Error Spec Value: 0.0000 kJ/h
 E-104 UA
 Type: UA Pass: Overall Spec Value: ---
 User Variables

RATING

Sizing

Overall Data
 Configuration
 # of Shells in Series 1 Tube Passes per Shell 2 Elevation (Base) 0.0000 m
 # of Shells in Parallel 1 Exchange Orientation Horizontal First Tube Pass Flow Direction Counter
 TEMA Type: A E L

Calculated Information

Shell HT Coeff --- Tube HT Coeff ---
 Overall U 2668 kJ/h-m²-C Overall UA 1.609e+005 kJ/C-h
 Shell DP 62.00 kPa Tube DP 62.00 kPa
 Shell Vol per Shell 2.272 m³ Tube Vol per Shell 0.1930 m³

HT Area per Shell 60.32 m²

Shell Data

Shell and Tube Bundle

Shell Diameter 739.0 Tube Pitch 50.00 Shell Fouling 0.0000
 (mm) (mm) (C-h-m²/kJ)

of Tubes per Shell 160 Tube Layout Angle Triangular (30 degrees)

Shell Baffles

Shell Baffle Type Single Shell Baffle Orientation Horizontal
 Baffle Cut (%Area) 20.00 Baffle Spacing 800.0 mm

Tube Data

Dimensions
 OD 20.00 ID 16.00 Tube Thickness 2.000 Tube Length 6.000
 (mm) (mm) (mm) (m)

Tube Properties

Tube Fouling 0.0000 Thermal Cond. 45.00 Wall Cp --- Wall Density ---
 (C-h-m²/kJ) (W/m-K) (kJ/kg-C) (kg/m³)

Nozzle Parameters

Base Elevation Relative to Ground Level 0.0000 m

	Cooled Reactor Product Refrigerant Propane Condensed Reactor Product
Diameter (m)	5.000e-002 5.000e-002 5.000e-002
Elevation (Base) (m)	0.0000 0.0000 0.0000
Elevation (Ground) (m)	0.0000 0.0000 0.0000
Elevation (% of Height) (%)	0.00 0.00 0.00

Vapor Propane

Diameter (m) 5.000e-002
 Elevation (Base) (m) 0.0000
 Elevation (Ground) (m) 0.0000
 Elevation (% of Height) (%) 0.00

DETAILS

Overall/Detailed Performance

Duty: 6.379e+06 kJ/h UA Curv. Error: 0.00e-01 kJ/C-h
 Heat Leak: 0.000e-01 kJ/h Hot Pinch Temp: -30.00 C
 Heat Loss: 0.000e-01 kJ/h Cold Pinch Temp: -30.70 C
 UA: 1.609e+05 kJ/C-h Ft Factor: ---
 Min. Approach: 0.6979 C Uncorrected Lmtd: 39.65 C
 Lmtd: 39.65 C

TABLES

Shell Side - Overall Phase

Temperature (C)	Pressure (kPa)	Heat Flow (kJ/h)	Enthalpy (kJ/kgmole)
-30.70	163.30	0.00	-117083.32

-42.19 101.30 6379448.55 -108650.50
UA Molar Vap Frac Mass Vap Frac Heat of Vap.
(kJ/C-h) (kJ/kgmole)
0.00 0.5021 0.5021 ---
0.00 1.0000 1.0000 ---

Shell Side - Vapour Phase

Mass Flow Molecular Wt Density Mass Sp Heat Viscosity Thermal Cond
(kg/h) (kg/m3) (kJ/kg-C) (cP) (W/m-K)
16748.19 44.10 3.75 1.49 0.01 0.01
33359.47 44.10 2.41 1.43 0.01 0.01
Std Gas Flow Z Factor Pseudo Pc Pseudo Tc Pseudo Zc Pseudo Omega
(STD_m3/h) (kPa) (C)
--- 0.95 4256.66 96.75 0.28 0.15
--- 0.97 4256.66 96.75 0.28 0.15

Shell Side - Light Liquid Phase

Mass Flow Density Mass Sp Heat Viscosity Thermal Cond Surface Tens
(kg/h) (kg/m3) (kJ/kg-C) (cP) (W/m-K) (dyne/cm)
16611.27 567.95 2.26 0.17 0.13 13.93
0.00 581.52 2.18 0.20 0.13 15.48
Molecular Wt Sp Gravity Pseudo Pc Pseudo Tc Pseudo Zc Pseudo Omega
(kPa) (C)
44.10 0.57 4256.66 96.75 0.28 0.15
44.10 0.58 4256.66 96.75 0.28 0.15

Shell Side - Heavy Liquid Phase

Mass Flow Density Mass Sp Heat Viscosity Thermal Cond Surface Tens
(kg/h) (kg/m3) (kJ/kg-C) (cP) (W/m-K) (dyne/cm)
--- --- --- --- --- ---
--- --- --- --- --- ---
Molecular Wt Sp Gravity Pseudo Pc Pseudo Tc Pseudo Zc Pseudo Omega
(kPa) (C)
--- --- --- --- --- ---
--- --- --- --- --- ---

Shell Side - Mixed Liquid

Mass Flow Density Mass Sp Heat Viscosity Thermal Cond Surface Tens
(kg/h) (kg/m3) (kJ/kg-C) (cP) (W/m-K) (dyne/cm)
16611.27 567.95 2.26 0.17 0.13 ---
0.00 581.52 2.18 0.20 0.13 ---
Molecular Wt Sp Gravity Pseudo Pc Pseudo Tc Pseudo Zc Pseudo Omega
(kPa) (C)
44.10 0.57 4256.66 96.75 0.28 0.15
44.10 0.58 4256.66 96.75 0.28 0.15

Tube Side - Overall Phase

Temperature Pressure Heat Flow Enthalpy
(C) (kPa) (kJ/h) (kJ/kgmole)
-30.00 913.96 0.00 -23123.73
24.11 950.79 3789108.02 -15896.12
177.02 975.96 6379448.55 -10955.12
UA Molar Vap Frac Mass Vap Frac Heat of Vap.
(kJ/C-h) (kJ/kgmole)

0.00 0.7633 0.6916 ---
0.00 1.0000 1.0000 ---
0.00 1.0000 1.0000 ---

Tube Side - Vapour Phase

Mass Flow Molecular Wt Density Mass Sp Heat Viscosity Thermal Cond
(kg/h) (kg/m3) (kJ/kg-C) (cP) (W/m-K)
4739.86 11.84 5.39 2.52 0.01 0.07
6853.11 13.07 5.10 2.43 0.01 0.07
6853.11 13.07 3.41 2.53 0.02 0.09
Std Gas Flow Z Factor Pseudo Pc Pseudo Tc Pseudo Zc Pseudo Omega
(STD_m3/h) (kPa) (C)
9462.09 0.99 3305.22 -161.29 0.29 -0.02
12395.71 0.99 5202.39 -91.56 0.29 0.04
12395.71 1.00 5202.39 -91.56 0.29 0.04

Tube Side - Light Liquid Phase

Mass Flow Density Mass Sp Heat Viscosity Thermal Cond Surface Tens
(kg/h) (kg/m3) (kJ/kg-C) (cP) (W/m-K) (dyne/cm)
2113.25 670.75 4.47 0.24 0.61 39.17
0.00 782.22 4.55 0.34 0.54 49.80
--- --- --- --- --- ---
Molecular Wt Sp Gravity Pseudo Pc Pseudo Tc Pseudo Zc Pseudo Omega

		(kPa)	(C)			
17.03	0.67	11321.51	133.33	0.27	0.26	
17.53	0.78	16827.30	256.14	0.27	0.30	
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Tube Side - Heavy Liquid Phase

Mass Flow	Density	Mass Sp	Heat	Viscosity	Thermal	Cond	Surface	Tens
(kg/h)	(kg/m ³)	(kJ/kg-C)	(cP)	(W/m-K)	(dyne/cm)			

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Molecular Wt	Sp Gravity	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega			
(kPa)	(C)							

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Tube Side - Mixed Liquid

Mass Flow	Density	Mass Sp	Heat	Viscosity	Thermal	Cond	Surface	Tens
(kg/h)	(kg/m ³)	(kJ/kg-C)	(cP)	(W/m-K)	(dyne/cm)			

2113.25	670.75	4.47	0.24	0.61	---			
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0.00	782.22	4.55	0.34	0.54	---			
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Molecular Wt	Sp Gravity	Pseudo Pc	Pseudo Tc	Pseudo Zc	Pseudo Omega			
(kPa)	(C)							

17.03	0.67	11321.51	133.33	0.27	0.26			
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17.53	0.78	16827.30	256.14	0.27	0.30			
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HTFS

Exchanger Design and Rating

RCY-1 (Recycle): Design

Recycle: RCY-1

CONNECTIONS

Inlet Stream

Stream Name From Unit Operation

Recycle without Purge TEE-100 Tee

Outlet Stream

Stream Name To Unit Operation

Recycle to Compressor MIX-101 Mixer

TOLEURANCE

Vapour Fraction: 10.00 Temperature: 10.00 Pressure: 10.00

Flow: 10.00 Enthalpy: 10.00 Composition: 10.00

NUMERICAL

Acceleration Type: Wegstein Iteration Type: Nested

Maximum Iterations: 10 Iteration Count: 0

Wegstein Count: 3 Q Minimum: -20.00 Q Maximum: 0.0000

Iteration History

Iteration Variable	Outlet Value	Inlet Value
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0 Converged	--	--
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User Variables

PFR-100 (Plug Flow Reactor): Design, Rating, Performance

Plug Flow Reactor: PFR-100

CONNECTIONS

Inlet Stream

STREAM NAME FROM UNIT OPERATION

Preheated Feed Named E-106 Heat Exchanger

Outlet Stream

STREAM NAME TO UNIT OPERATION

Reactor Product Named E-106 Heat Exchanger

Energy Stream

STREAM NAME TO UNIT OPERATION

PBR Jacket Cooling

PARAMETERS

Physical Parameters

Type : Ergun Equation Pressure Drop: 3.556e-002 kPa

Heat Transfer

Type : Direct Q Value Energy Stream : PBR Jacket Cooling Duty : 4.512e+006 kJ/h

Dimensions

Total Volume: 538.4 m³ Length: 18.42 m Diameter: 6.100 m Number of Tubes: 1

Wall Thickness: 5.000e-003 m Void Fraction: 0.9000 Void Volume: 484.6 m³

Reaction Info

Reaction Set: Set-1 Initialize From: Current

Integration Information

Number of Segments: 20 Minimum Step Fraction: 1.0e-06 Minimum Step Length: 1.8e-05 m

Catalyst DataParticle Diameter: 1.000e-003 m Particle Sphericity: 1.0000 Solid Density: 2500 kg/m³Bulk Density: 250.0 kg/m³ Solid Heat Capacity: 250.0 kJ/kg-C**User Variables**

RATING

Sizing

Tube DimensionsTotal Volume 538.4 m³ Length 18.42 m Diameter 6.100 m Number of Tubes 1 Wall Thickness 5.000e-003 m**Tube Packing**Void Fraction 0.9000 Void Volume 484.6 m³**Nozzle Parameters**

Base Elevation Relative to Ground Level 0.0000 m Diameter 6.100 m Length 18.42

Reactor Product Preheated Feed

Diameter (m) 5.000e-002 5.000e-002

Elevation (Base) (m) 0.0000 0.0000

Elevation (Ground) (m) 0.0000 0.0000

Conditions

Length (m)	Temperature (C)	Pressure (kPa)	Vapour Fraction Duty (kJ/h)
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0.461	455.0	1038.00	1.0000 7714838
1.382	460.0	1038.00	1.0000 -118455
2.303	465.0	1037.99	1.0000 -173385
3.224	470.0	1037.99	1.0000 -173477
4.145	475.0	1037.99	1.0000 -173236
5.066	480.0	1037.99	1.0000 -172984
5.987	485.0	1037.99	1.0000 -172724
6.909	490.0	1037.99	1.0000 -172456
7.830	495.0	1037.98	1.0000 -172179
8.751	500.0	1037.98	1.0000 -171895
9.672	505.0	1037.98	1.0000 -171603
10.593	510.0	1037.98	1.0000 -171303
11.514	515.0	1037.98	1.0000 -170997
12.435	520.0	1037.98	1.0000 -170684
13.357	525.0	1037.97	1.0000 -170365
14.278	530.0	1037.97	1.0000 -170040
15.199	535.0	1037.97	1.0000 -169709
16.120	540.0	1037.97	1.0000 -169373
17.041	545.0	1037.97	1.0000 -169032
17.962	550.0	1037.96	1.0000 -168687

Length (m)	Enthalpy (kJ/kgmole)	Entropy (kJ/kgmole-C)	Inside HTC (kJ/h-m ² -C)	Overall HTC (kJ/h-m ² -C)
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0.461	-4054	168.06	---	---
1.382	-3813	168.26	---	---
2.303	-3455	168.30	---	---
3.224	-3100	168.34	---	---
4.145	-2747	168.38	---	---
5.066	-2396	168.42	---	---
5.987	-2048	168.47	---	---
6.909	-1703	168.51	---	---
7.830	-1360	168.55	---	---
8.751	-1020	168.59	---	---
9.672	-682	168.63	---	---
10.593	-347	168.67	---	---
11.514	-14	168.71	---	---
12.435	317	168.75	---	---
13.357	645	168.80	---	---
14.278	971	168.84	---	---
15.199	1295	168.88	---	---
16.120	1616	168.92	---	---
17.041	1935	168.96	---	---
17.962	2252	169.01	---	---

Flows

Length (m)	Molar Flow (kgmole/h)	Mass Flow (kg/h)	Volumetric Flow (m ³ /h)	Heat Flow (kJ/h)
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0.461	498.754	6853.10	2913.296	-2.022e+006
1.382	499.204	6853.10	2936.036	-1.903e+006
2.303	500.684	6853.10	2964.947	-1.730e+006
3.224	502.159	6853.10	2993.945	-1.556e+006
4.145	503.624	6853.10	3022.993	-1.383e+006
5.066	505.077	6853.10	3052.089	-1.210e+006

5.987	506.520	6853.10	3081.231	-1.038e+006
6.909	507.952	6853.10	3110.417	-8.651e+005
7.830	509.373	6853.10	3139.646	-6.929e+005
8.751	510.782	6853.10	3168.917	-5.210e+005
9.672	512.181	6853.11	3198.227	-3.494e+005
10.593	513.568	6853.11	3227.575	-1.781e+005
11.514	514.944	6853.11	3256.960	-7077
12.435	516.308	6853.11	3286.379	1.636e+005
13.357	517.661	6853.11	3315.833	3.340e+005
14.278	519.003	6853.11	3345.318	5.040e+005
15.199	520.333	6853.11	3374.834	6.737e+005
16.120	521.652	6853.11	3404.378	8.431e+005
17.041	522.959	6853.11	3433.951	1.012e+006
17.962	524.255	6853.11	3463.550	1.181e+006

Segment Overall Reaction Rates (kgmole/m3-s)

Length (m) Rxn-1

0.4606	8.461e-004
1.382	-2.580e-006
2.303	-8.484e-006
3.224	-8.457e-006
4.145	-8.396e-006
5.066	-8.334e-006
5.987	-8.271e-006
6.909	-8.208e-006
7.830	-8.144e-006
8.751	-8.081e-006
9.672	-8.017e-006
10.59	-7.951e-006
11.51	-7.886e-006
12.44	-7.823e-006
13.36	-7.757e-006
14.28	-7.691e-006
15.20	-7.624e-006
16.12	-7.559e-006
17.04	-7.493e-006
17.96	-7.428e-006

Component Production Rates (kgmole/m3-s)

Length (m)	Hydrogen	Nitrogen	Ammonia	Oxygen
0.4606	-2.538e-003	-8.461e-004	1.692e-003	0.0000
1.382	7.740e-006	2.580e-006	-5.160e-006	0.0000
2.303	2.545e-005	8.484e-006	-1.697e-005	0.0000
3.224	2.537e-005	8.457e-006	-1.691e-005	0.0000
4.145	2.519e-005	8.396e-006	-1.679e-005	0.0000
5.066	2.500e-005	8.334e-006	-1.667e-005	0.0000
5.987	2.481e-005	8.271e-006	-1.654e-005	0.0000
6.909	2.462e-005	8.208e-006	-1.642e-005	0.0000
7.830	2.443e-005	8.144e-006	-1.629e-005	0.0000
8.751	2.424e-005	8.081e-006	-1.616e-005	0.0000
9.672	2.405e-005	8.017e-006	-1.603e-005	0.0000
10.59	2.385e-005	7.951e-006	-1.590e-005	0.0000
11.51	2.366e-005	7.886e-006	-1.577e-005	0.0000
12.44	2.347e-005	7.823e-006	-1.565e-005	0.0000
13.36	2.327e-005	7.757e-006	-1.551e-005	0.0000
14.28	2.307e-005	7.691e-006	-1.538e-005	0.0000
15.20	2.287e-005	7.624e-006	-1.525e-005	0.0000
16.12	2.268e-005	7.559e-006	-1.512e-005	0.0000
17.04	2.248e-005	7.493e-006	-1.499e-005	0.0000
17.96	2.228e-005	7.428e-006	-1.486e-005	0.0000

Length (m) H2O Propane

0.4606	0.0000	0.0000
1.382	0.0000	0.0000
2.303	0.0000	0.0000
3.224	0.0000	0.0000
4.145	0.0000	0.0000
5.066	0.0000	0.0000
5.987	0.0000	0.0000
6.909	0.0000	0.0000
7.830	0.0000	0.0000
8.751	0.0000	0.0000
9.672	0.0000	0.0000
10.59	0.0000	0.0000
11.51	0.0000	0.0000
12.44	0.0000	0.0000

13.36	0.0000	0.0000
14.28	0.0000	0.0000
15.20	0.0000	0.0000
16.12	0.0000	0.0000
17.04	0.0000	0.0000
17.96	0.0000	0.0000

Transport

Length (m)	Viscosity (cP)	Molecular Weight (kg/m3)	Density (kJ/kgmole-C)	Heat Capacity (dyne/cm)	Surface Tension ---	Z Factor 1.001
0.4606	2.219e-002	13.74	2.352	37.889	---	1.001
1.382	2.231e-002	13.73	2.334	37.935	---	1.002
2.303	2.241e-002	13.69	2.311	37.926	---	1.002
3.224	2.252e-002	13.65	2.289	37.916	---	1.002
4.145	2.263e-002	13.61	2.267	37.906	---	1.002
5.066	2.274e-002	13.57	2.245	37.895	---	1.002
5.987	2.286e-002	13.53	2.224	37.885	---	1.002
6.909	2.297e-002	13.49	2.203	37.874	---	1.002
7.830	2.309e-002	13.45	2.183	37.863	---	1.002
8.751	2.321e-002	13.42	2.163	37.852	---	1.002
9.672	2.333e-002	13.38	2.143	37.841	---	1.002
10.59	2.345e-002	13.34	2.123	37.830	---	1.002
11.51	2.357e-002	13.31	2.104	37.818	---	1.002
12.44	2.369e-002	13.27	2.085	37.807	---	1.002
13.36	2.382e-002	13.24	2.067	37.795	---	1.002
14.28	2.394e-002	13.20	2.049	37.784	---	1.002
15.20	2.407e-002	13.17	2.031	37.772	---	1.002
16.12	2.420e-002	13.14	2.013	37.760	---	1.002
17.04	2.433e-002	13.10	1.996	37.749	---	1.002
17.96	2.446e-002	13.07	1.979	37.737	---	1.002

Component Molar Flowrates (kgmole/h)

Length (m)	Hydrogen	Nitrogen	Ammonia	Oxygen
0.4606	188.4770	101.7847	203.2166	4.7205
1.382	189.1521	102.0098	202.7665	4.7205
2.303	191.3719	102.7497	201.2867	4.7205
3.224	193.5849	103.4874	199.8113	4.7205
4.145	195.7818	104.2197	198.3468	4.7205
5.066	197.9623	104.9465	196.8931	4.7205
5.987	200.1265	105.6679	195.4503	4.7205
6.909	202.2742	106.3838	194.0185	4.7205
7.830	204.4053	107.0942	192.5978	4.7205
8.751	206.5196	107.7989	191.1882	4.7205
9.672	208.6171	108.4981	189.7898	4.7205
10.59	210.6978	109.1917	188.4027	4.7205
11.51	212.7615	109.8796	187.0269	4.7205
12.44	214.8082	110.5618	185.6625	4.7205
13.36	216.8378	111.2383	184.3094	4.7205
14.28	218.8503	111.9092	182.9678	4.7205
15.20	220.8456	112.5743	181.6376	4.7205
16.12	222.8237	113.2336	180.3188	4.7205
17.04	224.7846	113.8873	179.0115	4.7205
17.96	226.7283	114.5352	177.7157	4.7205
Length (m)	H2O	Propane		
0.4606	0.5550	0.0000		
1.382	0.5550	0.0000		
2.303	0.5550	0.0000		
3.224	0.5550	0.0000		
4.145	0.5550	0.0000		
5.066	0.5550	0.0000		
5.987	0.5550	0.0000		
6.909	0.5550	0.0000		
7.830	0.5550	0.0000		
8.751	0.5550	0.0000		
9.672	0.5550	0.0000		
10.59	0.5550	0.0000		
11.51	0.5550	0.0000		
12.44	0.5550	0.0000		
13.36	0.5550	0.0000		
14.28	0.5550	0.0000		
15.20	0.5550	0.0000		
16.12	0.5550	0.0000		
17.04	0.5550	0.0000		
17.96	0.5550	0.0000		

Component Mole Fractions				
Length (m)	Hydrogen	Nitrogen	Ammonia	Oxygen
0.4606	0.3779	0.2041	0.4074	0.0095
1.382	0.3789	0.2043	0.4062	0.0095
2.303	0.3822	0.2052	0.4020	0.0094
3.224	0.3855	0.2061	0.3979	0.0094
4.145	0.3887	0.2069	0.3938	0.0094
5.066	0.3919	0.2078	0.3898	0.0093
5.987	0.3951	0.2086	0.3859	0.0093
6.909	0.3982	0.2094	0.3820	0.0093
7.830	0.4013	0.2102	0.3781	0.0093
8.751	0.4043	0.2110	0.3743	0.0092
9.672	0.4073	0.2118	0.3706	0.0092
10.59	0.4103	0.2126	0.3669	0.0092
11.51	0.4132	0.2134	0.3632	0.0092
12.44	0.4160	0.2141	0.3596	0.0091
13.36	0.4189	0.2149	0.3560	0.0091
14.28	0.4217	0.2156	0.3525	0.0091
15.20	0.4244	0.2164	0.3491	0.0091
16.12	0.4272	0.2171	0.3457	0.0090
17.04	0.4298	0.2178	0.3423	0.0090
17.96	0.4325	0.2185	0.3390	0.0090
Length (m) H ₂ O				
Propane				
0.4606	0.0011	0.0000		
1.382	0.0011	0.0000		
2.303	0.0011	0.0000		
3.224	0.0011	0.0000		
4.145	0.0011	0.0000		
5.066	0.0011	0.0000		
5.987	0.0011	0.0000		
6.909	0.0011	0.0000		
7.830	0.0011	0.0000		
8.751	0.0011	0.0000		
9.672	0.0011	0.0000		
10.59	0.0011	0.0000		
11.51	0.0011	0.0000		
12.44	0.0011	0.0000		
13.36	0.0011	0.0000		
14.28	0.0011	0.0000		
15.20	0.0011	0.0000		
16.12	0.0011	0.0000		
17.04	0.0011	0.0000		
17.96	0.0011	0.0000		

TEE-100 (Tee): Design, Rating

Tee: TEE-100

CONNECTIONS

Inlet Stream
 STREAM NAME FROM UNIT OPERATION
 Overhead Recycle V-100 Separator
 Outlet Stream

STREAM NAME TO UNIT OPERATION
Recycle without Purge RCY-1 Recycle

PARAMETERS Flow Ratios Dynamic Valve Openings

Value Control: Multiple Stream

Valve Control. User Variables

USCI vam

RATING

Base Elevation Relative to Ground Level 0.0000 m

Base Elevation Relative to Ground Level 0.0000 m

Overhead Recycle Recycle without Purge

Diameter (m) 5.000e-002 5.000e-002

Diameter (in) 3.000e-02 3.000e-02
 Elevation (Base) (m) 0.0000 0.0000

Elevation (Ground) (m) 0.0000 0.0000

VLV-100 (Valve); Design, Rating

Valve: VI.V-100

CONNECTIONS
Inlet Stream
STREAM NAME FROM UNIT OPERATION
Condensed Propane AC-100 Air cooler
Outlet Stream
STREAM NAME TO UNIT OPERATION
Refrigerant Propane Named E-107 Heat Exchanger

PARAMETERS
Physical Properties
Pressure Drop: 1456 kPa
User Variables
RATING
Sizing
Sizing Conditions
Inlet Pressure 1619 kPa Molecular Weight 44.10 Current
Valve Opening 50.00 % Delta P 1456 kPa Flow Rate 3.336e+004 kg/h
Valve Sizing Method and Type
Sizing Method: ANSI/ISA
Valve Operating Characteristic and Sizing Information
Linear Sized Coefficient: Cv (standard) cal/min.sqrt(psi)
FI 0.9000 Cv 30.01 USGPM(60F,1psi) Cg 1004 Fp 1.000 Xt 0.7000 Rigorous Cp/Cv Method

Nozzle Parameters
Base Elevation Relative to Ground Level 0.0000 m
Condensed Propane Refrigerant Propane
Diameter (m) 5.000e-002 5.000e-002
Elevation (Base) (m) 0.0000 0.0000
Elevation (Ground) (m) 0.0000 0.0000
Elevation (% of Height) (%)

AC-100 (Air cooler): Design, Rating, Performance, HTFS - ACOL

Air cooler: AC-100
CONNECTIONS
Inlet Stream
STREAM NAME FROM UNIT OPERATION
Second Stage Compressed Propane K-102 Compressor
Outlet Stream
STREAM NAME TO UNIT OPERATION
Condensed Propane VLV-100 Valve

DESIGN PARAMETERS

Pressure Drop: 2.000 kPa UA: 6.453e+005 kJ/C-h
Inlet Air Temp: 25.00 C Outlet Air Temp: 51.20 C
Configuration: one tube row, one pass
User Variables

SIZING

Number of Fans 1
Fan Fan 0
Speed (rpm) 60.00
Speed (rpm) 60.00
Max Acceleration (rpm) ---
Design Speed (rpm) 60.00
Design airflow (ACT_m3/h) 3.600e+005
Current airflow (ACT_m3/h) 3.600e+005

NOZZLE PARAMETERS

Base Elevation Relative to Ground Level 0.0000 m
Second Stage Compressed Propane Condensed Propane
Diameter (m) 5.000e-002 5.000e-002
Elevation (Base) (m) 0.0000 0.0000
Elevation (Ground) (m) 0.0000 0.0000

PERFORMANCE RESULTS

Working Fluid Duty: -1.080e+007 kJ/h Correction Factor: 0.6973
UA: 6.453e+005 kJ/C-h LMTD: 15.89 C
Feed Temp: 62.07 C Prod Temp: 47.24 C
Air Feed Temp: 25.00 C Air Prod Temp: 51.20 C
Volumetric Air Flow: 3.600e+005 ACT_m3/h Mass Air Flow: 4.067e+005 kg/h

PERFORMANCE TABLE

Overall Phase
Temperature Pressure Heat Flow Enthalpy

(C)	(kPa)	(kJ/h)	(kJ/kgmole)			
62.07	1620.80	0.00	-102811.71			
47.29	1620.60	-1079650.22	-104238.88			
47.29	1620.40	-2159300.44	-105666.04			
47.28	1620.20	-3238950.65	-107093.20			
47.28	1620.00	-4318600.87	-108520.36			
47.27	1619.80	-5398251.09	-109947.52			
47.27	1619.60	-6477901.31	-111374.68			
47.26	1619.40	-7557551.53	-112801.84			
47.25	1619.20	-8637201.75	-114229.00			
47.25	1619.00	-9716851.96	-115656.16			
47.24	1618.80	-10796502.18	-117083.32			
Vapour Fraction	Vap Phase Mass Frac	Heat of Vap	(kJ/kgmole)			
1.0000	1.0000	---				
0.9990	0.9990	---				
0.8879	0.8879	---				
0.7769	0.7769	---				
0.6659	0.6659	---				
0.5549	0.5549	---				
0.4439	0.4439	---				
0.3329	0.3329	---				
0.2219	0.2219	---				
0.1110	0.1110	---				
0.0000	0.0000	---				
Vapour Phase						
Mass Flow	Molecular Wt	Density	Mass Sp	Heat	Viscosity	Thermal Cond
(kg/h)	(kg/m3)	(kJ/kg-C)	(cP)	(W/m-K)		
33359.47	44.10	33.00	2.16	0.01	0.02	
33324.45	44.10	36.51	2.19	0.01	0.02	
29620.50	44.10	36.50	2.19	0.01	0.02	
25917.08	44.10	36.50	2.19	0.01	0.02	
22213.19	44.10	36.49	2.19	0.01	0.02	
18510.13	44.10	36.49	2.19	0.01	0.02	
14807.02	44.10	36.48	2.19	0.01	0.02	
11104.70	44.10	36.48	2.19	0.01	0.02	
7403.09	44.10	36.47	2.19	0.01	0.02	
3701.25	44.10	36.47	2.19	0.01	0.02	
Std Gas Flow	Z Factor	Pseudo	Pc	Pseudo	Tc	Pseudo
(STD._m3/h)	(kPa)	(C)		Zc		Omega
17887.06	0.78	4256.66	96.75	0.28	0.15	
17868.29	0.73	4256.66	96.75	0.28	0.15	
15882.26	0.73	4256.66	96.75	0.28	0.15	
13896.52	0.73	4256.66	96.75	0.28	0.15	
11910.52	0.73	4256.66	96.75	0.28	0.15	
9924.98	0.73	4256.66	96.75	0.28	0.15	
7939.40	0.73	4256.66	96.75	0.28	0.15	
5954.24	0.73	4256.66	96.75	0.28	0.15	
3969.47	0.73	4256.66	96.75	0.28	0.15	
1984.58	0.73	4256.66	96.75	0.28	0.15	
Light Liquid Phase						
Mass Flow	Density	Mass Sp	Heat	Viscosity	Thermal Cond	Surface Tens
(kg/h)	(kg/m3)	(kJ/kg-C)	(cP)	(W/m-K)	(dyne/cm)	
---	---	---	---	---	---	
35.02	454.30	3.30	0.08	0.08	4.38	
3738.97	454.31	3.30	0.08	0.08	4.38	
7442.38	454.33	3.30	0.08	0.08	4.38	
11146.28	454.33	3.30	0.08	0.08	4.38	
14849.33	454.34	3.30	0.08	0.08	4.38	
18552.45	454.35	3.30	0.08	0.08	4.38	
22254.77	454.36	3.30	0.08	0.08	4.38	
25956.38	454.38	3.30	0.08	0.08	4.38	
29658.22	454.38	3.30	0.08	0.08	4.38	
33359.47	454.40	3.30	0.08	0.08	4.38	
Molecular Wt	Sp Gravity	Pseudo	Pc	Pseudo	Tc	Pseudo
(kg/mol)	(kPa)	(C)		Zc		Omega
---	---	---	---	---	---	
44.10	0.45	4256.66	96.75	0.28	0.15	
44.10	0.45	4256.66	96.75	0.28	0.15	
44.10	0.45	4256.66	96.75	0.28	0.15	
44.10	0.45	4256.66	96.75	0.28	0.15	
44.10	0.45	4256.66	96.75	0.28	0.15	
44.10	0.45	4256.66	96.75	0.28	0.15	

44.10	0.45	4256.66	96.75	0.28	0.15
44.10	0.45	4256.66	96.75	0.28	0.15
44.10	0.45	4256.66	96.75	0.28	0.15

Heavy Liquid Phase

Mass Flow (kg/h)	Density (kg/m ³)	Mass Sp Heat (kJ/kg-C)	Viscosity (cP)	Thermal Cond (W/m-K)	Surface Tens (dyne/cm)
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35.02	454.30	3.30	0.08	0.08	4.38
3738.97	454.31	3.30	0.08	0.08	4.38
7442.38	454.33	3.30	0.08	0.08	4.38
11146.28	454.33	3.30	0.08	0.08	4.38
14849.33	454.34	3.30	0.08	0.08	4.38
18552.45	454.35	3.30	0.08	0.08	4.38
22254.77	454.36	3.30	0.08	0.08	4.38
25956.38	454.38	3.30	0.08	0.08	4.38
29658.22	454.38	3.30	0.08	0.08	4.38
33359.47	454.40	3.30	0.08	0.08	4.38

Molecular Wt	Sp Gravity	Pseudo Pc (kPa)	Pseudo Tc (C)	Pseudo Zc	Pseudo Omega
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44.10	0.45	4256.66	96.75	0.28	0.15
44.10	0.45	4256.66	96.75	0.28	0.15
44.10	0.45	4256.66	96.75	0.28	0.15
44.10	0.45	4256.66	96.75	0.28	0.15
44.10	0.45	4256.66	96.75	0.28	0.15
44.10	0.45	4256.66	96.75	0.28	0.15
44.10	0.45	4256.66	96.75	0.28	0.15
44.10	0.45	4256.66	96.75	0.28	0.15
44.10	0.45	4256.66	96.75	0.28	0.15
44.10	0.45	4256.66	96.75	0.28	0.15