

A FINE ATMOSPHERIC ANALYSIS OF  
THE STAR THETA URSAE MAJORIS

By

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## PREFACE

This dissertation is concerned with performing a detailed fine atmospheric analysis of the atmosphere of the star Theta Ursae Majoris using a detailed computer program which computes a pressure opacity-flux model for a given temperature distribution. A grid of sixteen model atmospheres with scaled solar-type distribution was computed for a range of effective temperatures ( $6200 \text{ }^{\circ}\text{K} \leq T_{\text{eff}} \leq 6650 \text{ }^{\circ}\text{K}$ ), surface gravities ( $3.8 \leq \log g \leq 4.4$ ), and the solar abundance (log of the summation of the number of hydrogen atoms divided by the number of metal atoms = 3.23, and the number of helium atoms divided by the number of hydrogen atoms = 0.1250).

Theoretical UBV colors, corrected for line blanketing, were computed for each model and compared to observed values in order to determine if a model can be selected as representing the star Theta Ursae Majoris.

Hydrogen line profiles,  $H\alpha$ ,  $H\beta$ ,  $H\gamma$ , and  $H\delta$ , for each of the models were computed and compared to the observed profiles. The hydrogen line profiles will also be used to select a model atmosphere for the star. In addition, the model dictated by the UBV colors will be compared with the model dictated by the hydrogen line profiles in order to determine if the selected models are the same or if the UBV colors selects a model having a higher or lower temperature than the model predicted by the hydrogen line profiles.

I wish to express my sincere gratitude to Dr. L. W. Schroeder, my

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## CHAPTER I

### INTRODUCTION

#### Statement of the Problem

The purpose of this study is to perform a fine atmospheric analysis of the star  $\theta$  Ursae Majoris employing a detailed model atmosphere computation. A digital computer program which computes a pressure-opacity-flux model for a given temperature distribution and solar abundance was modified and adapted to our investigation. A grid of sixteen model stellar atmospheres with scaled solar-type temperature distributions and with four different values of effective temperatures and surface gravities was computed.

The blanketing and blanketing-free effects for the theoretical UBV colors were computed for each model in order to determine the effect and need for considering line blanketing in calculation of the theoretical colors. The line blanketing effect was computed by multiplying the theoretically computed flux by the absorption factors. The computed values of the UBV colors will be compared to the observed values in order to determine which model of the stellar atmosphere will be selected as the model best describing the star.

The hydrogen line profiles for each model will be computed and compared with Balmer line profiles from tracings made at the Dominion Astrophysical Observatory. The hydrogen line profiles will be used to determine or select a model atmosphere that agrees best with observed values

of the star. The model dictated by the hydrogen line profiles will be compared to those dictated by the UBV colors in order to determine if a single model can be selected as representative for  $\theta$  Ursae Majoris.

## CHAPTER II

### THE MODEL ATMOSPHERE

#### Stellar Atmospheres

The atmosphere of a star may be defined as those layers from which a photon, emitted in the outward direction, has a high probability of escaping before it can be absorbed, or, the atmosphere may be defined as those layers of a star directly accessible to observation, in the sense that a detectable amount of radiation which is characteristic of those layers reaches the observer without being absorbed or scattered.

Stellar atmospheres range from 500 to 1,000 km in thickness and the mass of the stellar atmosphere is negligible compared to the mass of the star. Since the radiation we receive from the star was emitted somewhere in the atmosphere of the star, the character of the radiation is determined by the physical conditions in the atmosphere.

#### Model Stellar Atmospheres

The model atmosphere is the variation of the physical variables--temperature, pressure, electron pressure, density, opacity, and energy flux--as functions of a suitably defined depth variable.

The development of the model atmosphere concept originated in an attempt to explain the details of the emergent intensity from the solar surface and the emergent flux from stars. Certain basic assumptions concerning the geometry, equilibrium, and conservation equations, which

are consistent with observational evidence, were made in order to reduce the complexity of the model atmosphere.

The spectral distribution of stellar radiation is usually approached on a theoretical basis using the model stellar atmosphere concept. The general problem of representing a real stellar atmosphere by a model is neither mathematically or physically feasible; therefore, several assumptions are made which limit the reality of the model. The theoretical models enable one to calculate properties of the stellar atmosphere, but certain variable parameters must be given before it is possible to construct a model. Once the parameters are specified, the model is used to compute quantities which can be compared with actual stellar observations.

The complexity of the model increases with the number and types of parameters used in the model. Simplifications are introduced in our stellar model, but this forces our model to depart from the real model which is being investigated. This approach is a valid theoretical tool for determining stellar properties and processes because the results of the model atmosphere methods are in good agreement with many observed spectral properties and processes. In order to reduce the complexity of the problem, seven assumptions are made in this study.

#### Assumptions for the Model Atmosphere

A preliminary fine atmospheric analysis of the star  $\theta$  Ursae Majoris\* was made using a detailed atmospheric computation. The assumptions made

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\* Listed by Johnson and Morgan as a subgiant (spectral type F6, Luminosity class IV). Visual magnitude is 3.3 and its coordinates are  $\alpha(1900) = 9^{\text{h}}26^{\text{m}}$ ,  $\delta(1900) = +52^{\circ}08'$  (Keenan and Morgan 1951).

in this investigation are: (i) The star is assumed to be spherically symmetric, non-rotating, and with the linear extent of the atmosphere small compared to the radius. (ii) The atmosphere is assumed to be stratified in homogeneous steady-state, plane parallel layers. (iii) The outer boundary is defined by the condition that no significant quantity of radiation flows into the star across the boundary. (iv) The atmosphere is assumed to contain no significant sources or sinks of energy. (v) The atmosphere is assumed to be in a state of hydrostatic equilibrium under the action of a uniform gravitational field with no radiation, magnetic, or mechanical forces. (vi) The gases are assumed to be in local thermodynamic equilibrium, and (vii) the formation of the line and the continuous spectrum may be treated separately.

The seven assumptions stated will impose certain restrictions on different parameters used in the model. A clarification of some of the assumptions will be stated. Assumption (ii) requires that each layer is defined by a single variable, for instance the geometrical depth,  $t$ . Assumption (iv) assumes no significant sources or sinks of energy. Radiative equilibrium is not assumed in this investigation. If we impose the condition of strict radiative equilibrium, we would have been using the classical restricted problem of Milne (Kourganoff 1952). Assumption (v) states that the total pressure at each layer is just the gas pressure. Assumptions (vi) and (vii) concern the nature of the interaction of the gas and radiation fields. Assumption (vi) is equivalent to saying that for each layer the source function for the radiation field is just the Planck function of the local electron temperature. Scattering is neglected and pure absorption is considered as the only mechanism for the formation of the radiation field. Within the region

that is responsible for the observed spectrum, it is a reasonable assumption (Bohm 1960; Aller 1963a).

The assumption that the atmosphere is non-magnetic may seem inconsistent. The magnetic forces are not totally neglected because an effective surface gravity was used rather than the dynamical gravity. The magnetic forces produce a magnetic pressure which acts to distend the atmosphere in opposition to the dynamical surface gravity.

The state of the atmosphere is assumed to be one of local thermodynamic equilibrium. At each layer the gas molecules obey Maxwell-Boltzmann statistics so that the ionization and excitation equilibria are determined by the Saha and Boltzmann equations respectively, for the electron kinetic temperature. In local thermodynamic equilibrium the source function, the ratio of the emission coefficient to the absorption coefficient, is the Planck function. Scattering is neglected and pure absorption is assumed to be the only mechanism for the formation of the radiation field.

#### Temperature Distribution

The temperature is one of the thermodynamic variables that specify the model atmosphere. In thermodynamic equilibrium, the temperature distribution is determined by the energy incident at the bottom of the atmosphere from the deep interior, the mechanism for energy transport, and the sources of continuous absorption. The assumptions that the net flux must be constant at each layer in the atmosphere, the transport mechanisms being either strictly radiative or combined radiative and convective, and the source of continuous opacity, are sufficient to determine the temperature with depth in the atmosphere.

The use of limb-darkening observations together with the energy distribution at the center of the solar disk may be used to determine an empirical temperature distribution for  $-1.0 \leq x \leq 0.3$ . The depth,  $x$ , is equal to the logarithm of the optical depth,  $\tau_o$ . The subscript "o" denotes the value of the optical depth at  $\lambda = 5,000$  Angstroms. A comparison of such a temperature distribution with theoretical results indicates a discrepancy. This discrepancy may be related to the blanketing by absorption lines and temperature inhomogenities due to turbulent and convective velocity fields.

An empirical solar temperature distribution by Elste (1955) was used in this study. The scaling of Elste's solar temperature distribution is accomplished in the following manner. Multiply the empirical solar temperature at each optical depth,  $\log \tau_o$ , by the ratio of the desired stellar to solar effective temperatures. The solar effective temperature,  $T_{\text{eff}}$ , was taken to be  $5780^\circ\text{K}$  (Aller 1963a). The solar temperature is given at twenty-seven points between the limits of  $-4.0 \leq x \leq +1.2$ . Table I states the relationships between the solar effective temperature and the scale factors for  $\theta$  Ursae Majoris using Elste's Model 10. The temperature distributions are given in terms of  $\theta$  where  $\theta$  is 5040 divided by the temperature in degrees Kelvin.

The stellar effective temperature is not a true effective temperature because the total integrated flux is not obtained by using this temperature in the Stefan-Boltzmann law. The temperature is an approximation and it will be referred to as the model temperature.

#### The Pressure-Opacity-Flux Model

The model atmosphere is the variation of the physical variables

TABLE I  
 SCALED SOLAR TYPE-MODEL FOR  $\theta$  URSAE MAJORIS

| Spectral Type | Elste Model 10      | F4     | F5     | F6     | F8     |
|---------------|---------------------|--------|--------|--------|--------|
| T(eff)<br>°K  | 5780                | 6650   | 6500   | 6350   | 6200   |
| Scale Factor  | 1.0000              | 0.8692 | 0.8892 | 0.9102 | 0.9323 |
| Log $\tau_0$  | $\theta (= 5040/T)$ |        |        |        |        |
| -4.0          | 1.1431              | 0.9936 | 1.0164 | 1.0404 | 1.0657 |
| -3.8          | 1.1425              | 0.9931 | 1.0159 | 1.0399 | 1.0652 |
| -3.6          | 1.1414              | 0.9921 | 1.0149 | 1.0389 | 1.0641 |
| -3.4          | 1.1398              | 0.9907 | 1.0135 | 1.0374 | 1.0626 |
| -3.2          | 1.1379              | 0.9891 | 1.0118 | 1.0357 | 1.0609 |
| -3.0          | 1.1350              | 0.9865 | 1.0092 | 1.0331 | 1.0582 |
| -2.8          | 1.1310              | 0.9831 | 1.0057 | 1.0294 | 1.0544 |
| -2.6          | 1.1250              | 0.9779 | 1.0004 | 1.0240 | 1.0488 |
| -2.4          | 1.1180              | 0.9718 | 0.9941 | 1.0176 | 1.0423 |
| -2.2          | 1.1070              | 0.9622 | 0.9843 | 1.0076 | 1.0321 |
| -2.0          | 1.0930              | 0.9500 | 0.9719 | 0.9948 | 1.0190 |
| -1.8          | 1.0760              | 0.9353 | 0.9568 | 0.9794 | 1.0032 |
| -1.6          | 1.0560              | 0.9179 | 0.9390 | 0.9612 | 0.9845 |
| -1.4          | 1.0340              | 0.8988 | 0.9194 | 0.9411 | 0.9640 |
| -1.2          | 1.0090              | 0.8770 | 0.8972 | 0.9184 | 0.9407 |
| -1.0          | 0.9820              | 0.8536 | 0.8732 | 0.8938 | 0.9155 |
| -0.8          | 0.9520              | 0.8275 | 0.8465 | 0.8665 | 0.8875 |
| -0.6          | 0.9180              | 0.7979 | 0.8163 | 0.8356 | 0.8559 |
| -0.4          | 0.8790              | 0.7640 | 0.7816 | 9.8001 | 0.8195 |
| -0.2          | 0.8340              | 0.7249 | 0.7416 | 0.7591 | 0.7775 |
| 0.0           | 0.7840              | 0.6815 | 0.6971 | 0.7136 | 0.7309 |
| 0.2           | 0.7300              | 0.6345 | 0.6491 | 0.6644 | 0.6806 |
| 0.4           | 0.6750              | 0.5867 | 0.6002 | 0.6144 | 0.6293 |
| 0.6           | 0.6330              | 0.5502 | 0.5629 | 0.5762 | 0.5901 |
| 0.8           | 0.6030              | 0.5241 | 0.5362 | 0.5489 | 0.5622 |
| 1.0           | 0.5840              | 0.5076 | 0.5193 | 0.5316 | 0.5445 |
| 1.2           | 0.5720              | 0.4972 | 0.5086 | 0.5206 | 0.5333 |



as functions of an appropriately defined depth variable. Elste (1955) and Weidmann (1955) discuss the value and convenience of using a logarithmic optical depth scale rather than the actual physical depth because of the relationship between the two. The logarithmic optical depth scale is approximately linearly proportional to the physical depth making it a more desirable variable to use than the optical depth.

The logarithm of the continuum optical depth is related to the physical depth scale  $t$  by the relation

$$x = \log \tau_0 = \log \int_0^t \frac{\kappa_0(t)}{m_0 \sum_i \epsilon_i \mu_i} \rho(t) dt, \quad (2-1)$$

where  $\kappa_0(t)$  = the continuous absorption coefficient per hydrogen particle at 5000 Angstroms,

$m_0$  = the mass in grams of a unit atomic weight,

$\mu_i$  = the atomic weight of species  $i$ ,

$\epsilon_i = n_i/n_H$  = the number abundance of element  $i$  relative to hydrogen,

$\rho(t)$  = the density of stellar material.

The reciprocal of  $m_0 \sum_i \epsilon_i \mu_i$  is the number of hydrogen particles per gram of material.

The atmosphere was divided into twenty-seven layers extending from -4.0 to +1.2 in the logarithm of the optical depth. The corresponding geometrical depth at each layer of the atmosphere may be calculated by inverting and solving Equation (2-1) and assigning a geometrical depth of zero at an optical depth of 0.01

#### Ionization Equilibrium

We assumed the atmosphere to be one in local thermodynamic equilib-

rium. This assumption implies that the gas particles obey the Maxwell-Boltzmann statistics so that the Boltzmann and Saha equations are valid. If we assume only neutral and singly ionized constituents and neglect helium ionization and all molecules, the Saha equation and the perfect gas law determine the contribution of various species to the total gas pressure and the electron pressure. Programs have been developed assuming the ionization of helium, but the effect of the ionization of helium is negligible over the temperature range covered in this study.

The Saha equation for the ratio of single ions to neutral particles of species  $i$  is given by (Aller 1963a)

$$\frac{n_1}{n_0} = 10^{\log(u_1/u_0) + (9.0801 - 2.5 \log \theta - \log P_e) - \chi_0 \theta} \equiv \frac{\phi_i}{P_e}, \quad (2-2)$$

where  $u_r(\theta)$  = the partition function of the  $r$ th ionization stage,

$\theta$  = the reciprocal of the temperature.  $\theta = 5040/T^0(K)$ ,

$P_e$  = the electron pressure,

$\chi_r$  = the ionization potential between the  $r$ th and  $(r + 1)$ st ionization stages in electron volts,

$n_1$  = the number density of singly ionized particles of species  $i$ ,

$n_0$  = the number density of neutral particles of species  $i$ ,

$\phi_i/P_e$  = the Saha equation for the ratio of single ions to neutral particles of species  $i$ .

The degree of ionization--the ratio of the number density of ions to atoms and ions--is given by

$$\left(\frac{n_1}{n_0 + n_1}\right)_i = \frac{\phi_i/P_e}{1 + \phi_i/P_e} \equiv X_i. \quad (2-3)$$

If we neglect helium ionization, molecular dissociation, and negative ions, and assume one ionization stage, the number density of free electrons due to the ionization of a particular species is equal to the number density of ions of that species. The ratio of all atoms, ions, and electrons to electrons is

$$\frac{n}{n_e} = \frac{n_{\text{He}} + \sum_i (n_o + n_i + n_e)_i}{\sum_i (n_e)_i}, \quad (2-4)$$

where  $n_{\text{He}}$  = the helium number density. Dividing the numerator and denominator of Equation (2-4) by the number of hydrogen particles,  $n_{\text{H}}$ , introducing  $\epsilon_i$ , and use the perfect gas law to convert to a ratio of pressure, Equation (2-4) becomes

$$\frac{P_g}{P_e^2} = \frac{\sum_i \epsilon_i (1 + X_i)}{P_e \sum_i \epsilon_i X_i}. \quad (2-5)$$

The reason for dividing both sides of Equation (2-5) by  $P_e$  is  $P_g/P_e^2$  is less sensitive to  $P_e$  than to  $\theta$  (Weidemann 1955) which is important in the actual computations.

#### Gas Pressure

The equation for hydrostatic equilibrium can be written in terms of the continuous absorption coefficient at 5000 Å, the effective surface gravity, and a conversion to a logarithm optical depth scale. This form of the equation is

$$dP_g = \frac{g \sum_i \epsilon_i \mu_i}{\kappa_o} \left( \frac{\tau_o}{\text{Mod}} \right) dx, \quad (2-6)$$

where  $g$  = the effective surface gravity,

$$\text{Mod} = \log_{10} e = 0.43429.$$

Multiplying Equation (2-6) by  $P^{1/2}$  and integrating from the outer boundary or the top of the atmosphere, where  $P_g = 0$ , to the depth  $x$ , an expression for the gas pressure at the point  $x$  is obtained (Evans 1966). In logarithmic form the equation is

$$\log P_g = \frac{2}{3} \log \left( \frac{3}{2} \frac{\kappa}{\text{Mod}} \right) + \frac{2}{3} \log \int_{-\infty}^x \sqrt{\frac{P_g}{P_e}} \frac{\tau_o}{(\kappa_o/P_e)} dx', \quad (2-7)$$

where  $\kappa = m_o g \sum \epsilon_i \mu_i$ .

The pressure model computation is an iteration on the electron pressure which can be obtained by the relation (Evans 1966)

$$\log P_e = \frac{1}{2} \left[ \log P_g - \log P_g / P_e^2 \right]. \quad (2-8)$$

The density in each layer can be computed using the perfect gas law written in logarithmic form by the relation

$$\log P = \log P_g = \log (m_o \sum \epsilon_i \mu_i) - \log k - \log (5040/\theta), \quad (2-9)$$

where  $k$  = the Boltzmann constant.

### The Sources of Continuous Absorption

The major assumptions involved in the calculations of the continuous absorption coefficient are: (a) the neglect of all molecular absorption except  $H_2^+$ ; (b) the neglect of all negative ion absorption except  $H^-$ ; and (c) the use of a hydrogenic approximation for metal absorption. The total absorption coefficient  $\kappa_\lambda$  includes, in order of importance, bound-free (bf) and free-free (ff) absorption due to  $H^-$ ,  $H$ ,  $H_2^+$ , and a total absorption coefficient for all metals (Evans 1966, Elste 1965).

The metal absorption coefficient was integrated over the ionization continuum rather than summing to obtain a smooth curve. In addition, the total absorption coefficient is multiplied by a correction term for stimulated emission of radiation and this product has added to it a scattering coefficient for Rayleigh scattering by neutral hydrogen and Thompson scattering by free electrons. The total monochromatic absorption coefficient per hydrogen particle per unit electron pressure at any depth in the atmosphere can be written in the form

$$\frac{\kappa_{\lambda}}{P_e} = \frac{\kappa_{\lambda}(\text{H}_{\text{bf,ff}})}{P_e} + \frac{\kappa_{\lambda}(\text{H}_{\text{bf}}^-)}{P_e} + \frac{\kappa_{\lambda}(\text{H}_{\text{ff}}^-)}{P_e} + \frac{\kappa_{\lambda}(\text{H}_2^{\text{+bf,ff}})}{P_2} + \quad (2-10)$$

$$\frac{\kappa_{\lambda}(\text{Metals}_{\text{bf,ff}})}{P_e} \left(1 - e^{-\frac{hc}{\lambda kT}}\right) + \frac{\sigma(\text{H}, e^-)}{P_e} .$$

#### The Atomic Data

The adopted chemical composition used to compute the ionization equilibrium and the continuous absorption is made up of hydrogen, helium and a number of metals. The effect of several metals of similar ionization potential can be obtained by grouping them together in one abundance and using the ionization potential of the most abundant of the group. This has been done in Table II where the secondary elements are shown in parentheses. The relative abundance by number is taken from Goldberg, Müller and Aller (1960) for the sun. The abundance for helium is estimated from other investigations. The necessary atomic quantities such as partition functions, atomic weights, ionization potentials, et cetera, used in the calculations have been tabulated by Evans (1966).

TABLE II  
ADOPTED ATMOSPHERIC ABUNDANCE FOR THE MODEL COMPUTATIONS

| Element | log $\epsilon$ | Element   | log $\epsilon$ |
|---------|----------------|-----------|----------------|
| H(O,N)  | 0.004          | K         | -7.300         |
| He      | -0.824         | Ca        | -6.120         |
| C(S,P)  | -3.116         | Cr(Ti,V)  | -6.910         |
| Na      | -5.700         | Fe(Co,Cu) | -5.570         |
| Mg      | -4.600         | Ni(Mn)    | -6.090         |
| Si      | -4.500         |           |                |

### Surface Flux

Aller (1963a) gives the solution to the equation of radiative transfer for the surface flux. A transfer equation can be written for the monochromatic radiant intensity from whose solution an integral equation may be derived for the emergent flux (Kourganoff 1952):

$$F_{\lambda}(0) = 2 \int_0^{\infty} S_{\lambda}(\tau_{\lambda}) E_2(\tau_{\lambda}) d\tau_{\lambda}, \quad (2-11)$$

where the optical depth at the wavelength  $\lambda$  is given by

$$\tau_{\lambda}(x) = \int_{-\infty}^x \frac{\kappa_{\lambda}(t)}{\kappa_0(t)} \left( \frac{\tau_0}{\text{Mod}} \right) dt, \quad (2-12)$$

where  $S_{\lambda}$  = the source function which is the Planck function,

$E$  = the second exponential-integral function given by

$$E_2 = \int_{-\infty}^t e^{-\frac{t\omega}{2}} d\omega. \quad (2-13)$$

The actual flux is given by  $\pi F_{\lambda}(0)$ .

### Computational Procedures

The computer program was developed by Elste and later modified by

Evans (1969). The input parameters used in the computations are: (i) effective surface gravity; (ii) the temperature distribution; (iii) chemical composition; (iv) an initial estimate of the electron pressure. Using the initial electron pressure, the value of  $P_g/P_e^2$  is calculated from Equation (2-5). The temperature distribution and initial electron pressure are used in Equation (2-10) to determine  $\kappa_o/P_e$  where  $\kappa_o$  represents the continuous absorption coefficient at  $\lambda$  5000. The value of  $\kappa_o/P_e$ , the chemical composition, the logarithm of the effective surface gravity, and previously computed quantity  $P_g/P_e^2$  are used in Equation (2-7) to calculate an initial estimate of the gas pressure  $P_g$ . Using Equation (2-8),  $\log P_g$ , and  $P_g/P_e^2$  are used to compute a new estimate for the electron pressure. This procedure is then repeated until it converges to a consistent value for the electron pressure. In practice the convergence does not depend strongly on the initial electron pressure since  $P_g/P_e^2$  and  $\kappa_o/P_e$  are stronger functions of temperature than electron pressure. For the opacity model, the absorption coefficient for wavelengths other than 5000 angstroms is computed from Equation (2-10) and optical depth for these wavelengths is computed by integrating Equation (2-12). The emitted flux is obtained from the same wavelengths as the opacity model by integrating Equation (2-11). The opacity flux model was computed for the interval  $\lambda\lambda$ 2,000 - 21,000 with twenty-seven values between 2,000 and 10,000 angstroms and one each for 15,000 and 21,000 angstroms.

This method of computation is desirable for the range of temperatures encountered in the A5 to G5 stars because of the rapid convergence and the relative insensitivity to the initial estimate of  $P_e$ .

The computational procedure will give a table of the variation of

the thermodynamic parameters with the depth  $x$  and a table relating the different optical depth scales as a function of  $x$ . In addition, this information will be used as part of the data input for the hydrogen line programs.

### The Computed Models

A grid of sixteen stellar model atmospheres with scaled solar type (Elste Model 10) temperature distributions was computed for a range of effective temperatures ( $6200^{\circ}\text{K} \leq T_{\text{eff}} \leq 6650^{\circ}\text{K}$ ), surface gravities ( $3.8 \leq \log g \leq 4.4$ ) and the solar abundance. A representative model atmosphere is listed in Table III for which  $T_{\text{eff}} = 6500^{\circ}\text{K}$  and  $\log g = 4.2$ . "B", the helium to hydrogen number density ratio, was set at 0.1250. This value is somewhat less than that indicated by Table II since we are concerned with stars of earlier spectral type (and, therefore, presumably younger) than the sun. From Table II a value of 3.2306 was assigned for "A", where  $A = \log n_{\text{H}}/\Sigma n_{\text{metals}}$ .



TABLE III  
REPRESENTATIVE MODEL ATMOSPHERE

SOLAR TYPE MODEL (ELSTE MODEL 10) F5 V

T(EFF) = 6500.00    LDG G = 4.2000    B = 0.1250    A = 3.2306    NO. ITERATIONS = 5

| LOG TAU<br>(5000) | THE TA<br>MODEL | TEMP.<br>(K) | LOG PE  | LOG PG | LOG K/PE<br>(5000) | MEAN<br>MOL. WT. | LOG<br>DENSITY | TURBULENCE<br>(KM/SEC) |
|-------------------|-----------------|--------------|---------|--------|--------------------|------------------|----------------|------------------------|
| -4.00             | 1.0164          | 4959.        | -0.9655 | 2.8943 | -25.0394           | 1.3597           | -8.5874        | 0.0                    |
| -3.80             | 1.0159          | 4961.        | -0.9217 | 2.9590 | -25.0458           | 1.3597           | -8.5230        | 0.0                    |
| -3.60             | 1.0149          | 4966.        | -0.8340 | 3.0884 | -25.0573           | 1.3597           | -8.3940        | 0.0                    |
| -3.40             | 1.0135          | 4973.        | -0.7437 | 3.2159 | -25.0681           | 1.3597           | -8.2671        | 0.0                    |
| -3.20             | 1.0118          | 4981.        | -0.6518 | 3.3414 | -25.0783           | 1.3597           | -8.1423        | 0.0                    |
| -3.00             | 1.0092          | 4994.        | -0.5559 | 3.4647 | -25.0891           | 1.3597           | -8.0202        | 0.0                    |
| -2.80             | 1.0057          | 5011.        | -0.4568 | 3.5856 | -25.1006           | 1.3597           | -7.9008        | 0.0                    |
| -2.60             | 1.0004          | 5038.        | -0.3514 | 3.7039 | -25.1144           | 1.3597           | -7.7848        | 0.0                    |
| -2.40             | 0.9941          | 5070.        | -0.2436 | 3.8198 | -25.1294           | 1.3597           | -7.6716        | 0.0                    |
| -2.20             | 0.9843          | 5120.        | -0.1233 | 3.9329 | -25.1500           | 1.3597           | -7.5628        | 0.0                    |
| -2.00             | 0.9719          | 5186.        | 0.0062  | 4.0425 | -25.1747           | 1.3597           | -7.4587        | 0.0                    |
| -1.80             | 0.9568          | 5268.        | 0.1466  | 4.1482 | -25.2038           | 1.3597           | -7.3598        | 0.0                    |
| -1.60             | 0.9390          | 5367.        | 0.3001  | 4.2494 | -25.2374           | 1.3597           | -7.2668        | 0.0                    |
| -1.40             | 0.9194          | 5482.        | 0.4645  | 4.3455 | -25.2743           | 1.3597           | -7.1798        | 0.0                    |
| -1.20             | 0.8972          | 5617.        | 0.6457  | 4.4359 | -25.3159           | 1.3596           | -7.1000        | 0.0                    |
| -1.00             | 0.8732          | 5772.        | 0.8409  | 4.5199 | -25.3611           | 1.3596           | -7.0278        | 0.0                    |
| -0.80             | 0.8465          | 5954.        | 1.0564  | 4.5970 | -25.4119           | 1.3595           | -6.9643        | 0.0                    |
| -0.60             | 0.8163          | 6174.        | 1.2982  | 4.6661 | -25.4700           | 1.3593           | -6.9110        | 0.0                    |
| -0.40             | 0.7816          | 6448.        | 1.5738  | 4.7263 | -25.5373           | 1.3589           | -6.8698        | 0.0                    |
| -0.20             | 0.7416          | 6796.        | 1.8892  | 4.7766 | -25.6145           | 1.3581           | -6.8425        | 0.0                    |
| 0.0               | 0.6971          | 7230.        | 2.2382  | 4.8168 | -25.6974           | 1.3563           | -6.8298        | 0.0                    |
| 0.20              | 0.6491          | 7765.        | 2.6131  | 4.8476 | -25.7767           | 1.3519           | -6.8314        | 0.0                    |
| 0.40              | 0.6002          | 8397.        | 2.9934  | 4.8701 | -25.8342           | 1.3418           | -6.8462        | 0.0                    |
| 0.60              | 0.5629          | 8954.        | 3.2834  | 4.8870 | -25.8516           | 1.3260           | -6.8623        | 0.0                    |
| 0.80              | 0.5362          | 9399.        | 3.4912  | 4.9017 | -25.8460           | 1.3070           | -6.8749        | 0.0                    |
| 1.00              | 0.5193          | 9705.        | 3.6244  | 4.9167 | -25.8352           | 1.2905           | -6.8794        | 0.0                    |
| 1.20              | 0.5086          | 9910.        | 3.7088  | 4.9262 | -25.8253           | 1.2777           | -6.8833        | 0.0                    |

## CHAPTER III

### THE THEORETICAL UBV COLORS

#### The UBV System

In modern work all magnitude and color standards are calibrated by photoelectric photometry because of the greater accuracy achieved by this method. Several color systems have been developed and used for special cases, but different systems have advantages and disadvantages. One of the most widely used color systems is the UBV three-color photometry system.

The UBV system (U = ultraviolet, B = blue, and V = visual) developed by Johnson and Morgan (1953) is a three-color system which has proved extremely useful for work on problems of stellar evolution and galactic structure. It employs an RCA type 1P21 multiplier phototube with appropriate filters. The Johnson-Morgan system has a number of important advantages in that it reduces difficulties caused by the Balmer jump in the older magnitudes, includes stars of all luminosity and spectral classes well distributed over the sky, and permits one to assess the effects and amount of space reddening.

Some of the values assigned to the UBV system are (i) the approximate effective wavelengths of U, B, and V are, respectively 3500, 4350, and 5500 angstroms; (ii) the V magnitudes are very close to the old visual magnitudes and may be regarded as essentially equivalent to them, but the B magnitudes differ from the international photographic magni-

tudes because they do not include the Balmer limit; (iii) the zero points of the B and U magnitudes are fixed by the requirement that the U-B and B-V color indices are both equal to zero for the mean of six bright stars of spectral class A0 V.

If appropriate sensitivity and optical transmissivity curves for the UBV magnitude systems were known it would be possible to correctly predict stellar colors from energy scans. Such a procedure has not proven possible and the UBV system must be regarded as empirically defined in terms of measurements made on certain standard stars. The failure may be in the energy distribution, uncertainties in the basic response curves of the photoelectric cell, filter, and telescope. Stellar colors are often available when energy distributions are not and we must use colors to obtain checks on stellar temperatures.

It must be emphasized that the UBV magnitudes of a star depend not only on its intrinsic luminosity and surface temperature, but also on its chemical composition and the role of chemical composition must be kept in mind particularly when dealing with stars of abnormal H/metal ratios.

Some general principals that should be used in designing any color system are as follows. (i) The larger the number of colors, the narrower will be the bandwidths, resulting in a smaller response per band. (ii) The bands should be spaced as widely as possible in order to preserve the ability of color index to indicate physical parameters. (iii) Design a color system, if possible, to match a standard color system of known magnitudes and colors for a large variety of stars.

## Matsushima-Hall Method

Matsushima and Hall (1969) investigated the magnitude of the correction required by the new calibration for the transformation formula used by Mihalas (1966) to normalize the theoretical colors to the Johnson-Morgan UBV system. The transformation relation used by Mihalas was derived by Matthews and Sandage (1963) on the basis of the energy spectra of seven stars measured on the old photometric calibration.

Matsushima and Hall assumed the observed colors, B-V or U-B, to have a linear relation with the unnormalized theoretical colors, b-v or u-b, such that

$$B-V = A(b-v) + B, \quad (3-1)$$

where

$$b-v = 2.5 \log \int_0^{\infty} F_{\lambda} S_v(\lambda) d\lambda - 2.5 \log \int_0^{\infty} F_{\lambda} S_b(\lambda) d\lambda, \quad (3-2)$$

$F_{\lambda}$  is the flux per unit wavelength at wavelength  $\lambda$ ,

$S_v$  and  $S_b$  represent the response function of the V and B filter-photometer systems,

A and B are constants to be determined by an empirical fit between the observed colors and the colors computed from Equation (3-2).

The S functions are tabulated by Matthews and Sandage. A numerical integration of Equation (3-2) was performed in order to examine possible discrepancies that may exist. The most important fact determined from the integration of Equation (3-2) was that an effective temperature was obtained which was approximately ten to twenty per cent greater than the values determined by Mihalas.

The Matsushima-Hall and Matthews-Sandage computations do not take into account the flux removed by absorption lines. They expect that the blocking of energy by hydrogen lines will be large, while metal lines should be very weak in their spectra. They suggest a reasonable estimate of the magnitude of the energy removed by hydrogen lines may be made by taking the difference between theoretical colors computed with and without the lines from a model closely representing the star. The correction for hydrogen lines gives a transformation similar to those given by Matthews and Sandage. A method of least square fits of the stars excluding those of luminosity classes other than the main sequence, yields

$$U-B = 0.896 (u-b) - 1.288, \quad (3-3)$$

$$B-V = 0.982 (b-v) + 0.791. \quad (3-4)$$

The validity of the transformations given by Equations (3-3) and (3-4) may be limited because they do not include line blanketing effects and the basic data include only blue stars.

Equations (3-3) and (3-4) are similar to the equations derived by Matthews and Sandage in both the color dependency and the constant term. The difference in theoretical colors obtained from the two transformation relations differ by 0.01 to 0.02 magnitudes. This close agreement is expected since neither method allowed any correction for line blocking in the derivations of the equations. An error in the estimation of the hydrogen content could change the U-B relation by a significant amount, while the corresponding change for B-V may be negligible.

## Matthews and Sandage Method

It is possible, and many times desirable, to compute the UBV colors of radiant sources with given energy distribution. The computation can be performed once the transmission functions,  $S(\lambda)$ , of the U,B,V system are known. Melbourne (1960) showed that the  $S(\lambda)$  functions tabulated by Johnson will not predict exactly the U-B and B-V colors for real stars of known energy distribution unless a systematic zero-point correction of -0.13 is applied to the computed natural b-v magnitude and +0.17 is added to the computed u-b magnitude before applying Johnson's (1953) empirically determined transformation equation. These corrections assume that there is no color equation between the theoretical colors based on  $S(\lambda)$  and the U-B and B-V values adapted for standard stars in the sky.

Matthews and Sandage (1963) confirm Melbourne's zero point procedure for B-V colors. They derive equations that can be used to convert theoretical calculations based on the adopted  $S(\lambda)$  to the empirical U,B,V system. Predicted U-B and B-V colors for any arbitrary flux distribution function  $F(\lambda)$  can be obtained also. The transmission functions used by Matthews and Sandage were taken from Melbourne's thesis. Table IV lists the transmission functions from Melbourne's thesis and these transmission functions are used in this study to compute the U-B and B-V colors. A complete derivation and explanation of the equations are given by Matthews and Sandage (1963).

The procedure used by Matthews and Sandage for computing the U-B and B-V colors for any arbitrary energy distribution  $F(\lambda)$  was done in the following manner. (1) Use the  $S(\lambda)$  functions of Table IV and Equations (3-5) and (3-6) to compute the colors u-b and b-v.

TABLE IV  
ADOPTED TRANSMISSION FUNCTIONS AFTER MELBOURNE AND CODE

| $\lambda$<br>°<br>A | S( $\lambda$ ) |       |       |
|---------------------|----------------|-------|-------|
|                     | u              | b     | v     |
| 3000                | 0.025          |       |       |
| 3100                | 0.250          |       |       |
| 3200                | 0.680          |       |       |
| 3300                | 1.137          |       |       |
| 3400                | 1.650          |       |       |
| 3500                | 2.006          | 0.000 |       |
| 3600                | 2.250          | 0.006 |       |
| 3700                | 2.337          | 0.080 |       |
| 3800                | 1.925          | 0.337 |       |
| 3900                | 0.650          | 1.425 |       |
| 4000                | 0.197          | 2.253 |       |
| 4100                | 0.070          | 2.806 |       |
| 4200                | 0.000          | 2.950 |       |
| 4300                |                | 3.000 |       |
| 4400                |                | 2.937 |       |
| 4500                |                | 2.780 |       |
| 4600                |                | 2.520 |       |
| 4700                |                | 2.230 |       |
| 4800                |                | 1.881 | 0.020 |
| 4900                |                | 1.550 | 0.175 |
| 5000                |                | 1.275 | 0.900 |
| 5100                |                | 0.975 | 1.880 |
| 5200                |                | 0.695 | 2.512 |
| 5300                |                | 0.430 | 2.850 |
| 5400                |                | 0.210 | 2.820 |
| 5500                |                | 0.055 | 2.625 |
| 5600                |                | 0.000 | 2.370 |
| 5700                |                |       | 2.050 |
| 5800                |                |       | 1.720 |
| 5900                |                |       | 1.413 |
| 6000                |                |       | 1.068 |
| 6100                |                |       | 0.795 |
| 6200                |                |       | 0.567 |
| 6300                |                |       | 0.387 |
| 6400                |                |       | 0.250 |
| 6500                |                |       | 0.160 |
| 6600                |                |       | 0.110 |
| 6700                |                |       | 0.081 |
| 6800                |                |       | 0.061 |
| 6900                |                |       | 0.045 |
| 7000                |                |       | 0.028 |
| 7100                |                |       | 0.017 |
| 7200                |                |       | 0.007 |

$$u-b = 2.5 \log \frac{\int_0^{\infty} S_b(\lambda) F(\lambda) d\lambda}{\int_0^{\infty} S_u(\lambda) F(\lambda) d\lambda} . \quad (3-5)$$

$$b-v = 2.5 \log \frac{\int_0^{\infty} S_v(\lambda) F(\lambda) d\lambda}{\int_0^{\infty} S_b(\lambda) F(\lambda) d\lambda} . \quad (3-6)$$

(ii) Use Equations (3-7) and (3-8) to compute the U-B and B-V colors.

$$U-B = 0.921 (u-b) - 1.308. \quad (3-7)$$

$$B-V = 1.024 (b-v) + 0.81. \quad (3-8)$$

#### Theoretical Colors Without Line Blanketing

The model atmosphere program was designed to compute the flux distribution function,  $F(\lambda)$ , for twenty-two different wavelengths between  $\lambda 2000$  and  $\lambda 7460$ . Four different values of  $\log g$  and four different values of effective temperature, indicative of four different spectral types, were considered, resulting in a grid of sixteen model atmospheres. In order to use the adopted transmission functions,  $S(\lambda)$ , given by Matthews and Sandage (1963), the values of  $F(\lambda)$  must be known at each one hundred angstroms over the interval under investigation.  $F(\lambda)$  was plotted as a function of wavelength using the values computed from the atmosphere program and a smooth curve was drawn through the plotted points in order that the values of  $F(\lambda)$  might be read at the desired intervals. Table V gives the values of  $F(\lambda) \times 10^{-5}$  and  $\log F(\lambda) \times 10^{-8}$  rather than the values obtained from the computer program. Figure 1 illustrates the variation of the computed flux for a solar-type star over the interval  $\lambda \lambda 3000-7200$ .

The transmission functions were then multiplied by the appropriate



TABLE V  
THEORETICAL FLUX DISTRIBUTIONS

| Spectral Type | $T_{\text{eff}}$<br>°K | log g  | $\lambda$ | $F(\lambda) \times 10^{-5}$ | $\log F(\lambda) - 8$ |
|---------------|------------------------|--------|-----------|-----------------------------|-----------------------|
| F4 V          | 6650                   | 3.8    | 2000.00   | 00.72                       | 4.8569                |
|               |                        |        | 2500.00   | 26.92                       | 6.4300                |
|               |                        |        | 3000.00   | 43.65                       | 6.6402                |
|               |                        |        | 3200.00   | 44.88                       | 6.6521                |
|               |                        |        | 3400.00   | 45.61                       | 6.6591                |
|               |                        |        | 3645.00   | 45.50                       | 6.6580                |
|               |                        |        | 3650.00   | 76.10                       | 6.8814                |
|               |                        |        | 3889.05   | 76.35                       | 6.8828                |
|               |                        |        | 4000.00   | 74.75                       | 6.8736                |
|               |                        |        | 4104.74   | 74.56                       | 6.8725                |
|               |                        |        | 4200.00   | 73.25                       | 6.8648                |
|               |                        |        | 4340.47   | 70.37                       | 6.8474                |
|               |                        |        | 4600.00   | 65.65                       | 6.8172                |
|               |                        |        | 4861.33   | 60.58                       | 6.7823                |
|               |                        |        | 5150.00   | 56.48                       | 6.7519                |
|               |                        |        | 5383.37   | 53.16                       | 6.7256                |
|               |                        |        | 5560.00   | 50.41                       | 6.7025                |
|               |                        |        | 5895.92   | 45.90                       | 6.6618                |
|               |                        |        | 6050.00   | 43.78                       | 6.6413                |
|               |                        |        | 6562.82   | 37.79                       | 6.5774                |
| 7000.00       | 33.21                  | 6.5213 |           |                             |                       |
| 7460.00       | 29.14                  | 6.4645 |           |                             |                       |
| F4 V          | 6650                   | 4.0    | 2000.00   | 00.73                       | 4.8606                |
|               |                        |        | 2500.00   | 28.19                       | 6.4501                |
|               |                        |        | 3000.00   | 45.67                       | 6.6596                |
|               |                        |        | 3200.00   | 46.75                       | 6.6698                |
|               |                        |        | 3400.00   | 47.38                       | 6.6756                |
|               |                        |        | 3645.00   | 47.10                       | 6.6730                |
|               |                        |        | 3650.00   | 75.91                       | 6.6730                |
|               |                        |        | 3889.05   | 76.21                       | 6.8820                |
|               |                        |        | 4000.00   | 74.61                       | 6.8728                |
|               |                        |        | 4101.47   | 74.46                       | 6.8719                |
|               |                        |        | 4200.00   | 73.17                       | 6.8643                |
|               |                        |        | 4340.47   | 70.31                       | 6.8470                |
|               |                        |        | 4600.00   | 65.60                       | 6.8169                |
|               |                        |        | 4861.33   | 60.56                       | 6.7822                |
|               |                        |        | 5150.00   | 56.49                       | 6.7520                |
|               |                        |        | 5385.37   | 53.17                       | 6.7257                |
|               |                        |        | 5560.00   | 50.44                       | 6.7028                |
|               |                        |        | 5895.92   | 45.94                       | 6.6622                |
|               |                        |        | 6050.00   | 43.82                       | 6.6417                |
|               |                        |        | 6562.82   | 37.84                       | 6.5779                |
| 7000.00       | 33.26                  | 6.5219 |           |                             |                       |
| 7460.00       | 29.19                  | 6.4652 |           |                             |                       |

TABLE V (Continued)

| Spectral Type | $T_{\text{eff}}$<br>°K | log g  | $\lambda$ | $F(\lambda) \times 10^{-5}$ | $\log F(\lambda) - 8$ |
|---------------|------------------------|--------|-----------|-----------------------------|-----------------------|
| F4 V          | 6650                   | 4.2    | 2000.00   | 00.73                       | 4.8649                |
|               |                        |        | 2500.00   | 11.10                       | 6.0419                |
|               |                        |        | 3000.00   | 47.66                       | 6.6782                |
|               |                        |        | 3200.00   | 48.63                       | 6.6869                |
|               |                        |        | 3400.00   | 49.16                       | 6.6915                |
|               |                        |        | 3645.00   | 48.70                       | 6.6875                |
|               |                        |        | 3650.00   | 75.72                       | 6.8792                |
|               |                        |        | 3889.05   | 76.07                       | 6.8812                |
|               |                        |        | 4000.00   | 74.51                       | 6.8722                |
|               |                        |        | 4104.74   | 74.35                       | 6.8713                |
|               |                        |        | 4200.00   | 73.08                       | 6.8638                |
|               |                        |        | 4340.47   | 70.25                       | 6.8466                |
|               |                        |        | 4600.00   | 65.57                       | 6.8167                |
|               |                        |        | 4861.33   | 60.55                       | 6.7821                |
|               |                        |        | 5150.00   | 56.51                       | 6.7521                |
|               |                        |        | 5385.37   | 53.20                       | 6.7259                |
|               |                        |        | 5560.00   | 50.47                       | 6.7030                |
|               |                        |        | 5895.92   | 45.97                       | 6.6625                |
|               |                        |        | 6050.00   | 43.87                       | 6.6421                |
|               |                        |        | 6562.82   | 37.88                       | 6.5784                |
| 7000.00       | 33.30                  | 6.5224 |           |                             |                       |
| 7460.00       | 29.23                  | 4.6580 |           |                             |                       |
| F4 V          | 6650                   | 4.4    | 2000.00   | 00.74                       | 4.8701                |
|               |                        |        | 2500.00   | 30.71                       | 6.4872                |
|               |                        |        | 3000.00   | 49.66                       | 6.6960                |
|               |                        |        | 3200.00   | 50.50                       | 6.7033                |
|               |                        |        | 3400.00   | 50.91                       | 6.7068                |
|               |                        |        | 3645.00   | 50.28                       | 6.7014                |
|               |                        |        | 3650.00   | 75.58                       | 6.8784                |
|               |                        |        | 3889.05   | 75.78                       | 6.8806                |
|               |                        |        | 4000.00   | 74.41                       | 6.8716                |
|               |                        |        | 4104.74   | 74.27                       | 6.8708                |
|               |                        |        | 4200.00   | 73.01                       | 6.8634                |
|               |                        |        | 4340.47   | 70.25                       | 6.8463                |
|               |                        |        | 4600.00   | 65.55                       | 6.8166                |
|               |                        |        | 4861.33   | 60.53                       | 6.7820                |
|               |                        |        | 5150.00   | 56.51                       | 6.7521                |
|               |                        |        | 5385.37   | 53.21                       | 6.7260                |
| 5560.00       | 50.48                  | 6.7031 |           |                             |                       |
| 5895.92       | 46.00                  | 6.6628 |           |                             |                       |
| 6050.00       | 43.88                  | 6.6423 |           |                             |                       |
| 6562.82       | 37.91                  | 6.5788 |           |                             |                       |
| 7000.00       | 33.33                  | 6.5228 |           |                             |                       |
| 7460.00       | 29.27                  | 6.4664 |           |                             |                       |
| F5 V          | 6500                   | 3.8    | 2000.00   | 00.43                       | 4.6339                |
|               |                        |        | 2500.00   | 22.38                       | 6.3499                |

TABLE V (Continued)

| Spectral Type | $T_{\text{eff}}$<br>°K | log g  | $\lambda$ | $F(\lambda) \times 10^{-5}$ | $\log F(\lambda) - 8$ |         |
|---------------|------------------------|--------|-----------|-----------------------------|-----------------------|---------|
| F5 V          | 6500                   | 3.8    | 3000.00   | 39.85                       | 6.6004                |         |
|               |                        |        | 3200.00   | 41.13                       | 6.6142                |         |
|               |                        |        | 3400.00   | 42.00                       | 6.6232                |         |
|               |                        |        | 3645.00   | 42.03                       | 6.6236                |         |
|               |                        |        | 3650.00   | 66.44                       | 6.8224                |         |
|               |                        |        | 3889.05   | 67.53                       | 6.8295                |         |
|               |                        |        | 4000.00   | 66.41                       | 6.8222                |         |
|               |                        |        | 4101.74   | 66.56                       | 6.8232                |         |
|               |                        |        | 4200.00   | 65.55                       | 6.8166                |         |
|               |                        |        | 4340.47   | 63.18                       | 6.8006                |         |
|               |                        |        | 4600.00   | 59.27                       | 6.7728                |         |
|               |                        |        | 4861.33   | 55.00                       | 6.7404                |         |
|               |                        |        | 5150.00   | 51.52                       | 6.7120                |         |
|               |                        |        | 5383.37   | 48.67                       | 6.6873                |         |
|               |                        |        | 5560.00   | 46.28                       | 6.6654                |         |
|               |                        |        | 5895.92   | 42.33                       | 6.6267                |         |
|               |                        |        | 6050.00   | 40.46                       | 6.6070                |         |
|               |                        |        | 6562.82   | 35.12                       | 6.5455                |         |
|               |                        |        | 7000.00   | 30.98                       | 6.4911                |         |
|               |                        |        | F5 V      | 6500                        | 4.0                   | 7460.00 |
| 2000.00       | 00.43                  | 4.6372 |           |                             |                       |         |
| 2500.00       | 23.39                  | 6.3690 |           |                             |                       |         |
| 3000.00       | 41.60                  | 6.6191 |           |                             |                       |         |
| 3200.00       | 42.78                  | 6.6312 |           |                             |                       |         |
| 3400.00       | 43.54                  | 6.6389 |           |                             |                       |         |
| 3645.00       | 43.43                  | 6.6378 |           |                             |                       |         |
| 3650.00       | 66.33                  | 6.8217 |           |                             |                       |         |
| 5             | 3889.05                | 67.46  |           |                             |                       | 6.8290  |
|               | 4000.00                | 66.34  |           |                             |                       | 6.8218  |
|               | 4104.74                | 66.48  |           |                             | 6.8227                |         |
|               | 4200.00                | 65.51  |           |                             | 6.8163                |         |
|               | 4340.47                | 63.10  |           |                             | 6.8004                |         |
|               | 4600.00                | 59.24  |           |                             | 6.7726                |         |
|               | 4861.33                | 54.99  |           |                             | 6.7403                |         |
|               | 5150.00                | 51.52  |           |                             | 6.7120                |         |
|               | 5358.37                | 48.70  |           |                             | 6.6875                |         |
|               | 5560.00                | 46.29  |           |                             | 6.6655                |         |
| 5             | 5898.92                | 42.35  |           |                             | 6.6269                |         |
|               | 6050.00                | 40.43  |           |                             | 6.6072                |         |
|               | 6562.82                | 35.15  | 6.5459    |                             |                       |         |
|               | 7000.00                | 31.02  | 6.4916    |                             |                       |         |
|               | 7460.00                | 27.33  | 6.4366    |                             |                       |         |
|               | F5 V                   | 6500   | 4.2       | 2000.00                     | 00.44                 | 4.6414  |
|               |                        |        |           | 2500.00                     | 24.38                 | 6.3870  |
|               |                        |        |           | 3000.00                     | 43.33                 | 6.6368  |
|               |                        |        |           | 3200.00                     | 44.41                 | 6.6475  |

TABLE V (Continued)

| Spectral Type | $T_{\text{eff}}$<br>°K | log g  | $\lambda$ | $F(\lambda) \times 10^{-5}$ | $\log F(\lambda) - 8$ |         |       |        |
|---------------|------------------------|--------|-----------|-----------------------------|-----------------------|---------|-------|--------|
| F5 V          | 6500                   | 4.2    | 3400.00   | 45.08                       | 6.6540                |         |       |        |
|               |                        |        | 3645.00   | 44.82                       | 6.6515                |         |       |        |
|               |                        |        | 3650.00   | 66.24                       | 6.8211                |         |       |        |
|               |                        |        | 3889.05   | 67.39                       | 6.8286                |         |       |        |
|               |                        |        | 4000.00   | 66.28                       | 6.8160                |         |       |        |
|               |                        |        | 4104.74   | 66.44                       | 6.8224                |         |       |        |
|               |                        |        | 4200.00   | 65.46                       | 6.8160                |         |       |        |
|               |                        |        | 4340.47   | 63.11                       | 6.8001                |         |       |        |
|               |                        |        | 4600.00   | 59.22                       | 6.7725                |         |       |        |
|               |                        |        | 4861.33   | 54.98                       | 6.7402                |         |       |        |
|               |                        |        | 5150.00   | 51.52                       | 6.7120                |         |       |        |
|               |                        |        | 5385.37   | 48.71                       | 6.6876                |         |       |        |
|               |                        |        | 5560.00   | 46.30                       | 6.6656                |         |       |        |
|               |                        |        | 5895.92   | 42.37                       | 6.6271                |         |       |        |
|               |                        |        | 6050.00   | 40.49                       | 6.6074                |         |       |        |
|               |                        |        | 6562.82   | 35.17                       | 6.5462                |         |       |        |
|               |                        |        | 7000.00   | 31.04                       | 6.4919                |         |       |        |
|               |                        |        | 7460.00   | 27.36                       | 6.4371                |         |       |        |
|               |                        |        | F5 V      | 6500                        | 4.4                   | 2000.00 | 00.44 | 4.6465 |
|               |                        |        |           |                             |                       | 2500.00 | 25.35 | 6.4039 |
| 3000.00       | 45.06                  | 6.6538 |           |                             |                       |         |       |        |
| 3200.00       | 46.04                  | 6.6631 |           |                             |                       |         |       |        |
| 3400.00       | 46.61                  | 6.6685 |           |                             |                       |         |       |        |
| 3645.00       | 46.20                  | 6.6646 |           |                             |                       |         |       |        |
| 3650.00       | 66.18                  | 6.8207 |           |                             |                       |         |       |        |
| 3889.05       | 67.34                  | 6.8283 |           |                             |                       |         |       |        |
| 4000.00       | 66.24                  | 6.8211 |           |                             |                       |         |       |        |
| 4104.74       | 66.39                  | 6.8221 |           |                             |                       |         |       |        |
| 4200.00       | 65.42                  | 6.8157 |           |                             |                       |         |       |        |
| 4340.47       | 63.08                  | 6.7999 |           |                             |                       |         |       |        |
| 4600.00       | 59.21                  | 6.7724 |           |                             |                       |         |       |        |
| 4861.33       | 54.98                  | 6.7402 |           |                             |                       |         |       |        |
| 5150.00       | 51.54                  | 6.7121 |           |                             |                       |         |       |        |
| 5385.37       | 48.71                  | 6.6876 |           |                             |                       |         |       |        |
| 5560.00       | 46.31                  | 6.6657 |           |                             |                       |         |       |        |
| 5895.92       | 42.39                  | 6.6273 |           |                             |                       |         |       |        |
| 6050.00       | 40.51                  | 6.6076 |           |                             |                       |         |       |        |
| 6562.82       | 35.19                  | 6.5464 |           |                             |                       |         |       |        |
| 7000.00       | 31.06                  | 6.4922 |           |                             |                       |         |       |        |
| 7460.00       | 27.38                  | 6.4374 |           |                             |                       |         |       |        |
| F6 V          | 6350                   | 3.8    | 2000.00   | 00.27                       | 4.4163                |         |       |        |
|               |                        |        | 2500.00   | 18.80                       | 6.2572                |         |       |        |
|               |                        |        | 3000.00   | 36.00                       | 6.5566                |         |       |        |
|               |                        |        | 3200.00   | 37.37                       | 6.5725                |         |       |        |
|               |                        |        | 3400.00   | 38.34                       | 6.5836                |         |       |        |
|               |                        |        | 3645.00   | 38.52                       | 6.5857                |         |       |        |

TABLE V (Continued)

| Spectral Type | $T_{\text{eff}}$<br>°K | log g  | $\lambda$ | $F(\lambda) \times 10^{-5}$ | $\log F(\lambda) - 8$ |
|---------------|------------------------|--------|-----------|-----------------------------|-----------------------|
| F6 V          | 6350                   | 3.8    | 3650.00   | 57.65                       | 6.7608                |
|               |                        |        | 3889.05   | 59.44                       | 6.7741                |
|               |                        |        | 4000.00   | 58.72                       | 6.7688                |
|               |                        |        | 4104.74   | 59.13                       | 6.7718                |
|               |                        |        | 4200.00   | 58.28                       | 6.7665                |
|               |                        |        | 4340.47   | 56.48                       | 6.7519                |
|               |                        |        | 4600.00   | 53.26                       | 6.7264                |
|               |                        |        | 4861.33   | 49.72                       | 6.6965                |
|               |                        |        | 5150.00   | 46.78                       | 6.6700                |
|               |                        |        | 5385.37   | 44.38                       | 6.6472                |
|               |                        |        | 5560.00   | 42.30                       | 6.6263                |
|               |                        |        | 5895.92   | 38.88                       | 6.5897                |
|               |                        |        | 6050.00   | 37.21                       | 6.5707                |
|               |                        |        | 6562.82   | 32.49                       | 6.5118                |
|               |                        |        | 7000.00   | 28.79                       | 6.4593                |
|               |                        |        | 7460.00   | 25.47                       | 6.4060                |
|               |                        |        | F6 V      | 6360                        | 4.0                   |
| 2500.00       | 18.85                  | 6.2753 |           |                             |                       |
| 3000.00       | 37.53                  | 6.5744 |           |                             |                       |
| 3200.00       | 38.80                  | 6.5888 |           |                             |                       |
| 3400.00       | 39.68                  | 6.5986 |           |                             |                       |
| 3645.00       | 39.73                  | 6.5991 |           |                             |                       |
| 3650.00       | 57.62                  | 6.7606 |           |                             |                       |
| 3889.05       | 59.42                  | 6.7739 |           |                             |                       |
| 4000.00       | 58.70                  | 6.7686 |           |                             |                       |
| 4104.74       | 59.10                  | 6.7716 |           |                             |                       |
| 4200.00       | 58.39                  | 6.7663 |           |                             |                       |
| 4340.47       | 56.46                  | 6.7517 |           |                             |                       |
| 4600.00       | 53.25                  | 6.7263 |           |                             |                       |
| 4861.33       | 49.72                  | 6.6965 |           |                             |                       |
| 5150.00       | 46.77                  | 6.6700 |           |                             |                       |
| 5385.37       | 44.39                  | 6.6473 |           |                             |                       |
| 5560.00       | 42.31                  | 6.6264 |           |                             |                       |
| 5895.92       | 38.89                  | 6.5898 |           |                             |                       |
| 6050.00       | 37.23                  | 6.5709 |           |                             |                       |
| 6562.82       | 32.51                  | 6.5120 |           |                             |                       |
| 7000.00       | 28.82                  | 6.4596 |           |                             |                       |
| 7460.00       | 25.49                  | 6.4063 |           |                             |                       |
| F6 V          | 6350                   | 4.2    | 2000.00   | 00.27                       | 4.4240                |
|               |                        |        | 2500.00   | 19.61                       | 6.2922                |
|               |                        |        | 3000.00   | 39.30                       | 6.5914                |
|               |                        |        | 3200.00   | 39.85                       | 6.6042                |
|               |                        |        | 3400.00   | 40.77                       | 6.6128                |
|               |                        |        | 3645.00   | 40.93                       | 6.6120                |
|               |                        |        | 3650.00   | 57.61                       | 6.7605                |
|               |                        |        | 3889.05   | 59.40                       | 6.7738                |

TABLE V (Continued)

| Spectral Type | $T_{\text{eff}}$<br>°K | log g  | $\lambda$ | $F(\lambda) \times 10^{-5}$ | $\log F(\lambda) - 8$ |
|---------------|------------------------|--------|-----------|-----------------------------|-----------------------|
| F6 V          | 6350                   | 4.2    | 4000.00   | 58.68                       | 6.7685                |
|               |                        |        | 4101.74   | 59.08                       | 6.7714                |
|               |                        |        | 4200.00   | 58.42                       | 6.7662                |
|               |                        |        | 4340.47   | 56.44                       | 6.7516                |
|               |                        |        | 4600.00   | 53.25                       | 6.7263                |
|               |                        |        | 4861.33   | 49.72                       | 6.6964                |
|               |                        |        | 5150.00   | 46.79                       | 6.6701                |
|               |                        |        | 5385.37   | 44.39                       | 6.6473                |
|               |                        |        | 5560.00   | 42.31                       | 6.6264                |
|               |                        |        | 5895.92   | 38.81                       | 6.5889                |
|               |                        |        | 6050.00   | 37.24                       | 6.5710                |
|               |                        |        | 6562.82   | 32.45                       | 6.5112                |
|               |                        |        | 7000.00   | 28.83                       | 6.4598                |
|               |                        |        | 7460.00   | 25.51                       | 6.4066                |
|               |                        |        | F6 V      | 6350                        | 4.4                   |
| 2500.00       | 20.34                  | 6.3082 |           |                             |                       |
| 3000.00       | 40.50                  | 6.6074 |           |                             |                       |
| 3200.00       | 41.58                  | 6.6189 |           |                             |                       |
| 3400.00       | 42.31                  | 6.6264 |           |                             |                       |
| 3645.00       | 42.09                  | 6.6242 |           |                             |                       |
| 3650.00       | 57.61                  | 6.7605 |           |                             |                       |
| 3889.05       | 59.40                  | 6.7738 |           |                             |                       |
| 4000.00       | 58.73                  | 6.7684 |           |                             |                       |
| 4101.74       | 59.06                  | 6.7713 |           |                             |                       |
| 4200.00       | 58.36                  | 6.7661 |           |                             |                       |
| 4340.47       | 56.43                  | 6.7515 |           |                             |                       |
| 4600.00       | 53.24                  | 6.7262 |           |                             |                       |
| 4861.33       | 49.71                  | 6.6964 |           |                             |                       |
| 5150.00       | 46.79                  | 6.6701 |           |                             |                       |
| 5383.37       | 44.39                  | 6.6473 |           |                             |                       |
| 5560.00       | 42.32                  | 6.6265 |           |                             |                       |
| 5895.92       | 38.91                  | 6.5900 |           |                             |                       |
| 6050.00       | 37.25                  | 6.5711 |           |                             |                       |
| 6562.82       | 32.53                  | 6.5123 |           |                             |                       |
| 7000.00       | 28.84                  | 6.4599 |           |                             |                       |
| 7560.00       | 25.52                  | 6.4069 |           |                             |                       |
| F8 V          | 6200                   | 3.8    | 2000.00   | 00.16                       | 4.2029                |
|               |                        |        | 2500.00   | 14.11                       | 6.1496                |
|               |                        |        | 3000.00   | 32.22                       | 6.5081                |
|               |                        |        | 3200.00   | 33.61                       | 6.5265                |
|               |                        |        | 3400.00   | 34.67                       | 6.5399                |
|               |                        |        | 3645.00   | 34.99                       | 6.5439                |
|               |                        |        | 3650.00   | 49.72                       | 6.6965                |
|               |                        |        | 3889.05   | 52.04                       | 6.7163                |
|               |                        |        | 4000.00   | 51.66                       | 6.7131                |
|               |                        |        | 4101.74   | 52.28                       | 6.7183                |
|               |                        |        | 4200.00   | 51.78                       | 6.7142                |

TABLE V (Continued)

| Spectral Type | $T_{\text{eff}}$<br>°K | log g  | $\lambda$ | $F(\lambda) \times 10^{-5}$ | $\log F(\lambda) - 8$ |         |       |        |
|---------------|------------------------|--------|-----------|-----------------------------|-----------------------|---------|-------|--------|
| F8 V          | 6200                   | 3.8    | 4340.47   | 50.23                       | 6.7010                |         |       |        |
|               |                        |        | 4600.00   | 47.63                       | 6.6779                |         |       |        |
|               |                        |        | 4861.33   | 44.72                       | 6.6505                |         |       |        |
|               |                        |        | 5150.00   | 42.27                       | 6.6260                |         |       |        |
|               |                        |        | 5385.37   | 40.27                       | 6.6050                |         |       |        |
|               |                        |        | 5560.00   | 38.48                       | 6.5852                |         |       |        |
|               |                        |        | 5895.92   | 35.54                       | 6.5507                |         |       |        |
|               |                        |        | 6050.00   | 34.09                       | 6.5326                |         |       |        |
|               |                        |        | 6562.82   | 29.94                       | 6.4762                |         |       |        |
|               |                        |        | 7000.00   | 26.64                       | 6.4256                |         |       |        |
|               |                        |        | 7460.00   | 23.67                       | 6.3742                |         |       |        |
|               |                        |        | F8 V      | 6200                        | 4.0                   | 2000.00 | 00.17 | 4.2066 |
|               |                        |        |           |                             |                       | 2500.00 | 14.70 | 6.1666 |
| 3000.00       | 33.50                  | 6.5251 |           |                             |                       |         |       |        |
| 3200.00       | 34.83                  | 6.5419 |           |                             |                       |         |       |        |
| 3400.00       | 35.81                  | 6.5540 |           |                             |                       |         |       |        |
| 3645.00       | 36.02                  | 6.5565 |           |                             |                       |         |       |        |
| 3650.00       | 49.75                  | 6.6968 |           |                             |                       |         |       |        |
| 3889.05       | 52.06                  | 6.7165 |           |                             |                       |         |       |        |
| 4000.00       | 51.67                  | 6.7132 |           |                             |                       |         |       |        |
| 4101.47       | 52.28                  | 6.7183 |           |                             |                       |         |       |        |
| 4200.00       | 51.78                  | 6.7142 |           |                             |                       |         |       |        |
| 4340.47       | 50.23                  | 6.7010 |           |                             |                       |         |       |        |
| 4600.00       | 47.62                  | 6.6779 |           |                             |                       |         |       |        |
| 4861.33       | 44.72                  | 6.6505 |           |                             |                       |         |       |        |
| 5150.00       | 42.27                  | 6.6260 |           |                             |                       |         |       |        |
| 5385.37       | 40.37                  | 6.6050 |           |                             |                       |         |       |        |
| 5560.00       | 38.51                  | 6.5852 |           |                             |                       |         |       |        |
| 5895.92       | 35.54                  | 6.5507 |           |                             |                       |         |       |        |
| 6050.00       | 34.09                  | 6.5326 |           |                             |                       |         |       |        |
| 6562.82       | 29.94                  | 6.4763 |           |                             |                       |         |       |        |
| 7000.00       | 26.66                  | 6.4258 |           |                             |                       |         |       |        |
| 7460.00       | 23.67                  | 6.3743 |           |                             |                       |         |       |        |
| F8 V          | 6200                   | 4.2    | 2000.00   | 00.16                       | 4.2117                |         |       |        |
|               |                        |        | 2500.00   | 15.23                       | 6.1828                |         |       |        |
|               |                        |        | 3000.00   | 34.79                       | 6.5414                |         |       |        |
|               |                        |        | 3200.00   | 36.03                       | 6.5566                |         |       |        |
|               |                        |        | 3400.00   | 36.94                       | 6.5675                |         |       |        |
|               |                        |        | 3645.00   | 37.03                       | 6.5686                |         |       |        |
|               |                        |        | 3650.00   | 49.81                       | 6.6973                |         |       |        |
|               |                        |        | 3889.05   | 52.08                       | 6.7167                |         |       |        |
|               |                        |        | 4000.00   | 51.69                       | 6.7134                |         |       |        |
|               |                        |        | 4101.74   | 52.29                       | 6.7184                |         |       |        |
|               |                        |        | 4200.00   | 51.80                       | 6.7143                |         |       |        |
|               |                        |        | 4340.47   | 50.24                       | 6.7011                |         |       |        |
|               |                        |        | 4600.00   | 47.64                       | 6.6780                |         |       |        |

TABLE V. (Concluded)

| Spectral Type | $T_{\text{eff}}$<br>°K | log g  | $\lambda$ | $F(\lambda) \times 10^{-5}$ | $\log F(\lambda) - 8$ |
|---------------|------------------------|--------|-----------|-----------------------------|-----------------------|
| F8 V          | 6200                   | 4.2    | 4861.33   | 44.73                       | 6.6506                |
|               |                        |        | 5150.00   | 42.28                       | 6.6261                |
|               |                        |        | 5385.37   | 40.28                       | 6.6051                |
|               |                        |        | 5560.00   | 38.49                       | 6.5853                |
|               |                        |        | 5895.92   | 35.55                       | 6.5509                |
|               |                        |        | 6050.00   | 34.09                       | 6.5327                |
|               |                        |        | 6562.82   | 29.96                       | 6.4765                |
|               |                        |        | 7000.00   | 26.66                       | 6.4259                |
|               |                        |        | 7460.00   | 23.69                       | 6.3746                |
|               |                        |        | F8 V      | 6200                        | 4.4                   |
| 2500.00       | 15.76                  | 6.1976 |           |                             |                       |
| 3000.00       | 36.01                  | 6.5564 |           |                             |                       |
| 3200.00       | 37.18                  | 6.5703 |           |                             |                       |
| 3400.00       | 38.94                  | 6.5802 |           |                             |                       |
| 3645.00       | 38.01                  | 6.5799 |           |                             |                       |
| 3650.00       | 49.84                  | 6.6976 |           |                             |                       |
| 3889.05       | 52.11                  | 6.7169 |           |                             |                       |
| 4000.00       | 51.69                  | 6.7134 |           |                             |                       |
| 4101.74       | 52.28                  | 6.7183 |           |                             |                       |
| 4200.00       | 51.78                  | 6.7142 |           |                             |                       |
| 4340.47       | 50.23                  | 6.7010 |           |                             |                       |
| 4600.00       | 47.63                  | 6.6779 |           |                             |                       |
| 4861.33       | 44.72                  | 6.6505 |           |                             |                       |
| 5150.00       | 42.27                  | 6.6260 |           |                             |                       |
| 5385.37       | 40.32                  | 6.6050 |           |                             |                       |
| 5560.00       | 38.48                  | 6.5852 |           |                             |                       |
| 5895.92       | 35.55                  | 6.5508 |           |                             |                       |
| 6050.00       | 34.09                  | 6.5326 |           |                             |                       |
| 6562.82       | 29.95                  | 6.4764 |           |                             |                       |
| 7000.00       | 26.66                  | 6.4259 |           |                             |                       |
| 7460.00       | 23.69                  | 6.3746 |           |                             |                       |



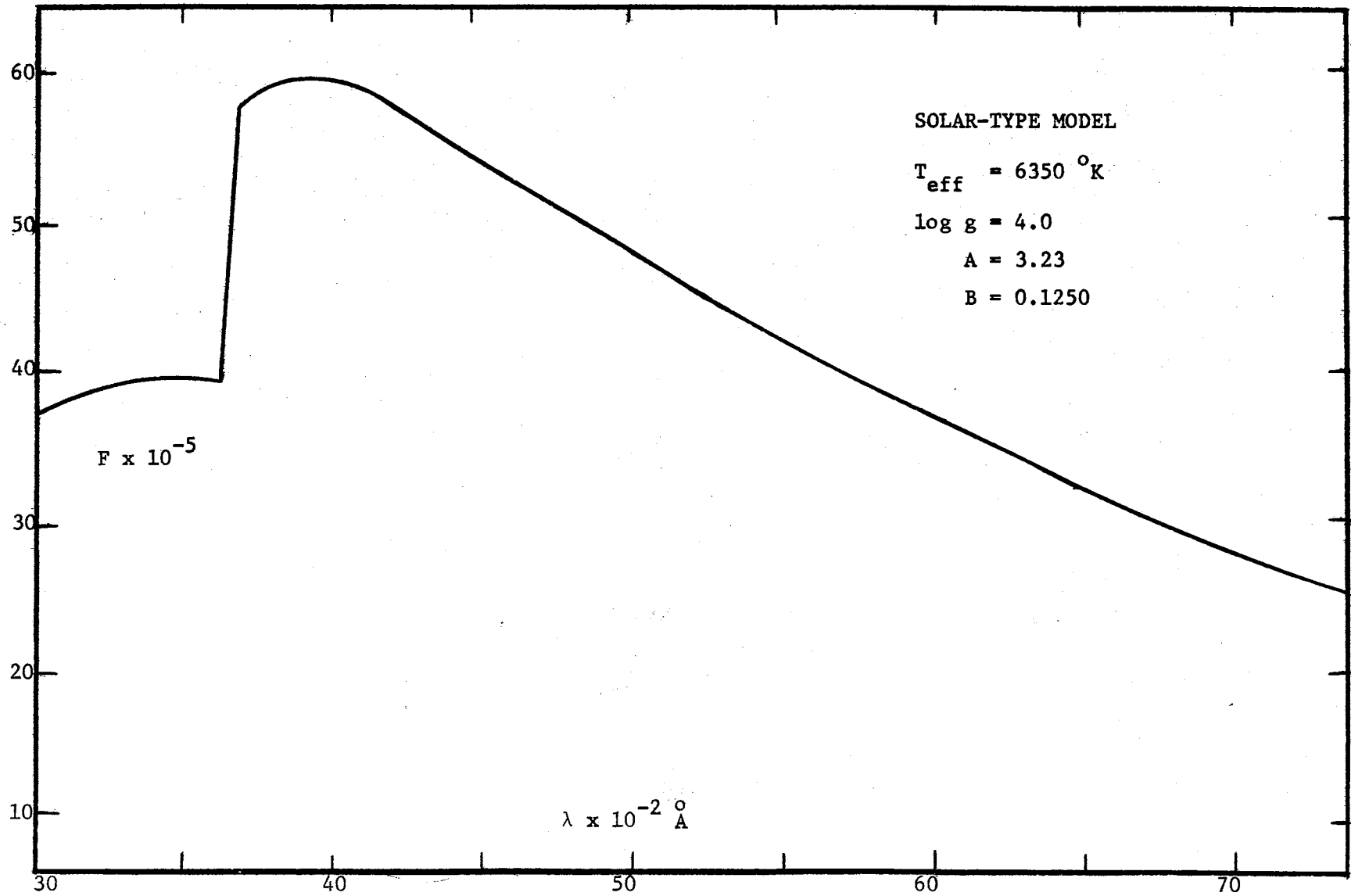


Figure 1. Theoretical Flux Distribution

values of the flux, read from the plotted figure, and then tabulated. A graph of  $F(\lambda) S(\lambda)$  versus  $\lambda$  is shown in Figure 2 where the summations of  $F(\lambda) S(\lambda)$  are the areas under the curves in this figure. Instead of a numerical integration, a summation process employing a desk calculator was used to evaluate these areas. This procedure enables one to calculate the  $u-b$  and  $b-v$  values from Equations (3-5) and (3-6) where the integrals are replaced by the summations or the areas under the curves. Using the values of  $u-b$  and  $b-v$  thus obtained, the  $U-B$  and  $B-V$  colors may be calculated using Equations (3-3) and (3-4) or (3-7) and (3-8).

An objection may be raised concerning the calculations using the Matthews and Sandage method. The true  $F(\lambda)$  may not be known because of the effects of line blanketing with the result that the predicted  $u-b$  colors may be in error. This objection is valid for some stars, but it is not significant for hot stars with extremely weak Fraunhofer lines. The blanketing effect is almost nil for these stars, but the effect in stars like the sun should be taken into account before using the  $F(\lambda)$  function in the above equations.

The theoretical colors, neglecting line blanketing, were calculated for effective temperatures of 6200, 6350, 6500, and 6650  $^{\circ}$ K and  $\log g = 3.8, 4.0, 4.2,$  and  $4.4$ . The results of the calculations are shown in Table VI. It is evident that the computed values of the  $U-B$  and  $B-V$  colors are not in agreement with the observed colors for Theta Ursae Majoris:  $U-B = 0.06$  and  $B-V = 0.46$ . These observed colors are from the Arizona-Tonantzintla Catalogue (Iriarte, et al, 1965). In order to determine if a model better fitting the observations could be obtained, the theoretical colors were calculated with the effects of line blanketing taken into consideration.

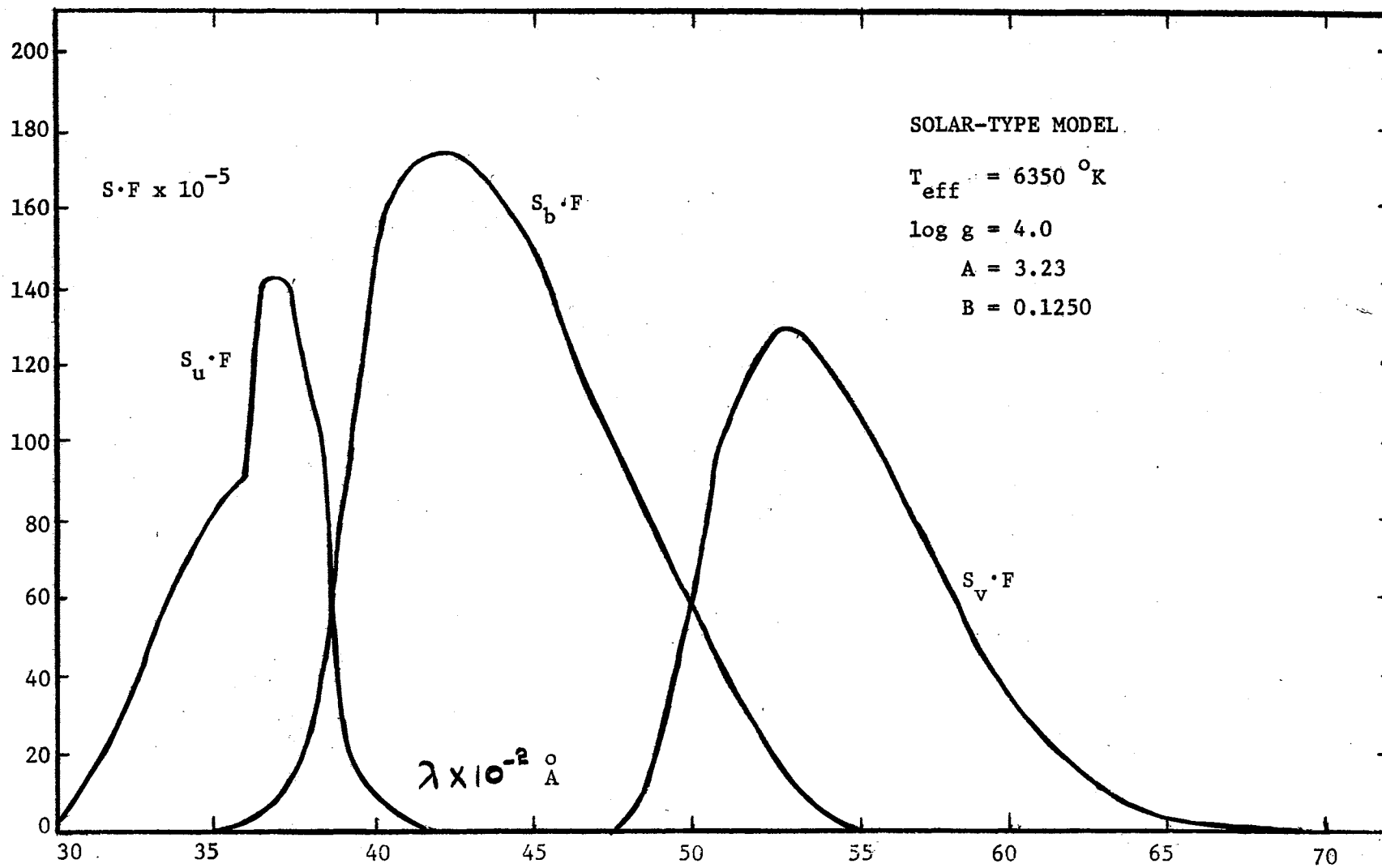


Figure 2. Theoretical Three-Color Flux Transmissions

TABLE VI  
THEORETICAL COLORS WITHOUT LINE BLANKETING

| Effective<br>Temperature ( $^{\circ}$ K) | log g | U-B                 |                    | B-V                 |                    |
|--|-------|---------------------|--------------------|---------------------|--------------------|
|  |       | Matthews<br>Sandage | Matsushima<br>Hall | Matthews<br>Sandage | Matsushima<br>Hall |
| 6650                                     | 3.8   | -0.305              | -0.351             | 0.265               | 0.268              |
|  | 4.0   | -0.343              | -0.377             | 0.266               | 0.269              |
|  | 4.2   | -0.367              | -0.399             | 0.273               | 0.276              |
|  | 4.4   | -0.371              | -0.404             | 0.266               | 0.270              |
| 6500                                     | 3.8   | -0.329              | -0.364             | 0.278               | 0.281              |
|  | 4.0   | -0.346              | -0.380             | 0.287               | 0.289              |
|  | 4.2   | -0.379              | -0.412             | 0.295               | 0.297              |
|  | 4.4   | -0.371              | -0.404             | 0.289               | 0.292              |
| 6350                                     | 3.8   | -0.337              | -0.372             | 0.307               | 0.308              |
|  | 4.0   | -0.359              | -0.365             | 0.304               | 0.305              |
|  | 4.2   | -0.362              | -0.368             | 0.323               | 0.324              |
|  | 4.4   | -0.349              | -0.383             | 0.309               | 0.310              |
| 6200                                     | 3.8   | -0.323              | -0.358             | 0.331               | 0.332              |
|  | 4.0   | -0.321              | -0.356             | 0.336               | 0.337              |
|  | 4.2   | -0.353              | -0.387             | 0.324               | 0.325              |
|  | 4.4   | -0.375              | -0.401             | 0.334               | 0.334              |

### Theoretical Colors With Line Blanketing

The first calculation of the UBV colors, with the line blanketing considered, was done using the blanketing coefficients of the star Procyon in the region between 3000 and 4200 angstroms and the blanketing coefficients of the star Gamma Serpentis in the region between 4200 and 7200 angstroms. The stars Procyon and Gamma Serpentis were selected because they are similar to the star  $\theta$  Ursae Majoris which is an F6 IV star. Procyon is classified as an F5 IV-V star and Gamma Serpentis as an F6 IV-V star. Tables VII and VIII list the blanketing coefficients for the stars Gamma Serpentis (Kegel, 1962) and Procyon (Talbert and Edmonds, 1966).

TABLE VII

#### BLANKETING COEFFICIENTS FOR $\gamma$ SERPENTIS

| $\lambda^*$ | $\gamma$ |
|-------------|----------|
| 4200        | .850     |
| 4300        | .840     |
| 4400        | .895     |
| 4500        | .910     |
| 4600        | .935     |
| 4700        | .945     |
| 4800        | .915     |
| 4900        | .950     |
| 5000        | .940     |
| 5100        | .925     |
| 5200        | .935     |
| 5300        | .950     |
| 5400        | .960     |
| 5500        | .965     |
| 5600        | .970     |
| 5700        | .980     |
| 5800        | .985     |
| 5900        | .990     |
| 6000        | .985     |
| 6100        | .975     |

TABLE VII (Continued)

| $\lambda^*$ | $\gamma$ |
|-------------|----------|
| 6200        | .980     |
| 6300        | .977     |
| 6400        | .972     |
| 6500        | .940     |
| 6600        | .995     |
| 6700        | .990     |
| 6800        | .997     |
| 6900        | .997     |
| 7000        | .992     |
| 7100        | .992     |
| 7200        | .992     |
| 7300        | .992     |
| 7400        | .992     |
| 7500        | .990     |

\*The lower limit of the 100-Å interval is tabulated as  $\lambda$ .

TABLE VIII

## BLANKETING COEFFICIENTS FOR PROCYON

| $\lambda^*$ | $\gamma$ |
|-------------|----------|
| 3025        | .643     |
| 3050        | .673     |
| 3075        | .710     |
| 3100        | .721     |
| 3125        | .711     |
| 3150        | .723     |
| 3175        | .689     |
| 3200        | .733     |
| 3225        | .674     |
| 3250        | .792     |
| 3275        | .799     |
| 3300        | .799     |
| 3325        | .827     |
| 3350        | .775     |
| 3375        | .805     |
| 3400        | .808     |
| 3425        | .797     |
| 3450        | .776     |
| 3475        | .738     |
| 3500        | .775     |

TABLE VIII (Continued)

| $\lambda^*$ | $\gamma$ |
|-------------|----------|
| 3525        | .796     |
| 3550        | .761     |
| 3575        | .722     |
| 3600        | .718     |
| 3625        | .737     |
| 3650        | .805     |
| 3675        | .725     |
| 3700        | .675     |
| 3725        | .620     |
| 3750        | .638     |
| 3775        | .676     |
| 3800        | .748     |
| 3825        | .578     |
| 3850        | .785     |
| 3875        | .651     |
| 3900        | .780     |
| 3925        | .552     |
| 3950        | .615     |
| 3975        | .819     |
| 4000        | .762     |
| 4025        | .826     |
| 4050        | .841     |
| 4075        | .832     |

\*The lower limit of the 25- $\overset{\circ}{\text{A}}$  interval is tabulated as  $\lambda$ .

Table IX gives the calculated values of the U-B and B-V colors using the methods of Matthew and Sandage and of Matsushima and Hall. The values of the colors when line blanketing is considered are closer to observed values than in the blanketing-free case, but a discrepancy still exists between the theoretical and observed colors. An attempt will be made to reduce these differences using recently measured (Myrick, 1970) line blanketing effects for Theta Ursae Majoris.

TABLE IX

THEORETICAL COLORS WITH BLANKETING FROM GAMMA SERPENTIS AND PROCYON

| Effective<br>Temperature ( $^{\circ}$ K) | log g | U-B                 |                    | B-V                 |                    |
|--|-------|---------------------|--------------------|---------------------|--------------------|
|  |       | Matthews<br>Sandage | Matsushima<br>Hall | Matthews<br>Sandage | Matsushima<br>Hall |
| 6650                                     | 3.8   | -0.147              | -0.158             | 0.388               | 0.387              |
|  | 4.0   | -0.171              | -0.182             | 0.379               | 0.378              |
|  | 4.2   | -0.188              | -0.199             | 0.384               | 0.383              |
|  | 4.4   | -0.193              | -0.203             | 0.380               | 0.379              |
| 6500                                     | 3.8   | -0.154              | -0.165             | 0.326               | 0.327              |
|  | 4.0   | -0.169              | -0.180             | 0.399               | 0.397              |
|  | 4.2   | -0.201              | -0.211             | 0.406               | 0.404              |
|  | 4.4   | -0.207              | -0.216             | 0.401               | 0.399              |
| 6350                                     | 3.8   | -0.161              | -0.172             | 0.419               | 0.416              |
|  | 4.0   | -0.135              | -0.189             | 0.421               | 0.418              |
|  | 4.2   | -0.193              | -0.203             | 0.423               | 0.420              |
|  | 4.4   | -0.176              | -0.186             | 0.421               | 0.418              |
| 6200                                     | 3.8   | -0.145              | -0.157             | 0.440               | 0.437              |
|  | 4.0   | -0.144              | -0.156             | 0.436               | 0.432              |
|  | 4.2   | -0.175              | -0.185             | 0.433               | 0.430              |
|  | 4.4   | -0.199              | -0.210             | 0.443               | 0.439              |



The blanketing coefficient is defined according to the equation

$$Y = \int_{\lambda - \frac{\Delta\lambda}{2}}^{\lambda + \frac{\Delta\lambda}{2}} \frac{F_{\lambda} d\lambda}{F_c d\lambda}, \quad (3-9)$$

where  $F_{\lambda}$  is the observed flux at some wavelength  $\lambda$ ,

$F_c$  is the corresponding continuum flux,

$\Delta\lambda$  is an arbitrary interval.

The blanketing coefficient is a measure of the fraction of the continuum flux which is emitted in the  $\Delta\lambda$  band pass. The blanketing coefficient is determined by integrating Equation (3-9) or it can be determined from observational measurements.

The theoretical UBV colors, considering line blanketing, were computed again using the appropriate blanketing coefficients of  $\theta$  Ursae Majoris over twenty-five angstrom intervals. The method of calculation of the UBV colors considering line blanketing is accomplished by multiplying  $F(\lambda) S(\lambda)$  for each twenty-five angstrom interval by the appropriate blanketing coefficient for the wavelength interval and summing the products over the entire wavelength for the desired color computed. Using this method to calculate the UBV colors, Equations (3-5) and (3-6) will become

$$u-b = 2.5 \log \frac{\int_0^{\infty} Y_{S_b}(\lambda) F(\lambda) d\lambda}{\int_0^{\infty} Y_{S_v}(\lambda) F(\lambda) d\lambda}, \quad (3-10)$$

$$b-v = 2.5 \log \frac{\int_0^{\infty} Y_{S_u}(\lambda) F(\lambda) d\lambda}{\int_0^{\infty} Y_{S_b}(\lambda) F(\lambda) d\lambda}. \quad (3-11)$$

The blanketing coefficients determined by Myrick (1970) for  $\theta$  Ursae Majoris included the wavelengths from 3920 to 6610 angstroms. In order

to employ appropriate blanketing coefficients between 3000 to 3920 angstroms and 6610 and 7200 angstroms, two similar stars with known blanketing coefficients were used. In the region of 3000 to 3920 angstroms an extrapolation was made using the blanketing coefficients of the star Procyon (Talbert and Edmonds, 1966). Extrapolation gave the same values for the blanketing coefficients for the two stars. In the region between 6600 and 7200 angstroms, an extrapolation was made using the blanketing coefficients of the star Gamma Serpentis (Kegel, 1962). The extrapolation found was

$$\gamma(\theta \text{ Ursae Majoris}) = 0.986 \gamma(\text{Gamma Serpentis}). \quad (3-11)$$

Figure 3 illustrates the difference between the theoretical flux distribution of a solar-type model star with and without line blanketing. Tables VII and VIII give the blanketing coefficients used in the extrapolations while Table X lists the blanketing coefficients used for Theta Ursae Majoris.

The intensitometer tracings used to determine the blanketing coefficients for  $\theta$  Ursae Majoris include those used for the study of the hydrogen lines described in Chapter IV.

The computed values of the UBV colors for  $\theta$  Ursae Majoris, using the absorption coefficients for  $\theta$  Ursae Majoris, gave values that are in good agreement with the observed values of the B-V colors using three-, five-, or eight-color photometry systems. The value of B-V, for the model atmosphere with effective temperature of 6200  $^{\circ}$ K and having  $\log g = 3.8$  or 4.0, is 0.46, which is the observed value given by the Lunar and Planetary Laboratory of the University of Arizona. Table XI lists the values of the U-B and B-V colors calculated by the Matthews-Sandage and

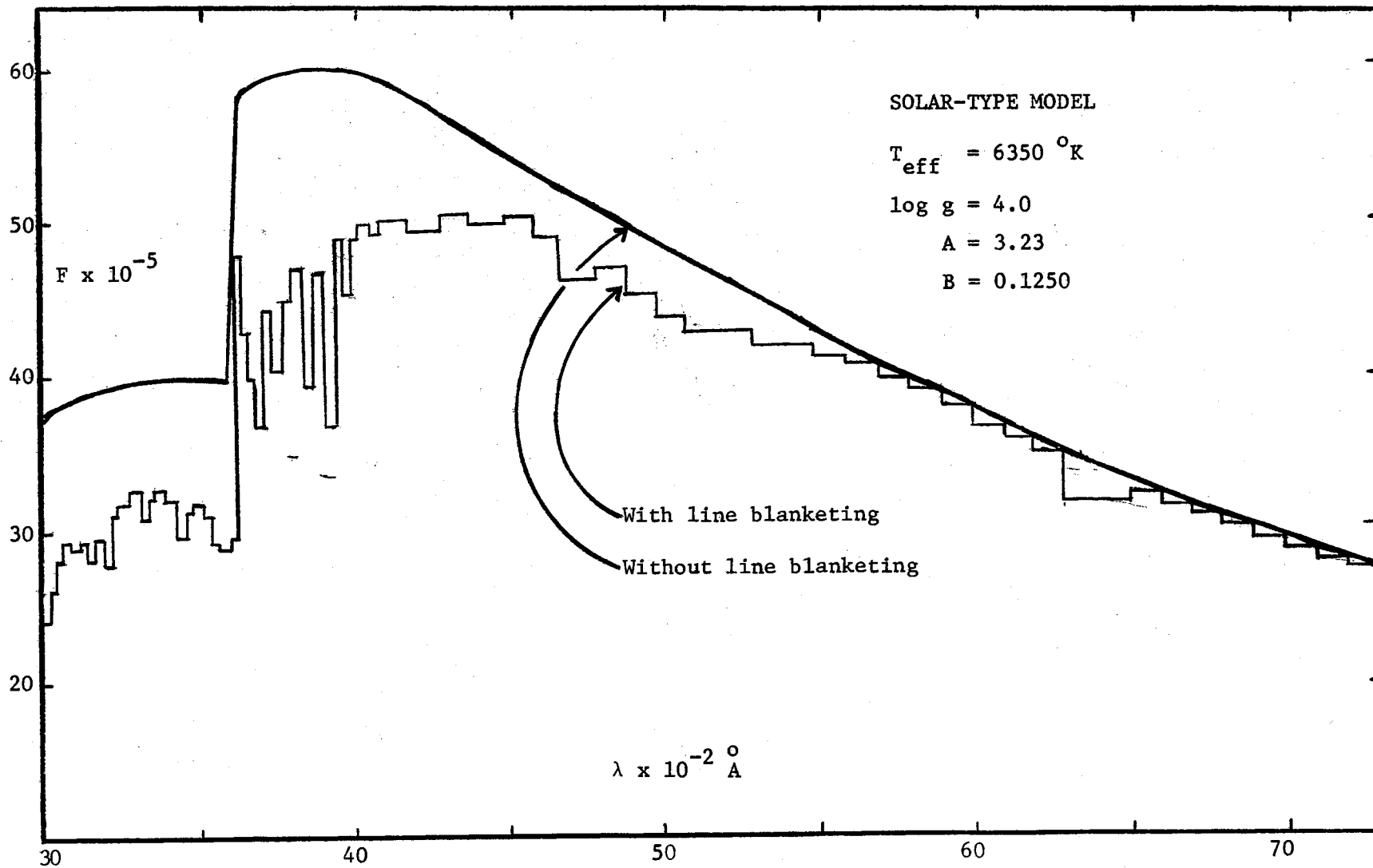


Figure 3. Theoretical Flux Distribution With Line Blanketing

TABLE X  
 BLANKETING COEFFICIENTS FOR  $\theta$  URSAE MAJORIS ( $25\text{-}\overset{\circ}{\text{A}}$  INTERVALS)

| $\lambda^*$ | $\gamma$ | $\lambda^*$ | $\gamma$ |
|-------------|----------|-------------|----------|
| 3025        | 0.643    | 4150        | 0.842    |
| 3050        | 0.673    | 4175        | 0.784    |
| 3075        | 0.710    | 4200        | 0.852    |
| 3100        | 0.721    | 4225        | 0.775    |
| 3125        | 0.711    | 4250        | 0.874    |
| 3150        | 0.723    | 4275        | 0.855    |
| 3175        | 0.689    | 4300        | 0.757    |
| 3200        | 0.733    | 4325        | 0.822    |
| 3225        | 0.674    | 4350        | 0.778    |
| 3250        | 0.792    | 4375        | 0.894    |
| 3275        | 0.799    | 4400        | 0.847    |
| 3300        | 0.799    | 4425        | 0.886    |
| 3325        | 0.827    | 4450        | 0.843    |
| 3350        | 0.775    | 4475        | 0.898    |
| 3375        | 0.805    | 4500        | 0.896    |
| 3400        | 0.808    | 4525        | 0.835    |
| 3425        | 0.797    | 4550        | 0.845    |
| 3450        | 0.776    | 4575        | 0.889    |
| 3475        | 0.738    | 4600        | 0.904    |
| 3500        | 0.775    | 4625        | 0.941    |
| 3525        | 0.796    | 4650        | 0.910    |
| 3550        | 0.761    | 4675        | 0.920    |
| 3575        | 0.722    | 4700        | 0.904    |
| 3600        | 0.718    | 4725        | 0.933    |
| 3625        | 0.737    | 4750        | 0.926    |
| 3650        | 0.805    | 4775        | 0.925    |
| 3675        | 0.725    | 4800        | 0.929    |
| 3700        | 0.675    | 4825        | 0.895    |
| 3725        | 0.620    | 4850        | 0.795    |
| 3750        | 0.638    | 4875        | 0.802    |
| 3775        | 0.676    | 4900        | 0.902    |
| 3800        | 0.748    | 4925        | 0.856    |
| 3825        | 0.578    | 4950        | 0.922    |
| 3850        | 0.785    | 4975        | 0.922    |
| 3875        | 0.651    | 5000        | 0.894    |
| 3900        | 0.780    | 5025        | 0.889    |
| 3925        | 0.572    | 5050        | 0.914    |
| 3950        | 0.638    | 5075        | 0.909    |
| 3975        | 0.489    | 5100        | 0.929    |
| 4000        | 0.776    | 5125        | 0.906    |
| 4025        | 0.829    | 5150        | 0.916    |
| 4050        | 0.803    | 5175        | 0.090    |
| 4075        | 0.774    | 5200        | 0.903    |
| 4100        | 0.684    | 5225        | 0.915    |
| 4125        | 0.826    | 5275        | 0.903    |
| 5300        | 0.942    | 6250        | 0.939    |

TABLE X (Concluded)

| $\lambda^*$ | $\gamma$ | $\lambda^*$ | $\gamma$ |
|-------------|----------|-------------|----------|
| 5325        | 0.914    | 6275        | 0.932    |
| 5350        | 0.954    | 6300        | 0.943    |
| 5375        | 0.928    | 6325        | 0.974    |
| 5400        | 0.917    | 6350        | 0.968    |
| 5425        | 0.928    | 6375        | 0.969    |
| 5450        | 0.950    | 6400        | 0.964    |
| 5475        | 0.924    | 6425        | 0.972    |
| 5500        | 0.908    | 6450        | 0.959    |
| 5525        | 0.931    | 6475        | 0.960    |
| 5550        | 0.952    | 6500        | 0.953    |
| 5575        | 0.950    | 6525        | 0.979    |
| 5600        | 0.926    | 6550        | 0.908    |
| 5625        | 0.951    | 6575        | 0.945    |
| 5650        | 0.943    | 6600        | 0.973    |
| 5675        | 0.961    | 6625        | 0.982    |
| 5700        | 0.942    | 6650        | 0.982    |
| 5725        | 0.960    | 6675        | 0.982    |
| 5750        | 0.950    | 6700        | 0.977    |
| 5775        | 0.946    | 6725        | 0.977    |
| 5800        | 0.967    | 6750        | 0.977    |
| 5825        | 0.988    | 6775        | 0.977    |
| 5850        | 0.968    | 6800        | 0.984    |
| 5875        | 0.988    | 6825        | 0.098    |
| 5900        | 0.950    | 6850        | 0.984    |
| 5925        | 0.703    | 6875        | 0.984    |
| 5950        | 0.964    | 6900        | 0.984    |
| 5975        | 0.975    | 6925        | 0.984    |
| 6000        | 0.976    | 6950        | 0.984    |
| 6025        | 0.960    | 6975        | 0.984    |
| 6050        | 0.972    | 7000        | 0.979    |
| 6075        | 0.971    | 7025        | 0.979    |
| 6100        | 0.972    | 7050        | 0.979    |
| 6125        | 0.948    | 7075        | 0.979    |
| 6150        | 0.961    | 7075        | 0.979    |
| 6175        | 0.954    | 7100        | 0.979    |
| 6200        | 0.970    | 7125        | 0.979    |
| 6225        | 0.964    | 7150        | 0.979    |
|             |          | 7175        | 0.979    |
|             |          | 7200        | 0.979    |

\*The lower limit of the 25- $\overset{\circ}{\text{A}}$  interval is tabulated as  $\lambda$ .

TABLE XI  
THEORETICAL COLORS WITH BLANKETING FROM  $\theta$  URSAE MAJORIS

| Effective<br>Temperature ( $^{\circ}$ K) | Log g | U-B                 | U-B                | B-V                 | B-V                |
|--|-------|---------------------|--------------------|---------------------|--------------------|
|  |       | Matthews<br>Sandage | Matsushima<br>Hall | Matthews<br>Sandage | Matsushima<br>Hall |
| 6650                                     | 3.8   | -0.201              | -0.211             | 0.41                | 0.41               |
|  | 4.0   | -0.230              | -0.259             | 0.42                | 0.41               |
|  | 4.2   | -0.191              | -0.221             | 0.36                | 0.36               |
|  | 4.4   | -0.231              | -0.260             | 0.39                | 0.39               |
| 6500                                     | 3.8   | -0.194              | -0.204             | 0.40                | 0.40               |
|  | 4.0   | -0.144              | -0.202             | 0.42                | 0.42               |
|  | 4.2   | -0.224              | -0.23              | 0.43                | 0.42               |
|  | 4.4   | -0.225              | -0.244             | 0.40                | 0.40               |
| 6350                                     | 3.8   | -0.181              | -0.193             | 0.41                | 0.41               |
|  | 4.0   | -0.200              | -0.210             | 0.42                | 0.41               |
|  | 4.2   | -0.216              | -0.226             | 0.42                | 0.42               |
|  | 4.4   | -0.195              | -0.205             | 0.45                | 0.44               |
| 6200                                     | 3.8   | -0.169              | -0.180             | 0.46                | 0.46               |
|  | 4.0   | -0.167              | -0.178             | 0.46                | 0.46               |
|  | 4.2   | -0.201              | -0.211             | 0.44                | 0.44               |
|  | 4.4   | -0.223              | -0.233             | 0.44                | 0.43               |

Matsushima-Hall methods. The observed values of U-B and B-V are 0.06 and 0.46 respectively. Results will be discussed in detail in the Chapter V.

## CHAPTER IV

### HYDROGEN LINE PROFILES

#### Stellar Absorption Lines

The physical processes of line formation assume two extreme points of view. One method assumes that a unique temperature completely determines the emission and absorption processes in a given volume element and Kirchhoff's law holds. This condition is called local thermodynamic equilibrium. It is referred to as absorption and the radiation from the center of a strong line will correspond to the temperature of the uppermost stratum. The second method assumes the atoms are not in temperature equilibrium with the radiation field, but simply scatter quanta reaching them from greater depths. A particular light quantum may be absorbed and re-emitted many times on its way through the atmosphere, and since it may be thrown either backward, forward, or sideways, its chance of reaching the surface is small. A line formed according to this mechanism of scattering (also labeled monochromatic radiative equilibrium) will have a black center unless it is quite weak.

There is a tendency for resonance lines to favor the scattering mechanism and high level subordinate lines to lean toward the local thermodynamic mechanism. In the hydrogen spectrum the Lyman alpha line tends to follow the scattering mechanism, whereas the Balmer lines, and more particularly the Paschen and Brackett lines, will follow the local thermodynamic equilibrium scheme.



### Formulation of the Absorption Line Program

This investigation assumes the absorption lines are formed in local thermodynamic equilibrium and the source function is the Planck function. This assumption is more valid for lines formed by absorption, than for those formed by scattering.

The formation of the equation specifying the line depth in flux is given by Gussman (1963). The line depth is given as

$$R(\Delta\lambda) = \frac{F_{\lambda}(0) - F_{\Delta\lambda}(0)}{F_{\lambda}(0)}, \quad (4-1)$$

where  $F_{\lambda}(0)$  = the emergent continuum flux,

$F_{\Delta\lambda}(0)$  = the emergent flux in the line at the point  $\Delta\lambda$  from the line center,

and the quantity  $F_{\lambda}(0)$  is obtained from the model atmosphere computations. It is practical to use a wavelength region of 100 or 200 Å in the computation of the line depth because the continuum intensity is not a strong variable with wavelength throughout the visible region, except near absorption discontinuities. In order to calculate the line depth the quantity  $F_{\Delta\lambda}(0)$  must be determined.

A gradient method which was modified by Evans (1966) was used in calculating the line depth. This method gives the line depth as

$$R(\Delta\lambda) = \int_{-\infty}^{\infty} \frac{dB_{\lambda}}{dx} [E_3(\tau_{\lambda}) - E_3(\tau_{\lambda} + \tau_{\ell})] \frac{2}{F_{\lambda}(0)} dx, \quad (4-2)$$

where  $\tau_{\ell}(x, \Delta\lambda)$  = the optical depth in the line and it is given by

$$\tau_{\ell}(x, \Delta\lambda) = \int_{-\infty}^x \frac{\kappa_{\ell}}{\kappa_0} \left[ \frac{\tau_0}{\text{Mod}} \right] dx, \quad (4-3)$$

$\kappa_{\ell}(x, \Delta\lambda)$  = the line absorption coefficient per hydrogen particle,

$$B_{\lambda} = \frac{2hc^2}{\lambda^5} \left[ \frac{1}{e^{hc/\lambda\kappa\tau} - 1} \right], \quad (4-4)$$

$$\frac{dB_{\lambda}}{dx} = \left( \frac{B_{\lambda}(x + \Delta x) - B_{\lambda}(x - \Delta x)}{2\Delta x} \right), \quad (4-5)$$

and  $\kappa_0(x)$  and  $\tau_0(x)$  are obtained from the model atmosphere calculations.

If  $\tau_{\ell} \ll \tau_{\lambda}$ , a Taylor expansion is used for  $E_3$  resulting in

$$E_3(\tau_{\lambda}) - E_3(\tau_{\lambda} + \tau_{\ell}) = \tau_{\ell} E_2(\tau_{\lambda}); \quad (4-6)$$

$\tau_{\lambda} \approx \tau_{\ell}$ , the straight difference is computed;

$\tau_{\lambda} \ll \tau_{\ell}$ , the approximation is made

$$E_3(\tau_{\lambda}) - E_3(\tau_{\lambda} + \tau_{\ell}) = E_3(\tau_{\lambda}). \quad (4-7)$$

The line absorption coefficient is computed as a function of  $\Delta\lambda$  and  $x$  so that the integrand of the optical depth in the line [Equation (4-3)] can be formed.

The line depth integration is performed by a summation over the desired integration range. The integrand decreases rapidly in the outer and deeper layers making this method quite accurate. The mean depth of formation is found by multiplying the line depth integrand by  $x$ , summing over the integration range, and dividing by the line depth.

The problem of calculation of the line depth reduces to the specification of the absorption coefficient in the line and its variation with  $\Delta\lambda$ .

### Hydrogen Line Absorption Coefficient

The core of the Balmer lines are formed above  $x = -3.0$  where deviations from local thermodynamic equilibrium are important. Since this study is concerned with the wings of the Balmer lines, Doppler broadening and radiation damping are neglected because they are negligible when compared to linear Stark broadening.

A complete formulation, computer program, derivations, and theory of the hydrogen line absorption coefficient is not given in this study due to the length of a complete discussion of each of the programs. A detailed description of the hydrogen line absorption coefficient is given by Evans (1966). This study will summarize some of the most important formulations, equations, assumptions, the computer program, and select a formulation that will be used to compute the  $H\alpha$ ,  $H\beta$ ,  $H\gamma$ , and  $H\delta$  lines.

The line absorption coefficient per hydrogen particle may be written as (Aller 1963a).

$$\kappa_l(x, \Delta\lambda) = [1 - 10^{x\lambda^\theta}] \frac{N}{N_H} \frac{\sqrt{\pi} e^2}{mc^2} \frac{\lambda^2}{\Delta\lambda_D} f\phi_{\Delta\lambda}, \quad (4-8)$$

where  $(1 - 10^{-x\lambda^\theta})$  = the correction for simulated emission,

$N$  = the number of absorbing particles in the lower level of the transition of interest per unit volume,

$N_H$  = the number of hydrogen particles per unit volume,

$\Delta\lambda_D$  = the Doppler width =  $\frac{\lambda}{c} \sqrt{E_{th}^2 + E_t^2}$ ,

$E_{th}$  = the most probable thermal velocity,

$$= 2RT/\mu_1 = 83.83/\mu_1 \theta,$$

- $E_i$  = the most probable microturbulent velocity,  
 $f$  = the oscillator strength,  
 $\phi_{\Delta\lambda}$  = the broadening function.

The number of absorbing particles per unit volume,  $N$ , is obtained from a system of Saha and Boltzman equations and may be written as

$$N = \left( \frac{n_{p,s}}{n_q} \right) \left( \frac{n_p}{\sum n_q} \right) N_i \quad (4-9)$$

where  $n_{p,s}$  = the number density of particles in the  $p$ -th ionization stage and the  $s$ -th excitation stage,

$$\begin{aligned} \sum n_q &= \text{the summation over all ionization stages,} \\ &= N_i. \end{aligned}$$

Equation (4-8) is simplified by Evans (1966) by letting  $r$  be the most abundant ionization state for the temperature and pressure of interest,  $r-1$  the ionization stage below  $r$ ,  $r+1$  the ionization stage above  $r$ ,  $U_r$  the partition function of the  $r$ -th stage of ionization, and  $q_{p,s}$  the statistical weight of the lower level. Equation (4-8) may be written as

$$\begin{aligned} \kappa_\ell &= \frac{\epsilon_i \sqrt{\pi} e^2}{mc^2} \frac{\lambda^2}{\Delta\lambda_D} \frac{g_{p,s}}{U} [10^{\Delta\chi\theta} + h(9.0301 - 2.5 \log \theta - \log P_e)] \\ & \quad [1 - 10^{-\chi_\lambda \theta}] [f\phi], \end{aligned} \quad (4-10)$$

$$h = -1 \text{ if } p = r-1,$$

$$h = 0 \text{ if } p = r,$$

$$h = +1 \text{ if } p = r+1,$$

$\chi_{r,s}$  = the excitation potential in eV,

$$U = U_r \left[ \frac{n_{r-1}}{n_r} + 1 + \frac{n_{r+1}}{n_r} \right].$$

$$\log\left(\frac{n_{p,s}^U}{n_r}\right) = \log g_{p,s} + \Delta\chi\theta + h [9.0801 - 2.5 \log \theta - \log P_e]. \quad (4-11)$$

#### Griem Formulation

The Griem, Kolb, and Shen (1959) formulation is used here for the electron broadening. This formulation utilized the impact theory of Baranger (1958) for electron broadening along with a modification of the Holtsmark ion field distribution including Debye shielding, ion-ion correlations, and non-adiabatic transitions. The improvement in the ion field distribution effects only the line core and is unimportant for the wings. This study used the Griem, Kolb, and Shen formulation of the absorption coefficient of hydrogen to compute the Balmer lines  $H\alpha$ ,  $H\beta$ ,  $H\gamma$ , and  $H\delta$ . Griem (1962) made an additional modification for quasi-static treatment of the electron fields in the far wings. This latter modification is the one most used by astrophysicists.

#### Computer Program for the Balmer Lines

A detailed description of the hydrogen line program is given by Evans (1966). Some modifications were made in order for the program to compute more lines and to compute more points in order to improve the accuracy of the hydrogen lines. The model atmosphere program described in Chapter II generated output needed in the hydrogen line programs. At twenty-seven different depths in the atmosphere, the output on punched data cards included the mean molecular weight and logarithms of the electron pressure, the gas pressure, the density, and the ratio of the absorption coefficient,  $K_0$ , to the electron pressure.

The wings of the Balmer lines,  $H\alpha$ ,  $H\beta$ ,  $H\gamma$ , and  $H\delta$  were computed for

each of our 16 atmospheric models. These data are tabulated in Table XII where the line depth in terms of the continuum as unity is listed as a function of  $\Delta\lambda$ , distance from the line center, beginning with one angstrom and extending to nineteen angstroms in intervals of two angstroms.

### Spectrograms and Tracings

The spectrograms used in this study were taken at the Cassegrain focus of the seventy-two inch telescope of the Dominion Astrophysical Observatory by Dr. K. O. Wright.

The dispersion of the different spectrographs ranged from 7.5 A/mm, for the second order spectra in the range  $\lambda\lambda 4800-6750$  for the Littrow spectrograph with a Wood grating (15,000 lines/inch), 4.5 A/mm for the third order spectra in the range  $\lambda\lambda 3750-4500$ , 3.2 A/mm in the second order for the Baush and Lomb grating No. 496 (30,000 lines/inch), and for the three-prism spectrograph the variation was from 5 A/mm to 15 A/mm over the entire wavelength range under consideration.

The intensitometer and microphotometer tracings were done by Dr. L. W. Schroeder at Victoria, Canada. The magnification of the tracings is 200. Data concerning the wavelength range, Victoria plate number, microphotometer and intensitometer tracings numbers and spectrographs, used in this investigation can be obtained from the Physics Department of Oklahoma State University at Stillwater, Oklahoma.

### Comparison With Observations

Measurements were made of all the Balmer line profiles represented by the intensitometer tracings described in the previous section. The

TABLE XII

## COMPUTED VALUES FOR HYDROGEN LINE PROFILES

|                 |                   |         |         |         |         |         |         |         |         |         |         |         |   |                |  |
|-----------------|-------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---|----------------|--|
| $H_{\delta}$    | $\lambda 4101.74$ |         |         |         |         |         |         |         |         |         |         | F4 V    | $T_{\text{eff}} = 6650^{\circ}\text{K}$ | $\log g = 3.8$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |  |
| Line Depth      | 0.48950           | 0.28827 | 0.19784 | 0.14368 | 0.10880 | 0.08442 | 0.06652 | 0.05313 | 0.04291 | 0.03498 | 0.02876 | 0.02382 |   |                |  |
| $H_{\gamma}$    | $\lambda 4340.47$ |         |         |         |         |         |         |         |         |         |         | F4 V    | $T_{\text{eff}} = 6650^{\circ}\text{K}$ | $\log g = 3.8$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |  |
| Line Depth      | 0.46800           | 0.27373 | 0.18764 | 0.13707 | 0.10416 | 0.08153 | 0.06498 | 0.05251 | 0.04295 | 0.03550 | 0.02961 | 0.02489 |   |                |  |
| $H_{\beta}$     | $\lambda 4861.33$ |         |         |         |         |         |         |         |         |         |         | F4 V    | $T_{\text{eff}} = 6650^{\circ}\text{K}$ | $\log g = 3.8$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |  |
| Line Depth      | 0.42776           | 0.24557 | 0.16678 | 0.12218 | 0.09294 | 0.07274 | 0.05831 | 0.04757 | 0.03929 | 0.03280 | 0.02764 | 0.02349 |   |                |  |
| $H_{\alpha}$    | $\lambda 6562.82$ |         |         |         |         |         |         |         |         |         |         | F4 V    | $T_{\text{eff}} = 6650^{\circ}\text{K}$ | $\log g = 3.8$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |  |
| Line Depth      | 0.34463           | 0.18807 | 0.12301 | 0.08696 | 0.06464 | 0.04965 | 0.03903 | 0.03129 | 0.02552 | 0.02111 | 0.01768 | 0.01496 |   |                |  |

TABLE XII (Continued)

|                 |                   |         |         |         |         |         |         |         |         |         |         |         |   |                |  |
|-----------------|-------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---|----------------|--|
| $H_{\delta}$    | $\lambda 4101.74$ |         |         |         |         |         |         |         |         |         |         | F4 V    | $T_{\text{eff}} = 6650^{\circ}\text{K}$ | $\log g = 4.0$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |  |
| Line Depth      | 0.48895           | 0.28760 | 0.19732 | 0.14332 | 0.10864 | 0.08445 | 0.06668 | 0.05336 | 0.04318 | 0.03527 | 0.02905 | 0.02413 |   |                |  |
| $H_{\gamma}$    | $\lambda 4340.47$ |         |         |         |         |         |         |         |         |         |         | F4 V    | $T_{\text{eff}} = 6650^{\circ}\text{K}$ | $\log g = 4.0$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |  |
| Line Depth      | 0.46771           | 0.27339 | 0.18738 | 0.13696 | 0.10415 | 0.08165 | 0.06520 | 0.05278 | 0.04326 | 0.03581 | 0.02992 | 0.02520 |   |                |  |
| $H_{\beta}$     | $\lambda 4861.33$ |         |         |         |         |         |         |         |         |         |         | F4 V    | $T_{\text{eff}} = 6650^{\circ}\text{K}$ | $\log g = 4.0$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |  |
| Line Depth      | 0.42876           | 0.24568 | 0.16692 | 0.12239 | 0.09320 | 0.07301 | 0.05860 | 0.04778 | 0.03962 | 0.03313 | 0.02798 | 0.02381 |   |                |  |
| $H_{\alpha}$    | $\lambda 6562.82$ |         |         |         |         |         |         |         |         |         |         | F4 V    | $T_{\text{eff}} = 6650^{\circ}\text{K}$ | $\log g = 4.0$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |  |
| Line Depth      | 0.34611           | 0.18949 | 0.12426 | 0.08806 | 0.06563 | 0.05054 | 0.03982 | 0.03199 | 0.02614 | 0.02167 | 0.01818 | 0.01541 |   |                |  |



TABLE XII (Continued)

|                 |         |                   |         |         |         |         |         |   |         |         |                |         |
|-----------------|---------|-------------------|---------|---------|---------|---------|---------|---|---------|---------|----------------|---------|
| $H_{\delta}$    |         | $\lambda 4104.74$ |         |         |         | F4 V    |         | $T_{\text{eff}} = 6650^{\circ}\text{K}$ |         |         | $\log g = 4.2$ |         |
| $\Delta\lambda$ | 1.0     | 3.0               | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.48847 | 0.28697           | 0.19679 | 0.14292 | 0.10840 | 0.08439 | 0.06673 | 0.05348                                 | 0.04335 | 0.03547 | 0.02926        | 0.02433 |
| $H_{\gamma}$    |         | $\lambda 4104.74$ |         |         |         | F4 V    |         | $T_{\text{eff}} = 6650^{\circ}\text{K}$ |         |         | $\log g = 4.2$ |         |
| $\Delta\lambda$ | 1.0     | 3.0               | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.46747 | 0.27309           | 0.18714 | 0.13684 | 0.10411 | 0.08173 | 0.06537 | 0.05301                                 | 0.04350 | 0.03608 | 0.03019        | 0.02546 |
| $H_{\beta}$     |         | $\lambda 4340.47$ |         |         |         | F4 V    |         | $T_{\text{eff}} = 6650^{\circ}\text{K}$ |         |         | $\log g = 4.2$ |         |
| $\Delta\lambda$ | 1.0     | 3.0               | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.42795 | 0.24579           | 0.16706 | 0.12257 | 0.09343 | 0.07326 | 0.05888 | 0.04817                                 | 0.03993 | 0.03344 | 0.02826        | 0.02409 |
| $H_{\alpha}$    |         | $\lambda 4861.33$ |         |         |         | F4 V    |         | $T_{\text{eff}} = 6650^{\circ}\text{K}$ |         |         | $\log g = 4.2$ |         |
| $\Delta\lambda$ | 1.0     | 3.0               | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.34755 | 0.19083           | 0.12543 | 0.08907 | 0.06651 | 0.05132 | 0.04050 | 0.03260                                 | 0.02669 | 0.02216 | 0.01852        | 0.01581 |

TABLE XII (Continued)

|                 |                   |         |         |         |         |         |         |         |         |         |         |         |   |                |
|-----------------|-------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---|----------------|
| $H_{\delta}$    | $\lambda 4104.74$ |         |         |         |         |         |         |         |         |         |         | F4 V    | $T_{\text{eff}} = 6650^{\circ}\text{K}$ | $\log g = 4.4$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.48806           | 0.28643 | 0.19631 | 0.15254 | 0.10816 | 0.08430 | 0.06674 | 0.05356 | 0.04347 | 0.03562 | 0.02943 | 0.02450 |   |                |
| $H_{\gamma}$    | $\lambda 4340.47$ |         |         |         |         |         |         |         |         |         |         | F4 V    | $T_{\text{eff}} = 6650^{\circ}\text{K}$ | $\log g = 4.4$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.46727           | 0.27280 | 0.18689 | 0.13667 | 0.10400 | 0.08172 | 0.06544 | 0.05313 | 0.04366 | 0.03624 | 0.03036 | 0.02563 |   |                |
| $H_{\beta}$     | $\lambda 4861.33$ |         |         |         |         |         |         |         |         |         |         | F4 V    | $T_{\text{eff}} = 6650^{\circ}\text{K}$ | $\log g = 4.4$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.42807           | 0.24591 | 0.16719 | 0.12273 | 0.09361 | 0.07344 | 0.05908 | 0.04839 | 0.04016 | 0.03368 | 0.02850 | 0.02431 |   |                |
| $H_{\alpha}$    | $\lambda 6562.82$ |         |         |         |         |         |         |         |         |         |         | F4 V    | $T_{\text{eff}} = 6650^{\circ}\text{K}$ | $\log g = 4.4$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.34895           | 0.19214 | 0.12654 | 0.09003 | 0.06734 | 0.05204 | 0.04114 | 0.03317 | 0.02719 | 0.02262 | 0.01903 | 0.01619 |   |                |

TABLE XII (Continued)

|                 |                   |         |         |         |         |         |         |         |         |         |         |         |   |                |
|-----------------|-------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---|----------------|
| $H_{\delta}$    | $\lambda 4104.74$ |         |         |         |         |         |         |         |         |         |         | F5 V    | $T_{\text{eff}} = 6500^{\circ}\text{K}$ | $\log g = 3.8$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.46110           | 0.25855 | 0.17294 | 0.12220 | 0.09104 | 0.06944 | 0.05396 | 0.04258 | 0.03402 | 0.02749 | 0.02241 | 0.01844 |   |                |
| $H_{\gamma}$    | $\lambda 4340.47$ |         |         |         |         |         |         |         |         |         |         | F5 V    | $T_{\text{eff}} = 6500^{\circ}\text{K}$ | $\log g = 3.8$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.44040           | 0.24527 | 0.16359 | 0.11657 | 0.08737 | 0.06741 | 0.05300 | 0.04235 | 0.03431 | 0.02811 | 0.02327 | 0.01943 |   |                |
| $H_{\beta}$     | $\lambda 4861.33$ |         |         |         |         |         |         |         |         |         |         | F5 V    | $T_{\text{eff}} = 6500^{\circ}\text{K}$ | $\log g = 3.8$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.40186           | 0.22035 | 0.14554 | 0.10428 | 0.07786 | 0.06027 | 0.04785 | 0.03863 | 0.03162 | 0.02619 | 0.02192 | 0.01851 |   |                |
| $H_{\alpha}$    | $\lambda 6562.82$ |         |         |         |         |         |         |         |         |         |         | F5 V    | $T_{\text{eff}} = 6500^{\circ}\text{K}$ | $\log g = 3.8$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.32455           | 0.16905 | 0.10771 | 0.07478 | 0.05485 | 0.04158 | 0.03236 | 0.02577 | 0.02090 | 0.01721 | 0.01435 | 0.01209 |   |                |

TABLE XII (Continued)

|                 |                   |         |         |         |         |         |         |         |         |         |         |         |   |                |  |
|-----------------|-------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---|----------------|--|
| $H_{\delta}$    | $\lambda 4101.74$ |         |         |         |         |         |         |         |         |         |         | F5 V    | $T_{\text{eff}} = 6500^{\circ}\text{K}$ | $\log g = 4.0$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |  |
| Line Depth      | 0.46070           | 0.25800 | 0.17152 | 0.12189 | 0.09092 | 0.06947 | 0.05405 | 0.04272 | 0.03420 | 0.02767 | 0.02259 | 0.01861 |   |                |  |
| $H_{\gamma}$    | $\lambda 4340.47$ |         |         |         |         |         |         |         |         |         |         | F5 V    | $T_{\text{eff}} = 6500^{\circ}\text{K}$ | $\log g = 4.0$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |  |
| Line Depth      | 0.44021           | 0.24498 | 0.16336 | 0.11642 | 0.08733 | 0.06748 | 0.05314 | 0.04253 | 0.03450 | 0.02831 | 0.02347 | 0.01963 |   |                |  |
| $H_{\beta}$     | $\lambda 4861.33$ |         |         |         |         |         |         |         |         |         |         | F5 V    | $T_{\text{eff}} = 6500^{\circ}\text{K}$ | $\log g = 4.0$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |  |
| Line Depth      | 0.40198           | 0.22046 | 0.14565 | 0.01044 | 0.07902 | 0.06045 | 0.04806 | 0.03886 | 0.03185 | 0.02642 | 0.02214 | 0.01872 |   |                |  |
| $H_{\alpha}$    | $\lambda 6562.82$ |         |         |         |         |         |         |         |         |         |         | F5 V    | $T_{\text{eff}} = 6500^{\circ}\text{K}$ | $\log g = 4.0$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |  |
| Line Depth      | 0.32597           | 0.17031 | 0.10876 | 0.07567 | 0.05562 | 0.04224 | 0.03295 | 0.02629 | 0.02136 | 0.01762 | 0.01471 | 0.01242 |   |                |  |

TABLE XII (Continued)

|                 |                   |         |         |         |         |         |         |   |         |         |                |         |
|-----------------|-------------------|---------|---------|---------|---------|---------|---------|---|---------|---------|----------------|---------|
| $H_{\delta}$    | $\lambda 4104.74$ |         |         | F5 V    |         |         |         | $T_{\text{eff}} = 6500^{\circ}\text{K}$ |         |         | $\log g = 4.2$ |         |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.46036           | 0.25746 | 0.17106 | 0.12153 | 0.09075 | 0.06942 | 0.05410 | 0.03282                                 | 0.03432 | 0.02780 | 0.02273        | 0.01875 |
| $H_{\gamma}$    | $\lambda 4340.47$ |         |         | F5 V    |         |         |         | $T_{\text{eff}} = 6500^{\circ}\text{K}$ |         |         | $\log g = 4.2$ |         |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.44005           | 0.24471 | 0.16315 | 0.11627 | 0.08727 | 0.06753 | 0.05325 | 0.04267                                 | 0.03466 | 0.02849 | 0.02364        | 0.01979 |
| $H_{\beta}$     | $\lambda 4861.33$ |         |         | F5 V    |         |         |         | $T_{\text{eff}} = 6500^{\circ}\text{K}$ |         |         | $\log g = 4.2$ |         |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.40211           | 0.22054 | 0.14573 | 0.10454 | 0.07814 | 0.06060 | 0.04824 | 0.03907                                 | 0.03206 | 0.02663 | 0.02234        | 0.01892 |
| $H_{\alpha}$    | $\lambda 6562.82$ |         |         | F5 V    |         |         |         | $T_{\text{eff}} = 6500^{\circ}\text{K}$ |         |         | $\log g = 4.2$ |         |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.32734           | 0.17153 | 0.10976 | 0.07652 | 0.05634 | 0.04287 | 0.03349 | 0.02677                                 | 0.02179 | 0.01800 | 0.01506        | 0.01274 |

TABLE XII (Continued)

|                 |         |                   |         |         |         |         |         |   |         |         |                |         |
|-----------------|---------|-------------------|---------|---------|---------|---------|---------|---|---------|---------|----------------|---------|
| $H_{\delta}$    |         | $\lambda 4101.74$ |         |         |         | F5 V    |         | $T_{\text{eff}} = 6500^{\circ}\text{K}$ |         |         | $\log g = 4.4$ |         |
| $\Delta\lambda$ | 1.0     | 3.0               | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.46010 | 0.25704           | 0.17069 | 0.12122 | 0.09058 | 0.06936 | 0.05408 | 0.04285                                 | 0.03438 | 0.02790 | 0.02284        | 0.01886 |
| $H_{\gamma}$    |         | $\lambda 4340.47$ |         |         |         | F5 V    |         | $T_{\text{eff}} = 6500^{\circ}\text{K}$ |         |         | $\log g = 4.4$ |         |
| $\Delta\lambda$ | 1.0     | 3.0               | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.43994 | 0.24448           | 0.16295 | 0.11610 | 0.08718 | 0.06753 | 0.05330 | 0.04276                                 | 0.03477 | 0.02860 | 0.02377        | 0.01993 |
| $H_{\beta}$     |         | $\lambda 4861.33$ |         |         |         | F5 V    |         | $T_{\text{eff}} = 6500^{\circ}\text{K}$ |         |         | $\log g = 4.4$ |         |
| $\Delta\lambda$ | 1.0     | 3.0               | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.40225 | 0.22064           | 0.14581 | 0.10465 | 0.07825 | 0.06072 | 0.04839 | 0.03923                                 | 0.03223 | 0.02680 | 0.02250        | 0.01907 |
| $H_{\alpha}$    |         | $\lambda 6562.82$ |         |         |         | F5 V    |         | $T_{\text{eff}} = 6500^{\circ}\text{K}$ |         |         | $\log g = 4.4$ |         |
| $\Delta\lambda$ | 1.0     | 3.0               | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.32871 | 0.17272           | 0.11072 | 0.07730 | 0.05700 | 0.04342 | 0.03396 | 0.02718                                 | 0.02215 | 0.01832 | 0.01534        | 0.01298 |

TABLE XII (Continued)

|                 |                   |         |         |         |         |         |         |         |         |         |         |         |   |                |
|-----------------|-------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---|----------------|
| $H_{\delta}$    | $\lambda 4101.74$ |         |         |         |         |         |         |         |         |         |         | F6 V    | $T_{\text{eff}} = 6350^{\circ}\text{K}$ | $\log g = 3.8$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.43013           | 0.22928 | 0.14674 | 0.10240 | 0.07472 | 0.05597 | 0.04286 | 0.03339 | 0.02638 | 0.02109 | 0.01704 | 0.01392 |   |                |
| $H_{\gamma}$    | $\lambda 4330.47$ |         |         |         |         |         |         |         |         |         |         | F6 V    | $T_{\text{eff}} = 6350^{\circ}\text{K}$ | $\log g = 3.8$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.41062           | 0.21702 | 0.13976 | 0.00757 | 0.07193 | 0.05453 | 0.04227 | 0.03337 | 0.02675 | 0.02173 | 0.01784 | 0.01479 |   |                |
| $H_{\beta}$     | $\lambda 4861.33$ |         |         |         |         |         |         |         |         |         |         | F6 V    | $T_{\text{eff}} = 6350^{\circ}\text{K}$ | $\log g = 3.8$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.37405           | 0.10453 | 0.12505 | 0.08711 | 0.06409 | 0.04906 | 0.03846 | 0.03069 | 0.02488 | 0.02043 | 0.01698 | 0.01425 |   |                |
| $H_{\alpha}$    | $\lambda 6562.82$ |         |         |         |         |         |         |         |         |         |         | F6 V    | $T_{\text{eff}} = 6350^{\circ}\text{K}$ | $\log g = 3.8$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.39283           | 0.14995 | 0.09266 | 0.06323 | 0.04555 | 0.03406 | 0.02628 | 0.02079 | 0.01676 | 0.01372 | 0.01139 | 0.00956 |   |                |

TABLE XII (Continued)

|                 |                   |         |         |         |         |         |         |         |         |         |         |         |   |                |
|-----------------|-------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---|----------------|
| $H_{\delta}$    | $\lambda 4104.74$ |         |         |         |         |         |         |         |         |         |         | F6 V    | $T_{\text{eff}} = 6350^{\circ}\text{K}$ | $\log g = 4.0$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.42987           | 0.22882 | 0.14632 | 0.10211 | 0.07459 | 0.05592 | 0.04286 | 0.03343 | 0.02646 | 0.02118 | 0.01713 | 0.01400 |   |                |
| $H_{\gamma}$    | $\lambda 4340.47$ |         |         |         |         |         |         |         |         |         |         | F6 V    | $T_{\text{eff}} = 6350^{\circ}\text{K}$ | $\log g = 4.0$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.41052           | 0.21679 | 0.13959 | 0.09747 | 0.07196 | 0.05463 | 0.04241 | 0.03353 | 0.02692 | 0.02189 | 0.01799 | 0.01494 |   |                |
| $H_{\beta}$     | $\lambda 4861.33$ |         |         |         |         |         |         |         |         |         |         | F6 V    | $T_{\text{eff}} = 6350^{\circ}\text{K}$ | $\log g = 4.0$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.37421           | 0.19462 | 0.12512 | 0.08720 | 0.06418 | 0.04919 | 0.03862 | 0.03085 | 0.02503 | 0.02058 | 0.01712 | 0.01440 |   |                |
| $H_{\alpha}$    | $\lambda 6562.82$ |         |         |         |         |         |         |         |         |         |         | F6 V    | $T_{\text{eff}} = 6350^{\circ}\text{K}$ | $\log g = 4.0$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.30419           | 0.15109 | 0.09357 | 0.06397 | 0.04616 | 0.03458 | 0.02674 | 0.02118 | 0.01710 | 0.01402 | 0.01165 | 0.00979 |   |                |



TABLE XII (Continued)

|                 |         |                   |         |         |         |         |         |   |         |         |                |         |
|-----------------|---------|-------------------|---------|---------|---------|---------|---------|---|---------|---------|----------------|---------|
| $H_{\delta}$    |         | $\lambda 4101.74$ |         |         |         | F6 V    |         | $T_{\text{eff}} = 6350^{\circ}\text{K}$ |         |         | $\log g = 4.2$ |         |
| $\Delta\lambda$ | 1.0     | 3.0               | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.42968 | 0.22843           | 0.14597 | 0.10118 | 0.07450 | 0.05591 | 0.04290 | 0.03351                                 | 0.02655 | 0.02127 | 0.01723        | 0.01410 |
| $H_{\gamma}$    |         | $\lambda 4340.47$ |         |         |         | F6 V    |         | $T_{\text{eff}} = 6350^{\circ}\text{K}$ |         |         | $\log g = 4.2$ |         |
| $\Delta\lambda$ | 1.0     | 3.0               | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.41047 | 0.21659           | 0.13941 | 0.09732 | 0.07191 | 0.05464 | 0.04244 | 0.03359                                 | 0.02699 | 0.02196 | 0.01806        | 0.01500 |
| $H_{\beta}$     |         | $\lambda 4861.33$ |         |         |         | F6 V    |         | $T_{\text{eff}} = 6350^{\circ}\text{K}$ |         |         | $\log g = 4.2$ |         |
| $\Delta\lambda$ | 1.0     | 3.0               | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.37437 | 0.19470           | 0.12520 | 0.08728 | 0.06427 | 0.04930 | 0.02875 | 0.03101                                 | 0.02519 | 0.02074 | 0.01727        | 0.01500 |
| $H_{\alpha}$    |         | $\lambda 6562.82$ |         |         |         | F6 V    |         | $T_{\text{eff}} = 6350^{\circ}\text{K}$ |         |         | $\log g = 4.2$ |         |
| $\Delta\lambda$ | 1.0     | 3.0               | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.30553 | 0.15220           | 0.09443 | 0.06467 | 0.04674 | 0.03506 | 0.02715 | 0.02154                                 | 0.01742 | 0.01430 | 0.01190        | 0.01001 |

TABLE XII (Continued)

|                 |                   |         |         |         |         |         |         |         |         |         |         |         |   |                |  |
|-----------------|-------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---|----------------|--|
| $H_{\delta}$    | $\lambda 4104.74$ |         |         |         |         |         |         |         |         |         |         | F6 V    | $T_{\text{eff}} = 6350^{\circ}\text{K}$ | $\log g = 4.4$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |  |
| Line Depth      | 0.42954           | 0.22810 | 0.14567 | 0.10167 | 0.07441 | 0.05589 | 0.04293 | 0.03356 | 0.02660 | 0.02134 | 0.01730 | 0.01417 |   |                |  |
| $H_{\gamma}$    | $\lambda 4340.47$ |         |         |         |         |         |         |         |         |         |         | F6 V    | $T_{\text{eff}} = 6350^{\circ}\text{K}$ | $\log g = 4.4$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |  |
| Line Depth      | 0.41004           | 0.21641 | 0.13925 | 0.09721 | 0.07189 | 0.05469 | 0.04252 | 0.03369 | 0.02710 | 0.02209 | 0.01819 | 0.01513 |   |                |  |
| $H_{\beta}$     | $\lambda 4861.33$ |         |         |         |         |         |         |         |         |         |         | F6 V    | $T_{\text{eff}} = 6350^{\circ}\text{K}$ | $\log g = 4.4$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |  |
| Line Depth      | 0.37452           | 0.19478 | 0.12525 | 0.08734 | 0.06434 | 0.04940 | 0.03887 | 0.03114 | 0.02532 | 0.02086 | 0.01739 | 0.01465 |   |                |  |
| $H_{\alpha}$    | $\lambda 6562.82$ |         |         |         |         |         |         |         |         |         |         | F6 V    | $T_{\text{eff}} = 6350^{\circ}\text{K}$ | $\log g = 4.4$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |  |
| Line Depth      | 0.30684           | 0.16329 | 0.09526 | 0.06532 | 0.04727 | 0.03551 | 0.02754 | 0.02188 | 0.01772 | 0.01457 | 0.01213 | 0.01022 |   |                |  |

TABLE XII (Continued)

|                 |                   |         |         |         |         |         |         |         |         |         |         |         |  |   |  |                |  |
|-----------------|-------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--|---|--|----------------|--|
| $H_{\delta}$    | $\lambda 4104.74$ |         |         |         |         |         |         |         |         |         |         | F8 V    |  | $T_{\text{eff}} = 6200^{\circ}\text{K}$ |  | $\log g = 3.8$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |  |   |  |                |  |
| Line Depth      | 0.39713           | 0.20013 | 0.12329 | 0.08417 | 0.05990 | 0.04402 | 0.03319 | 0.02549 | 0.01989 | 0.01573 | 0.01261 | 0.01022 |  |   |  |                |  |
| $H_{\gamma}$    | $\lambda 4340.47$ |         |         |         |         |         |         |         |         |         |         | F8 V    |  | $T_{\text{eff}} = 6200^{\circ}\text{K}$ |  | $\log g = 3.8$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |  |   |  |                |  |
| Line Depth      | 0.37842           | 0.18955 | 0.11711 | 0.08035 | 0.05795 | 0.04312 | 0.03294 | 0.02569 | 0.02037 | 0.01638 | 0.01333 | 0.01098 |  |   |  |                |  |
| $H_{\beta}$     | $\lambda 4861.33$ |         |         |         |         |         |         |         |         |         |         | F8 V    |  | $T_{\text{eff}} = 6200^{\circ}\text{K}$ |  | $\log g = 3.8$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |  |   |  |                |  |
| Line Depth      | 0.34453           | 0.16900 | 0.10509 | 0.07134 | 0.05183 | 0.03908 | 0.03018 | 0.02379 | 0.01909 | 0.01555 | 0.01282 | 0.01068 |  |   |  |                |  |
| $H_{\alpha}$    | $\lambda 6562.82$ |         |         |         |         |         |         |         |         |         |         | F8 V    |  | $T_{\text{eff}} = 6200^{\circ}\text{K}$ |  | $\log g = 3.8$ |  |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |  |   |  |                |  |
| Line Depth      | 0.27936           | 0.13103 | 0.07947 | 0.05239 | 0.03701 | 0.02738 | 0.02096 | 0.01645 | 0.01317 | 0.01072 | 0.00885 | 0.00740 |  |   |  |                |  |

TABLE XII (Continued)

|                 |                   |         |         |         |         |         |         |         |         |         |         |         |   |                |
|-----------------|-------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---|----------------|
| $H_{\delta}$    | $\lambda 4101.74$ |         |         |         |         |         |         |         |         |         |         | F8 V    | $T_{\text{eff}} = 6200^{\circ}\text{K}$ | $\log g = 4.0$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.39701           | 0.19981 | 0.12297 | 0.08401 | 0.05983 | 0.04401 | 0.03321 | 0.02552 | 0.01993 | 0.01578 | 0.01267 | 0.01028 |   |                |
| $H_{\gamma}$    | $\lambda 4340.47$ |         |         |         |         |         |         |         |         |         |         | F8 V    | $T_{\text{eff}} = 6200^{\circ}\text{K}$ | $\log g = 4.0$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.37842           | 0.18937 | 0.11694 | 0.08026 | 0.05795 | 0.04316 | 0.03299 | 0.02576 | 0.02044 | 0.01644 | 0.01340 | 0.01103 |   |                |
| $H_{\beta}$     | $\lambda 4861.33$ |         |         |         |         |         |         |         |         |         |         | F8 V    | $T_{\text{eff}} = 6200^{\circ}\text{K}$ | $\log g = 4.0$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.34470           | 0.16906 | 0.10513 | 0.07139 | 0.05192 | 0.03919 | 0.03032 | 0.02393 | 0.01923 | 0.01568 | 0.01295 | 0.01081 |   |                |
| $H_{\alpha}$    | $\lambda 6562.82$ |         |         |         |         |         |         |         |         |         |         | F8 V    | $T_{\text{eff}} = 6200^{\circ}\text{K}$ | $\log g = 4.0$ |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0    | 17.0    | 19.0    | 21.0    | 23.0    |   |                |
| Line Depth      | 0.28065           | 0.13203 | 0.07921 | 0.05295 | 0.03746 | 0.02775 | 0.02128 | 0.01672 | 0.01340 | 0.01093 | 0.00903 | 0.00756 |   |                |

TABLE XII (Continued)

|                 |         |                   |         |         |         |         |         |   |         |         |                |         |
|-----------------|---------|-------------------|---------|---------|---------|---------|---------|---|---------|---------|----------------|---------|
| $H_{\delta}$    |         | $\lambda 4104.74$ |         |         |         | F8 V    |         | $T_{\text{eff}} = 6200^{\circ}\text{K}$ |         |         | $\log g = 4.2$ |         |
| $\Delta\lambda$ | 1.0     | 3.0               | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.39698 | 0.19957           | 0.12274 | 0.08390 | 0.05980 | 0.04402 | 0.03326 | 0.02559                                 | 0.02000 | 0.01585 | 0.01274        | 0.01034 |
| $H_{\gamma}$    |         | $\lambda 4340.47$ |         |         |         | F8 V    |         | $T_{\text{eff}} = 6200^{\circ}\text{K}$ |         |         | $\log g = 4.2$ |         |
| $\Delta\lambda$ | 1.0     | 3.0               | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.37849 | 0.18929           | 0.11686 | 0.08026 | 0.05801 | 0.04324 | 0.03309 | 0.02585                                 | 0.02053 | 0.01653 | 0.01348        | 0.01111 |
| $H_{\beta}$     |         | $\lambda 4861.33$ |         |         |         | F8 V    |         | $T_{\text{eff}} = 6200^{\circ}\text{K}$ |         |         | $\log g = 4.2$ |         |
| $\Delta\lambda$ | 1.0     | 3.0               | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.34493 | 0.16916           | 0.19520 | 0.07144 | 0.05199 | 0.03929 | 0.03043 | 0.02404                                 | 0.01933 | 0.01579 | 0.01304        | 0.01090 |
| $H_{\alpha}$    |         | $\lambda 6562.82$ |         |         |         | F8 V    |         | $T_{\text{eff}} = 6200^{\circ}\text{K}$ |         |         | $\log g = 4.2$ |         |
| $\Delta\lambda$ | 1.0     | 3.0               | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.28210 | 0.13312           | 0.0800  | 0.05356 | 0.03794 | 0.02815 | 0.02162 | 0.01801                                 | 0.01365 | 0.01114 | 0.00921        | 0.00772 |

TABLE XII (Concluded)

|                 |                   |         |         |         |         |         |         |   |         |         |                |         |
|-----------------|-------------------|---------|---------|---------|---------|---------|---------|---|---------|---------|----------------|---------|
| $H_{\delta}$    | $\lambda 4104.74$ |         |         | F8 V    |         |         |         | $T_{\text{eff}} = 6200^{\circ}\text{K}$ |         |         | $\log g = 4.4$ |         |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.39691           | 0.19931 | 0.12248 | 0.08375 | 0.05973 | 0.04400 | 0.03325 | 0.02561                                 | 0.02004 | 0.01589 | 0.01278        | 0.01038 |
| $H_{\gamma}$    | $\lambda 4340.47$ |         |         | F8 V    |         |         |         | $T_{\text{eff}} = 6200^{\circ}\text{K}$ |         |         | $\log g = 4.4$ |         |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.37850           | 0.18912 | 0.1167  | 0.08014 | 0.05796 | 0.04323 | 0.03310 | 0.02589                                 | 0.02058 | 0.01659 | 0.01354        | 0.01117 |
| $H_{\beta}$     | $\lambda 4861.33$ |         |         | F8 V    |         |         |         | $T_{\text{eff}} = 6200^{\circ}\text{K}$ |         |         | $\log g = 4.4$ |         |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.34507           | 0.16921 | 0.10523 | 0.07146 | 0.05204 | 0.03935 | 0.03049 | 0.02411                                 | 0.01940 | 0.01585 | 0.01310        | 0.01095 |
| $H_{\alpha}$    | $\lambda 6562.82$ |         |         | F8 V    |         |         |         | $T_{\text{eff}} = 6200^{\circ}\text{K}$ |         |         | $\log g = 4.4$ |         |
| $\Delta\lambda$ | 1.0               | 3.0     | 5.0     | 7.0     | 9.0     | 11.0    | 13.0    | 15.0                                    | 17.0    | 19.0    | 21.0           | 23.0    |
| Line Depth      | 0.28322           | 0.13407 | 0.08071 | 0.05410 | 0.03837 | 0.02851 | 0.02191 | 0.01726                                 | 0.01387 | 0.01133 | 0.00938        | 0.00787 |

measured line depths were then plotted to a uniform scale as a function of distance from the line center. The 64 theoretical profiles were then plotted on transparent paper to the same scale and superposed on the observed plots in an attempt to find the best agreement or fit between theory and observations. Observations best fit by the theoretical curves of a single model are listed in Table XIII. Figures 4, 5, 6, and 7 are comparisons between the calculated hydrogen line profiles--H $\alpha$ , H $\beta$ , H $\gamma$ , and H $\delta$ --and the observed profiles for a star having an effective temperature of 6500  $^{\circ}$ K,  $\log g = 4.2$ , and with the solar abundance. This is the single model in best agreement with observations.

TABLE XIII  
OBSERVED HYDROGEN LINE PROFILES

|                     |                   |       |       |       |       |       |       |       |       |       |       |       |                          |       |       |       |                  |  |
|---------------------|-------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------------------------|-------|-------|-------|------------------|--|
| H $\delta$          | $\lambda 4101.74$ |       |       |       |       |       |       |       |       |       |       |       | Victoria Plate No. 50092 |       |       |       | Tracing No. 1797 |  |
| $\Delta\lambda$ (Å) | 0.0               | 0.5   | 1.0   | 1.5   | 2.0   | 2.5   | 3.0   | 3.5   | 4.0   | 6.0   | 8.0   | 10.0  | 12.0                     |       |       |       |                  |  |
| Line Depth          | .8571             | .6408 | .5019 | .4503 | .3257 | .2859 | .2541 | .2302 | .2112 | .1667 | .1239 | .0877 | .0395                    |       |       |       |                  |  |
| H $\gamma$          | $\lambda 4340.47$ |       |       |       |       |       |       |       |       |       |       |       | Victoria Plate No. 37112 |       |       |       | Tracing No. 1914 |  |
| $\Delta\lambda$ (Å) | 0.0               | 0.5   | 1.0   | 1.5   | 2.0   | 2.5   | 3.0   | 3.5   | 4.0   | 6.00  | 8.00  | 10.0  | 12.0                     | 14.0  | 16.0  | 18.0  |                  |  |
| Line Depth          | .8741             | .6775 | .5191 | .4122 | .3569 | .2987 | .2753 | .2214 | .1975 | .1326 | .1011 | .0902 | .0730                    | .0455 | .0267 | .0115 |                  |  |
| H $\beta$           | $\lambda 4861.33$ |       |       |       |       |       |       |       |       |       |       |       | Victoria Plate No. 38133 |       |       |       | Tracing No. 1815 |  |
| $\Delta\lambda$ (Å) | 0.0               | 0.5   | 1.0   | 1.5   | 2.0   | 2.5   | 3.0   | 3.5   | 4.0   | 6.0   | 8.0   | 10.0  | 12.0                     | 14.0  | 16.0  | 18.0  |                  |  |
| Line Depth          | .9769             | .6574 | .4815 | .3773 | .3218 | .2847 | .2454 | .2222 | .1901 | .1435 | .1157 | .0949 | .0741                    | .0510 | .0278 | .0093 |                  |  |
| H $\alpha$          | $\lambda 6562.82$ |       |       |       |       |       |       |       |       |       |       |       | Victoria Plate No. 36795 |       |       |       | Tracing No. 1819 |  |
| $\Delta\lambda$ (Å) | 0.0               | .05   | 1.0   | 1.5   | 2.0   | 2.5   | 3.0   | 3.5   | 4.0   | 6.0   | 8.0   | 10.0  | 12.0                     |       |       |       |                  |  |
| Line Depth          | .8181             | .6920 | .4117 | .3233 | .2667 | .2227 | .1768 | .1617 | .1415 | .0910 | .0682 | .0455 | .0228                    |       |       |       |                  |  |



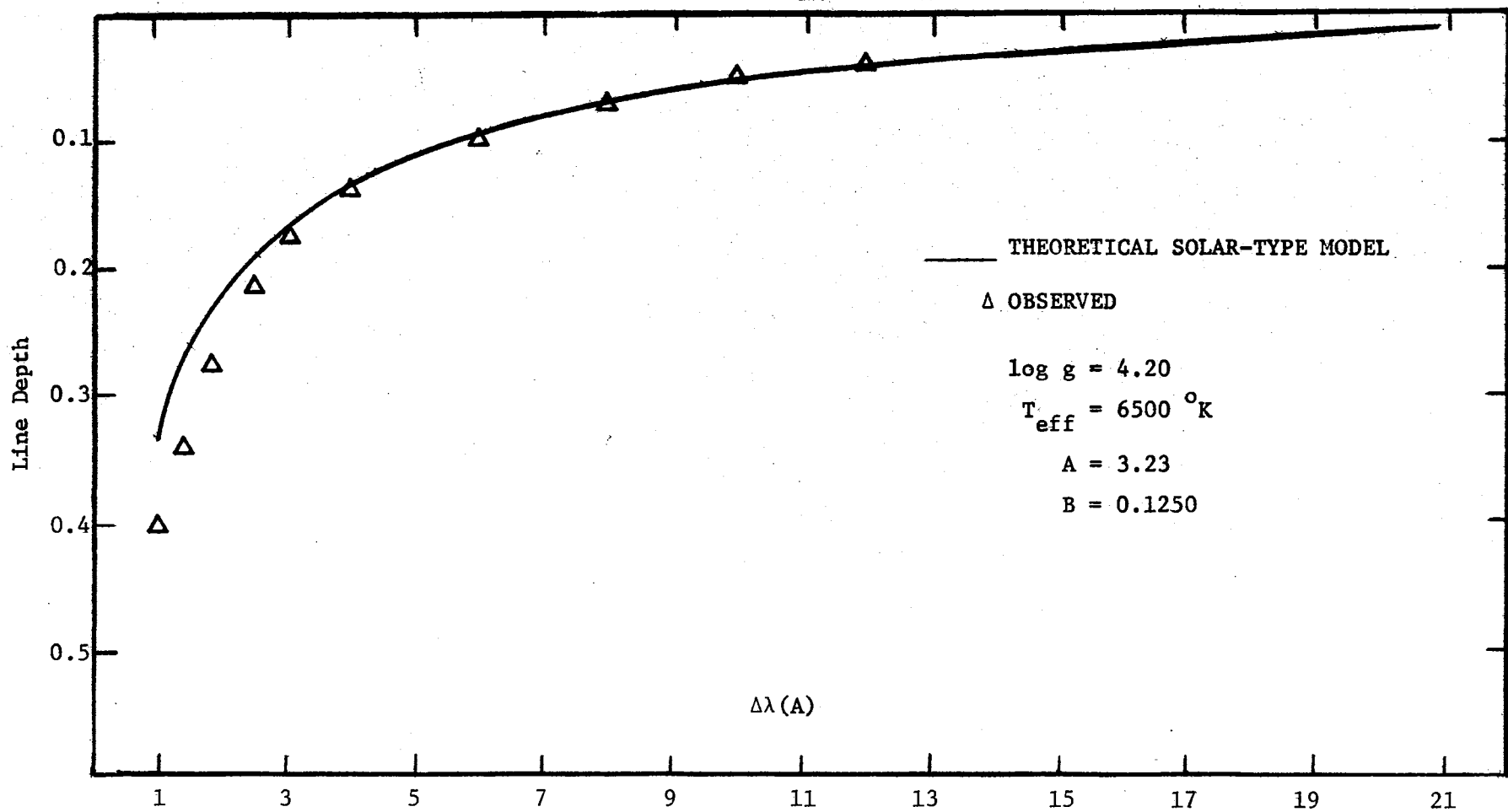


Figure 4. Observed and Theoretical Line Profiles for H $\alpha$

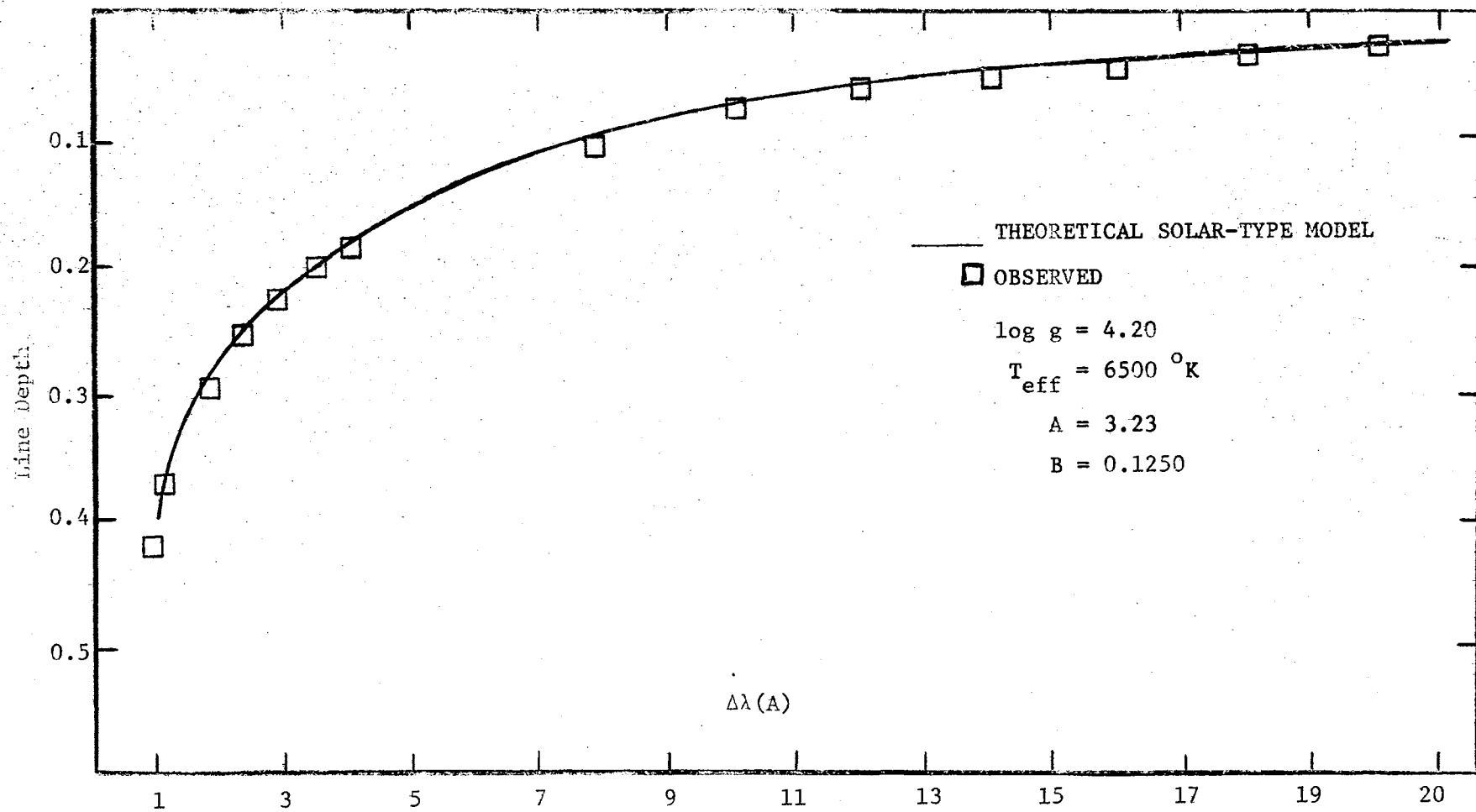


Figure 5. Observed and Theoretical Line Profiles for H $\beta$

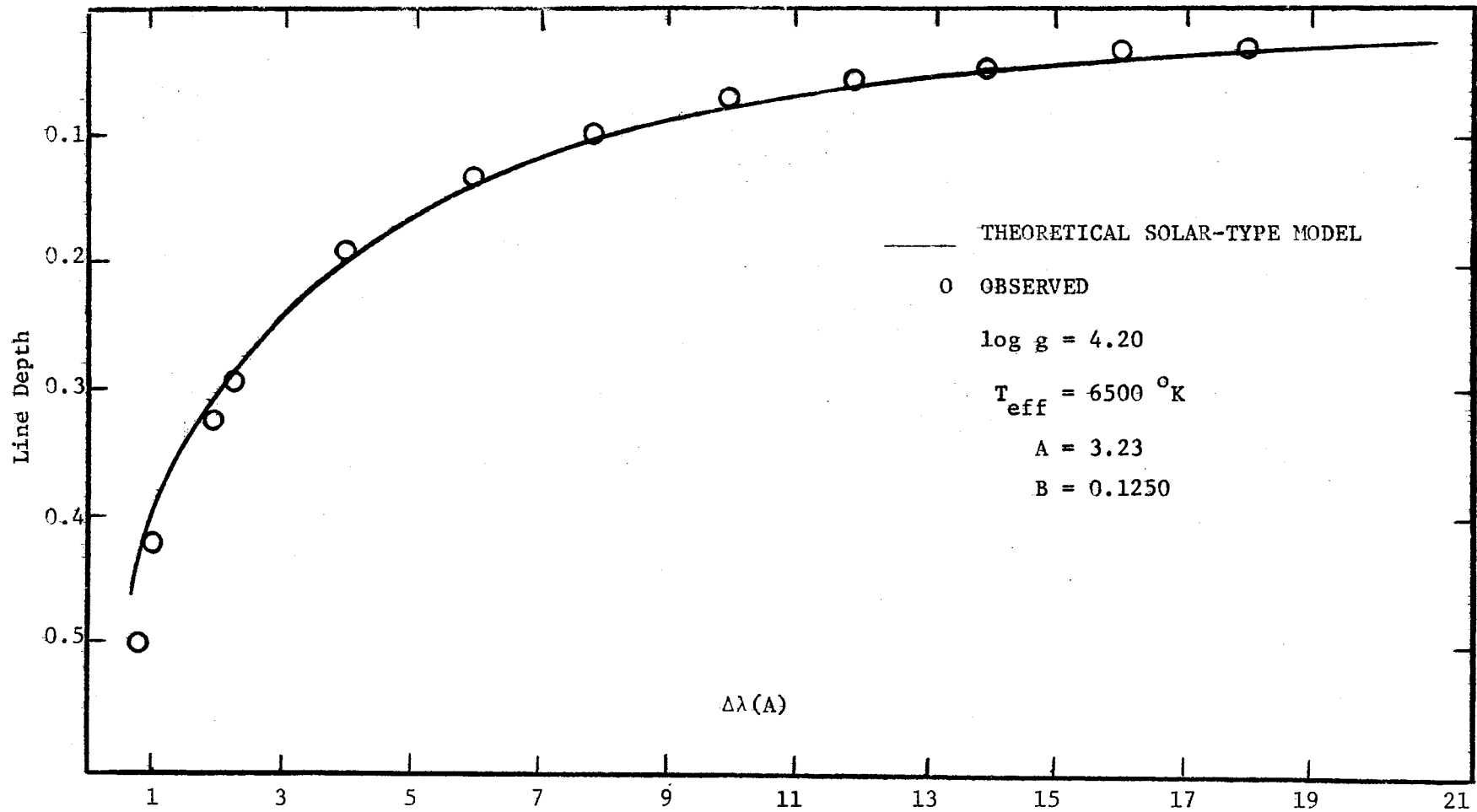


Figure 6. Observed and Theoretical Line Profiles for H $\gamma$

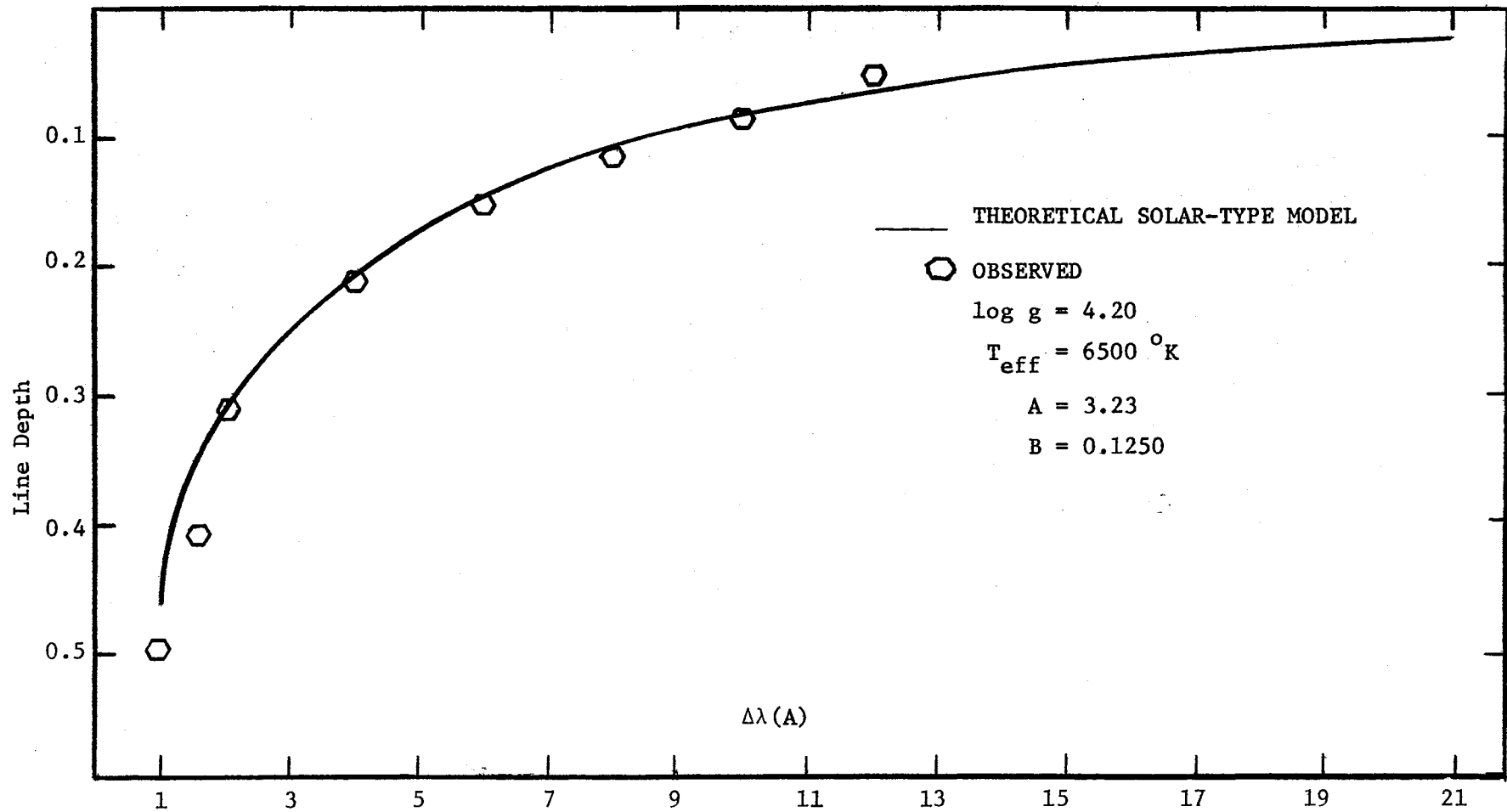


Figure 7. Observed and Theoretical Line Profiles for H $\delta$

## CHAPTER V

### SUMMARY

#### The Model

A detailed fine atmospheric analysis of the atmosphere of the star Theta Ursae Majoris was performed using a computer program which computes a pressure opacity-flux model for a given temperature distribution. A grid of sixteen model atmospheres, having effective temperatures between  $6200^{\circ}\text{K}$  and  $6650^{\circ}\text{K}$  and surface gravities between  $\log g = 3.8$  and  $4.4$ , was calculated in order to determine if a theoretical model of the star could be developed.

Using seven basic assumptions, the theoretical UBV colors and hydrogen line profiles were calculated for the star and compared to the observed values of the UBV colors and the hydrogen line profiles to determine which model was representative of the star Theta Ursae Majoris.

#### Analysis of the UBV Colors

The first calculation of the UBV colors did not include the effect of line blanketing. The computed values of U-B and B-V, given in Table VI, are obviously not in agreement with the observed values of  $U-B = 0.06$  and  $B-V = 0.46$ . Our model of the atmosphere for Theta Ursae Majoris was incorrect or line blanketing is an important factor in the computation of the UBV colors.

The second calculation of the UBV colors was performed using the

blanketing coefficients from the star Procyon, given by Talbert and Edmonds (1966), in the wavelength region  $\lambda = 3000$  to  $4200$  angstroms, and the blanketing coefficients from the star Gamma Serpentis, given by Kegel (1962), in the wavelength region  $\lambda = 4200$  to  $7200$  angstroms. The calculated theoretical colors, using line blanketing from these similar stars, indicated a better agreement between our model and the observed values for the star, but better agreement was desired.

The third calculation of the UBV colors was performed using the blanketing coefficients for the star Theta Ursae Majoris. Myrick (1970) calculated the blanketing coefficients and factors for Theta Ursae Majoris in the wavelength region  $\lambda = 3920$  to  $6610$  angstroms. The blanketing coefficients for the wavelength region  $\lambda = 3000$  to  $3920$  and  $\lambda = 6600$  to  $7200$  angstroms were determined by extrapolation using the stars Procyon and Gamma Serpentis. Using the blanketing coefficients for the star Theta Ursae Majoris, the computed values of the UBV colors are in very good agreement with the stated values for the B-V colors. The best agreement was found to be for an F8 V model having an effective temperature of  $6200^{\circ}\text{K}$  and surface gravity of  $\log g = 3.8$  or  $4.0$ . The computed values of the U-B colors did not show a good agreement between our model and the observed values. The poor agreement exists because the true continuum for the ultraviolet region has not been definitely established and the true values of the blanketing coefficients in this region are quite uncertain. Once the true continuum for the ultraviolet region is determined, the blanketing coefficients for this region can be determined with a high degree of accuracy. This will enable one to determine the blanketing coefficients in this wavelength region and to calculate the B-V colors with greater accuracy. The disparity between theoretic-

cal and observed U-B colors was so great that no one model could be selected as representative of the star Theta Ursae Majoris.

#### Analysis of the Hydrogen Line Profiles

The Balmer  $H\alpha$ ,  $H\beta$ ,  $H\gamma$ , and  $H\delta$  line profiles were computed and plotted graphically for the sixteen grid models in order to compare the theoretical hydrogen line profiles with the observed profiles. This comparison was used as a criterion to determine which model would be selected as the representative model for the star Theta Ursae Majoris. The model representative of the star was an FV 5 star having an effective temperature of  $6500^{\circ}\text{K}$  and surface gravity of  $\log g = 4.2$ . Although one model might show good agreement between one observed and calculated line, the FV 5 model indicates the best agreement when all four hydrogen lines were considered.

The observed and calculated values for all four hydrogen lines are in good agreement in the wings. The  $H\beta$  and  $H\gamma$  lines show good agreement as close as one angstrom from the core of the line. The agreement between observed and calculated values for the  $H\delta$  line is good when at a distance of only two angstroms from the line core. The greatest discrepancy near the center of the line core exists in the  $H\alpha$  line, but good agreement is obtained at a distance of three angstroms from the line core.

#### Conclusions

The theoretical UBV colors did not predict the same model of the star Theta Ursae Majoris as did the graphical comparison between the computed and observed values of the Balmer  $H\alpha$ ,  $H\beta$ ,  $H\gamma$ , and  $H\delta$  line pro-

files. The model selected by the UBV colors was a star having a lower temperature, 6200 °K compared to 6500 °K, and a lower effective surface gravity,  $\log g = 3.8$  or  $4.0$  compared to  $4.2$ , than the model dictated by the hydrogen line profiles. The UBV colors predict Theta Ursae Majoris to be an F8 V star while the hydrogen line profiles predict an F5 V star. Since so much disparity exists between the theoretical and observed U-B colors, the value of the U-B colors can not be used here as a good criterion to predict the model atmosphere for the star.

The blanketing coefficients for Theta Ursae Majoris in the region between 3920 and 6600 angstroms were calculated from tracings of the star itself. The blanketing coefficients in the region between 3000 to 3900 and 6600 to 7200 angstroms were calculated from similar stars and there could be an error in the calculated values of the blanketing coefficients. The use of the blanketing coefficients from similar stars could be one reason for the poor agreement between the theoretical and observed values of the U-B colors. The true continuum in the ultraviolet region has not been established with any known certainty and it is impossible to calculate the true blanketing coefficients in this region. Although our values of the U-B colors are too large by a factor of three, they show closer agreement than any other computed models for similar stars.

The hydrogen line profiles select an F5 V star as representative of Theta Ursae Majoris. This model is closer to the spectral classification of the star, F6 IV, than the model predicted by the UBV colors. It is acknowledged that there could be some error in the tracings of the hydrogen line profiles, but the probability of the error in the tracings is smaller than the error in the determination of the blanketing.



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