A SEMIEMPIRICAL DETERMINATION OF ALPHA PARTICLE

ENERGIES AND HALF-LIVES IN THE

HEAVY ELEMENT REGION

By

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Thesis Approved:

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PREFACE

In his search for new nuclides showing alpha decay, the experimentalist first looks at semiempirical predictions of alpha decay energies and half-lives to find likely places where his labors may bear fruit. This was my main objective in this thesis, to aid the experimentalist.

A secondary aim was to provide data for the possible improvement of the mass formula used.

I wish to acknowledge my indebtedness to my adviser, Dr. H. Kuemmel for his invaluable suggestions and assistance throughout the completion of this thesis; and to Dr. M. Nurmia who suggested this topic for study. Also I wish to acknowledge the aid which I received from Mr. Gene Pulley, Mr. Edgar Butler, and the rest of the staff at the computer center of Oklahoma State University; and to my wife who typed the manuscript.

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CHAPTER I

INTRODUCTION

For many years numerous formulas have been obtained which give the binding energy as a function of the number of protons and neutrons in the nucleus.^{1,2,3} Such relations are called mass formulas. These mass formulas usually have several terms, the form of which are known but whose relative importance is not known quantitatively. By multiplying each term by a parameter determined by empirical methods, results are obtained which agree fairly well with experiment. The experimental trend of the binding energy per nucleon may be seen in Fig. 1.

By knowing the binding energy of the parent and daughter in an alpha decay, the Q-value for the reaction may be obtained in the following way:

$E_{P} = E_{d} + E_{H} + Q_{c}$

where E_{p} , E_{d} , and E_{H} are the total rest energies of the parent, daughter and alpha particle. But:

¹A. G. W. Cameron, "A Revised Semiempirical Atomic Mass Formula," <u>Canadian Journal of Physics</u>, 35 (1957), pp. 1021-1032.

²E. Feenberg, "Semi-Empirical Theory of the Nuclear Energy Surface," <u>Reviews of Modern Physics</u>, 19 (1947), pp. 239-258.

³A. E. S. Green and D. F. Edwards, "Dicsontinuities in the Nuclear Mass Surface," Physical Review, 91 (1953), pp. 46-63.

$$E_{\mathbf{p}} = (ZM_{\mathbf{z}} + NM_{\mathbf{N}})c^{2} - B_{\mathbf{p}}$$

$$E_{\mathbf{d}} = \left[(Z - 2)M_{\mathbf{z}} + (N-2)M_{\mathbf{N}} \right] c^{2} - B_{\mathbf{d}}$$

$$E_{\mathbf{\mu}} = (2M_{\mathbf{z}} + 2M_{\mathbf{N}})c^{2} - B_{\mathbf{d}}$$

where M_{z} is the mass of a proton

 ${\rm M}_{\rm N}$ is the mass of a neutron

Z is the number of the protons in the parent

N is the number of neutrons in the parent

 B_{p} , B_{d} , and B_{s} are the binding energies of the parent, daughter and alpha particle.

Substituting these values into the equation above and solving for Q it is found that:

From this the alpha particle energy, E_{sc} , can be obtained by using consevation of momentum and energy. Let T_d be the kinetic energy of the daughter after decay, V, be the velocity of the daughter, M_d , be the mass of the daughter, v, be the velocity of the alpha particle, and m_{sc} , its mass.

$$Q = E_{x} + T_{d}$$
$$m_{x} v = M_{d}V$$
$$T_{d} = \frac{1}{2}M_{d}V^{2}$$
$$E_{x} = \frac{1}{2}m_{x}V^{2}$$

Eliminating T_{d} , V, and v from these equations:

$$Q = E_{\sigma} \left[1 + \frac{m_{\sigma} c}{M_{d}} \right] = E_{\sigma} \left[1 + \frac{4}{A - 4} \right]$$

where A is the atomic mass number of the parent nucleus solving this for E_{\checkmark} :

(2)

$$\mathbf{E}_{\mathbf{x}} \stackrel{:}{=} \mathbb{Q}\left[1 - \frac{4}{A}\right].$$

In other words the daughter nucleus carries away $\frac{4}{A}$ of the total amount of kinetic energy available. Using relations (1) and (2) above, an equation is obtained giving the alpha particle energy as a function of the number of protons and neutrons in the parent.

In order to determine the parameters in the mass formula, the method of least squares can be applied using all of the experimental values of alpha particle energies available.

Now that a reasonably accurate formula has been obtained, two things may be accomplished. First, an experimental error can be seen by comparing the experimental value with that predicted by the formula. Second, by knowing the predicted alpha particle energy, the experimentalist will know what methods to use in looking for this energy. There are several people interested in this type of prediction in their work far away from the valley of stable nuclei.^{4,5} They have found unusually short life times in this region.

⁴ Antti Siivola, "On the Alpha Activity of Neurton Deficient Europium and Gadolinium Isotopes, "<u>Annales Academiae Scientiarum Fennicae</u>, VI. Physica, 109, 1962.

⁵M. Karras, G. Andersson, and M. Nurmia, "Search for Alpha Activity in Neutron Deficient Isotopes of Pb, Tl, Hg, Pt, and Te," (unpub. paper, University of Helsinki, 1961).



Fig.1. Binding energy per particle for the nuclides



Fig.2. Deviation of experimental binding energy from B_{BW} close to magic numbers.

CHAPTER II

THE MASS FORMULA

One of the earliest mass formulas was the Bethe-Weizsacker formula which is based on the liquid drop model:

(3) B_{BW} (NZ) = aA - bA³ - c
$$\frac{Z(Z-1)}{A^3}$$
 - d $\frac{(N-Z)^2}{A}$ + e $\frac{f_{N,Z}}{A^3}$

where $B_{g_{NJ}}$ is the binding energy, N is the number of neutrons, Z is the number of protons, A is the mass number, $\int_{N,Z} 1_{N,Z} 2_{N,Z} 1_{N,Z} 2_{N,Z} 1_{N,Z} 2_{N,Z} 2_{$

¹H. A. Bethe and R. F. Bacher, "Nuclear Physics," <u>Reviews</u> of <u>Modern</u> <u>Physics</u>, 8 (1936), pp. 165-167.

fact that if the number of protons or neutrons are at a magic number, they form a closed shell thus making the binding energy higher than would be accounted for by the Bethe-Weizsäcker formula. See Fig. 2.

In order to correct the Bethe-Weizsäcker formula, the shell model must be considered.² Let the n'th level above the lowest level in the i'th shell be denoted by E_i . The expansion for E_i in terms of n would be:

E.
$$(n) = A_{+} + B_{-} (n-1) + C_{-} (n-1)^{+} + \dots$$

where A, is the bottom of the i'th shell, B, is a linear approximation to the level distance, and C, is a correction to this. If N' is the number of neutrons in this shell and N" is the number of holes (unoccupied levels), assuming $A \gg B \gg C$, the contribution to the binding energy is given by:

(4)
$$B'(N') = \sum_{n=1}^{\infty} E_{i}(n) \doteq fN' - \frac{1}{2} (h + iN') N'N'$$

where f is the "center of the shell" and h is approximately the level distance. In terms of the old constants:

$$f \doteq A + \frac{1}{2} B N$$

where N. is the number of levels in the i'th shell, $B_1 \doteq h$ and i is proportional to C. The form of equation (4) will hold true also for protons letting say Z' be the number of protons in the shell and Z" be the number of holes in it. Also there may be a term which accounts for possible coupling between neutrons and protons. Such a term should

²H. Kuemmel et al., "A New Nuclidic Mass Law," (unpub., Second International Conference on Nuclidic Masses, 1964).

show less coupling for empty and filled shells than for say a shell that was half filled. This seems reasonable because closed shells are "inert", and thus have no interactions with other nucleons. Also second order perturbation theory predicts that the coupling should be proportional to the number of particles and holes of both kinds of particles in each shell. Thus there should be a term of the form

Putting these terms together the mass formula which was used in this thesis is obtained:

(5)
$$B(N,Z) = aA - bA^{3} - c \frac{Z(Z-1)}{A^{3}} - d \frac{(N-Z)^{2}}{A} e \frac{S_{N,Z}}{A^{3}} + fN^{1} + gZ^{1}$$

 $-\frac{1}{2}(h+iN^{1}) N^{1}N^{1} - \frac{1}{2}(j+kZ^{1}) Z^{1}Z^{1} + 1N^{1}N^{1}Z^{1}Z^{1}$

By using this corrected formula along with (1) a fairly accurate formula for Q is obtained:

(6)
$$Q_{\mathbf{x}} = B_{\mathbf{x}} + a \left[A^{\frac{2}{3}} - (A - 4)^{\frac{2}{3}} \right] + b \left[\frac{Z(Z-1)}{A^{\frac{1}{3}}} - \frac{(Z-2)(Z-3)}{(A-4)^{\frac{1}{3}}} \right] \\ + c(N-Z)^{\frac{1}{2}} \left[\frac{1}{A} - \frac{1}{A-4} \right] - 2d + \frac{1}{2}e \left[N'N'' - (N'-2)(N''+2) \right] \\ + \frac{1}{2}r \left[N'^{\frac{1}{3}} N'' - (N'-2)^{\frac{1}{3}} (N''+2) \right] + \frac{1}{2}g \left[Z'Z'' - (Z'-2)(Z''+2) \right] \\ + \frac{1}{2}h \left[Z'^{\frac{1}{3}} Z'' - (Z'-2)^{\frac{1}{3}} (Z''-2) \right] + i \left[(N'-2)(N''+2)(Z'+2)(Z''+2) - N'N''Z'Z'' \right]$$

where B is the binding energy of the alpha particle. The pairing energy has been omitted because its contribution to Q_{∞} is negligable ($\div 6$ kev) due to the weak A dependence. The first term reduces to a constant. Also the first two terms of the correction terms reduce to constants. In order to determine the parameters the 82xZ < 126, 126<N<184 region was chosen since in these shells - decay is most prevalent. Thus not only will more accurate values for the parameters be obtained but also the formula will be of more use to the experimenter since this is the region where \sim - decay is most likely to be found. In this shell

$$N' = N - 126$$

 $N'' = 184 - N$
 $Z' = Z - 82$
 $Z'' = 126 - Z$

After E_{a} has been determined the half-life can be calculated by the use of a formula derived by Bethe³ and modified by Nurmia.⁴ In the derivation of this formula a potential is assumed such as the one shown in Fig. 3. The radial wave function:

$$\Psi = \Psi \exp(-iQ_{t})$$

is assumed. Letting 6=r 4 the equation,

$$\frac{d^{\mathbf{a}}\boldsymbol{\phi}}{dr^{\mathbf{a}}} + \frac{2M}{\hbar^{\mathbf{a}}} \left(Q - \frac{L(L+1)\hbar^{\mathbf{a}}}{2Mr^{\mathbf{a}}} - V(r) \right) \boldsymbol{\phi} = 0,$$

must be satisfied. M is the reduced mass of the alpha particle. It is assumed that the alpha particle does not undergo a spin change, thus L = 0. The equation is solved in all three regions, the WKB approximation method being applied in regions (ii) and (iii).

For region (i): (r) = A, sin k (r)

 $k_{i} = \left[2M(Q_{ac} - U) \right]^{\prime} / t_{i}$

where

³E. Segre et al, <u>Experimental Nuclear Physics</u> <u>III</u>, (New York, 1959), pp. 76-81.

⁴R. Taagepera and M. Nurmia, "On the Relations between Half-Life and Energy Release in Alpha Decay," <u>Annales Academiae Scientiarum Fennicae</u>, VII Physica, 76, 1961.





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For region (ii) near r=R:

where

For region (iii) for very large r,6(r) must represent a pure outgoing

wave:
$$(r) = A_{exp(ikr)}$$

where $k = (2MQ_{e})^{2/n}$.

By using the boundary conditions between the regions relations between the A's are found:

$$A_{j} \stackrel{:}{:} A_{a}k_{j} \stackrel{I}{\times} A_{a}(R) \exp \left[K_{a}(R)\right]$$
$$A_{j} \stackrel{:}{:} A_{a} \stackrel{I}{\times} A_{a} \left[\frac{1+i}{2k}\right]^{1/2}$$

By normalizing the wave function, it is found that:

$$\mathbf{A}_{\mathbf{1}}^{2} = \frac{1}{2\mathbf{r}^{R}} \, .$$

Since the wave function has been normalized, the decay constant is obtained directly from the solution in region (iii) for large r by

where v is the relative velocity of sparation between the alpha particle and the daughter nucleus. By substituting in the values for the A's and k's, the Bethe equation is obtained:

(7)
$$h = \frac{\partial^{2}\pi \partial h^{2}}{M^{2}R_{d}(B - Q)^{2}} \exp\left[-\frac{2^{2BR}}{\pi v}(\mathbf{x} - \sin\mathbf{x}\cos\mathbf{x})\right]$$

where R_d is the radius and B is the Coulomb barrier height of the daughter nucleus and \prec is given by $\cos^2 = EB$. The first part of the product in the Bethe equation is the frequency that the alpha particle strikes the sides of the potential well. The exponential part gives the

probability of transmission through the Coulomb barrier. To arrive at Nurmia's approximation several assumptions were made. The first part of the product in equation (7) is considered to be a constant, C_o , R_d is assumed to be equal to $r_o A_d$ where A_d is the atomic mass number of the daughter and $r_o = 1.5 \times 10^{-13}$ cm. With A_d approximated by 2.5 Z_d , $R_d = 1.36 r_o Z_d$ ¹³. It is assumed that B>Q making cos small, Sins = 1 and $s = \pi/2 - \cos s$. Also Q may be approximated by E_s . Since $B = 2Z_d e^3 R_d$ and $\cos^2 s = EB^{-1}$,

$$\cos \alpha = \frac{(1.36r)^2}{2^2 e} \frac{E_{\alpha}}{Z_{a}}$$

Thus equation (7) becomes:

$$T = C_{exp} \left[-\frac{2\pi 2^{2} e^{2} M^{2}}{\pi} \frac{Z_{d}}{E_{c}} + \frac{8eM^{2}(1.36r_{o})}{\pi} \frac{Z_{d}}{Z_{d}} \right]$$

Converting this to $\log_{10} T$ where T is the half life in years:

(8)
$$\log_{10}T = C_{E_{10}} - C_{3} Z^{3} - C_{3} Z^{3}$$

where $C_{=}=1.70(\text{MeV})^2$, $C_{=}=30.0$, $C_{=}=1.00(\text{MeV})^2$ and E_{x} is measured in MeV. This is the equation that was used in this thesis.

CHAPTER III

DETERMINATION OF PARAMETERS

The method of least squares was used to determine the parameters for this region. To apply this method let y_i be the i'th value of $Q_{\dot{s}} - B_{s_i}$ an experimental value, and let $f_i(N,Z)$ be the theoretical value of $B_d - B_s$ for the i'th parent nuclei. Therefore:

(9)
$$f_{i}(N,Z) = \sum_{j=1}^{q} a_{j}x_{ij}$$

where a_j is the j'th parameter and x_{ij} is the j'th term using the N and Z values for the i'th parent nuclei. According to the method of least squares:

(10)
$$\sum_{i=1}^{n} \left[y_{i} - f_{i}(N,Z) \right] x_{ik} = 0 \quad k = 1,2,...,9$$

where n is the number of experimental observations. Substituting the value of $f_i(N,Z)$ from (5) into (6) and writting in matrix form:

$$X'(Y - XA) = C$$

where Y is a column matrix whose elements are the y_{i} , A is a column matrix whose elements are the a_{i} , X is a matrix whose elements are the x_{i} , the j'th term using the N and Z value of the i'th parent nuclei, and X' is the transpose of X. This equation represents a set of nine equations whose unknowns are the nine parameters. These equations are the conditions set on the parameters, which minimizes the sum of the squares of the residuals between the experimental values, y; and the theoretical values, f;(N,Z). They must now be solved for the a;: (11) $A = (X'X)^{-1}(X'Y)$

In order to perform these operations a computer program was written which calculated the elements of the X and Y matrix, stored them in the proper locations, and then performed the indicated matrix operations. A difficulty arose when the computer inverted the X'X matrix. This matrix being nine by nine and the computer which was used (IBM 650) being of limited word length, the accuracy of the elements of the inverted matrix was limited. To overcome this difficulty only three parameters were calculated at a time. Older estimates of the values for the other parameters were used. In this manner the y; became, for example:

$$y_i = Q_a - B_a - \sum_{j=1}^{d} a_j x_{ij}$$

while

$$f_{i}(N,Z) = \sum_{j=1}^{9} a_{j}x_{ij}.$$

It was found that the parameters were sufficiently independent of each other in the minimization of the residuals that one interation would bring the values of the parameters to well within the accuracy of the formula. (See Table II.) With the parameters thus determined the corrected mass formula can now be used to predict the alpha particle energies for this region.

CHAPTER IV

DATA

The experimental data used in calculating the y; is listed in Table I.¹ Some of the data in this region was not used. If all of the data that was available had been taken, the alpha particle energies which are more suitable to experimental techniques would perhaps have been given undue emphasis. There were few examples of odd-odd nuclei. However it is doubtful that this did much to invalidate the predictions because as was mentioned before the pairing energy term is negligable. Also the energies which had a sizable error (\doteq .1 MeV) were omitted where possible. (In several areas where insufficient data was available, these more inaccurate energies were used). The alpha particle energies for bismuth (Z = 83) and polonium (Z = 84) were omitted because the daughter nuclei would lie in the next lower shell thus making equation (4) invalid.

Hans Heinrich Landolt and Richard Börnstein, "Numerical Data and Functional Relationships in Science and Technology," Group I, (Berlin, Heidelberg, Göttingen, 1961), Part 3.

CHAPTER V

RESULTS AND CONCLUSIONS

The parameters which were obtained from the data above are listed in Table II. The alpha particle energies, which were predicted from these parameters, are shown in Table III. The first column gives the name of the element, the second gives the number of protons in the parent nuclei, the third gives the number of protons, the fourth gives the predicted alpha particle energy in kev, and the fifth gives the difference between the experimental value and the predicted value in kev, the negative sign indicates that the predicted value is too high by this much. The \log_{10} of the half life in years is given in the last column. The errors in \log_{10} are fairly large ($\sigma=1$), and thus \log_{10} T can only be used to determine the methods to use in order to look for the alpha activities.

By studying the differences between experiment and the predictions, it can be seen that instead of being randomly distributed there are sections where the predictions are too high and sections where they are too low. For example note the elements Pu, Am, Cm, Bk, and Cf with neutron numbers 146, 147 and 148. In this section all the predictions are too low. There are several other examples of this type of systematic differences. In Fig. 4. the deviations are shown. (For the nuclides which do not have crosshatching, either the deviation was small, ∠100 kev,



Fig. 4. Deviations of predicted alpha particle energies from experiment

or no data was available.) An attempt was made to explain this by sub-shell structure. However, in this region the nuclear deformations are quite large, and the sub-shell structure is no longer apparent.¹ According to theory, for spherical nuclei there should be a sub-shell at Z = 92, N = 136, N = 150.

No clear evidence of a strong pairing effect can be seen by studying the deviations in detail. In some regions the alpha particle energy of the even-even nuclei are higher, while in others that of the odd-odd are higher. However there can definitly be seen some type of even-odd relationship although not the one included in the Bethe-Weizsacker formula.

Considering all the deviations available the root-mean-square error is 180 kev or an error of about 3% for an average E_{x} . It is doubtful that better predictions could be made with this formula by adjusting the parameters using all of the data on binding energy available such as beta decay and other reactions. By considering these other reactions, the values of the parameters may be shifted due to something inherent to the particular type of reaction that is not present in alpha decay. Perhaps for regions where sufficient data is available, more accurate results could be obtained by simply extrapolating the experimental data.² Say by keeping Z constant and fitting a polynomial

¹S. G. Nilsson and B. R. Mottelson, "The Intrinsic States of Odd-A Nuclei Having Ellipsoidal Equilibrium Shape," <u>Mathematisk</u> - <u>Fysiske</u> Skrifter Danske Videnskabernes Selskab, 1957-1961.

²Yamada Matumodo, "Nuclear Ground State Energies," <u>Physical Society</u> of Japan Journal, 16(1961) pp. 1497-1500.

in N to the known data. However, this would have two disadvantages. First, in regions where little data is available or some local effect is strong, the results may be inaccurate. Secondly, nothing could be learned about the nature of the nucleus, and the polynomials would only have practical significance.

TABLE I

EXPERIMENTAL ALPHA PARTICIE ENERGIES

| Element | E (MeV) | Element | E (MeV) | Element | E (MeV) |
|----------|----------------|----------|----------------|------------------|---------------------|
| NT OFF | 0.6 | va ele | | | 6 |
| *Lw257 | 0.0 | *Am243 | 5.340 | *Th227 | 6.036±.001 |
| *No255 | 8.2 | *Am241 | 5.5408±.0006 | Th226 | 6.330 |
| *No253 | 8.5 | *Am239 | 5.75 | Th225 | $6.57 \pm .03$ |
| *Md255 | 7.34 | *Am237 | 6.01 | *Th224 | $7.13 \pm .02$ |
| *Fm255 | $7.03 \pm .01$ | Pu244 | 4.55 | Th223 | $7.55 \pm .10$ |
| *Fm254 | $7.20 \pm .01$ | *Pu242 | 4.898 | *Ac227 | 4.949±.002 |
| *Fm253 | 6.94 | *Pu241 | 4.893 | *Ac225 | 5.8185±.0015 |
| *Fm252 | $7.05 \pm .02$ | *Pu240 | 5.1589±.0005 | Ac224 | 6.17 ±.03 |
| Fm251 | 6.89 ±.05 | Pu239 | 5.147 | *Ac223 | 6.6570±.0007 |
| *Fm250 | 7.43 | *Pu238 | 5.491±.001 | *Ac222 | 6.96 ±.05 |
| *Es254 | 6.40 ±.02 | Pu237 | $5.65 \pm .02$ | Ac221 | 7.6 |
| *Es253 | 6.633±.005 | *Pu236 | 5.763 | *Ra226 | 4.777±.003 |
| Es252 | 6.64 | Pu235 | $5.85 \pm .02$ | *Ra224 | 5.681 |
| *Es251 | 6.48 | Pu234 | 6.19 | *Ra223 | 5.867 |
| *Es249 | 6.76 | *Pu233 | 6.30 | Ra222 | 6.55 |
| Es248 | 6.87 | *Pu232 | 6.58 | Ra221 | $6.71 \pm .03$ |
| Es247 | 7.35 | *Np237 | 4.872 | *Ra220 | 7.43 +.02 |
| *Es246 | 7.35 | *Np235 | 5.06 +.02 | Ra219 | 8.0 ±.1 |
| *Cf252 | 6.112 | *Nn233 | 5.53 | *Fr223 | $5.34 \pm .08$ |
| Cf251 | 5.841 | *Nn231 | 6.28 | *Fr221 | 6.332+.010 |
| *Cf250 | 6.024 | *11 238 | 4.195+.005 | *Fr220 | 6.69 ± 03 |
| *Cf249 | 6.194 | *11 236 | 4.490+.004 | Fr219 | $7.30 \pm .02$ |
| Cf248 | $6.23 \pm .03$ | 11 235 | 4 550 | *Fr218 | 7.85 +.05 |
| *Cf246 | 6.753 | 11 234 | 4.768 | Fr217 | 8.3 |
| Cf245 | 7.11 +.02 | *11 233 | 4 8157+ 0005 | *Rn222 | 5 4860+ 0005 |
| *Cf244 | 7.17 | *11 232 | 5 318+ 002 | Rn221 | 6.0 +.1 |
| *Bk240 | 5 417+ 015 | 11 221 | 5 15 | *Rn220 | 6 282+ 004 |
| *Bk2/17 | 5 67 | | 5 88/4 005 | *Rn210 | 6 813+ 002 |
| *Bkoh5 | 6.37 ± 02 | 11 220 | 5.004±.005 | Rn218 | $7 12 \pm 01$ |
| *B1-0)1 | 6.67 ± 015 | ¥U 008 | 0.42 ±.02 | -111210 Rn217 | 7 7 1 + 02 |
| *BI-0/12 | 6 72 | NU 220 | 6 9 1 7 | *Pn216 | $1 \cdot 14 \pm 03$ |
| *Cm2)18 | 5 05/4 015 | -U 221 | 0.0 ±.1 | Pro15 | 86 ± 1 |
| *Cm240 | 5.004±.010 | *Paz31 | 5.040 | *A+OIO | 6 07 |
| Cm240 | 5.3(3±.010 | *Pa229 | 5.005±.001 | At019 | 6.62 |
| Cm245 | 2.42 | *Pa228 | 6.1380 | AUZIO | 0.03 |
| *Cm244 | 5.001 | *Pa227 | 6.526 | *At217 | 7.051±.010 |
| *Um243 | 0.00L | *Pa226 | 6.81 ±.05 | AtZIO | (.19±.03 |
| Cm242 | 6.110 | *Th232 | 4.007±.005 | ATZIS | $0.00 \pm .02$ |
| Cm241 | 5.95 ±.02 | *'I'h230 | 4.682±.010 | *At214 | 0.70 ±.05 |
| *Cm240 | 0.25 | Th229 | 5.02 | AT213 | 9.2 |
| _Cm238 | 6.50 | *Th228 | 5.421±.001 | | |
| | | | 5 A. 1. | | |

*Nuclides used in the determination of the parameters.

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TABLE II

THE PARAMETERS

| Parameter | First Iteration | Second Iteration |
|-----------|-----------------|------------------|
| a | 20.673 | 21.949 |
| b | 0.57418 | 0.56447 |
| с | 17.250 | 17.465 |
| đ | 28.113 | 27.914 |
| е | 0.0495 | 0.0457 |
| f | -0.000186 | -0.000138 |
| g | 0.0311 | 0.0321 |
| h | -0.00120 | -0.00113 |
| i | 0.0000762 | 0.0000776 |

TABLE III

| ELEMENT | Z | N | E, | ΔE. | LOG T |
|---------|----|-----|------|------|--------|
| AT | 85 | 129 | 8713 | 70 | -15.03 |
| | 85 | 130 | 8185 | -200 | -13.35 |
| | 85 | 131 | 7624 | 170 | -11.74 |
| | 85 | 132 | 7136 | - 86 | -10.02 |
| | 85 | 133 | 6645 | - 10 | - 8.17 |
| | 85 | 134 | 6135 | 130 | - 5.97 |
| | 85 | 135 | 5623 | | - 3.33 |
| | 85 | 136 | 5153 | | - 0.70 |
| RN | 86 | 127 | 9767 | | -17.64 |
| | 86 | 128 | 9203 | | -16.14 |
| | 86 | 129 | 8694 | -100 | -14.71 |
| | 86 | 130 | 8152 | -140 | -13.19 |
| | 86 | 131 | 7681 | 60 | -11.56 |
| | 86 | 132 | 7207 | - 80 | - 9.83 |
| | 86 | 133 | 6714 | 98 | - 7.98 |
| | 86 | 134 | 6218 | 63 | - 5.77 |
| | 86 | 135 | 5763 | 200 | - 3.62 |
| | 86 | 136 | 5320 | 165 | - 1.03 |
| | 86 | 137 | 4889 | | + 1.20 |
| | 86 | 138 | 4515 | | + 3.92 |
| | 86 | 139 | 4061 | | + 7.92 |
| | 86 | 140 | 3648 | | +11.64 |
| FR | 87 | 127 | 9658 | | -16.91 |
| | 87 | 128 | 9169 | | -15.52 |
| | 87 | 129 | 8648 | | -14.22 |
| | 87 | 130 | 8194 | 100 | -12.85 |
| | 87 | 131 | 7738 | 110 | -11.39 |
| | 87 | 132 | 7263 | 40 | - 9.65 |
| | 87 | 133 | 6784 | - 90 | - 7.80 |
| | 87 | 134 | 6345 | - 13 | - 6.03 |
| | 87 | 135 | 5916 | | - 4.15 |
| | 87 | 136 | 5500 | -160 | - 1.88 |
| | 87 | 137 | 5139 | | + 0.56 |
| | 87 | 138 | 4699 | | + 3.52 |
| | 87 | 139 | 4299 | | + 6.42 |
| | 87 | 140 | 3942 | | + 9.23 |
| RA | 88 | 127 | 9611 | | -16.47 |
| | 88 | 128 | 9110 | | -15.22 |
| | 88 | 129 | 8675 | | -13.90 |
| | 88 | 130 | 8237 | | -12.69 |
| | 88 | 131 | 7780 | 200 | -11.23 |
| | 88 | 132 | 7319 | 110 | - 9.68 |
| | 88 | 133 | 6897 | -190 | - 7.83 |
| | 88 | 134 | 6484 | 70 | - 6.07 |
| | 88 | 135 | 6083 | -216 | - 4.20 |
| | 88 | 136 | 5735 | - 55 | - 2.46 |
| | 88 | 137 | 5310 | | - 0.06 |

PREDICTED ALPHA DECAY ENERGIES, THE RESIDUALS, AND THE PREDICTED LOG HALF LIFE

| ELEMENT | Z | N | E | ۵E | LOG T |
|------------|----|-----|------|------|--------|
| RA | 88 | 138 | 4924 | -148 | + 2.22 |
| 5.373(13)) | 88 | 139 | 4579 | | + 4.68 |
| | 88 | 140 | 4213 | | + 7.33 |
| | 88 | 141 | 3904 | | +10.20 |
| | 88 | 142 | 3576 | | +13.72 |
| | 88 | 143 | 3257 | | +17.58 |
| AC | 89 | 128 | 9124 | | -14.91 |
| 2.0.00 | 89 | 129 | 8705 | | -13.92 |
| | 89 | 130 | 8267 | | -12.35 |
| | 89 | 131 | 7824 | | -11.07 |
| | 89 | 132 | 7419 | 200 | - 9.51 |
| | 89 | 133 | 7023 | - 60 | - 8.08 |
| | 89 | 134 | 6637 | 19 | - 6.34 |
| | 89 | 135 | 6305 | -140 | - 4.96 |
| | 89 | 136 | 5895 | - 77 | - 3.02 |
| | 89 | 137 | 5523 | | - 0.95 |
| | 89 | 138 | 5191 | -242 | + 0.97 |
| | 89 | 139 | 4838 | | + 3.33 |
| 8 | 89 | 140 | 4541 | | + 5.54 |
| | 89 | 141 | 4223 | | + 7.55 |
| | 89 | 142 | 3915 | | +10.80 |
| | 89 | 143 | 3617 | | +13.95 |
| | 89 | 144 | 3314 | | +17.37 |
| тн | 90 | 129 | 8722 | | -13.42 |
| | 90 | 130 | 8299 | | -12.19 |
| | 90 | 131 | 7912 | | -11.08 |
| | 90 | 132 | 7534 | | - 9.73 |
| | 90 | 133 | 7164 | 390 | - 8.10 |
| | 90 | 134 | 6847 | 280 | - 7.03 |
| 5 | 90 | 135 | 6453 | 120 | - 5.23 |
| | 90 | 136 | 6096 | 233 | - 8.10 |
| | 90 | 137 | 5778 | 258 | - 1.80 |
| | 90 | 138 | 5439 | - 18 | + 0.07 |
| | 90 | 139 | 5153 | -130 | + 2.05 |
| | 90 | 140 | 4848 | -166 | + 3.86 |
| | 90 | 141 | 4551 | | + 6.09 |
| | 90 | 142 | 4263 | 257 | + 8.13 |
| | 90 | 143 | 3971 | | +11.04 |
| | 90 | 144 | 3717 | | +13.37 |
| | 90 | 145 | 3442 | | +16.29 |
| | 90 | 146 | 3177 | | +19.91 |
| PΔ | 91 | 130 | 8375 | | -12.04 |
| 1.0 | 91 | 131 | 8015 | 5 | -11.11 |
| | 91 | 132 | 7664 | | - 9.77 |
| | 91 | 133 | 7362 | | - 8.56 |
| | 91 | 134 | 6985 | | - 7-08 |
| | 91 | 135 | 6644 | 170 | - 5.75 |
| | 91 | 136 | 6339 | 186 | - 4.35 |
| | 91 | 137 | 6015 | 123 | - 2.89 |
| | 91 | 138 | 5742 | - 81 | - 1.08 |
| | | | | | |

III (CONTINUED)

(4)

| PA 91 139 5449 + 0.26 91 140 5164 -119 + 2.25 91 141 4888 + 4.06 91 142 4606 + 6:30 91 143 4362 + 8:34 91 144 4097 +10:50 91 145 3841 +12:79 91 146 3623 +15:23 91 146 3199 +20:13 91 146 3199 +20:13 92 132 7850 -9:99 92 133 7490 -8:59 92 134 7165 -7:33 92 136 6566 100 -4:87 92 137 6307 110 -3:68 92 140 5491 -174 0:74 92 142 4987 -2:20 3:97 92 144 4486 13 +7:53 92 144 4486 13 +7:53 92 | ELEMENT | Z | N | E 🕳 | ∆ E _≂ | LOG T |
|--|--------------|----|-----|------|-------------------------|--------|
| 91 140 5164 -119 + 2.25 91 141 4888 + 406 91 142 4606 + 6:30 91 143 4362 + 8:34 91 145 3841 +12:79 91 146 3623 +15:23 91 146 3623 +15:23 91 146 3199 +20:13 92 132 7850 -9:99 92 133 7490 -8:59 92 135 6876 100 -6:24 92 136 6566 100 -4:87 92 137 6307 110 -3:66 92 138 6027 -124 -2:44 92 141 5221 -406 +2:46 92 142 4987 -220 +3:97 92 144 4486 13 +7:53 92 144 4486 < | PA | 91 | 139 | 5449 | | + 0.26 |
| 91 141 4888 + 4.06 91 142 4606 + 6:30 91 144 4907 +10:50 91 145 3841 +12:79 91 146 3623 +15:23 91 146 3623 +15:23 91 146 3199 +20:13 91 148 3199 +20:13 91 146 3665 -7:93 92 131 8135 -11:32 92 133 7490 -8:59 92 134 7165 -7:33 92 136 6566 100 -6:42 92 137 6307 110 -3:68 92 140 5491 -174 + 0:74 92 143 4733 -174 + 5:86 92 144 4486 13 + 7:53 92 143 4733 -174 + 5:86 92 144 4486 13 + 10:42 92 146 </td <td></td> <td>91</td> <td>140</td> <td>5164</td> <td>-119</td> <td>+ 2.25</td> | | 91 | 140 | 5164 | -119 | + 2.25 |
| 91 142 4606 + 6:30 91 143 4362 + 8:34 91 144 4097 +10:50 91 145 3841 +12:79 91 146 3623 +15:23 91 147 3384 +17:83 91 146 3199 +20:13 92 131 8135 -11:32 92 132 7850 -999 92 134 7165 -7:33 92 135 6876 100 -6:24 92 137 6307 110 -3:68 92 136 6566 100 -4:87 92 137 6307 110 -3:68 92 140 5491 -174 +0:74 92 141 5221 -406 +2:46 92 142 4987 -220 +3:97 92 145 4277 +9:63 <td></td> <td>91</td> <td>141</td> <td>4888</td> <td>19407583</td> <td>+ 4.06</td> | | 91 | 141 | 4888 | 19407583 | + 4.06 |
| 91 143 4362 + 8.34 91 144 4097 +10.50 91 145 3841 +12.79 91 146 3623 +15.23 91 146 3199 +20.13 91 148 3199 +20.13 92 132 7850 -9.99 92 133 7490 -8.59 92 135 6876 100 -6.24 92 136 6566 100 -4.87 92 137 6307 110 -3.68 92 138 6027 -124 -2.44 92 140 5491 -174 + 0.74 92 141 5221 -406 + 2.46 92 142 4987 -220 + 3.97 92 143 4733 -174 + 5.86 92 144 4486 13 + 7.53 92 143 | | 91 | 142 | 4606 | | + 6:30 |
| 91 144 4097 +10.50 91 145 3841 +12.79 91 146 3623 +15.23 91 147 3384 +17.83 91 147 3384 +17.83 91 148 3199 +20.13 92 131 6135 -11.32 92 133 7490 -8.59 92 134 7165 -7.33 92 135 6876 100 -6.24 92 137 6307 110 -3.68 92 137 6307 110 -3.68 92 137 6307 110 -3.68 92 140 5491 -174 -0.744 92 141 5221 -406 +2.46 92 142 4987 -220 +3.97 92 143 4733 -174 +5.86 92 144 4486 | | 91 | 143 | 4362 | | + 8.34 |
| 91 145 3841 +12.79 91 146 3623 +15.23 91 147 3384 +17.83 91 148 3199 +20.13 92 132 7850 -9999 92 133 7490 - 92 134 7165 - 7.33 92 135 6876 100 - 6.24 92 136 6566 100 - 4.87 92 137 6307 110 - 3.68 92 138 6027 -124 - 2.44 92 141 5221 -406 + 2.46 92 142 4987 -220 + 3.97 92 143 4733 -174 + 5.66 92 144 486 13 + 7.53 92 144 486 149 + 11.66 92 144 48653 + 11.66 92 < | | 91 | 144 | 4097 | | +10.50 |
| 91 146 3623 +15.23 91 147 3384 +17.83 91 148 3199 +20.13 92 131 8135 -11.32 92 132 7850 - 9.99 92 133 7400 - 8.59 92 134 7165 - 7.33 92 136 6566 100 - 6.487 92 136 6566 100 - 4.87 92 137 6307 110 - 3.688 92 140 5491 - 7.4 + 0.74 92 142 4987 - 22.0 + 3.97 92 143 4733 - 7.4 + 5.86 92 144 4486 13 + 7.53 92 144 4486 13 + 7.53 92 144 4486 13 + 7.53 92 144 3653 <td></td> <td>91</td> <td>145</td> <td>3841</td> <td></td> <td>+12.79</td> | | 91 | 145 | 3841 | | +12.79 |
| 91 147 3384 +17.83 91 148 3199 +20.13 92 131 8135 -11.32 92 132 7850 -9999 92 133 7490 -8.59 92 134 7165 -7.33 92 135 6876 100 -6.24 92 137 6307 110 -3.68 92 138 6027 -124 -2.44 92 140 5491 -174 +0.74 92 142 4987 -220 +3.97 92 142 4987 -220 +3.97 92 143 4733 -174 + 5.86 92 144 4486 13 + 7.53 92 144 4486 13 + 7.53 92 144 4486 149 +11.86 92 144 4486 149 +11.86 92 146 3462 +17.61 -9.05 93 133 | | 91 | 146 | 3623 | | +15.23 |
| 91 148 3199 +20.13 92 131 8135 -11.32 92 133 7490 -8.59 92 133 7490 -8.59 92 135 6876 100 -6.24 92 136 6566 100 -4.87 92 137 6307 110 -3.68 92 138 6027 -124 -2.44 92 139 5756 -310 -0.88 92 140 5491 -174 +0.74 92 141 5221 -406 +2.46 92 142 4987 -220 +3.97 92 1445 4486 13 +7.53 92 1445 4486 149 +11.86 92 1447 3868 +13.02 92 1447 3868 -5.85 92 1447 3868 -5.85 93 | | 91 | 147 | 3384 | | +17.83 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 91 | 148 | 3199 | | +20.13 |
| 92 132 7850 -9.99 92 133 7490 -8.59 92 134 7165 -7.33 92 135 6876 100 -6.24 92 136 6566 100 -4.87 92 137 6307 110 -3.68 92 138 6027 -124 -2.44 92 139 5756 -310 -0.688 92 140 5491 -174 +0.74 92 141 5221 -406 +2.466 92 142 4987 -220 #3.97 92 144 4486 13 +7.53 92 144 4486 13 +7.653 92 144 4486 13 +7.653 92 144 4486 13 +7.653 92 144 4486 13 +7.653 92 144 3653 +11.66 92 92 147 3868 +13.02 | U | 92 | 131 | 8135 | | -11.32 |
| 92 133 7490 - 8.59 92 134 7165 - 7.33 92 135 6876 100 - 6.24 92 136 6566 100 - 4.87 92 137 6307 110 - 3.68 92 138 6027 - 124 - 2.44 92 139 5756 - 310 - 0.868 92 140 5491 - 174 + 0.744 92 142 4987 - 22.0 + 3.97 92 143 4733 - 174 + 5.86 92 144 4486 13 + 7.53 92 144 4486 13 + 7.53 92 144 4486 149 + 11.86 92 144 3653 + 16.72 | | 92 | 132 | 7850 | | - 9.99 |
| 92 134 7165 -7.33 92 135 6876 100 -6.24 92 136 6566 100 -4.87 92 138 6027 -124 -2.44 92 139 5756 -310 -0.88 92 140 5491 -174 +0.74 92 141 5221 -406 +2.46 92 142 4987 -220 +3.97 92 143 4733 -174 + 5.86 92 144 4486 13 +7.53 92 145 4277 + 9.63 92 146 4046 149 +11.86 92 147 3868 +15.02 92 148 3653 +15.46 92 147 3868 +15.02 92 148 3653 =4.47 93 132 7969 -10.42 93 133 7661 - 9.05 93 133 6073 - 2.01 <td></td> <td>92</td> <td>133</td> <td>7490</td> <td></td> <td>- 8.59</td> | | 92 | 133 | 7490 | | - 8.59 |
| 92 135 6876 100 -6.24 92 136 6566 100 -4.87 92 137 6307 110 -3.68 92 138 6027 -124 -2.44 92 139 5756 -310 -0.88 92 140 5491 -174 +0.74 92 141 5221 -406 +2.46 92 141 5221 -406 +2.46 92 143 4733 -174 +5.86 92 144 4486 13 +7.53 92 145 4277 +9.63 92 146 4046 149 +11.86 92 149 3462 +17.61 NP 93 132 7969 -10.42 93 133 7661 -9.05 93 93 134 7387 -8.23 -8.23 93 135 7093 -6.74 -3.75 93 136 6848 -5.85 | | 92 | 134 | 7165 | 1.8 | - 7.33 |
| 92 136 6566 100 - 4.87 92 137 6307 110 - 3.68 92 139 5756 -310 - 0.88 92 140 5491 -174 + 0.74 92 141 5221 -406 + 2.46 92 142 4987 -220 + 3.97 92 143 4733 -174 + 5.86 92 144 4486 13 + 7.53 92 144 4486 13 + 7.53 92 144 4486 13 + 7.53 92 144 4486 13 + 7.53 92 146 4046 149 +11.86 92 147 3868 +13.02 92 148 3653 +17.61 NP 93 132 7969 -10.42 93 137 6583 -4.47 93 135 7093 -6.74 93 136 6824 -40 -3.75 <tr< td=""><td></td><td>92</td><td>135</td><td>6876</td><td>100</td><td>- 6.24</td></tr<> | | 92 | 135 | 6876 | 100 | - 6.24 |
| 92 137 6307 110 - 3.68 92 138 6027 -124 - 2.44 92 139 5756 -310 - 0.88 92 140 5491 -174 + 0.74 92 141 5221 -406 + 2.46 92 142 4987 -220 + 3.97 92 143 4733 -174 + 5.86 92 144 4486 13 + 7.53 92 145 4277 + 9.63 92 146 4046 149 +11.86 92 146 4046 149 +11.86 92 147 3868 +13.02 92 148 3653 +17.61 93 132 7969 -10.42 93 135 7093 - 6.74 93 136 6848 - 5.85 93 137 6583 - 4.47 93 138 6324 - 40 - 3.75 93 140 <tb< td=""><td></td><td>92</td><td>136</td><td>6566</td><td>100</td><td>- 4.87</td></tb<> | | 92 | 136 | 6566 | 100 | - 4.87 |
| 92 138 6027 -124 -2.44 92 139 5756 -310 -0.88 92 140 5491 -174 +0.74 92 141 5221 -406 +2.46 92 142 4987 -220 +3.97 92 143 4733 -174 +5.86 92 144 4486 13 +7.53 92 144 4486 149 +11.86 92 146 4046 149 +11.86 92 147 3868 +13.02 92 148 3653 +15.46 92 149 3462 +17.61 93 132 7969 -10.42 93 135 7093 -6.74 93 136 6848 -5.85 93 137 6583 -4.47 93 138 6324 -40 -3.75 93 140 5815 -290 0.61 93 142 5349 | | 92 | 137 | 6307 | 110 | - 3.68 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | 92 | 138 | 6027 | -124 | - 2.44 |
| 92 140 5491 -174 + 0.74 92 141 5221 -406 + 2.46 92 142 4987 -220 + 3.97 92 143 4733 -174 + 5.86 92 144 4486 13 + 7.53 92 1445 4277 + 9.63 92 146 4046 149 +11.86 92 147 3868 +13.02 92 148 3653 +15.46 92 149 3462 +17.61 92 149 3462 +17.61 93 132 7969 -10.42 93 135 7093 - 6.74 93 136 6324 - 40 - 3.75 93 137 6583 - 4.47 93 93 140 5815 -290 - 0.71 93 142 5349 -290 + 0.64 93 <td></td> <td>92</td> <td>139</td> <td>5756</td> <td>-310</td> <td>- 0.88</td> | | 92 | 139 | 5756 | -310 | - 0.88 |
| 92 141 5221 -406 + 2.46 92 142 4987 -220 + 3.97 92 143 4733 -174 + 5.86 92 144 4486 13 + 7.53 92 145 4277 + 9.63 92 146 4046 149 +11.86 92 147 3868 +13.02 92 148 3653 +15.46 92 149 3462 +17.61 93 132 7969 -10.42 93 133 7661 - 9.05 93 134 7387 - 8.23 93 135 7093 - 6.74 93 136 6848 - 5.85 93 137 6583 - 4.47 93 138 6324 - 40 - 3.75 93 140 5815 -290 - 0.71 93 143 5112 + 3.55 93 93 143 5112 + 4.47 <t< td=""><td></td><td>92</td><td>140</td><td>5491</td><td>-174</td><td>+ 0.74</td></t<> | | 92 | 140 | 5491 | -174 | + 0.74 |
| 92 142 4987 -220 + 3.97 92 143 4733 -174 + 5.86 92 144 4486 13 + 7.53 92 145 4277 + 9.63 92 146 4046 149 +11.86 92 147 3868 +13.02 92 148 3653 +15.46 92 149 3462 +17.61 92 149 3462 +17.61 93 132 7969 -10.42 93 134 7387 - 8.23 93 135 7093 - 6.74 93 136 6848 - 5.85 93 137 6583 - 4.47 93 138 6324 - 40 - 3.75 93 139 6073 - 2.01 93 93 140 5815 -290 - 0.71 93 142 5349 -290 + 1.49 93 143 5112 + 3.55 <t< td=""><td></td><td>92</td><td>141</td><td>5221</td><td>-406</td><td>+ 2.46</td></t<> | | 92 | 141 | 5221 | -406 | + 2.46 |
| 92 143 4733 -174 + 5.86 92 144 4486 13 + 7.53 92 145 4277 + 9.63 92 146 4046 149 +11.86 92 147 3868 +13.02 92 148 3653 +15.46 92 149 3462 +17.61 93 132 7969 -10.42 93 133 7661 - 9.05 93 134 7387 - 8.23 93 135 7093 - 6.74 93 136 6848 - 5.85 93 137 6583 - 4.47 93 138 6324 - 40 - 3.75 93 140 5815 -290 - 0.71 93 142 5349 -290 + 0.64 93 142 5349 -290 + 1.49 93 143 5112 + 3.55 - 31 93 144 4912 - 41 + 4.78 < | | 92 | 142 | 4987 | -220 | + 3.97 |
| 92 144 4486 13 + 7.53 92 145 4277 + 9.63 92 146 4046 149 +11.86 92 147 3868 +13.02 92 148 3653 +15.46 92 149 3462 +17.61 NP 93 132 7969 -10.42 93 133 7661 - 9.05 93 134 7387 - 8.23 93 135 7093 - 6.74 93 136 6848 - 5.85 93 137 6583 - 4.47 93 138 6324 - 40 - 3.75 93 140 5815 -290 - 0.71 93 142 5349 -290 + 1.49 93 142 5349 -290 + 1.49 93 143 5112 + 3.555 93 144 4912 - 41 + 4.78 93 145 4690 + 6.71 + 3.455 93 | | 92 | 143 | 4733 | -174 | + 5.86 |
| 92 145 4277 + 9.63 92 146 4046 149 +11.86 92 147 3868 +13.02 92 148 3653 +15.46 92 149 3462 +17.61 NP 93 132 7969 -10.42 93 133 7661 - 9.05 93 134 7387 - 8.23 93 135 7093 - 6.74 93 136 6848 - 5.855 93 137 6583 - 4.47 93 138 6324 - 40 - 3.75 93 139 6073 - 2.01 - 93 140 5815 -290 - 0.711 93 142 5349 -290 + 1.49 93 143 5112 + 3.555 93 143 5112 + 41.49 93 145 4690 + 6.71 <t< td=""><td></td><td>92</td><td>144</td><td>4486</td><td>13</td><td>+ 7.53</td></t<> | | 92 | 144 | 4486 | 13 | + 7.53 |
| 92 146 4046 149 +11.86 92 147 3868 +13.02 92 148 3653 +15.46 92 149 3462 +17.61 NP 93 132 7969 -10.42 93 133 7661 -9.05 93 134 7387 -8.23 93 135 7093 -6.74 93 136 6848 -5.85 93 137 6583 -4.47 93 138 6324 -40 -3.75 93 139 6073 -2.01 -3.75 93 140 5815 -290 -0.71 93 142 5349 -290 +1.49 93 142 5349 -290 +1.49 93 143 5112 +3.55 -3.144 93 144 4912 -41 +4.78 93 145 | | 92 | 145 | 4277 | Real Provider | + 9.63 |
| 92 147 3868 +13.02 92 148 3653 +15.46 92 149 3462 +17.61 93 132 7969 -10.42 93 133 7661 -9.05 93 134 7387 -8.23 93 135 7093 -6.74 93 136 6848 -5.85 93 137 6583 -4.47 93 138 6324 -40 -3.75 93 139 6073 -2.01 93 140 5815 -290 -0.71 93 142 5349 -290 + 1.49 93 142 5349 -290 + 1.49 93 144 4912 - 41 + 4.78 93 1445 4690 + 6.71 - 93 1445 4690 + 6.71 - 93 1445 4690 + 6.71 - 93 1445 4690 + 6.71 - - | | 92 | 146 | 4046 | 149 | +11.86 |
| 92 148 3653 +15.46 92 149 3462 +17.61 NP 93 132 7969 -10.42 93 133 7661 -9.05 93 134 7387 -8.23 93 135 7093 -6.74 93 136 6848 -5.85 93 137 6583 -4.47 93 138 6324 -40 -3.75 93 139 6073 -2.01 93 140 5815 -290 -0.71 93 142 5349 -290 +1.49 93 142 5349 -290 +1.49 93 144 4912 -41 +4.78 93 145 4690 +6.71 +3.55 93 145 4690 +6.71 +3.45 93 145 4690 +6.71 +7.72 93 145 < | | 92 | 147 | 3868 | | +13.02 |
| 92 149 3462 +17.61 NP 93 132 7969 -10.42 93 133 7661 -9.05 93 134 7387 -8.23 93 135 7093 -6.74 93 136 6848 -5.85 93 137 6583 -4.47 93 138 6324 -40 -3.75 93 139 6073 -2.01 -2.01 93 140 5815 -290 -0.71 93 142 5349 -290 +0.64 93 143 5112 +3.55 93 144 4912 -41 +4.78 93 145 4690 +6.71 +3.55 93 145 4690 +6.71 +3.45 93 146 4519 +7.72 +3.148 +11.30 93 147 4313 +9.47 +9.47 +3.148 <td></td> <td>92</td> <td>148</td> <td>3653</td> <td></td> <td>+15.46</td> | | 92 | 148 | 3653 | | +15.46 |
| NP 93 132 7969 -10.422 93 133 7661 -9.05 93 134 7387 -8.23 93 135 7093 -6.74 93 136 6848 -5.85 93 137 6583 -4.47 93 138 6324 -40 -3.75 93 139 6073 -2.01 93 140 5815 -290 -0.71 93 142 5349 -290 + 0.64 93 143 5112 + 3.55 93 93 143 5112 + 3.55 93 144 4912 - 41 + 4.78 93 145 4690 + 6.71 93 146 4519 + 7.72 93 144 4912 - 41 + 4.28 + 11.30 93 146 4519 + 7.72 93 147 4313 + 9.47 93 149 3951 + 12.83 93 150 3780 + 14.43 <td></td> <td>92</td> <td>149</td> <td>3462</td> <td></td> <td>+17.61</td> | | 92 | 149 | 3462 | | +17.61 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | NP | 93 | 132 | 7969 | | -10-42 |
| 93 134 7387 -8.23 93 135 7093 -6.74 93 136 6848 -5.85 93 137 6583 -4.47 93 138 6324 -40 -3.75 93 139 6073 -2.01 93 140 5815 -290 -0.71 93 142 5349 -290 + 0.64 93 143 5112 + 3.55 93 144 4912 - 41 + 4.78 93 145 4690 + 6.71 + 3.55 93 144 4912 - 41 + 4.78 93 144 4912 - 41 + 4.78 93 144 4912 - 41 + 4.78 93 145 4690 + 6.71 + 7.72 93 146 4519 + 7.72 + 93 + 14.83 93 149 3951 + 12.83 + 11.30 93 150 3780 + 14.43 - 8.27 </td <td></td> <td>93</td> <td>133</td> <td>7661</td> <td></td> <td>- 9.05</td> | | 93 | 133 | 7661 | | - 9.05 |
| 93 135 7093 - 6.74 93 136 6848 - 5.85 93 137 6583 - 4.47 93 138 6324 - 40 - 3.75 93 139 6073 - 2.01 93 140 5815 -290 - 0.71 93 141 5592 + 0.664 93 142 5349 -290 + 1.49 93 143 5112 + 3.55 93 144 4912 - 41 + 4.78 93 145 4690 + 6.71 93 144 4912 - 41 + 4.78 93 144 4912 - 41 + 4.78 93 144 4912 - 41 + 4.78 93 145 4690 + 6.71 93 144 4912 - 41 + 4.78 93 145 4690 + 1.283 93 147 4313 + 9.47 93 148 4128 + 11.30 | | 93 | 134 | 7387 | | - 8-23 |
| 93 136 6848 - 5.85 93 137 6583 - 4.47 93 138 6324 - 40 - 3.75 93 139 6073 - 2.01 93 140 5815 -290 - 0.71 93 141 5592 + 0.64 93 142 5349 -290 + 1.49 93 143 5112 + 3.55 93 93 144 4912 - 41 + 4.78 93 145 4690 + 6.71 93 146 4519 + 7.72 93 147 4313 + 9.47 93 148 4128 +11.30 93 149 3951 + 12.83 93 150 3780 + 14.43 94 134 7596 - 8.27 | | 93 | 135 | 7093 | | - 6.74 |
| 93 137 6583 -4.47 93 138 6324 -40 -3.75 93 139 6073 -2.01 93 140 5815 -290 -0.71 93 141 5592 +0.64 93 142 5349 -290 +1.49 93 143 5112 +3.55 93 144 4912 -41 +4.78 93 145 4690 +6.71 93 145 4690 +7.72 93 148 4128 +11.30 93 149 3951 +12.83 93 150 3780 +14.43 94 134 7596 - 8.27 | | 93 | 136 | 6848 | | - 5.85 |
| 93 138 6324 -40 -3.75 93 139 6073 -2.01 93 140 5815 -290 -0.71 93 141 5592 +0.64 93 142 5349 -290 +1.49 93 143 5112 +3.55 93 143 5112 +3.55 93 144 4912 -41 +4.78 93 145 4690 +6.71 93 145 4690 +6.71 93 146 4519 +7.72 93 147 4313 +9.47 93 148 4128 +11.30 93 149 3951 +12.83 93 150 3780 +14.43 94 134 7596 - 8.27 | | 93 | 137 | 6583 | | - 4.47 |
| 93 139 6073 - 2.01 93 140 5815 -290 - 0.71 93 141 5592 + 0.64 93 142 5349 -290 + 1.49 93 143 5112 + 3.55 93 144 4912 - 41 + 4.78 93 145 4690 + 6.71 93 146 4519 + 7.72 93 147 4313 + 9.47 93 148 4128 +11.30 93 150 3780 +14.43 PU 94 134 7596 - 8.27 | | 93 | 138 | 6324 | - 40 | - 3.75 |
| 93 140 5815 -290 -0.71 93 141 5592 +0.64 93 142 5349 -290 +1.49 93 143 5112 +3.55 93 144 4912 -41 +4.78 93 145 4690 +6.71 93 146 4519 +7.72 93 147 4313 +9.47 93 148 4128 +11.30 93 150 3780 +14.43 94 134 7596 - 8.27 | (*) | 93 | 139 | 6073 | 40 | - 2.01 |
| 93 141 5592 + 0.64 93 142 5349 -290 + 1.49 93 143 5112 + 3.55 93 144 4912 - 41 + 4.78 93 145 4690 + 6.71 93 146 4519 + 7.72 93 147 4313 + 9.47 93 148 4128 +11.30 93 150 3780 + 14.43 94 134 7596 - 8.27 | | 93 | 140 | 5815 | -290 | - 0.71 |
| 93 142 5349 -290 + 1.49 93 143 5112 + 3.55 93 144 4912 - 41 + 4.78 93 145 4690 + 6.71 93 146 4519 + 7.72 93 147 4313 + 9.47 93 148 4128 +11.30 93 149 3951 + 12.83 93 150 3780 + 14.43 PU 94 134 7596 - 8.27 | | 93 | 141 | 5592 | 2,0 | + 0.64 |
| 93 143 5112 + 3.55 93 144 4912 - 41 + 4.78 93 145 4690 + 6.71 93 146 4519 + 7.72 93 147 4313 + 9.47 93 148 4128 +11.30 93 149 3951 +12.83 93 150 3780 +14.43 PU 94 134 7596 - 8.27 | | 93 | 142 | 5349 | -290 | + 1.49 |
| 93 144 4912 -41 +4.78 93 145 4690 +6.71 93 146 4519 +7.72 93 147 4313 +9.47 93 148 4128 +11.30 93 149 3951 +12.83 93 150 3780 +14.43 PU 94 134 7596 - 8.27 | | 03 | 142 | 5112 | -290 | + 2.55 |
| 93 144 4712 41 4776 93 145 4690 + 6.71 93 146 4519 + 7.72 93 147 4313 + 9.47 93 148 4128 +11.30 93 149 3951 +12.83 93 150 3780 +14.43 PU 94 134 7596 - 8.27 | | 03 | 145 | 4912 | - 41 | + 4.78 |
| 93 146 4519 + 7.72 93 147 4313 + 9.47 93 148 4128 +11.30 93 149 3951 +12.83 93 150 3780 +14.43 PU 94 134 7596 - 8.27 | | 22 | 145 | 4690 | 41 | + 6.71 |
| 93 147 4313 + 9.47 93 148 4128 +11.30 93 149 3951 +12.83 93 150 3780 +14.43 PU 94 134 7596 - 8.27 | | 92 | 145 | 4610 | | + 7.72 |
| 93 148 4128 +11.30 93 149 3951 +12.83 93 150 3780 +14.43 PU 94 134 7596 - 8.27 | | 93 | 147 | 4313 | | + 9.47 |
| 93 149 3951 +12.83 93 150 3780 +14.43 PU 94 134 7596 - 8.27 | | 93 | 148 | 4128 | | +11.30 |
| 93 150 3780 +14.43 PU 94 134 7596 - 8.27 | | 92 | 149 | 2951 | | +12-83 |
| PU 94 134 7596 - 8.27 | | 93 | 150 | 3780 | | +14-43 |
| | PU | 94 | 134 | 7596 | | - 8-27 |
| 94 135 7366 _ 7.63 | | 94 | 125 | 7366 | | - 7.42 |

III (CONTINUED)

| ELEMENT | Z | N | E 🗪 | 4E. | LOG T |
|---------|----|-----|------|-------|------------|
| PU | 94 | 136 | 7115 | | - 6.35 |
| | 94 | 137 | 6871 | | - 5.45 |
| | 94 | 138 | 6633 | - 50 | - 4.29 |
| | 94 | 139 | 6388 | - 90 | - 3.08 |
| | 94 | 140 | 6177 | 10 | - 2.08 |
| | 94 | 141 | 5945 | -100 | - 1.04 |
| | 94 | 142 | 5720 | 043 | + 0.29 |
| | 94 | 143 | 5529 | 120 | + 0.84 |
| | 94 | 144 | 5317 | 173 | + 2.85 |
| | 94 | 145 | 5154 | - 8 | + 3.75 |
| | 94 | 146 | 4956 | 202 | + 4.98 |
| | 94 | 147 | 4779 | 114 | + 6.59 |
| | 94 | 148 | 4608 | 289 | + 7.59 |
| | 94 | 149 | 4444 | | + 8.97 |
| | 94 | 150 | 4317 | 230 | +10.04 |
| | 94 | 151 | 4153 | | +12.27 |
| | 94 | 152 | 4025 | | +13.05 |
| | 94 | 153 | 3874 | | +14.24 |
| AM | 95 | 137 | 7171 | | - 6.40 |
| 1000 | 95 | 138 | 6940 | | - 5.50 |
| | 95 | 139 | 6742 | | - 4.35 |
| | 95 | 140 | 6522 | | - 3.63 |
| | 95 | 141 | 6308 | | - 2.65 |
| | 95 | 142 | 6128 | -120 | - 1.64 |
| | 95 | 143 | 5927 | | - 0.60 |
| | 95 | 144 | 5773 | - 20 | + 0.47 |
| | 95 | 145 | 5584 | | + 1.59 |
| | 95 | 146 | 5414 | 126 | + 2.45 |
| | 95 | 147 | 5251 | | + 3.64 |
| | 95 | 148 | 5094 | 250 | + 4.25 |
| | 95 | 149 | 4972 | | + 5.82 |
| | 95 | 150 | 4814 | | + 6.79 |
| | 95 | 151 | 4690 | 4 | + 7.79 |
| | 95 | 152 | 4544 | | + 8.82 |
| | 95 | 153 | 4389 | | +10.25 |
| | 95 | 154 | 4285 | | +10.98 |
| CM | 96 | 138 | 7286 | | - 6.23 |
| | 96 | 139 | 7080 | | - 5.56 |
| | 96 | 140 | 6878 | | - 4.65 |
| | 96 | 141 | 6710 | | - 3.94 |
| | 96 | 142 | 6519 | - 20 | - 3.22 |
| | 96 | 143 | 6375 | | - 2.48 |
| | 96 | 144 | 6195 | 60 | - 1.46 |
| | 96 | 145 | 6035 | - 90 | - 0.68 |
| | 96 | 146 | 5880 | 230 | + 0.38 |
| | 96 | 147 | 5730 | , 331 | + 0.93 |
| | 96 | 148 | 5614 | 186 | + 1.78 |
| | 96 | 149 | 5462 | - 10 | + 2.64 |
| | 96 | 150 | 5344 | 29 | + 3.53 |
| | ~ | 161 | 6202 | 5540° | 1 1. 1. 1. |

III (CONTINUED)

| ELEMENT | Z | N | E | ۵E | LOG T |
|---------|-----|------|-------|------|---------|
| | 0.4 | 1.50 | 5050 | 2.1 | |
| CM | 96 | 152 | 5053 | 1 | + 5.37 |
| | 96 | 153 | 4952 | | + 6.33 |
| | 96 | 154 | 4842 | | + 6.99 |
| D.K | 96 | 155 | 4/38 | | + 1.65 |
| BK | 97 | 141 | 60611 | | - 5.17 |
| | 97 | 142 | 6701 | | - 4.11 |
| | 97 | 145 | 6641) | | - 3.11 |
| | 97 | 144 | 6403 | | - 3.05 |
| | 97 | 145 | 6475 | 370 | - 1.80 |
| | 97 | 140 | 63/3 | 430 | - 1.00 |
| | 97 | 147 | 6243 | 430 | - 1.29 |
| | 97 | 140 | 6096 | 210 | - 0.50 |
| | 97 | 149 | 5960 | 1.90 | + 0.29 |
| | 97 | 150 | 5001 | -180 | + 0.84 |
| | 97 | 151 | 5700 | -102 | + 1.07 |
| | 97 | 152 | 5603 | -192 | + 2.024 |
| | 97 | 155 | 5505 | | + 2.02 |
| | 97 | 154 | 5402 | | + 5.71 |
| | 91 | 155 | 5364 | | + 4.01 |
| 65 | 97 | 142 | 7270 | | - 5 90 |
| Çr | 90 | 142 | 7220 | | - 5.30 |
| | 90 | 145 | 71)02 | | - 5.25 |
| | 90 | 144 | 6060 | | - 4.11 |
| | 90 | 145 | 6960 | 210 | - 4.51 |
| | 90 | 140 | 6722 | 300 | - 2.11 |
| | 90 | 147 | 6616 | 127 | - 2.62 |
| | 70 | 140 | 6610 | 157 | - 2.02 |
| | 90 | 147 | 6407 | -110 | - 2.51 |
| | 90 | 150 | 6347 | - 62 | - 1.30 |
| | 90 | 152 | 6154 | -130 | - 0.32 |
| | 90 | 152 | 6057 | -216 | + ()-21 |
| | 90 | 154 | 5978 | 134 | + 0.21 |
| | 98 | 155 | 5904 | 134 | + 1.30 |
| | 0.0 | 156 | 5804 | | + 1.58 |
| | 90 | 157 | 5727 | | + 1.97 |
| ES | 90 | 143 | 7677 | | - 6-84 |
| ES | 99 | 144 | 7554 | | - 6.41 |
| | 99 | 145 | 7462 | | - 5.97 |
| | 99 | 146 | 7333 | | - 5.53 |
| | 99 | 140 | 7234 | 120 | - 4.84 |
| | 99 | 148 | 7112 | 240 | - 4.61 |
| | 99 | 149 | 6981 | -110 | - 3.91 |
| | 99 | 150 | 6894 | -130 | - 3-44 |
| | 99 | 151 | 6797 | 150 | - 2.95 |
| | 99 | 152 | 6703 | -220 | - 2.46 |
| | 99 | 153 | 6628 | 20 | - 2.46 |
| | 99 | 154 | 6557 | 76 | - 1.96 |
| 10 | 99 | 155 | 6461 | - 60 | - 1.45 |
| | 99 | 156 | 6383 | | - 0.94 |

III (CONTINUED)

| E _{oc} | ۸E., | LOG T |
|-----------------|------|--------|
| 6338 | | - 0.94 |
| 6254 | | - 0.41 |
| 3051 | | - 7.96 |
| 7931 | | - 7.55 |
| 7841 | | - 7.13 |
| 7727 | | - 6.70 |
| 7603 | | - 6.26 |
| 7522 | | - 5.82 |
| 7430 | 0 | - 5.60 |
| 7342 | -450 | - 5.38 |
| 7270 | -220 | - 4.92 |
| 7202 | -263 | - 4.46 |
| 7110 | 90 | - 4.23 |
| 7034 | 0 | - 3.76 |
| 6990 | | - 3.52 |
| 6907 | | - 3.28 |
| 6828 | | - 3.04 |
| 8330 | | - 8.43 |
| 8214 | 2 | - 8.02 |
| 8140 | | - 8.02 |
| 8054 | | - 7.60 |
| 7972 | | - 7.18 |
| 7905 | | - 7.18 |
| 7841 | | - 6.76 |

III (CONT

N

ELEMENT

ES

FM

Z

| | 1.1 | | 100 | | | | 0.550 |
|------|-----|----|-----|-----|------|------|--------|
| | | | 100 | 149 | 7522 | | - 5.82 |
| 1410 | | | 100 | 150 | 7430 | 0 | - 5.60 |
| | | | 100 | 151 | 7342 | -450 | - 5.38 |
| | | | 100 | 152 | 7270 | -220 | - 4.92 |
| | | | 100 | 153 | 7202 | -263 | - 4.46 |
| | | | 100 | 154 | 7110 | 90 | - 4.23 |
| | | | 100 | 155 | 7034 | 0 | - 3.76 |
| | | | 100 | 156 | 6990 | | - 3.52 |
| | | | 100 | 157 | 6907 | | - 3.28 |
| | | | 100 | 158 | 6828 | | - 3.04 |
| | MD | | 101 | 146 | 8330 | | - 8.43 |
| | | 8 | 101 | 147 | 8214 | | - 8.02 |
| | | | 101 | 148 | 8140 | | - 8.02 |
| | | | 101 | 149 | 8054 | | - 7.60 |
| | | Ŷ | 101 | 150 | 7972 | | - 7.18 |
| | | | 101 | 151 | 7905 | | - 7.18 |
| | | | 101 | 152 | 7841 | | - 6.76 |
| | | | 101 | 153 | 7752 | | - 6.32 |
| | | ×. | 101 | 154 | 7680 | -340 | - 6.11 |
| | | | 101 | 155 | 7637 | | - 6.11 |
| | | | 101 | 156 | 7557 | | - 5.66 |
| сe: | | | 101 | 157 | 7479 | | - 5.44 |
| | | | 101 | 158 | 7430 | | - 5.22 |
| | | | 101 | 159 | 7357 | | - 4.99 |
| | NO | | 102 | 148 | 8669 | | - 9.28 |
| | | | 102 | 149 | 8593 | | - 9.08 |
| | | | 102 | 150 | 8532 | | - 8.88 |
| | | | 102 | 151 | 8473 | 30 | - 8.68 |
| | | | 102 | 152 | 8389 | 1000 | - 8.48 |
| | | | 102 | 153 | 8320 | -100 | - 8.07 |
| | | | 102 | 154 | 8280 | | - 8.07 |
| | | | 102 | 155 | 8202 | | - 7.87 |
| | | | 102 | 156 | 8125 | | - 7.87 |
| | | | 102 | 157 | 8078 | | - 7.24 |
| | | | 102 | 158 | 8006 | | - 7.03 |
| | | | 102 | 159 | 7963 | | - 7.03 |
| | LW | | 103 | 150 | 9097 | | -10.50 |
| | | | 103 | 151 | 9018 | | -10.12 |
| | | | 103 | 152 | 8954 | | - 9.93 |
| | | | 103 | 153 | 8917 | | - 9.93 |
| | | | 103 | 154 | 8842 | -200 | - 9.55 |
| | | | 103 | 155 | 8769 | | - 9.35 |
| | | | | | | | |

| ELEMENT | Z | N | Er | ∆ E _{sc} | LOG T |
|---------|-----|-----|------|-------------------|---------|
| LW | 103 | 156 | 8723 | | - '9.35 |
| | 103 | 157 | 8652 | | - 8.96 |
| | 103 | 158 | 8609 | | - 8.96 |
| | 103 | 159 | 8581 | | - 8.76 |
| | 103 | 160 | 8514 | | - 8.56 |

 \mathbf{r}

III (CONTINUED)

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VITA

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Major Field: Physics

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