

DETERMINATION OF OPTIMAL PARAMETERS
FOR DYNAMICAL SYSTEMS

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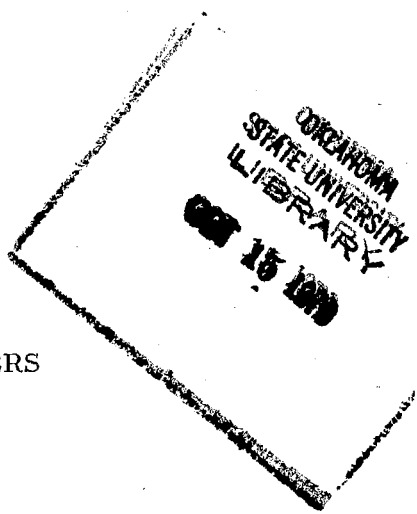
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CHAPTER I

INTRODUCTION AND LITERATURE SURVEY

Introduction

What is System Identification?

System identification is the process of determining a suitable mathematical model for a dynamic system. A schematic flow diagram is given in Figure 1. In order to explain this diagram in complete detail, it will be hypothesized that the system shown schematically in Figure 2 has been built and is undergoing experimental testing in the laboratory. The previous statement implies that the physical system must be subjected to some experimental runs in the laboratory before system identification can be performed.

In the system shown in Figure 2, it is assumed that the hydraulic ram has reached the end of its stroke and that a constant flow pump is still delivering oil to the system. Hence, the relief valve must open and allow the oil to return to tank. In this system, there are two variables which might conveniently be measured. The first is the movement, as a function of time, of the stem of the poppet in the poppet valve, and the second is the variation of the

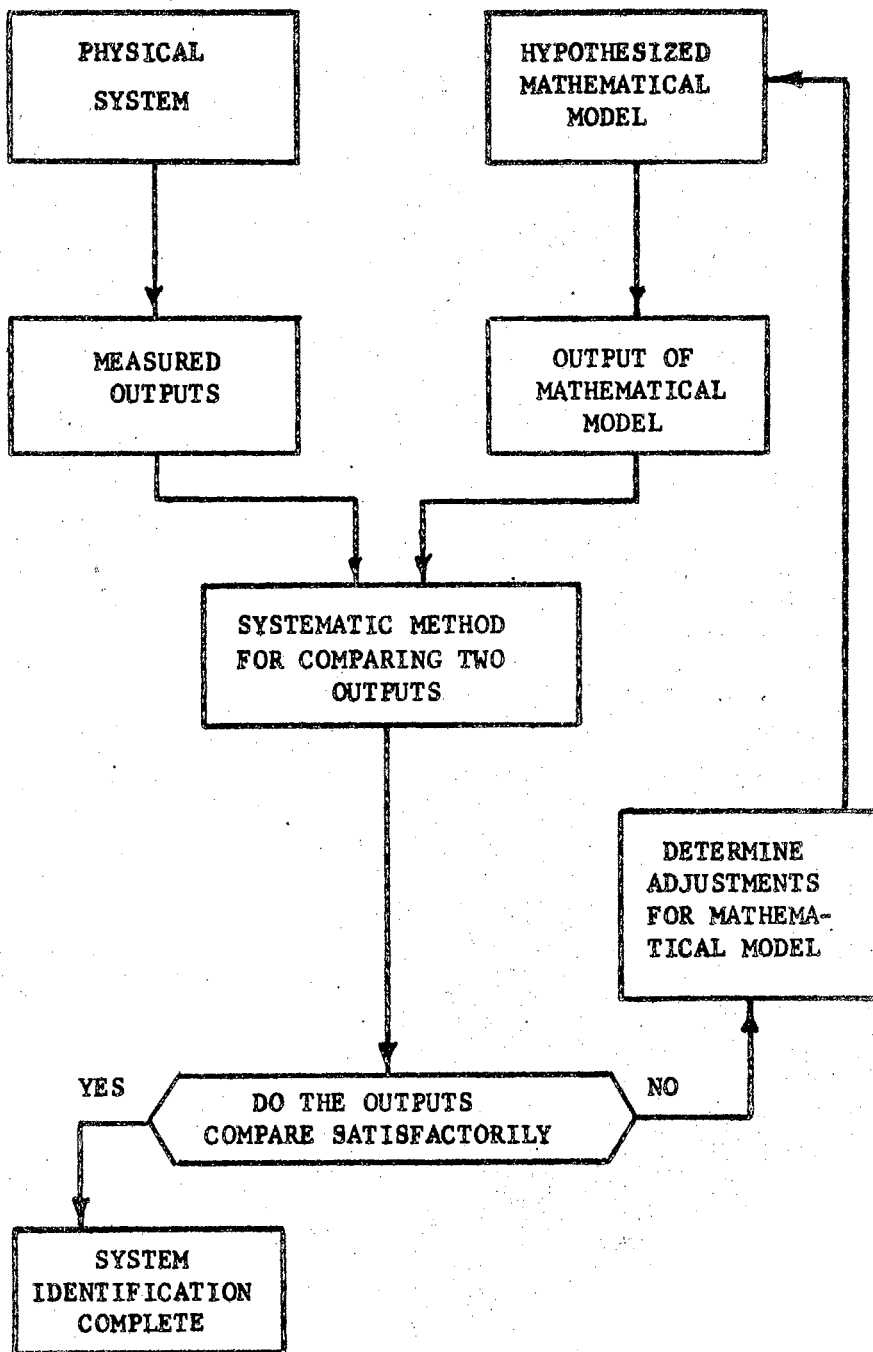


Figure 1. System Identification

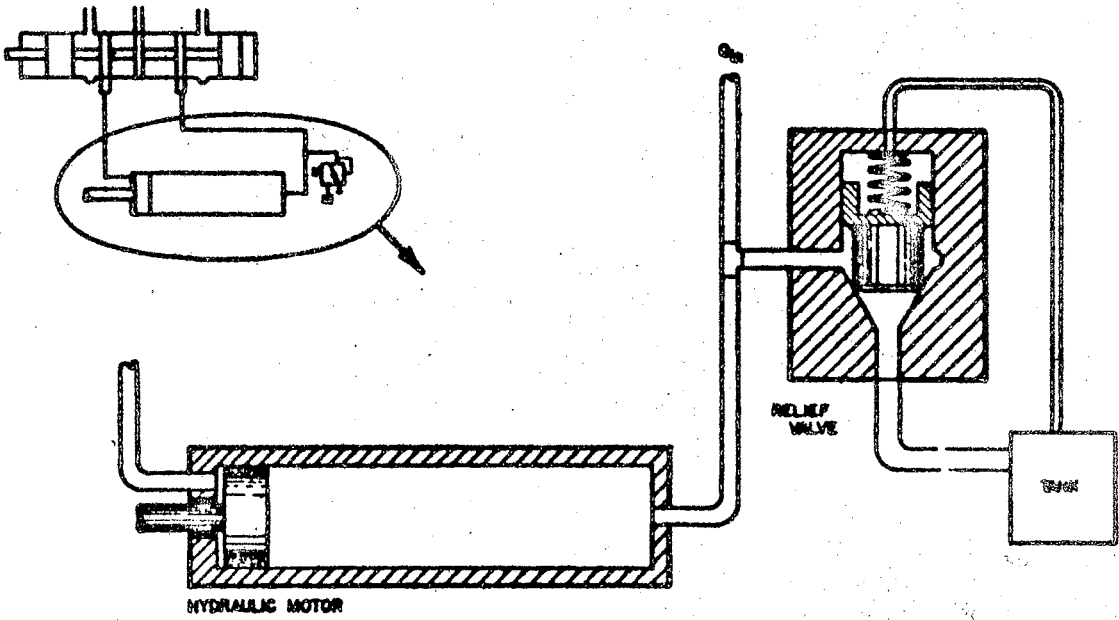


Figure 2. Hydraulic System

pressure in the inlet chamber of the poppet valve. If the valve were performing improperly, typical response plots might appear as shown in Figure 3.

The oscillating nature of the pressure and stem position as indicated in Figure 3 is undesirable, and it would be to the manufacturer's advantage if he could determine the cause of this improper performance. This is the point at which system identification enters into the problem. If a satisfactory mathematical model can be found which will yield a response which is identical to the response shown in Figure 3, the engineer can probably determine how to adjust the physical system to improve its responses by adjusting the mathematical model and observing how the mathematical model response varies as the model is varied.

At this point it is now possible to return to Figure 1 and explain the basic flow diagram for system identification in greater detail. First of all a physical system must be built and subjected to experimental tests in the laboratory. This yields the information in the upper left-hand portion of the flow diagram. Next, the user must hypothesize a mathematical model for the system, and this model is then used to simulate the response of the system. This provides the information in the upper right-hand portion of the flow diagram. The response of the mathematical model and the actual system must then be compared, and if they do not satisfactorily agree, the mathematical model must be adjusted until they do agree satisfactorily. There are various

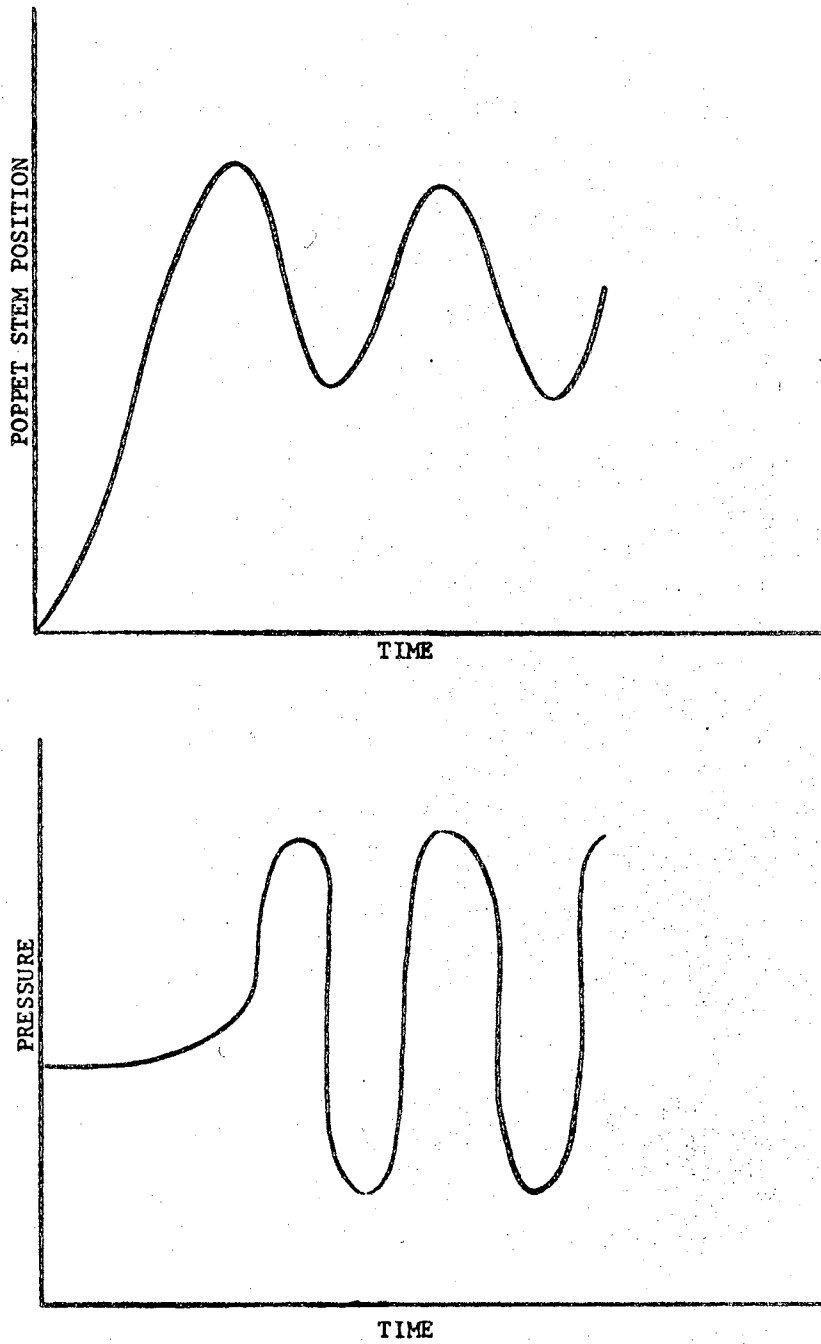


Figure 3. Initial Response of System of Figure 2

philosophies as to what is the best way of comparing the system response with the mathematical response and how the mathematical model should be varied if they do not agree satisfactorily.

As stated earlier, the user must hypothesize the basic form of the mathematical model which is to be used in the identification procedure. Hence, depending upon what the mathematical model is to be used for, the user may be interested in either a "black box" model or a "parameter estimation" model. An example of a situation in which the user might be interested in a "black box" mathematical model is that of determining the dynamic response of an internal combustion engine which is being used to supply power for a dynamic process. Since the user is sure in this situation that the structure of the internal combustion engine is not going to be varied during the experiments to be performed, he will be satisfied with any mathematical model which will predict the response speed of the engine versus its dynamical load. In other words, the parameters in the mathematical model need not have any relationship to the physical components of the engine.

The previous example of the hydraulic relief valve is a situation in which the user would be interested in a "parameter estimation" model. This is due to the fact that after the system has been satisfactorily identified, the user will want to adjust the mathematical model to improve the predicted response. If the user cannot, at this point,

relate the adjustments on the mathematical model to physical components in the system, his work cannot be used to its greatest advantage.

What is System Design?

One way of looking at a system design is to consider it as the process of determining the proper sizes of physical components in a system from its mathematical model. A schematic flow diagram for this view of system design is shown in Figure 4. It is interesting to note that in system design the first thing that must be specified is the desired system response. For the poppet relief valve example of the previous section, typical desired responses might be as shown in Figure 5.

The next step is to determine a relevant mathematical model for "parameter estimation". It must be a "parameter estimation" mathematical model since in the design problem you must be able to relate the parameters of the mathematical model to the physical components of the system. Once the mathematical model has been established, a systematic method for comparing the results of the response of the mathematical model with the desired response must be formulated. If the mathematical response does not compare favorably with the desired response, the mathematical model must be adjusted. When the model has been satisfactorily adjusted, the physical sizes of the components can then be determined.

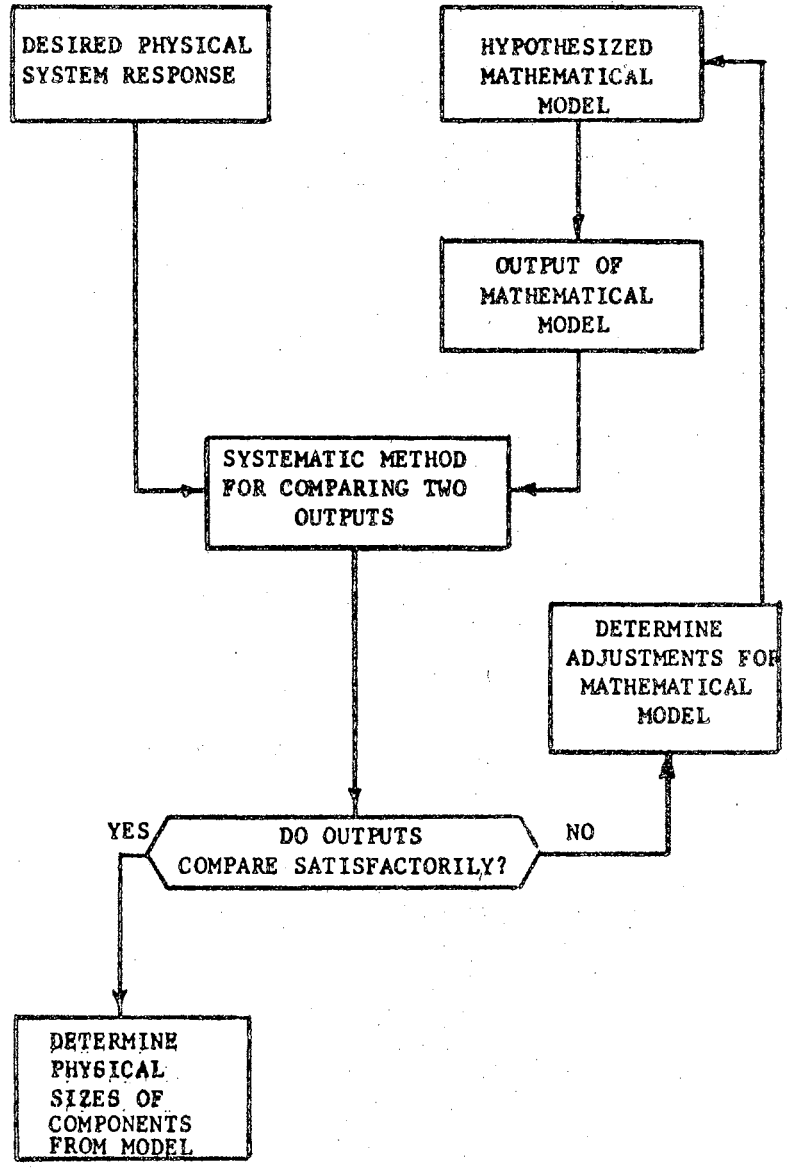


Figure 4. System Design

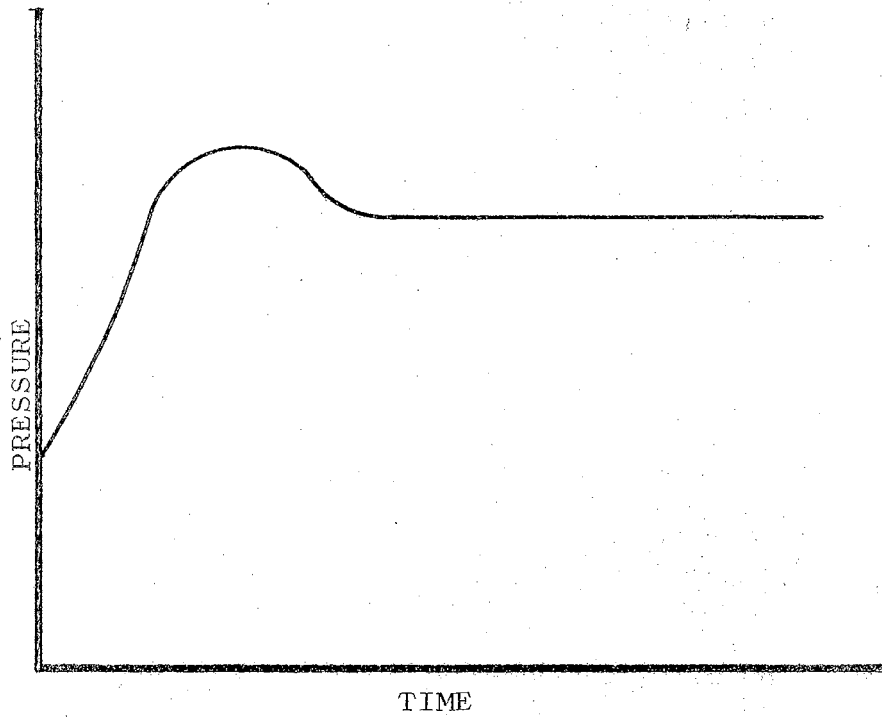
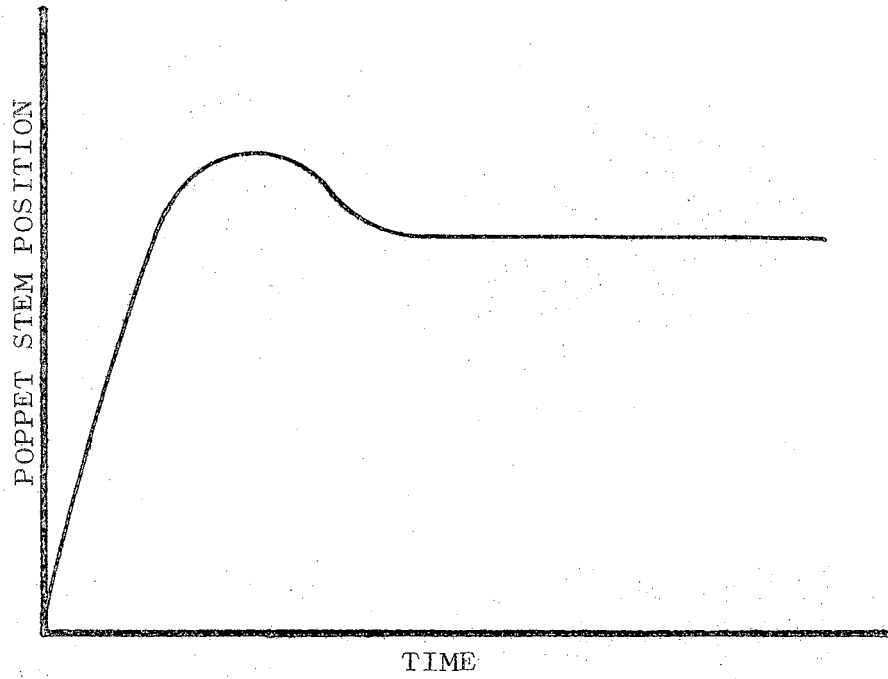


Figure 5. Desired Response of System of Figure 2

At this point it is very informative to compare the flow diagrams for System Design (Figure 4) and System Identification (Figure 1). The two diagrams are quite similar. Hence, it is not surprising that any method which can be used for system identification can also be used for system design.

Method Presented in This Thesis

The System Design and System Identification problem can be approached by either classical, statistical, or non-statistical methods. All three methods are discussed later in this chapter. Within this thesis a new non-statistical method is presented which is called the method of seeking principal planes.

In Chapter II the method of seeking principal planes is completely developed for the problem of determining the minimum of a function of several variables. Chapter II might be called a "capital goods expenditure" since the algebraic minimization techniques are not directly applicable to System Design and System Identification problems.

But in Chapter III it is demonstrated that optimal control theory can be used to convert a system design or identification problem into a two-point boundary value problem. The two-point boundary value problem can in turn be reformulated into an algebraic minimization problem, and the method of seeking principal planes becomes applicable.

If enough care is taken, the System Design or

Identification problem can be directly approached as an algebraic minimization problem. In Chapter IV the method of seeking principal planes is applied directly to System Design and Identification problems.

Chapter V presents some problems which arise when the dynamical systems which are being considered have certain types of discontinuities. Several approaches for resolving some of these difficulties are presented.

In Appendix A a description of a computational algorithm which is capable of analytically differentiating most mathematical expressions which can be written in the Fortran IV computer language is given. This algorithm was used extensively when programs were written to implement the method of seeking principal planes.

The analytical differentiation computational program relieves the user of the responsibility of determining the partial derivatives of the dynamical system equations. This eliminates most of the hand manipulations of the equations which the user must perform in order to use contemporary system identification techniques.

The rest of this introductory chapter presents the various methods available for solving System Design or Identification problems, a precise mathematical statement of the problem, and a comparison of presently available methods.

Classical Methods

The classical methods of system identification are based on s-plane analysis. The methods are applicable only to linear systems and, in general, only to systems which have one input and one output. The essential final result of s-plane analysis is that the characteristic roots are placed in positions such that the system is both stable and properly damped.

The use of classical methods of system identification requires that the input must be either sinusoidal, step, or impulse. When a sinusoidal input is used, the frequency of the input is varied and the amplitude of the response is noted. A log-magnitude (or Bode) versus frequency plot is then drawn and the systems is identified as well as possible from the shape of the plot.

Detailed discussion of the procedures of using frequency response methods for determining models is found in most texts on automatic control.

The main shortcomings of classical methods are: (1) they are applicable only to linear systems, (2) they are applicable only to systems with one input and one output, and (3) the system must be subjected to special inputs.

Statistical Methods

The three basic statistical methods used for system identification as presented by Aoki (1) are Least Squares Estimation, Maximum Likelihood Estimation, and Bayesian

Estimation. For linear systems with Gaussian (normal distribution) random noise, these three methods are equivalent. In order to estimate the parameters by Least Squares Estimation, nothing needs to be known about the various probability distributions. In order to use Maximum Likelihood Estimation or Bayesian Estimation, further statements concerning various probability distributions must be made.

Non-Statistical Methods

In the literature survey which was performed for this report, there were five non-statistical methods of system identification found. They are: (1) Optimal Control, (2) Differential Approximation, (3) Bacon's Method, (4) Parameter Influence Coefficients, and (5) Quasilinearization. A discussion of the basic philosophy of each of these methods will be presented later in this chapter.

Statement of Problem

Mathematical Model

In this section the identification and modeling problem will be stated in precise mathematical notation. The first thing which is necessary is for the user to supply the basic form of the differential equations in state variable notation.

$$\dot{X} = F(X, P, t). \quad (1-1)$$

In the above equation, X is the N dimensional state

variable vector, P is an M dimensional vector of unknown parameters, F is the functional form for the derivatives of the state variables, and t is the independent variable, time.

The precise values for the parameters in Equation (1-1) are not known, and the values for some of the state variable initial conditions may also not be known.

Specified or Measured Inputs and Responses

The inputs to Equation (1-1) need to be specified as functions of time. If the problem is an identification problem, the inputs to the physical system would be measured in the laboratory. If the problem is a system design problem, the input to the physical system and, hence, for the mathematical model must be specified.

The measured or desired responses for the mathematical equation must then be specified. For the poppet valve example, typical desired responses for state variables 1 and 3 (poppet position and chamber pressure) are shown in Figure 6.

Performance Index

Some measure must be set up to describe how "close" the response of the mathematical equation (1-1) is to conforming to the specified or measured response.

One standard performance index which is commonly used is the integral square error (ISE) which is defined as

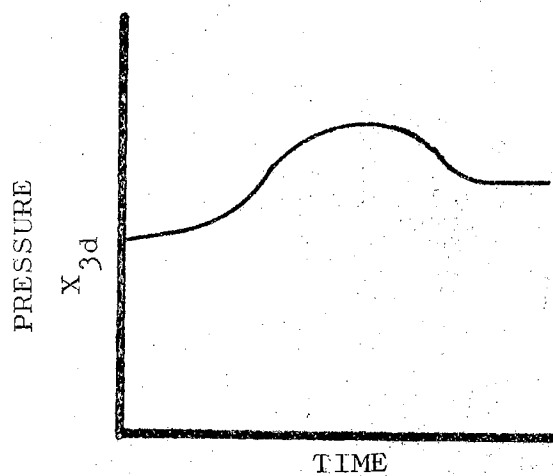
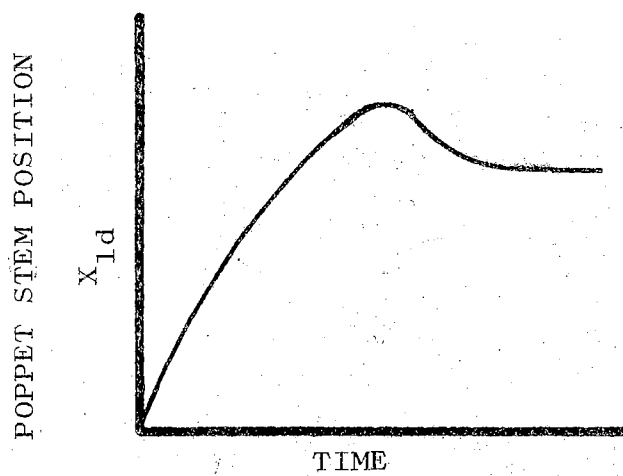


Figure 6. Typical Desired Response

follows for the poppet valve example:

$$PI = \int_{t_0}^{t_f} W_1 (X_1 - X_{1d})^2 + W_3 (X_3 - X_{3d})^2 dt. \quad (1-2)$$

In the above equation, W_1 and W_3 are weighting factors, X_1 and X_3 are the responses of state variables 1 and 3 in Equation (1-1), and X_{1d} and X_{3d} are the desired state variable responses as shown in Figure 6.

The weighting factors, W_1 and W_3 , must be specified by the user. If for instance, the weighting factors are chosen as $W_1 = 1.0$ and $W_3 = 0.0$, then the performance index depends only on the error which is present due to the amount that the mathematically predicted position of the poppet stem deviates from the desired position. If $W_1 = 0.0$ and $W_3 = 1.0$, then the performance index depends only on the error which is present due to the pressure predicted by the mathematical equation not agreeing with the desired pressure response. As a general rule, the weighting factors will be chosen so that their sum is unity. Hence, for this example,

$$W_1 + W_3 = 1.0. \quad \text{why?} \quad (1-3)$$

The other general rule to be used when choosing weighting factors is that the ratio of any two weighting factors should be inversely proportional to the square of the maximum expected error associated with each weighting factor. Hence, if the maximum expected errors in this example were $(X_1 - X_{1d})_{\max} = .001$ and $(X_3 - X_{3d})_{\max} = 10$,

the weighting factors should satisfy

$$\frac{W_1}{W_3} = \frac{(X_3 - X_{3d})^2_{\max}}{(X_1 - X_{1d})^2_{\max}} = \frac{(10)^2}{(.001)^2} = 10^8. \quad (1-4)$$

If Equations (1-3) and (1-4) are solved simultaneously, the following values are obtained:

$$W_1 = .999$$

$$W_3 = 10^{-8}. \quad (1-5)$$

Determination of Parameters

The system identification and modeling problem can now be summarized in the following short paragraph.

The parameter vector, P, and unknown initial conditions are to be determined so that the response of the system equation (1-1) will minimize the specified performance index. When these parameters and initial conditions have been determined, they represent the "best" values for the system equation according to the specified performance index. These parameters and initial conditions then represent the optimal "identification of the system" or the optimal values for system design.

Comparison of Non-Statistical Methods

In this section the following five methods of system identification are discussed: (1) Parameter Influence Coefficients, (2) Optimal Control, (3) Differential

Approximation, (4) Bacon's Method, (5) Quasilinearization, and (6) the method of seeking principal planes.

All of these methods, excepting Bacon's Method, determine the parameters for the state model, Equation (1-6), which will minimize a specified performance index, Equation (1-7).

$$\dot{X} = F(X, P, t) \quad (1-6)$$

$$PI = \int_{t_0}^{t_f} G(X, P, t) dt. \quad (1-7)$$

A special case of the above performance index is the integral error squared.

$$PI = \int_{t_0}^{t_f} (X_1 - X_{1d})^2 dt. \quad (1-8)$$

The term, X_{1d} , is the desired response for the first state variable.

Parameter Influence Coefficients

Meissenger (2) presents the basis for this powerful technique of parameter identification. It is based on the philosophy that if the gradient of the performance index with respect to the parameter vector can be determined, it will indicate the proper direction in which the parameter vector must be moved in order to reduce the performance index. Upon calculation of the gradient of the performance

index, it is realized that the parameter influence coefficients which are defined below are quite important.

$$\text{PARAMETER INFLUENCE COEFFICIENTS} = \frac{\partial X_i}{\partial P_j} \quad \begin{array}{l} i = 1, 2, \dots, N \\ j = 1, 2, \dots, M \end{array} \quad (1-9)$$

These parameter influence coefficients can be obtained by performing some mathematical manipulations and expanding the original state model.

The solution procedure is an iterative technique which utilizes the steepest descent. Each iteration requires the solution of $1+N+M+NM$ first order differential equations where N is the order of the state model and M is the number of parameters being optimized. This requires considerable computational time per iterative step.

Optimal Control Theory

Optimal control theory can be applied in a straightforward manner, to yield a set of $2(N+M)$ ordinary differential equations with split boundary conditions. These equations represent a set of necessary conditions which the optimal parameter vector must satisfy.

$$\dot{X} = F(X, P, t) \quad (1-10)$$

$$\dot{P} = 0$$

$$\dot{\lambda}_K = \frac{-\partial G}{\partial X_K} - \sum_{j=1}^N \lambda_j \frac{\partial F_j}{\partial X_K} \quad K = 1, 2, \dots, N$$

$$\dot{u}_K = \frac{-\partial G}{\partial P_K} - \sum_{j=1}^N \lambda_j \frac{\partial F_j}{\partial P_K} \quad K = 1, 2, \dots, M.$$

The boundary conditions which the above equations must satisfy are,

$$\begin{aligned} X(0) &= X_0 \\ \lambda(T) &= 0 \\ \mu(0) &= 0 \\ \mu(T) &= 0. \end{aligned} \tag{1-11}$$

Any method such as gradient techniques, quasilinearization, or dynamical programming can be used to solve the set of differential equations. This is not a simple problem and considerable effort is necessary for finding a solution.

Optimal Parameters for Linear Systems

Bacon (3, 4) has presented a method which is applicable to constant coefficient linear systems

$$\begin{aligned} \dot{X} &= [A]X + [B]U \\ Y &= [C]X + [D]U. \end{aligned} \tag{1-12}$$

In the above equation $[A]$, $[B]$, $[C]$, and $[D]$ are constant coefficient matrices. However, each individual element of these matrices can be a function of the parameters, and the procedure which Bacon develops optimizes the parameters and not the coefficients. This is a definite

advantage since it is quite common for one parameter to be involved in several coefficients.

The principle handicap of Bacon's procedure is that the desired response, Y , and system input, U , must be specified as linear combinations of analytic functions. These analytic functions must be of the class which is obtainable from the solution of a linear constant coefficient homogeneous state model. This means that the inputs and outputs obtained from measured data must be fitted with analytic functions.

The iterative procedure which determines the optimal parameters does not require that the state model, Equation (1-12), be solved over a time interval. Thus, this method requires relatively little computational effort as compared to other methods.

Differential Approximations

The method of differential approximation as presented by Bellman, Kalaba, and Sridhar (5) utilizes the fact that Equation (1-1) can be rewritten as,

$$\dot{X} - F(X, P, t) = 0. \quad (1-13)$$

From this simple observation, it is evident that if \dot{X} , and X , are known, then the correct parameter vector must minimize the following performance index.

$$PI = \int_0^T \langle \dot{X} - F(X, P, t), \dot{X} - F(X, P, t) \rangle dt. \quad (1-14)$$

In the above equation the symbols \langle, \rangle stand for the dot product of the two vectors.

The fact that the gradient of the performance index with respect to the parameter vector must be zero at the minimum point is utilized to obtain a general equation for determining the optimal coefficients. Bose (6) has developed this procedure for use with a discrete performance index. This is a powerful technique which does not require an iterative procedure for determining the optimal coefficients.

However, the differential approximation method requires that the entire state trajectory and the derivative of the state trajectory be known. This is an extremely large amount of information which is often quite difficult to obtain. This method requires the solution of a set of nonlinear algebraic equations if optimal parameters are to be determined. It often occurs that a change in one parameter will cause a change in several of the coefficients.

Quasilinearization

This approach as presented by Bellman, Kalaba, and Sridhar (5), and Allison (7) can be used to determine the parameters of the state model (1-1) which will minimize a general integral error squared performance index (1-2). This is accomplished by solving a sequence of linear models which approximate the original system. If this sequence of linear models converges to a final solution, the resulting

parameters are the optimal parameters for the original system model.

The major weakness of the method of quasilinearization is that the method may diverge rather than converge to the desired solution. A proof which is presented in Appendix C can be used to show that the method of quasilinearization may diverge from a desired parameter point regardless of how close to that point one starts if the mathematical response does not fit the desired response exactly.

Method of Seeking Principal Planes

This is a new method which is developed in this thesis. It is based upon the Taylor series expansion which is truncated after the second-order terms.

Comparison of Methods

Among the qualities which are of interest in comparing these methods are:

1. Is the method restricted to linear systems?
2. Does the method require knowledge of the entire state vector of the physical system, or is knowledge of just one of the system outputs sufficient?
3. Does the method require that a set of differential equations be integrated for each iterative step?

4. Can the method be used with data in graphical form?
5. Does the method require the solution of a system of differential equations with split boundary conditions?
6. Is the user free to specify the criteria which are used to determine the "goodness" of the parameters which are selected by the method?
7. Does the method determine the desired physical parameters or a set of coefficients for the mathematical equations?
8. Can limits be placed on the parameter values which the method selects?
9. Does the method converge from even a poor original guess of the actual system parameters?
10. Does the method converge when the parameter guesses become close to the optimal parameters?

The comparison of the various methods can most easily be presented in the form of a table which is given in Figure 7. An X has been placed over each undesirable characteristic.

From Figure 7 it is seen that the method of seeking principal planes has only one major weakness: It requires the solution of the entire state model over the time period of interest for each iterative step.

However, it has very good convergence characteristics.

In Chapter II this method is developed for the problem

Convergence characteristics when parameter guess is close to the optimal	POOR	Solution method unspecified	Excellent	Reasonable	?	Excellent
Stability problems if initial parameter guess is not close enough	NO	Solution method unspecified	NO	YES	YES	NO
Limits can be placed on parameter values	YES	NO	YES	YES	NO	NO
Can adjust parameters rather than coefficients	YES	YES	YES	YES	YES	YES
Type of performance index allowed	GENERAL	GENERAL	SPECIAL	SPECIAL	SPECIAL	GENERAL
Requires solution of nonlinear two-point boundary value problem	NO	YES	NO	NO	NO	NO
Desired response and input can be in graphical form	YES	YES	YES	NO	YES	YES
Requires solution of entire state model for each iterative step	YES	Solution method unspecified	NO	NO	YES	YES
Requires knowledge of entire state vector of physical system	NO	NO	YES	NO	NO	NO
Restricted to linear systems	NO	NO	NO	YES	NO	NO
	Parameter Influence Coefficients		Differential Approximation	Bacon's Method	Quasilinearization Method	Method of Seeking Principal Planes

Figure 7. Comparison of the Various Methods of Parameter Identification
 (An X has been placed over each of the undesirable characteristics.)

of determining the minimum of a function of several variables. Chapter III expands the method so it can be used to work two-point boundary value problems. Chapter IV uses the method of seeking principal planes directly on the problem of system design or identification, and Chapter V presents several approaches for minimizing problems which arise when the dynamical system is discontinuous.

CHAPTER II

MINIMIZATION OF A FUNCTION

OF SEVERAL VARIABLES

There are two basic methods for attacking the problem of determining optimal parameters for a dynamical system. The first approach which is called the direct method adjusts the free parameters until a minimum of the performance index is obtained. The second method which is called the indirect method and utilizes the fact that the gradient vector of the performance index must be zero at an extremum point. This provides a set of necessary conditions which must be satisfied. Indirect solution approaches then attempt to satisfy these necessary conditions.

Both the direct and indirect methods of approach for determining optimal parameters of a dynamical system can be restated as a problem of minimization of a function of several variables. Hence, it is seen that the problem of determining the minimum of a function of several variables is important. Chapter III discusses the indirect method; Chapter IV discusses direct methods,

The first section of this chapter summarizes briefly the standard approaches for the minimization problem. Next,

a new procedure which is called the method of seeking principal planes is presented. The third portion of this chapter is devoted to a discussion of methods for solving systems of algebraic equations which is an inherent part of the indirect procedures. Finally, several example problems which have been solved by the method of seeking principal planes are presented and compared with results obtained by other methods to illustrate the method's versatility.

Standard Methods for Determining a Minimum of a Function of Several Variables

An important problem both from a mathematical and practical viewpoint is to determine the minimum of a scalar function of several variables. The independent variables will be denoted by the vector X which is of dimension M , and the function to be minimized is

$$Y(X). \quad (2-1)$$

Extensive work has been performed to determine methods for minimizing a scalar function. There are many methods which have been devised for special scalar functions, but three methods of particular interest which handle general scalar functions are: (1) gradient techniques, (2) the Newton-Raphson method, and (3) the conjugate gradient method.

Gradient techniques normally proceed in the negative gradient direction. The distance traveled in the negative

gradient direction depends upon which method is being used, but it is quite common to travel in the negative gradient direction until a local minimum is reached. The gradient is then reevaluated and one proceeds in the new negative gradient direction to a local minimum. This is continued until one is sufficiently close to the desired minimum point. The principle shortcoming of gradient techniques is that they may be very slow in converging to a desired minimum. Another problem associated with gradient techniques is the determination of the initial estimate of how far one should proceed in the negative gradient direction as one searches for the local minimum.

The Newton-Raphson method as is described by Wilde and Beightler (10) utilizes the expansion of the scalar function in a Taylor series about some initial point, X .

The gradient and matrix of second partial derivatives of the scalar function are defined as

$$Y_X = \left[\frac{\partial Y}{\partial X_1}, \frac{\partial Y}{\partial X_2}, \dots, \frac{\partial Y}{\partial X_M} \right]$$

$$Y_{XX} = \begin{bmatrix} \frac{\partial}{\partial X_1} \frac{\partial Y}{\partial X_1} & \frac{\partial}{\partial X_1} \frac{\partial Y}{\partial X_2} & \dots & \frac{\partial}{\partial X_1} \frac{\partial Y}{\partial X_M} \\ \vdots & \vdots & \ddots & \vdots \\ \frac{\partial}{\partial X_M} \frac{\partial Y}{\partial X_1} & \frac{\partial}{\partial X_M} \frac{\partial Y}{\partial X_2} & \dots & \frac{\partial}{\partial X_M} \frac{\partial Y}{\partial X_M} \end{bmatrix}$$

The Taylor series expansion then becomes

$$Y(X) = Y(X_0) + Y_X(X_0)[X - X_0] + \frac{1}{2!} [X - X_0]^T Y_{XX}(X_0)[X - X_0] + \dots \quad (2-2)$$

It is assumed that the new function which is obtained by truncating the Taylor series after the first two terms describes the scalar function accurately. Then one looks at the required conditions for extremizing the local function which has been obtained by truncating the Taylor series. The result is that the new estimate for the minimum of the scalar function is

$$X_{\text{new}} = X_0 - Y_{XX}(X_0)^{-1} Y_X(X_0)^T. \quad (2-3)$$

In Equation (2-3) the superscripts -1 and T , respectively, represent the matrix inverse and matrix transpose.

The assumption that the truncated Taylor series expansion describes the scalar function accurately, in general, is not valid globally. This implies that if one is not close to the desired minimum, then the new point which is predicted by Equation (2-3) may not be a good estimate. The Newton-Raphson method will often diverge if one is not close enough to a desired minimum.

Another shortcoming of the Newton-Raphson method is that it requires evaluation of the gradient of the function and the matrix of second partial derivatives. This can amount to significant computational effort.

The feature of the Newton-Raphson method which is very desirable is that if one is sufficiently close to the desired minimum, then the method is quadratic in convergence.

Another method for minimizing a scalar function which has received recent attention is called the conjugate gradient method. Fletcher and Reeves (8) have demonstrated the computational feasibility of this method.

In the conjugate gradient method, the first step is normally taken in the negative gradient direction. It is required that a local minimum along the negative gradient direction be located. Then, a new direction is calculated which might be termed a deflected negative gradient direction. This deflected gradient direction is not the same as the true gradient direction, and this is the primary difference between conjugate gradient and normal gradient procedures.

The deflected negative gradient direction is such that if you proceed a small enough distance in this direction, you will obtain a smaller value for the scalar function which is to be minimized.

The next step of the procedure is to determine a local minimum along the deflected negative gradient direction. The iterative procedure of determining (1) a new deflected gradient direction and (2) a minimum along this direction is continued until one is sufficiently close to a desired minimum of the scalar function.

The basic reason that this method is so powerful is that it is quadratic in convergence. This means that once you are close to a desired minimum value, the method will converge very rapidly. Hence, the method of conjugate gradients eliminates the principal fault of gradient techniques, but it still does not remedy the selection of an initial estimate of the distance to be traveled along the selected direction.

Method of Seeking Principal Planes

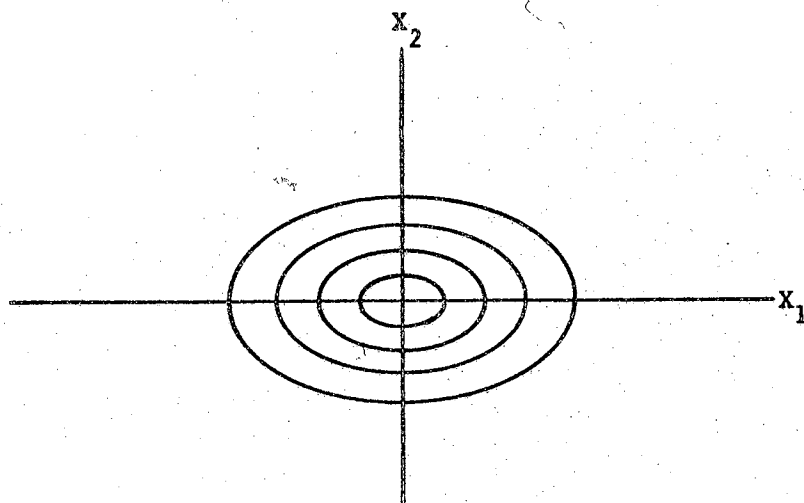
A good amount of insight into the scalar minimization problem can be obtained by investigating the scalar function

$$Y = C_1 X_1^2 + C_2 X_2^2$$

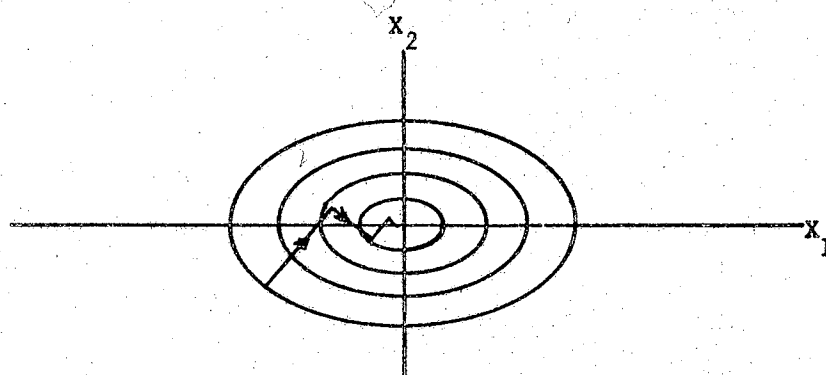
where C_1 and C_2 are both positive numbers. In Figure 8 contours of constant value for the scalar function have been drawn. They are concentric ellipses, and the amount of eccentricity is governed by the relative magnitudes of C_1 and C_2 .

It is informative to investigate how it would be possible to reach the exact minimum of this function by going successively in negative gradient directions.

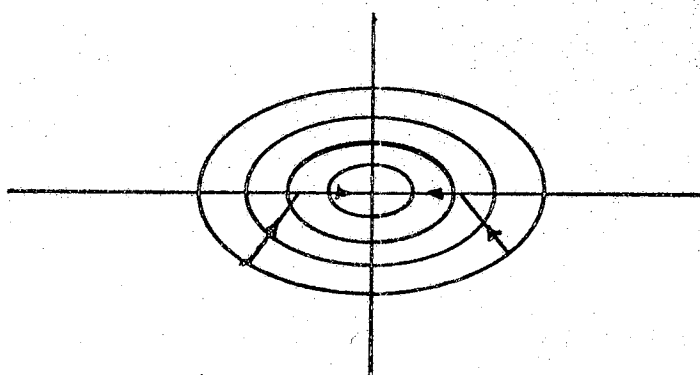
It is first noted that the normal gradient technique will never reach the minimum of the scalar function exactly. Starting from an arbitrary point, the standard gradient technique will zigzag back and forth about one of the principal axes, but it will never reach the exact



A. Contours of Constant Value for Y



B. Typical Trajectory for Gradient Technique



C. Trajectories Which Proceed Sequentially in Negative Gradient Direction and Which Reach the Exact Minimum

Figure 8. Minimization of $Y = C_1 X_1^2 + C_2 X_2^2$

minimum point. This is shown in part B of Figure 8.

In part C of Figure 8, several trajectories which proceed sequentially in negative gradient directions and which reach the exact minimum of the scalar function are shown. In general, two steps are required to reach the minimum for this particular problem.

The minimization procedure presented in this section is called the method of seeking principal planes. For the two-dimensional minimization problem in Figure 8, it is evident that the points at which the negative gradient direction intersects the axes are important; but the figure does not indicate why, in general, the points at which the negative gradient direction intersects the principal planes are important.

The three-dimensional minimization problems given by

$$Y = C_1 X_1^2 + C_2 X_2^2 + C_3 X_3^2;$$

will exemplify why the points of intersection of the principal planes are important. C_1 , C_2 , and C_3 are positive numbers in the preceding equation.

A contour of constant value for Y is shown in Figure 9. In general, constant value contours for Y will be ellipsoids, and the amount of eccentricity is governed by the relative magnitudes of C_1 , C_2 , and C_3 .

It will now be demonstrated that by proceeding three steps in the negative gradient direction the exact minimum point can be reached.

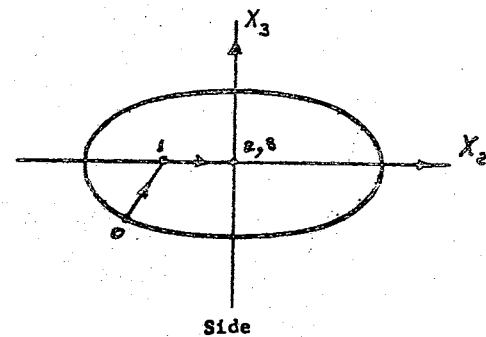
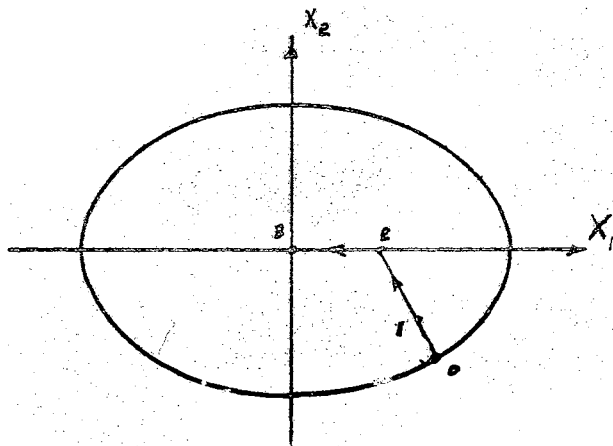
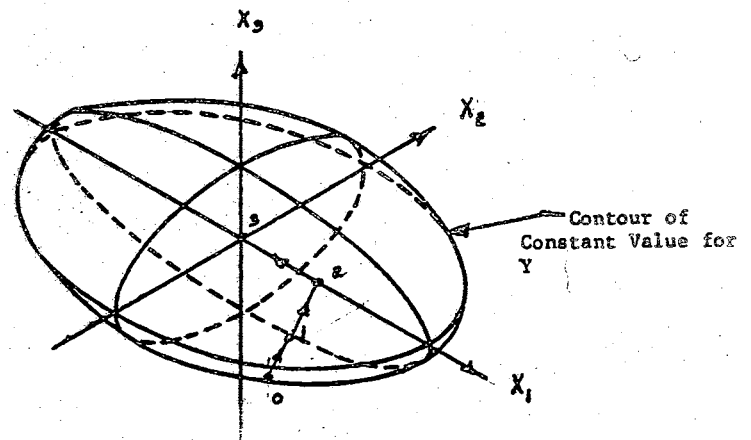
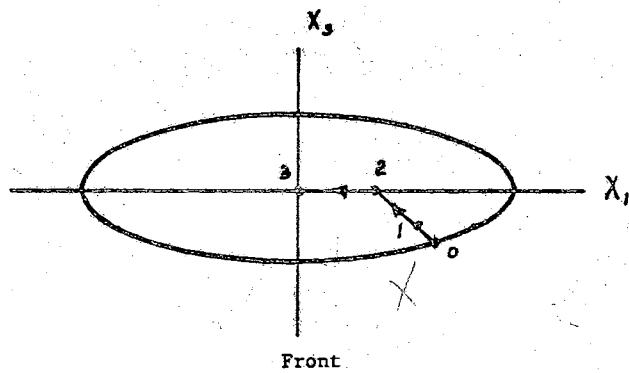


Figure 9. Minimization of $Y = C_1 X_1^2 + C_2 X_2^2 + C_3 X_3^2$ by Method of Seeking Principal Planes

An arbitrary point denoted by 0 in Figure 9 will be used as the starting point. The point 1 of Figure 9 is the point at which the negative gradient direction from point 0 intersects the plane which contains the axes X_1 and X_2 . The point 2 of Figure 9 is the point at which the negative gradient direction from point 1 intersects the plane which contains axes X_1 and X_3 . Similarly, point 3 of Figure 9 is the point at which the negative gradient direction from point 2 intersects the plane which contains axes X_2 and X_3 .

The mathematical development which indicates the distance to the intersection of the principal planes in negative gradient direction will now be presented.

The first step of the mathematical development is to expand the scalar function in a Taylor series such as in Equation (2-2).

Throughout the rest of this development, it will be assumed that all of the third partial derivatives of the scalar function are continuous in the neighborhood of X_0 . This implies that the matrix of second partial derivatives will be symmetric, and the scalar function can be approximated locally by truncating the Taylor series as

$$Y_{loc}(X) = Y(X_0) + Y_X(X_0)[X - X_0] + \frac{1}{2!} [X - X_0]^T Y_{XX}(X_0)[X - X_0]. \quad (2-4)$$

The gradient vector of the local approximation to the scalar function is

$$Y_{X_{loc}}(X) = Y_X(X_0) + [X - X_0]^T Y_{XX}(X_0). \quad (2-5)$$

The question which must now be answered is: How far in the negative gradient direction should one travel in proceeding from the present position of the independent variable, X_i , to the new independent variable, X_{i+1} . Note that the present position, X_i , will be equal to X_0 on the very first step, but in general X_i will not be the same as X_0 . Also, the subscript refers to the iteration number; that is, X_i implies the X vector at the i^{th} iteration.

In mathematical terms, this amounts to determining the magnitude of K in the following equation:

$$X_{i+1} = X_i - K Y_X^T(X_i). \quad (2-6)$$

An excellent approximation of $Y_X(X_i)$ is $Y_{X_{loc}}(X_i)$ which is given by Equation (2-5) provided that X_i is sufficiently close to X_0 . If it is assumed that they are exactly the same, Equation (2-5) can be substituted into Equation (2-6); and the resulting expression is

$$X_{i+1} = X_i - K[Y_X(X_0) + (X_i - X_0)^T Y_{XX}(X_0)]^T. \quad (2-7)$$

The predicted difference between the value of the scalar function at the point X_{i+1} and the point X_i provides valuable information for determining the magnitude of K in Equation (2-7). This predicted difference can be obtained from Equations (2-7) and (2-4), and the resulting

equations are

$$X_{i+1} = X_i = -K[Y_X(X_0) + [X_i - X_0]^T Y_{XX}(X_0)]^T \quad (2-8)$$

and

$$\begin{aligned} Y_{loc}(X_{i+1}) - Y_{loc}(X_i) &= Y_X(X_0) [X_{i+1} - X_i] \\ &+ \frac{1}{2}[X_{i+1} - X_0]^T Y_{XX}(X_0)[X_{i+1} - X_0] \\ &- \frac{1}{2}[X_i - X_0]^T Y_{XX}(X_0)[X_i - X_0]. \end{aligned} \quad (2-9)$$

Several coordinate transformations need to be performed so that Equations (2-8) and (2-9) can be better interpreted. These coordinate transformations involve the eigenvalues and eigenvectors of the matrix of second partial derivatives. Athans and Falb (9) show that all of the eigenvalues will be real numbers since the matrix of second partial derivatives is real and symmetric.

In general, there will be P positive eigenvalues, N negative eigenvalues, and Z zero eigenvalues. The eigenvalue matrix, λ , is arranged so that the positive eigenvalues are the first to appear on the diagonal, the negative eigenvalues appear next on the diagonal, and the zero eigenvalues appear last on the diagonal. Further, it is required that $\lambda_1 > \lambda_2 > \dots > \lambda_p$.

Throughout the rest of this paper, λ_i will mean the i^{th} eigenvalue which is located on the diagonal of the eigenvalue matrix,

The vector Z is defined by the following set of equations:

$$C_j = E_j^T Y_X^T(X_0) \quad j = 1, 2, \dots, p + N \quad (2-15)$$

$$C_j = 0 \quad j = p+N+1, \dots, M \quad (2-16)$$

$$Z = -EC + X_0. \quad (2-17)$$

The amount of the coordinate translation which is given by Equation (2-14) at first appears to be quite confusing, but it should be noted that if the matrix of second partial derivatives has no zero eigenvalues, then the resulting translation is to the extremum point of the local approximation for the scalar function, Equation (2-4). This will now be demonstrated.

If Equation (2-13) is premultiplied by E , post multiplied by E^T , and then inverted, the equation which results is

$$Y_{XX}(X_0)^{-1} = E \lambda^{-1} E^T. \quad (2-18)$$

Equations (2-17) and (2-18) can be combined and simplified to

$$Z = -Y_{XX}(X_0)^{-1} Y_X(X_0)^T + X_0$$

which is the stationary point of Equation (2-4).

A new coordinate system will now be introduced by rotating the W coordinate. The resulting coordinate system e is defined as

$$e = E^T W = E^T [X - X_0] + C. \quad (2-19)$$

If the following definitions are made,

$$e_0 = e(X_0) = C, \quad (2-20)$$

$$e_i = e(X_i) = E^T [X_i - X_0] + C \quad (2-21)$$

and

$$e_{i+1} = e(X_{i+1}) = E^T [X_{i+1} - X_0] + C; \quad (2-22)$$

then it follows that

$$X_i - X_0 = E[e_i - C] \quad (2-23)$$

$$X_{i+1} - X_0 = E[e_{i+1} - C] \quad (2-24)$$

and

$$X_{i+1} - X_i = E[e_{i+1} - e_i]. \quad (2-25)$$

The simplification of the equation which results from the substitution of Equations (2-23) through (2-25) into Equation (2-9) yields

$$Y_{loc}(X_{i+1}) - Y_{loc}(X_i) = [Y_X(X_0)E - C^T \lambda] [e_{i+1} - e_i] + \frac{1}{2} e_{i+1}^T \lambda e_{i+1} - \frac{1}{2} e_i^T \lambda e_i. \quad (2-26)$$

The new value in the e coordinate system as predicted by going in the negative gradient direction can be found by substituting Equations (2-23) and (2-25) into Equation (2-8).

The change of each of the individual components of the e coordinate system can be written by using a double subscript notation. The first subscript indicates the iteration number, and the second subscript indicates the component of the e coordinate vector. The resulting equations are:

$$e_{i+1,j} = [1 - K \lambda_j] e_{i,j} \quad ; \quad j = 1, 2, \dots, P+N \quad (2-27)$$

and

$$e_{i+1,j} = e_{i,j} - K E_j^T Y_X(X_0) \quad ; \quad j = P+N+1, \dots, M. \quad (2-28)$$

The substitution of Equations (2-27), (2-28), (2-15), and (2-16) into Equation (2-26) will yield the final desired form which predicts the resulting magnitude change of the scalar function in going from the i^{th} iteration point, X_i , to the point X_{i+1} in the negative gradient direction. The resulting equation is

$$Y_{\text{loc}}(X_{i+1}) - Y_{\text{loc}}(X_i) = \quad (2-29)$$

$$- \frac{K}{2} \sum_{j=1}^{P+N} [(2 - K \lambda_j) \lambda_j^2 e_{i,j}^2] - K \sum_{j=P+N+1}^M [Y_X(X_0) E_j]^2.$$

The systematic investigation of Equations (2-27), (2-28), and (2-29) enables one to envision an algebraic minimization procedure which is very general.

From Equation (2-27), it is noted that the first $P+N$ components of the e coordinate vector will never move from the value of zero once they become zero. This is true

regardless of the distance traveled in the gradient direction.

The method utilized for proceeding to the minimum of an algebraic function should be such that after each step in the negative gradient direction one will be at a smaller value for the scalar function. Hence, the magnitude chosen for K should be such that the predicted change of the scalar function, Equation (2-29), will be negative.

On the very first step in the negative gradient direction X_i will equal X_0 , the point at which the gradient vector and the matrix of second partial derivatives was evaluated. By setting $K = 1/\lambda_1$, the change predicted by Equation (2-29) is negative since each of the terms $(2 - K\lambda_j)$ will be positive. Equation (2-27) states that the first component of the e coordinate should become equal to zero on this first iterative step.

On the second iterative step, one proceeds in the predicted negative gradient direction, Equation (2-5), with the magnitude of K set at $K = 1/\lambda_2$. The first component of the e coordinate system was set equal to zero on the first iterative step, and Equation (2-27) states that the second component of e should become equal to zero on the second iterative step. Equation (2-29) predicts a negative change of the scalar function on this second iterative step since $(2 - K\lambda_j)$ is positive for $j = 2, 3, \dots, P$ and since component one of the e vector should be zero.

By proceeding in the general manner outlined in the

previous paragraphs, the first $P-1$ components of the e vector will be zero on the P^{th} iteration, and Equation (2-29) predicts a negative change of the scalar function on the P^{th} iteration since $(2-K\lambda_j)$ is positive for $j = P, \dots, P+N$.

After P iterations the first P components of the e coordinate system should be zero. Hence, on the $P+1^{\text{th}}$ iteration, K should be chosen as any positive value instead of $1/\lambda_{P+1}$ which would be a negative value. Equation (2-29) indicates that the magnitude of the predicted change of the scalar function will continue to increase negatively as K becomes a larger positive value. This due to the fact that the quantity $(2-K\lambda_j)$ will be positive for $j = P+1, \dots, P+N$, since all of the corresponding values for the λ_j will be negative. Hence, on the $P+1^{\text{th}}$ iteration, the value of K will be increased until the actual value of scalar function ceases to decrease. This will probably occur due to the fact that the change as predicted by Equation (2-29) is based upon the truncated Taylor series approximation for the function in question. In general, this approximation is not valid in a global sense. It is, however, a good approximation in the vicinity of X_0 .

Before presenting a flow chart of a minimization procedure based upon the equations that have thus far been derived, there are still two issues which should be clarified. First, it is desirable to understand the significance of the transformations which were performed in order to

obtain Equation (2-19). Second, it is informative to demonstrate that the method of principal planes will tend to follow a valley to the desired minimum. The second statement will be verified by the solution of the example problem called Rosenbrock's curved valley in the example problem section.

To better understand the coordinate transformations, it will be informative to substitute Equations (2-15), (2-16), and (2-23) into Equation (2-4). The local approximation for the scalar function becomes

$$Y_{\text{loc}}(X_i) = Y(X_0) - \frac{1}{2} \sum_{j=1}^{P+N} \frac{(Y_X(X_0)E_j)^2}{\lambda_j} + \quad (2-30)$$

$$\sum_{j=P+N+1}^M Y_X E_j e_{i,j} + \frac{1}{2} \sum_{j=1}^{P+N} \lambda_j e_{i,j}^2.$$

If, in addition, the point, X_0 , is such that the second partial matrix has all positive eigenvalues, then the inverse of Y_{XX} exists and Equation (2-30) will simplify to

$$Y_{\text{loc}}(X_i) = Y_{\text{loc}}(X_{\text{ext}}) + \frac{1}{2} \sum_{j=1}^P \lambda_j e_{i,j}^2. \quad (2-31)$$

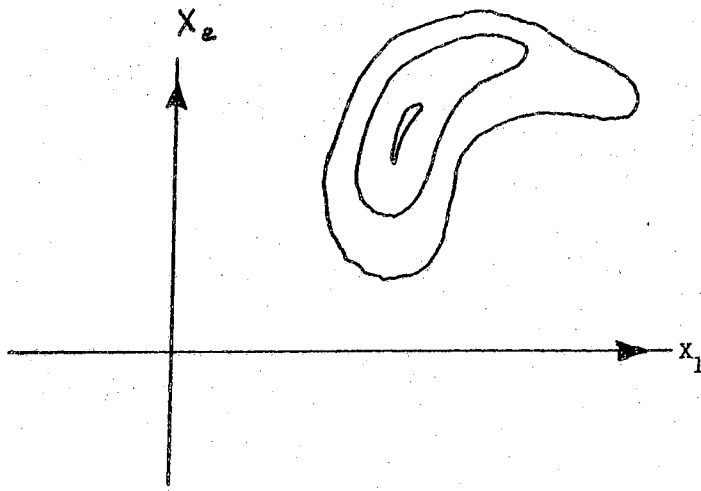
In Equation (2-31), the term $Y_{\text{loc}}(X_{\text{ext}})$ is the value of Equation (2-4) evaluated at its extremum point. Hence, under the assumption that all of the eigenvalues are positive, the truncated Taylor series approximation for the scalar

function in the vicinity of X_0 is an ellipsoid in M dimensional space. This is shown in Figure 10 for the case of $M = 2$.

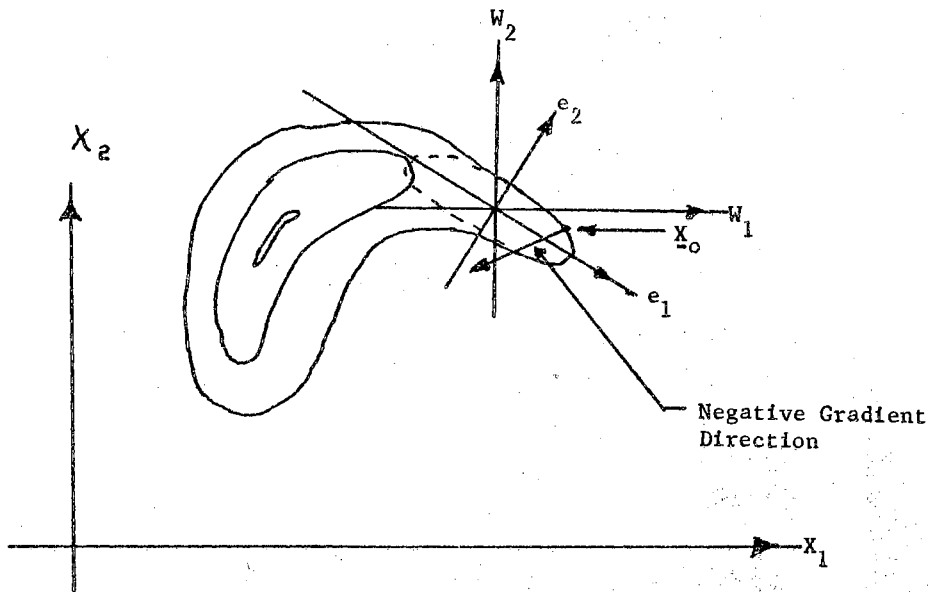
In part A of Figure 10, lines of constant contours for the hypothetical function under consideration have been drawn. The scalar function has a valley which curves from the extremum point upward and to the right. In part B of Figure 10, a line of constant contour that is predicted by the truncated Taylor series is shown as a dotted line. The magnitude predicted for the scalar function along this line of constant contour is $Y(X_0)$, and the predicted constant contour line is an ellipse.

The first coordinate transformation that was performed, Equation (2-14), was a transformation to the center of the ellipse which approximates the constant contour line at the point X_0 . These axes are denoted by W_1 and W_2 in part B of Figure 10. The next coordinate transformation which was performed was to rotate the axes as indicated by Equation (2-19). From Equation (2-31), it is known that the e coordinate system corresponds to the major axes of the ellipsoids which approximate the lines of constant contour for the scalar function. In part B of Figure 10, the e_1 and e_2 coordinates represent this new coordinate system and they correspond to the major and minor axes of the ellipse.

It is noted that the constant contour line predicted by the Taylor series in part B of Figure 9 is a good approximation in the vicinity of X_0 . However, the approximation



A. Contours of Constant Magnitude for Hypothetical Function



B. Diagram showing the co-ordinate transformations. The dotted line is the truncated Taylor series approximation for the constant contour line passing through X_0 .

Figure 10. Figure Demonstrating Meaning of the Coordinate Transformations

for the scalar function is not valid globally since the extremum point as predicted by the approximation is at the point where the axes e_1 and e_2 intersect. The true extremum point for the hypothetical function is located to the left and below this point.

The e_1 axis runs essentially parallel to the valley of the hypothetical function in the neighborhood of X_0 . For this particular problem, if one proceeds in the negative gradient direction to the point of intersection of the e_1 axis, one will be located in the immediate neighborhood of the true valley.

A desirable characteristic of a scalar minimization computational procedure is that it be able to locate a valley of the scalar function and follow the valley to the minimum. This seems to be the characteristic of the method of seeking principal planes.

The flow chart for the method of seeking principal planes is presented in Figure 11. It indicates that the first step in the minimization problem is to determine the value of the scalar function, the gradient vector, and the matrix of second partial derivatives at the initial point, X_0 .

The eigenvalues of the matrix of second partial derivatives are then determined.

Equation (2-7) gives the values of the independent variables by sequentially setting $K = 1/\lambda_i$, $i = 1, \dots, P$. It is necessary after each of these steps in the local

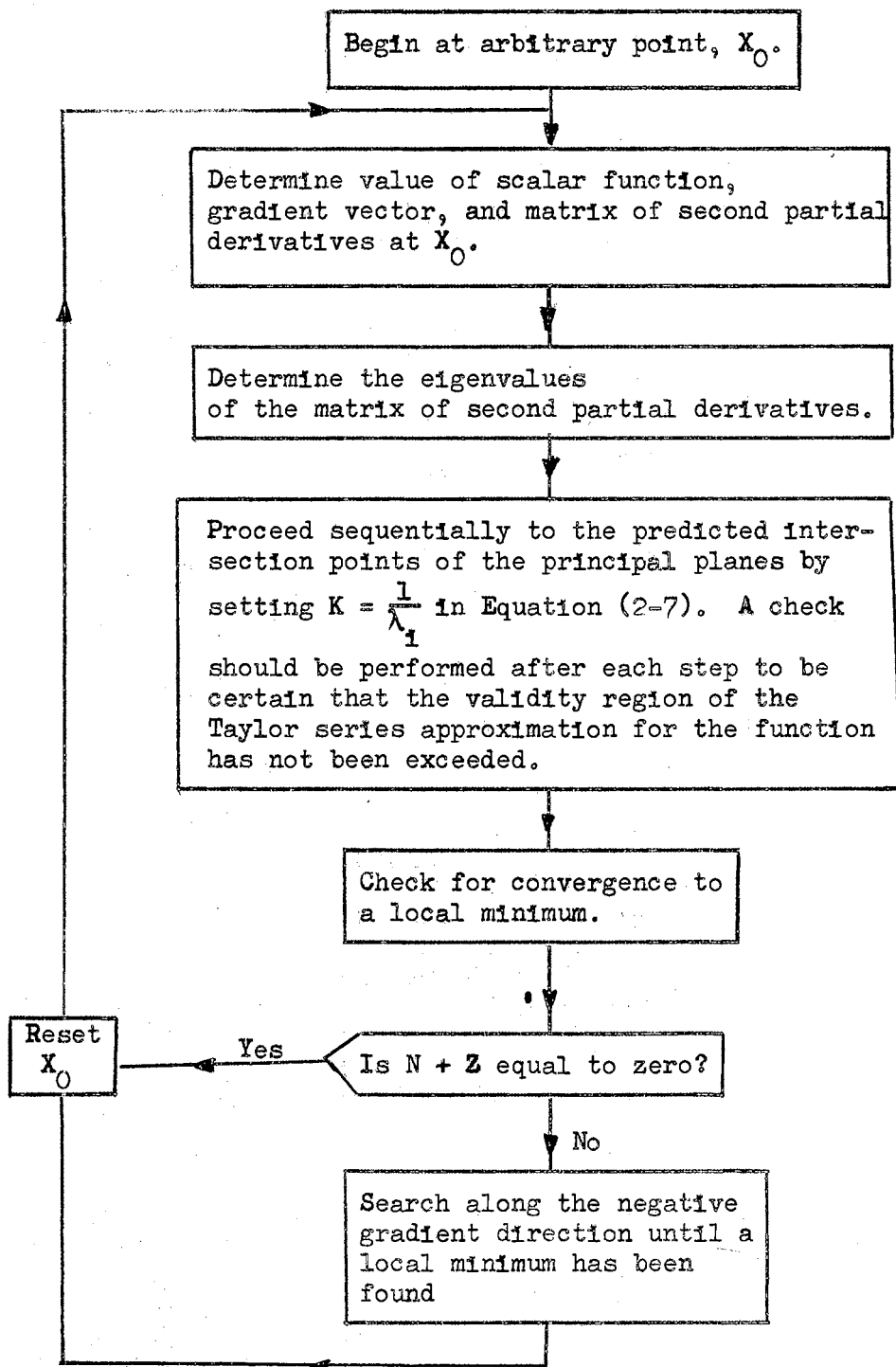


Figure 11. Flow Chart for the Minimization of a Scalar Function by the Method of Seeking Principal Planes

negative gradient direction to determine if the region of validity of the Taylor series approximation has been exceeded. If the scalar function increases after one of the steps or if the actual change of the scalar function is significantly different from the predicted change of the scalar function, the validity region has been exceeded.

A check for convergence is performed after having successfully proceeded P sequential steps in the negative gradient direction. A standard method for checking for convergence to a local minimum to determine if the magnitude of the gradient vector is equal to zero.

The next block in Figure 11 indicates a logic check to determine if the matrix of second partial derivatives has some zero or negative eigenvalues. If N plus Z is equal to zero, X_0 is reset to the present value of the independent vector and the minimization algorithm is reinitiated. When N plus Z is not equal to zero, a search is performed along the negative gradient direction until a local minimum is located. The value of X_0 is reset to the value of the independent variable at the local minimum, and the minimization procedure is reinitiated.

The method of seeking principal planes can be used for solving a system of algebraic equations. The insight obtained by studying this problem helps to explain why existing methods for solving two-point boundary value problems and for identifying the parameters of dynamical systems have not been completely satisfactory. Chapters III and IV will

refer to some of the results presented in the following section.

Solution of Systems of Algebraic Equations

The simplest set of algebraic equations which exist is the linear problem given by

$$AX = b. \quad (2-32)$$

In the above equation, A is an $M \times M$ matrix of constants; X is a vector of independent variables of dimension M; and b is a vector of constants of dimension M.

In order to formulate Equation (2-32) as a minimization problem, the following scalar function is defined:

$$Y(X) = \frac{1}{2}[AX - b]^T W[AX - b]. \quad (2-33)$$

In the above equation, W is a symmetric positive definite $M \times M$ matrix. It is not uncommon for W to be chosen as the identity matrix.

Since Equation (2-33) is a quadratic equation, the Taylor series which utilizes the first two terms will describe it exactly. This means that the method of principal planes as described in the previous section will be an exact method for the solution of the minimum of Equation (2-28) if roundoff error within the digital computer is ignored.

The equation for the gradient and matrix of second partial derivatives of Equation (2-33) are:

$$Y_X(X) = -b^T W A + X^T A^T W A \quad (2-34)$$

and

$$Y_{XX}(X) = A^T W A. \quad (2-35)$$

One good characteristic of the method of seeking principal planes is that if a solution for Equation (2-33) exists it will be found even in the situation where the matrix A is singular. If the matrix A is singular, there exists either no solution or an infinite number of solutions to Equation (2-33). When the solution is not unique, the solution which is found by the method of seeking principal planes depends upon the initial guess which the user provides for independent variable vector, X. It should be noted that if the user does not know a good approximation for the solution to Equation (2-33), the initial guess of $X = 0$ can always be used. In the situation where A is singular and Equation (2-33) does not have an exact solution, the method of seeking principal planes will provide a solution which minimizes Equation (2-33). If W is the identity matrix, this will be the best fit in the least square error sense.

Since the method of seeking principal planes is able to provide a solution even in the situation where A is singular, it is reasonable that this method should be a good solution technique for cases in which A is ill conditioned.

The independent variable which minimizes Equation (2-33) provides an approximate solution for Equation (2-32)

in the overconstrained case. This is the situation where A is a $R \times M$ constant matrix; X is the independent vector of M dimension; b is a constant vector of dimension R ; and R is larger than M . This set of equations does not have an exact solution except in special cases. If the matrix W is the identity matrix, the solution yielded by the method of seeking principal planes will be a "best" solution in the least square error sense.

In engineering and mathematical analysis, the need for solving a set of simultaneous nonlinear algebraic equations often arises. In mathematical terms, this means that it is necessary to determine a M dimensional independent vector, X , such that the M dimensional vector valued function, G , becomes equal to the zero vector.

$$G(X) = 0. \quad (2-36)$$

This problem can be treated in a manner similar to that used for the solution of linear algebraic equations. Hence, the scalar function,

$$Y(X) = \frac{1}{2} G(X)^T G(X), \quad (2-37)$$

is formed.

Since Equation (2-37) can never be less than zero, and the only points at which it can be exactly equal to zero are solution points, a minimization procedure can be used to determine the solution for Equation (2-36).

The first and second partial derivatives for the scalar

function need to be formulated. To write these equations, the following definitions are needed.

$$G_X(X) = \begin{bmatrix} \frac{\partial G_1}{\partial X_1} & \cdots & \frac{\partial G_1}{\partial X_M} \\ \vdots & & \vdots \\ \frac{\partial G_M}{\partial X_1} & \cdots & \frac{\partial G_M}{\partial X_M} \end{bmatrix} \quad (2-38)$$

$$B_j = \left[\frac{\partial}{\partial X_j} G_X(X)^T \right] G; \quad j = 1, 2, \dots, M \quad (2-39)$$

$$B = [B_1, \dots, B_M]. \quad (2-40)$$

The gradient vector and matrix of second partial derivatives then become

$$Y_X(X) = G(X)^T G_X(X) \quad (2-41)$$

and,

$$Y_{XX}(X) = G_X(X)^T G_X(X) + B. \quad (2-42)$$

Equations (2-37), (2-41), and (2-42) are the equations which are needed to use the method of seeking principal planes.

From Equation (2-39), it is noted that if one is quite close to the solution for Equation (2-36), the second half of Equation (2-42) will approach the zero matrix. Hence, in the neighborhood of the solution for the nonlinear set of

algebraic equations, the second partial matrix can be approximate by the simpler expression,

$$\underset{\text{Approx}}{Y_{XX}} = G_X^T G_X. \quad (2-43)$$

The reason for formulating Equation (2-43) is to demonstrate how the method of seeking principal planes is related to Gauss's method for least squares analysis as presented in Wilde and Beightler (10), and how it is related to the Newton-Raphson method as presented by Bellman and Kalaba (11).

The method of seeking principle planes will reach the extremum of the truncated Taylor series approximation for the scalar function in M iterative steps. The value for this extremum point can be approximated by substituting Equation (2-41) and (2-43) into Equation (2-2).

$$X = X_0 - [G_X(X_0)^T G_X(X_0)]^{-1} G_X(X_0)^T G(X_0). \quad (2-44)$$

If the Jacobian matrix, $G_X(X_0)$, is not singular, it can be shown that

$$[G_X(X_0)^T G_X(X_0)]^{-1} = G_X(X_0)^{-1} [G_X(X_0)^T]^{-1}. \quad (2-45)$$

Upon the substitution of Equation (2-45) into (2-44), the following equation is obtained:

$$X = X_0 - G_X(X_0)^{-1} G(X_0). \quad (2-46)$$

Equation (2-46) is the same as the Newton-Raphson method as presented by Bellman and Kalaba (11). Hence, in final convergence, the method of seeking principal planes behaves in the same manner as the Newton-Raphson technique for the solution of a set of nonlinear algebraic equations. This is a desirable characteristic since the Newton-Raphson method is very rapid in final convergence.

In Gauss's method for least squares analysis, the dimension of the vector G in Equation (2-36) will be larger than the dimension of the independent variable X . Hence, in general, it is not possible to find a solution such that Equation (2-36) will be satisfied exactly. A vector X can be determined such that the set of algebraic equations are satisfied in the least square error sense by minimizing Equation (2-37).

The iterative equation which Gauss uses for determining the minimum of Equation (2-37) is given by Equation (2-44). Equation (2-44) was obtained by assuming that the matrix of second partial derivatives as given by Equation (2-42) could be approximated by neglecting the term given by matrix B . For the situation where the system of equations can be satisfied exactly, Equation (2-39) indicates that matrix B will be the zero matrix at the minimum point; and it is legitimate within the neighborhood of a solution to approximate the matrix of second partial derivatives by neglecting the B matrix.

However, when the vector G is of larger dimension than

X, Equation (2-36) cannot, in general, be satisfied exactly. If the point which minimizes Equation (2-37) is actually a very poor solution for the original set of nonlinear equations, the matrix B may be a very significant portion of the matrix of second partial derivatives even at the exact location of a minimum point. In Appendix C, a mathematical proof is presented which demonstrates that Gauss's method as given by Equation (2-44) will under certain circumstances not converge to a minimum point regardless of how close to the minimum point one is. An example problem is given in the following section which demonstrates this characteristic.

A direct comparison of the computational effort required for all three methods is presented in Table I. The method of seeking principal planes required more computational time than the DFMFP and DFMCG methods. This was primarily due to using the analytic differentiation computation algorithm which is given in Appendix A within the SEEK algorithm. The equations generated by the analytic differentiation algorithm execute slower than standard Fortran IV statements.

Example Problems

Within this section, five example problems will be worked using the computational algorithm presented in Appendix B. The example problems have been specially chosen to demonstrate the widely varying capabilities of the method of seeking principal planes (SEEK).

TABLE I
COMPARISONS OF COMPUTATIONAL EFFORT REQUIRED
FOR EACH OF THE EXAMPLE PROBLEMS

		Analytical Minimum of Function	Value of Function at Termination of Program	Number of Function Evaluations	Number of Gradient Evaluations	Number of Matrix of Second Partial Derivatives Evaluations
Example 1	SEEK	0.0	0.0	2	2	1
	DFMFP		$.197 \times 10^{-29}$	17	17	None
	DFMCG		$.739 \times 10^{-30}$	25	25	None
Example 2	SEEK	0.0	$.426 \times 10^{-5}$	44	23	18
	DFMCG	0.0	$.312 \times 10^{-26}$	73	73	None
	DFMFP	0.0	$.818 \times 10^{-31}$	176	176	None
Example 3	SEEK	0.0	$.450 \times 10^{-14}$	37	15	11
	DFMCG	0.0	$.170 \times 10^{-27}$	107	107	None
	DFMFP	0.0	$.194 \times 10^{-69}$	87	87	None
Example 4	SEEK	0.0	$.211 \times 10^{-8}$	69	21	21
	DFMCG	0.0	$.534 \times 10^{-23}$	413	413	None
	DFMFP	0.0	$.260 \times 10^{-28}$	395	395	None
Example 5	SEEK		1.767037	7	3	3
	DFMCG		1.767037	37	37	None
	DFMFP		1.767037	183	183	None

The method of conjugate gradients is also a very powerful minimization technique. IBM has supplied two minimization programs in their Scientific Subroutine Package which are based on the conjugate gradient method as presented by Fletcher and Reeves (8). These programs are called DFMEP and DFMEG, and they require that the user provide an estimate for the minimum of the function (EST) and a value called EPS which is used to determine if final convergence has been obtained. The values of EST = 0.0 and EPS = 10.0^{-15} were used to generate the data which are presented in Table I. The SEEK algorithm is considered to have converged when the absolute value of each component of the gradient vector is less than 10^{-8} .

The first example problem is that of seeking the solution for a set of linear algebraic equations. The equations were specially chosen so that the matrix would be singular. The matrix A and the vector b were defined as

$$A = \begin{bmatrix} 1 & 2 & 3 & 4 \\ 5 & 6 & 7 & 8 \\ 9 & 10 & 11 & 12 \\ 13 & 14 & 15 & 16 \end{bmatrix} \quad b = \begin{bmatrix} 1 \\ 2 \\ 3 \\ 4 \end{bmatrix} \quad (2-47)$$

Each of the algorithms determined an exact solution for the linear equation by minimizing

$$Y = [AX - b]^T [AX - b]. \quad (2-48)$$

By starting from the point $X = (0,0,0,0)$, the solution $X = (-.05, .025, .1, .175)$ was found.

Table I indicates that the SEEK algorithm had to

evaluate the scalar function three times, the gradient of the scalar function twice, and the matrix of second partial derivatives once in order to determine a minimum point for Equation (2-48).

The computational effort which was required for the DFMCg and DFMEP algorithms is also given in Table I. This information is perhaps a little misleading since both DFMCg and DFMEP had reached the exact solution in four iterations. However, their convergence criteria did not terminate the program until after 17 and 25 iterations, respectively.

The second example which was worked is referred to by Fletcher and Reeves (8) as Rosenbrocks curved valley and its equation is

$$Y = 100.0 * (X_2 - X_1^2)^2 + (1 - X_1)^2. \quad (2-49)$$

In part A of Figure 12 a rough sketch of some lines of constant contour for Equation (2-49) are given. It can be seen that the function has a "valley" which curves from the point (-1, 1) through the origin to the point (1, 1). In part B of Figure 12 the locus of points which the SEEK algorithm traversed as it proceeded to the minimum point (1.0, 1.0) from the point (-1.2, 1.0) is given. It can be seen that the SEEK algorithm follows the "valley" to the minimum.

The third example Fletcher and Reeves (8) refer to as the helical curved valley, and its equation is

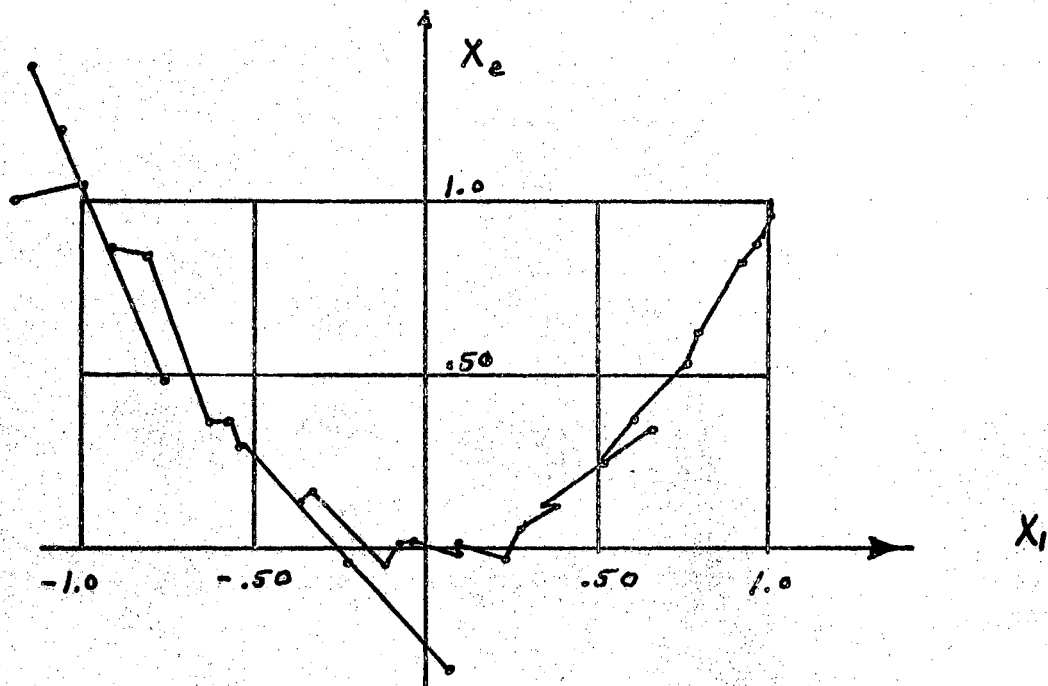
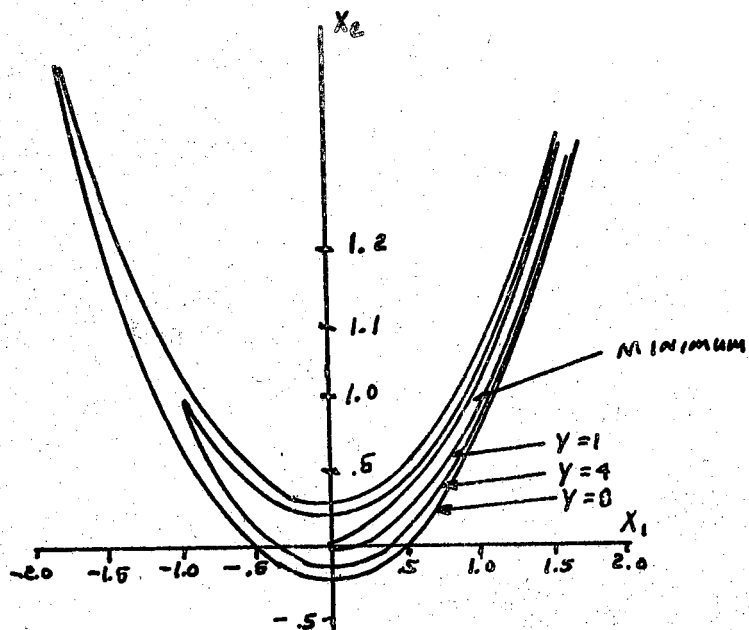


Figure 12. Solution for Rosenbrock's Curved Valley Problem

$$Y = 100.0 * (X_3 - 10.0 \cdot \text{TAN}^{-1}(X_2/X_1)/2\pi)^2 + \quad (2-50)$$

$$100.0 * (\sqrt{X_1^2 + X_2^2} - 1.0)^2 + X_3^2 \quad \text{if } X_1 > 0$$

$$Y = 100.0 * (X_3 - 10.0 (\text{TAN}^{-1}(X_2/X_1)/2\pi + .50))^2 +$$

$$100.0 * (\sqrt{X_1^2 + X_2^2} - 1.0)^2 + X_3^2 \quad \text{if } X_1 < 0.$$

The information given in Table I was generated by starting at the point (-1.0, 0.0, 0.0).

The fourth example worked was

$$Y = (X_1 + 10 X_2)^2 + 5(X_3 - X_4)^2 + (X_2 - 2 X_3)^4 + \\ + 10(X_1 - X_4)^4. \quad (2-51)$$

The information given in Table I was generated by starting at the point (3.0, -1.0, 0.0, 1.0).

The fifth example which was worked was that of determining the "best" solution of the following set of algebraic equations.

$$G_1 = X_1^2 + X_2^2 + .8786271 = 0$$

$$G_2 = .5^2 X_1^2 + X_2^2 + .8786271 = 0 \quad (2-52)$$

$$G_3 = X_1 - X_2 + .6207711 = 0.$$

A "best" solution in the least square error sense was determined by minimizing the function

$$Y = G_1^2 + G_2^2 + G_3^2. \quad (2-53)$$

It was found that the point $(-.159, .100)$ provides a local minimum for Equation (2-53). The information given in Table I was generated by starting from $(-.10, .05)$.

The eigenvalues for the matrix $Q^T Q$ when evaluated at the point $(-.159, .100)$ are 4.596×10^4 and 1.562. The matrix Q is defined in Appendix C. Since both of these eigenvalues are greater than one, Gauss's method will not converge to the solution point $(-.159, .10)$ regardless of how close to that solution point one starts. This example will be discussed in more detail in Chapter IV.

From the results which are presented in Table I, it is noted that deflected gradient methods often require many more evaluations of the function and its gradient than the SEEK algorithm. However, the SEEK algorithm requires the computation of the matrix of second partial derivatives.

In the final analysis, it is debatable if the method of seeking principal planes requires less computational effort than the DFMCG and DFMP algorithms. However, it provides valuable additional information since the eigenvalues of the matrix of second partial derivatives are computed. If all of the eigenvalues are positive when a converged solution is obtained, then Athans and Falb (9) state on page 227 that this provides both the necessary and sufficient conditions for a local minimum of the scalar function.

This chapter completely developed the method of seeking principal planes for the problem of determining the minimum of a function of several variables. In the next chapter,

the method of seeking principal planes is applied to two-point boundary value problems. This is a significant topic since optimal control theory can be used to convert a system design or identification problem into a two-point boundary value problem.

CHAPTER III

PARAMETER IDENTIFICATION FORMULATED AS

A TWO-POINT BOUNDARY VALUE PROBLEM

The problem of parameter identification of dynamical systems can be reformulated as a two-point boundary value problem through the use of optimal control theory. In general, the first necessary conditions of optimal control theory for dynamical systems result in a two-point boundary value problem. An efficient solution technique for the two-point boundary value problem is necessary.

At present the basic methods for the solution of two-point boundary value problems are perturbation, quasilinearization, and deflected gradient. These are iterative procedures in which the missing initial conditions are guessed, and the differential equations are integrated out to the final time. On the basis of the information that has been obtained by integrating the differential equations, the initial conditions are changed. The amount and manner in which these initial conditions are changed separate the procedures from one another.

Lewallen, Tapley, and Williams (12) have investigated the quasilinearization and perturbation procedures in considerable detail. After reviewing their paper, it was

decided that it would be desirable to have a gradient technique in which the size of the step in the gradient direction was determined by some systematic method.

The method of seeking principal planes as was presented in Chapter II for the solution of algebraic minimization problems does have the desirable characteristic of a systematic step selection in the negative gradient direction. In this chapter, it will be shown that the two-point boundary value problem can be reformulated into a scalar minimization problem. Hence, the method of seeking principal planes can be used for the solution of two-point boundary value problems.

Statement of Parameter Identification Problems

It is assumed that a mathematical model for the system has been formulated and written in state variable notation,

$$\dot{X} = F(X, P, t). \quad (3-1)$$

In the above equation, X is the N dimensional state variable, P is an M dimensional parameter vector, and t is the independent variable, time.

The initial condition vector is partitioned as

$$X(t_0) = \begin{bmatrix} \psi \\ X_0 \end{bmatrix} \begin{array}{l} \text{unknown} \\ \text{known.} \end{array} \quad (3-2)$$

In the above equation, ψ is a K dimensional vector of

unknown initial conditions, and X_0 is an N-K dimensional vector of the known initial conditions.

The entire parameter vector is unknown.

$$P = \text{unknown} \quad (3-3)$$

Values for the parameter vector, P, and the unknown initial conditions, ψ , need to be determined which will provide a local minimum for the performance index.

$$PI = \int_{t_0}^{t_f} G(X, t) dt. \quad (3-4)$$

Optimal control theory is presented by Athans and Falb (9) reformulates the problem presented by Equations (3-1) through (3-4) as a two-point boundary value problem. The dynamical equations which must be satisfied are:

$$\dot{X} = F(X, P, t) \quad (3-5)$$

$$\dot{P} = 0 \quad (3-6)$$

$$\dot{\lambda} = -G_X^T - F_X^T \lambda \quad (3-7)$$

$$\dot{\mu} = -F_P \lambda. \quad (3-8)$$

λ is an N dimensional vector; μ is a K dimensional vector; and G_X , G_P , F_X , and F_P are defined as:

$$G_X = \left[\frac{\partial G}{\partial X_1}, \dots, \frac{\partial G}{\partial X_M} \right], \quad (3-9)$$

$$F_X = \begin{bmatrix} \frac{\partial F_1}{\partial X_1} & \cdots & \frac{\partial F_1}{\partial X_N} \\ \vdots & & \\ \frac{\partial F_N}{\partial X_1} & \cdots & \frac{\partial F_N}{\partial X_N} \end{bmatrix}, \quad (3-11)$$

and

$$F_P = \begin{bmatrix} \frac{\partial F_1}{\partial P_1} & \cdots & \frac{\partial F_1}{\partial P_M} \\ \vdots & & \\ \frac{\partial F_N}{\partial P_1} & \cdots & \frac{\partial F_N}{\partial P_M} \end{bmatrix}. \quad (3-12)$$

The boundary conditions which Equations (3-5) through (3-8) must satisfy are:

$$X(t_0) = \begin{bmatrix} \psi \\ X_0 \end{bmatrix} \begin{array}{l} \text{- free} \\ \text{- specified} \end{array} \quad \begin{array}{l} X(t_f) = \text{- free} \\ P(t_f) = \text{- free} \end{array} \quad (3-13)$$

$$P(t_0) = \text{free}$$

$$\lambda(t_0) = \left. \begin{bmatrix} 0 \\ \lambda_{K+1}(t_0) \\ \vdots \\ \lambda_N(t_0) \end{bmatrix} \right\} \begin{array}{l} \text{- specified} \\ \text{free} \end{array} \quad \begin{array}{l} \lambda(t_f) = 0 \text{ - specified} \\ \mu(t_f) = 0 \text{ - specified} \end{array}$$

$$\mu(t_0) = 0 \quad \text{- specified}$$

The parameter identification problem has now been restated as a two-point boundary value problem. Equations (3-5) through (3-8) are the $2(N+M)$ first order dynamical equations which must be satisfied, and Equation (3-13) provides the set of $2(N+M)$ boundary conditions.

The following section outlines a method for solving a general two-point boundary value problem. The special two-point boundary value problem presented in this section falls within the framework of the material presented in the next section.

Statement of Two-Point Boundary Value Problem

The dynamical equations for the system are:

$$\dot{X} = F(X, t). \quad (3-14)$$

In the above equation, X is an N dimensional vector of dependent variables, and F is an N dimensional vector which is a function of the dependent variables and the independent variable, t .

The initial condition vector is partitioned as

$$X(t_0) = \begin{bmatrix} \psi \\ X_0 \end{bmatrix} \begin{array}{l} \text{- unknown} \\ \text{- known.} \end{array} \quad (3-15)$$

In the above equation, ψ is a K dimensional vector of unknown initial condition, and X_0 is an $N-K$ dimensional vector of known initial conditions.

The desired final boundary condition vector is

$$H(X)_{t_f} = 0. \quad (3-16)$$

H is a K dimensional vector. Each of the individual components of H can be written explicitly as a function of the components of the state vector evaluated at the specified final time, t_f .

Equations (3-14), (3-15), and (3-16) are a precise statement of the problem which needs now to be solved.

The relation between the problem statement in this and the previous one is clarified by noting that:

X
of this
section =

$$\begin{bmatrix} X_1 \\ \vdots \\ X_K \\ \lambda_{K+1} \\ \vdots \\ \lambda_N \\ P \\ \lambda_1 \\ \vdots \\ \lambda_K \\ X_{K+1} \\ \vdots \\ X_N \\ \mu \end{bmatrix}$$

of the previous
section

$$\begin{array}{l}
 H_{\text{of this}} \\
 \text{section}
 \end{array}
 =
 \begin{array}{c}
 \left[\begin{array}{c}
 X_{K+1} \\
 \vdots \\
 X_N \\
 X_{N+K+1} \\
 \vdots \\
 X_{N+2K} \\
 X_{N+1} \\
 \vdots \\
 X_{N+K} \\
 X_{N+2K+1} \\
 \vdots \\
 X_{2N+2K}
 \end{array} \right]
 \end{array}
 =
 \begin{array}{c}
 \left[\begin{array}{c}
 \lambda \\
 \mu
 \end{array} \right]
 \end{array}
 = 0
 \begin{array}{c}
 \text{of the previous} \\
 \text{section}
 \end{array}
 \end{array}
 \begin{array}{c}
 \text{of this section}
 \end{array}$$

$$\begin{array}{c}
 N_{\text{of this}} \\
 \text{section}
 \end{array}
 = 2(N+K)
 \begin{array}{c}
 \text{of the previous} \\
 \text{section}
 \end{array}$$

$$\begin{array}{c}
 K_{\text{of this}} \\
 \text{section}
 \end{array}
 = 2K
 \begin{array}{c}
 \text{of the previous} \\
 \text{section.}
 \end{array}$$

Sometimes the final boundary condition which results from optimal control theory is not precisely of the form given by Equation (3-16). This occurs when the final time is not specified in advance. Then, the final boundary condition is of the form

$$H(X, t) = 0. \tag{3-17}$$

To handle this problem two new state variables and a new independent variable, τ , are now introduced. Their

interrelations are given by Equations (3-18) through (3-23).

$$X_{N+1} = t - t_0 \quad (3-18)$$

$$X_{N+2} = \text{constant} \quad (3-19)$$

$$\tau = X_{N+1}/X_{N+2} = (t - t_0)/X_{N+2} \quad (3-20)$$

$$dt = X_{N+2} d\tau \quad (3-21)$$

$$dX_{N+1}/d\tau = X_{N+2} \quad (3-22)$$

$$dX_{N+2}/d\tau = 0. \quad (3-23)$$

Equation (3-24) results from substituting Equations (3-21) and (3-18) into Equation (3-23). Equations (3-22) and (3-23) are rewritten immediately below Equation (3-24) to provide the following complete set of dynamical equations.

$$dX/d\tau = X_{N+2} F(X, X_{N+1} + t_0) \quad (3-24)$$

$$dX_{N+1}/d\tau = X_{N+2} \quad (3-25)$$

$$dX_{N+2}/d\tau = 0. \quad (3-26)$$

The substitution of Equation (3-18) into (3-17) yields

$$H(X, X_{N+1} + t_0). \quad (3-27)$$

Equations (3-24) through (3-27) are equivalent in form to Equations (3-14) and (3-16). Hence, any method which

will solve the two-point boundary value problem presented at the start of this section can also be used to solve problems which have final boundary conditions of the form given by Equation (3-17).

Solution of Two-Point Boundary Value Problem by Method of Seeking Principal Planes

The method of seeking principal planes was developed in Chapter II for the minimization of a scalar function. The two-point boundary value problem can be converted into an algebraic minimization problem by defining the following scalar performance function.

$$Y(X(\psi)) = \frac{1}{2} H^T(X(\psi)) H(X(\psi))_{t_f}. \quad (3-28)$$

The scalar quantity, Y , is explicitly a function of the state vector, X , and implicitly a function of the unknown initial conditions, ψ .

This is more easily understood by studying the first two blocks of Figure 13. As the figure indicates the first step in the procedure for determining the value of the scalar function is to make a guess for the unknown initial conditions. The second step of the procedure is to numerically integrate the dynamical equations from the initial time to the final time, t_f . Hence, the value of the state vector at the final time is a function of ψ . Once the value of the state vector at the final time is known, the value for the scalar performance function can be

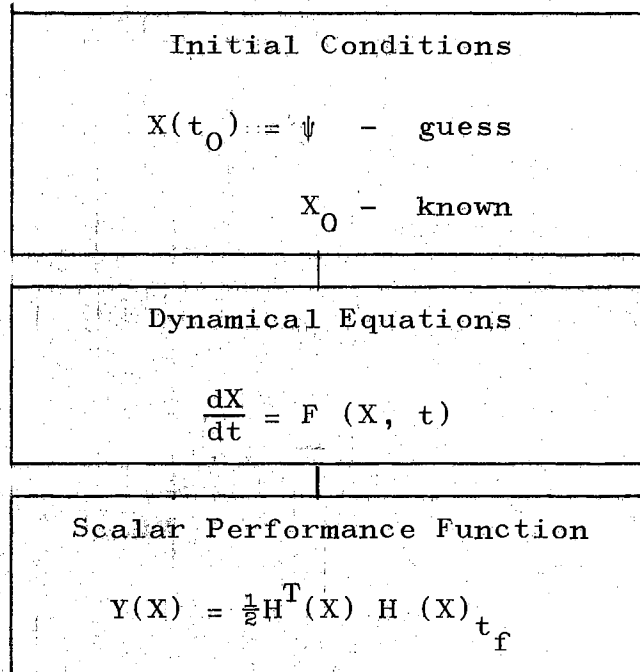


Figure 13. Equations Required to Determine the Value of the Scalar Performance Function

evaluated as indicated in block three of Figure 13. The equation for the scalar performance function is an explicit function of the state vector, X . But since the state vector is in turn a function of the unknown initial condition, ψ , the scalar performance function is implicitly a function of ψ .

The value of the scalar performance function must always be greater than or equal to zero since it is constructed as the sum of the components of the final boundary condition squared. If the scalar performance function equals zero, a solution for the two-point boundary value problem has been obtained.

The method of seeking principal planes requires computation of the gradient and the matrix of second partial derivatives of the scalar performance function.

In Figure 14 the necessary equations for determining the gradient of the scalar performance function are given. The notation used is

$$X_{\psi_i} = \frac{\partial X}{\partial \psi_i} \quad (3-29)$$

$$F_X = \begin{bmatrix} \frac{\partial F_1}{\partial X_1} & \dots & \frac{\partial F_1}{\partial X_N} \\ \vdots & & \vdots \\ \frac{\partial F_N}{\partial X_1} & \dots & \frac{\partial F_N}{\partial X_N} \end{bmatrix} \quad (3-30)$$

Initial Conditions for Dynamical Equations

$$X(t_0) = \psi \quad - \text{guess}$$

$$X_0 \quad - \text{known}$$

$$X_{\psi_i} = \begin{matrix} 0 & & i = 1, 2, \dots, K \\ 0 & & \\ 1 & \text{row } i & \\ 0 & & \\ 0 & & \end{matrix}$$

Dynamical Equations

$$\frac{dX}{dt} = F(X, t)$$

$$\frac{dX_{\psi_i}}{dt} = F_X X_{\psi_i} \quad i = 1, 2, \dots, K$$

Gradient of Scalar Performance Function

$$Y_{\psi_i} = Y_X X_{\psi_i} \quad i = 1, 2, \dots, K$$

Figure 14. Equations Required to Determine the Values for the Gradient of the Scalar Function

$$Y_{\psi_i} = \frac{\partial Y}{\partial \psi_i} \quad (3-31)$$

$$Y_{X_i} = \frac{\partial Y}{\partial X_i} \quad (3-32)$$

$$Y_X = [Y_{X_1}, \dots, Y_{X_N}]. \quad (3-33)$$

The first block of Figure 14 gives the proper initial conditions for the dynamical equations. The second block contains the dynamical equations which must be solved, and the third block has the equation for each of the components of the gradient vector.

The sensitivity of the state vector with respect to initial condition ψ_i is X_{ψ_i} . This is determined as a function of time by solving the set of homogeneous differential equations given in the second block. These equations are solved simultaneously with the equations for the basic dynamical system. Their mathematical development is given in Appendix D.

In Figure 15 the necessary equations for determining the elements of the matrix of second partial derivatives of the scalar performance function are given. The additional notation used is

$$X_{\psi_j \psi_i} = \frac{\partial X_{\psi_i}}{\partial \psi_j} \quad (3-34)$$

$$Y_{\psi_j \psi_i} = \frac{\partial Y_{\psi_i}}{\partial \psi_j} \quad (3-35)$$

Initial Conditions for Dynamical Equations

$$X(t_0) = \begin{bmatrix} \psi \\ X_0 \end{bmatrix} \begin{array}{l} \text{- guess} \\ \text{- known} \end{array}$$

$$X_{\psi_i} = \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \\ 0 \end{bmatrix} \text{ row } i \quad i = 1, 2, \dots, K$$

$$X_{\psi_j \psi_i} = 0 \quad \begin{array}{l} i = 1, 2, \dots, K \\ j = 1, 2, \dots, K \end{array}$$

Dynamical Equations

$$\frac{dX}{dt} = F(X, t)$$

$$\frac{dX_{\psi_i}}{dt} = F_X X_{\psi_i} \quad i = 1, 2, \dots, K$$

$$\frac{dX_{\psi_j \psi_i}}{dt} = F_X X_{\psi_j \psi_i} + \sum_{L=1}^N \left(\frac{\partial (F_X)}{\partial X_L} \frac{\partial X_L}{\partial \psi_j} \right) X_{\psi_i} \quad \begin{array}{l} i = 1, 2, \dots, K \\ j = 1, 2, \dots, K \end{array}$$

Elements of Matrix of Second Partial Derivatives of Scalar Performance Function

$$Y_{\psi_j \psi_i} = X_{\psi_i}^T Y_{XX} X_{\psi_j} + Y_X X_{\psi_j \psi_i} \quad \begin{array}{l} i = 1, 2, \dots, K \\ j = 1, 2, \dots, K \end{array}$$

Figure 15. Equations Required to Determine the Values for the Elements of the Matrix of Second Partial Derivatives of the Scalar Performance Function

$$Y_{X_i X_i} = \frac{\partial Y_{X_j}}{\partial X_i} \quad (3-36)$$

$$Y_{XX} = \begin{bmatrix} Y_{X_1 X_1} & \cdots & Y_{X_N X_1} \\ \vdots & & \vdots \\ Y_{X_1 X_N} & \cdots & Y_{X_N X_N} \end{bmatrix} \quad (3-37)$$

The sensitivity of X_{ψ_i} with respect to initial ψ_j is given by $X_{\psi_j \psi_i}$. This is determined as a function of time by solving the set of coupled dynamical equations given in the second block of Figure 15. The mathematical development of these equations is given in Appendix D.

The method of seeking principal planes can determine a solution for the two-point boundary value problems posed by Equations (3-14) through (3-16) by minimizing Equation (3-28). Figures 13, 14, and 15 provide the necessary equations for the method of seeking principal planes procedure presented in Chapter II.

Relation to Quasilinearization Procedures

In this section it will be demonstrated that the quasilinearization methods for solving two-point boundary value problems are really just partial second-order method. A true second-order method for determining the minimum of a scalar function is the Newton-Raphson method which is given by Equation (2-3). However, the computational effort required for determining the matrix of second partial

derivatives is sometimes very considerable. Hence, it is very tempting to try to find a satisfactory approximation for the matrix of second partial derivatives.

Figure 15 provides the following equation for the elements of the matrix of second partial derivatives of Equation (3-28).

$$Y_{\psi_j \psi_i} = X_{\psi_i}^T Y_{XX} X_{\psi_j} + Y_{X_i} Y_{\psi_j \psi_i}. \quad (3-38)$$

Equation (3-28) has the following partial derivatives:

$$Y_{X_i} = H_{X_i}^T H, \quad (3-39)$$

and

$$Y_{X_j X_i} = H_{X_j X_i}^T H + H_{X_i}^T H_{X_j}; \quad (3-40)$$

where

$$H_{X_i} = \frac{\partial H}{\partial X_i} \quad (3-41)$$

and

$$H_{X_j X_i} = \frac{\partial H_{X_i}}{\partial X_j}. \quad (3-42)$$

But, when one is close to the desired solution for the two-point boundary problem, it can be seen from Equation (3-16) that H should be approximately zero. Hence, Equation (3-39) and the last term of Equation (3-40) should be approximately zero. This in turn implies that a good approximation for Equation (3-38) is

$$Y_{\psi_j \psi_i} = X_{\psi_i}^T D^T D X_{\psi_j}, \quad (3-43)$$

Approx.

where D is a $K \times N$ matrix defined as

$$D = [H_{X_1}, \dots, H_{X_N}]. \quad (3-44)$$

The following equation is equivalent to the Newton-Raphson correction procedure given by Equation (2-3).

$$\psi_{\text{new}} = \psi_{\text{old}} - Y_{\psi\psi}^{-1} Y_{\psi}^T. \quad (3-45)$$

In Equation (3-45), the following notation is used:

$$Y_{\psi\psi} = \begin{bmatrix} Y_{\psi_1 \psi_1} & \dots & Y_{\psi_N \psi_1} \\ \vdots & & \vdots \\ Y_{\psi_1 \psi_N} & & Y_{\psi_N \psi_N} \end{bmatrix} \quad (3-46)$$

$$Y_{\psi} = [Y_{\psi_1}, \dots, Y_{\psi_K}]. \quad (3-47)$$

In Figure 14 the equation for the gradient vector is given as

$$Y_{\psi} = Y_X X_{\psi} \quad (3-48)$$

where

$$Y_X = [Y_{X_1}, \dots, Y_{X_N}], \quad (3-49)$$

and

$$X_{\psi} = [X_{\psi_1}, \dots, X_{\psi_K}]. \quad (3-50)$$

If Equations (3-48) and (3-39) are combined, and the notation of Equation (3-44) is used, the result is

$$Y_{\psi} = H^T D X_{\psi}. \quad (3-51)$$

If the element of the matrix of second partial derivatives are approximated by Equation (3-43), the following equation results

$$Y_{\psi\psi} = X_{\psi}^T D^T D X_{\psi}. \quad (3-52)$$

Approx.

When Equation (3-51) and the approximation given in Equation (3-52) are used, the Newton-Raphson correction method given by Equation (3-45) becomes

$$\psi_{\text{new}} = \psi_{\text{old}} - [X_{\psi}^T D^T D X_{\psi}]^{-1} X_{\psi}^T D^T H. \quad (3-53)$$

If the matrix $D X_{\psi}$ is not singular, the above equation simplifies to

$$\psi_{\text{new}} = \psi_{\text{old}} - [D X_{\psi}]^{-1} H. \quad (3-54)$$

Equation (3-54) is the basic equation which is used for the quasilinearization solution methods for two-point boundary value problems. Since it was obtained by approximating the matrix of second partial derivatives, it is only an approximate second-order method.

The Newton-Raphson method for minimizing a scalar function will sometimes diverge from a solution if the original independent vector guess is not close enough to the desired solution. Since the quasilinearization method given by Equation (3-54) is only an approximate Newton-Raphson procedure, it is not surprising that the quasilinearization procedure will sometimes diverge if the original guess for the unknown initial conditions is not close enough to a desired solution.

In Appendix C it is proved that if too much of the matrix of second partial derivatives is truncated, a modified Newton-Raphson method will not converge. This problem is not encountered by the quasilinearization method provided one is sufficiently close to the desired solution. This is true since the portion of the matrix of second partial derivatives which was truncated becomes the zero matrix at the solution point. However, when the starting point is not close to the desired solution, the portion of the matrix of second partial derivatives which is truncated may be very significant.

Example five in Chapter II demonstrates the importance of not truncating too much of the matrix of second partial derivatives. Since truncating a portion of the matrix of second partial derivatives can cause difficulties for relatively simple algebraic minimization problems, one should be careful when a solution technique for two-point boundary value problems is being used which utilizes an approximation

for the matrix of second partial derivatives.

The method of seeking principal planes is a true second-order method. A number of example problems have been solved by using this method. The results which are presented in the following section are encouraging.

Examples

The computational algorithm which was used for working these example problems is presented in Appendix E. The algorithm is very versatile, and it is designed so that the user need only supply the basic information.

The algorithm makes extensive use of the digital computer's capability to generate partial derivatives, and this relieves the user of the responsibility for providing the equations for the partial derivatives.

Linear Example

The first example which will be presented is that of solving a simple linear two-point boundary value problem. The dynamical equations used were

$$\begin{aligned} \dot{X}_1 &= X_2 \\ \dot{X}_2 &= -X_1 - X_2 + 1.0. \end{aligned} \tag{3-55}$$

Both of the initial boundary conditions were unspecified, and the desired final boundary conditions were

$$X_1(4.0) = 1.2$$

$$X_2(4.0) = 0.0.$$

The method of seeking principal planes determined that the initial conditions of

$$X_1(0) = -.12688$$

$$X_2(0) = -.54238$$

would cause the dynamical equations to reach the desired final boundary conditions. The original guess for the initial condition vector was $X_1(0) = 0.0$ and $X_2(0) = 0.0$. Eight steps were used in the numerical integration of the dynamical equations by a Runge-Kutta algorithm.

The method of seeking principal planes converged after two evaluations of the performance index, one evaluation of the gradient vector, and one evaluation of the matrix of second partial derivatives.

This information is summarized in Figure 16, and for the subsequent examples all of the information will be presented in a figure of the same format.

The second-order Taylor series describes a linear two-point boundary value problem exactly. Hence, if a linear two-point boundary value problem has K unknown initial conditions, the method of seeking principal planes will converge after K evaluations of the scalar performance index, one evaluation of the gradient vector, and one evaluation of the matrix of second partial derivatives. This first

Dynamical Equations

$$\dot{X}_1 = X_2$$

$$\dot{X}_2 = -X_1 - X_2 + 1.0$$

Scalar Performance Index

$$Y = (X_1 - 1.2)^2 + X_2^2$$

Initial Condition Guess

$$X_1 = 0.0 \quad X_2 = 0.0$$

Converged Initial Condition

$$X_1 = -.12688 \quad X_2 = -.54238$$

$$\text{Initial Time} = 0.0$$

$$\text{Final Time} = 4.0$$

$$\text{Number of Steps} = 8$$

Converged After:

- 2 Evaluations of performance index
 - 1 Evaluation of the gradient vector
 - 1 Evaluation of matrix of second partial derivatives
-

Figure 16. Linear Two-Point Boundary Value Problem

example provided a demonstration of this point.

Drag Racer Example

A very crude dynamical model for a drag racing car is

$$\begin{aligned}\dot{X}_1 &= X_2 \\ \dot{X}_2 &= P_1 + P_2 X_2^2.\end{aligned}\tag{3-56}$$

The above model is obtained by assuming that the coefficient of friction between the wheels and the pavement remains constant, and that the aerodynamic forces are proportional to the velocity of the vehicle squared. In January of 1967, an AA fuel drag car was able to travel the quarter of a mile in 6.95 seconds reaching a speed of 221 mph.

It would be interesting to determine the parameters P_1 and P_2 such that the mathematical model, Equation (3-56), would hit the point

$$X_1(6.9) = 1/4 \text{ mile} = 1320 \text{ ft.}$$

$$X_2(6.9) = 221 \text{ mph} \approx 310 \text{ ft/sec.}$$

when started with the initial condition

$$X_1(0) = 0.0$$

$$X_2(0) = 0.0.$$

If time is nondimensionalized by 10, and distance is nondimensionalized by 1000, Equation (3-56) becomes

$$\begin{aligned}
 \dot{X}_1 &= X_2 \\
 \dot{X}_2 &= X_3 + X_4 X_2^2 \\
 \dot{X}_3 &= 0 \\
 \dot{X}_4 &= 0
 \end{aligned}
 \tag{3-57}$$

where $X_3 = P_1/10$ and $X_4 = 1000 P_2$. The initial conditions become

$$\begin{aligned}
 X_1(0) &= 0.0 \\
 X_2(0) &= 0.0 \\
 X_3(0) &= ? \quad (\text{To be determined}) \\
 X_4(0) &= ? \quad (\text{To be determined})
 \end{aligned}
 \tag{3-58}$$

and the nondimensionalized desired final conditions become

$$\begin{aligned}
 X_1(.69) &= 1.32 \\
 X_2(.69) &= 3.10.
 \end{aligned}
 \tag{3-59}$$

The results for the parameter identification problem given by Equation (3-57) and boundary conditions (3-58) and (3-59) are presented in Figure 17.

The converged value for the initial condition on X_3 is 7.0826. This means that P_1 in Equation (3-56) equals 70.826 ft/sec², which is slightly greater than twice the acceleration of gravity. Hence, the crude mathematical model predicts that as a drag racer leaves the starting line it should accelerate at more than twice the acceleration of gravity. If you are unfamiliar with the drag racing sport,

Dynamical Equations

$$\dot{X}_1 = X_2$$

$$\dot{X}_2 = X_3 + X_4 X_2^2$$

$$\dot{X}_3 = 0$$

$$\dot{X}_4 = 0$$

Scalar Performance Index

$$Y = (X_1 - 1.32)^2 + (X_2 - 3.10)^2$$

Known Initial Condition

$$X_1 = 0 \quad X_2 = 0$$

Initial Condition Guess

$$X_3 = 6.0 \quad X_4 = -.05$$

Converged Initial Condition

$$X_3 = 7.0826 \quad X_4 = -.57584$$

Initial Time = 0.0

Final Time = .69

Number of Steps = 10

Converged After:

- 16 Evaluations of performance index
 - 5 Evaluations of gradient vector
 - 7 Evaluations of matrix of second partial derivatives
-

Figure 17. Drag Racer Parameter Identification Example

this may be a surprising prediction. But, among drag racing fans, it is a known fact that such high accelerations do occur.

Birta and Trushel Example

The dynamical equations used for this example were

$$\begin{aligned}
 \dot{X}_1 &= (1.0 - X_2^2) X_1 - X_2 - X_3/2.0 \\
 \dot{X}_2 &= X_1 \\
 \dot{X}_3 &= -2.0 X_1 - X_3 + X_3 X_2^2 - X_4 \\
 \dot{X}_4 &= -2.0 X_2 + 2.0 X_1 X_2 X_3 + X_3.
 \end{aligned}
 \tag{3-60}$$

Equations (3-60) are given by Birta and Trushel (13).

The method of seeking principle planes was used to solve the two-point boundary value problem, and the results are presented in Figure 18.

Birta and Trushel reported that after 11 iterations by the conjugate gradient method, final convergence for the problem presented in Figure 18 was obtained. Each iteration of a deflected gradient method often requires at least four evaluations of the performance index and four evaluations of the gradient vector.

Schlichting Example

On page 332 of Schlichting (14) a two-point boundary value problem which arises when considering natural flow in thermal boundary layers is presented. This two-point

Dynamical Equations

$$\dot{X}_1 = (1.0 - X_2^2) X_1 - X_2 - X_3/2.0$$

$$\dot{X}_2 = X_1$$

$$\dot{X}_3 = -2.0X_1 - X_3 + X_3 X_2^2 - X_4$$

$$\dot{X}_4 = -2.0 X_2 + 2.0 X_1 X_2 X_3 + X_3$$

Scalar Performance Index

$$Y = X_3^2 + X_4^2$$

Known Initial Condition

$$X_1 = 0.0 \quad X_2 = .10$$

Initial Condition Guess

$$X_3 = 0.0 \quad X_4 = 0.0$$

Converged Initial Condition

$$X_3 = .081176 \quad X_4 = .66941$$

Initial Time = 0.0

Final Time = 4.0

Number of Steps = 40

Converged After:

- 10 Evaluations of the performance index
 - 2 Evaluations of the gradient vector
 - 7 Evaluations of the matrix of second partial derivatives
-

Figure 18. Results for the Birta and Trushel Example

boundary value problem was worked, and the results are presented in Figure 19.

Lewallen, Tapley, and Williams Example

The final two-point boundary value problem to be presented has been extensively studied by Lewallen, Tapley, and Williams (12). In their paper, they reported regions of convergence for several two-point boundary value solution techniques.

The method of seeking principal planes was able to solve the two-point boundary value problem from a poor initial condition guess. The initial condition guess used was in error by 100 per cent for each of the free adjoint variables. Lewallen, Tapley, and Williams were unable to obtain convergence from this poor initial condition guess without resorting to solution techniques which were problem oriented.

The results for the Lewallen, Tapley, and Williams example are presented in Figure 20.

Some of the versatility of the method of seeking principal planes has been shown by the two-point boundary value examples worked in this chapter. The results of the Lewallen, Tapley, and Williams example were especially encouraging since the method of seeking principal planes is not a problem oriented technique.

In Chapter II, the method of seeking principal planes was developed for determining the minimum of a function of

Dynamical Equations

$$\dot{X}_1 = X_2$$

$$\dot{X}_2 = X_4$$

$$\dot{X}_3 = X_5$$

$$\dot{X}_4 = -3.0 X_1 X_4 + 2.0 X_2 X_2 - X_3$$

Scalar Performance Index

$$Y = X_2^2 + X_3^2$$

Known Initial Condition

$$X_1 = 0.0 \quad X_2 = 0.0 \quad X_3 = 1.0$$

Initial Condition Guess

$$X_4 = .60 \quad X_5 = -.60$$

Converged Initial Condition

$$X_4 = .64189 \quad X_5 = -.56743$$

Initial Time = 0.0

Final Time = 10.0

Number of Steps = 20

Converged After:

- 15 Evaluations of performance index
 - 7 Evaluations of gradient vector
 - 8 Evaluations of matrix of second partial derivatives
-

Figure 19. Results of Schlichting Example

 Dynamical Equations

$$\begin{aligned} \dot{X}_1 &= X_7 \left(X_2^2/X_3 - 1.0/X_3^2 - .1405 X_5/ \right. \\ &\quad \left. ((1.0 - .07487 T X_7) \sqrt{X_5^2 + X_6^2}) \right) \\ \dot{X}_2 &= X_7 \left(-X_1 X_2/X_3 - .1405 X_6/ \right. \\ &\quad \left. ((1.0 - .07487 T X_7) \sqrt{X_5^2 + X_6^2}) \right) \\ \dot{X}_3 &= X_7 X_1 \\ \dot{X}_4 &= X_7 \left(X_2^2 X_5/X_3^2 - 2.0 X_5/X_3^2 - X_1 X_2 X_6/X_3^2 \right) \\ \dot{X}_5 &= X_7 \left(X_2 X_6/X_3 - X_4 \right) \\ \dot{X}_6 &= X_7 \left(-2.0 X_2 X_5/X_3 + X_1 X_6/X_3 \right) \\ \dot{X}_7 &= 0 \end{aligned}$$

Scalar Performance Function

$$Y = X_1^2 + (X_2 - .8098)^2 + (X_3 - 1.525)^2$$

Known Initial Condition

$$X_1 = 0.0 \quad X_2 = 1.0 \quad X_3 = 1.0 \quad X_4 = -1.0$$

Guessed Initial Condition

$$X_5 = -.9880 \quad X_6 = -2.16 \quad X_7 = 3.32$$

Converged Initial Condition

$$X_5 = -.49450 \quad X_6 = -1.0795 \quad X_7 = 3.3193$$

Initial Time = 0.0

Final Time = 1.0

Number of Steps = 20

Converged After:

18 Evaluations of performance index
 4 Evaluations of gradient vector
 10 Evaluations of matrix of second
 partial derivatives

Figure 20. Lewallen, Tapley, and Williams
 Example

several variables. In Chapter IV, it will be shown that if enough care is taken, this development can be applied directly to system design and system identification problems.

CHAPTER IV

PARAMETER IDENTIFICATION BY DIRECT METHODS

In the previous chapter, it has been demonstrated that the method of seeking principal planes can be used to solve the problem of parameter identification of dynamical systems by an indirect approach. Within this chapter, the method of seeking principal planes will be used as a direct solution approach to the problem of parameter identification of dynamical systems.

The parameter identification problem was stated in Chapter III, but it will now be presented again so that one need not page from one chapter to the other.

Statement of Parameter Identification Problem

It is assumed that a mathematical model for the system has been formulated and written in state variable notation,

$$\dot{X} = F(X, P, t). \quad (4-1)$$

In the above equation, X is the N dimensional state variable, P is an M dimensional parameter vector, and t is the independent variable, time.

The initial condition vector is partitioned as

$$X(t_0) \begin{bmatrix} \psi \\ X_0 \end{bmatrix} \begin{array}{l} - \text{unknown} \\ - \text{known.} \end{array} \quad (4-2)$$

In the above equation ψ is a K dimensional vector of unknown initial conditions, and X_0 is an N-K dimensional vector of the known initial conditions.

The entire parameter vector is unknown.

$$P = \text{unknown} \quad (4-3)$$

Values for the parameter vector, P, and the unknown initial conditions, ψ , need to be determined which will provide a local minimum for the performance index,

$$Y = \int_{t_0}^{t_f} G(X, t) dt. \quad (4-4)$$

Direct Solution of Parameter Identification Problem by Method of Seeking Principal Planes

Since the performance index given by Equation (4-4) is a scalar function, the method of seeking principal planes as developed in Chapter II can be used to determine its minimum provided:

1. The performance index value can be determined when the values for the independent variables are specified,
2. The values for the gradient of the performance index can be determined when the values

for the independent variables are specified,
and

3. The values for the elements of the matrix of second partial derivatives of the performance index can be determined when the independent variables are specified.

The above three steps can be performed, but the procedure needs to be explained since the performance index, Equation (4-4), is an implicit function of the independent variables, P and ψ . This is more easily understood by studying Figure 21. As the figure indicates, the first step in the procedure for determining the value of the scalar performance index is to make a guess for the unknown initial conditions and the parameter vector. The second step of the procedure is to numerically integrate the dynamical differential equations for the initial time to the final time. Hence, the value of the state vector at each instant of time is a function of P and ψ . Simultaneously, the integral equation for the performance index can be numerically integrated as is indicated by block three of Figure 21. The integrand of the performance index is an explicit function of the state vector, X , and time. But, since the state vector is in turn a function of the free initial conditions, ψ , and the parameter vector, P ; the scalar performance index is an implicit function of P and ψ .

In Figure 22 the necessary equations for determining

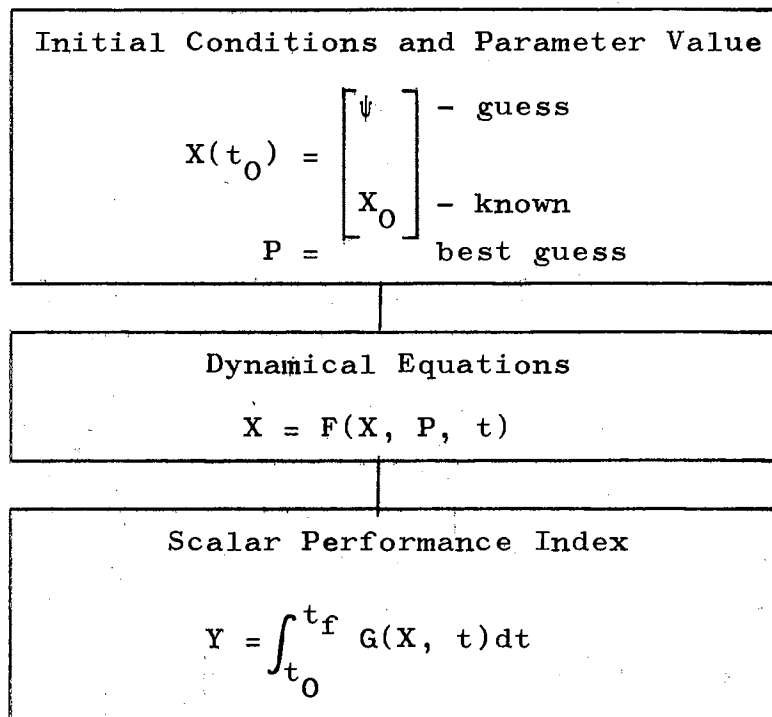


Figure 21. Equations Required to Determine the Value of the Scalar Performance Index

Initial Conditions and Parameter Value

$$X(t_0) = \begin{bmatrix} \psi \\ X_0 \end{bmatrix} \quad \begin{array}{l} \text{guess} \\ \text{known} \end{array}$$

$$X_{\psi_i} = \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \\ 0 \end{bmatrix} \quad \text{-- row } i \quad i = 1, 2, \dots, K$$

$$X_{P_i} = 0 \quad i = 1, 2, \dots, M$$

P = best guess

Dynamical Equations

$$\frac{dX}{dt} = F(X, P, t)$$

$$\frac{dX_{\psi_i}}{dt} = F_X X_{\psi_i} \quad i = 1, 2, \dots, K$$

$$\frac{dX_{P_i}}{dt} = F_X X_{P_i} + F_{P_i} \quad i = 1, 2, \dots, M$$

Gradient of Scalar Performance Index

$$Y_{\psi_i} = \int_{t_0}^{t_f} G_X X_{\psi_i} dt \quad i = 1, 2, \dots, K$$

$$Y_{P_i} = \int_{t_0}^{t_f} G_X X_{P_i} dt \quad i = 1, 2, \dots, M$$

Figure 22. Equations Required to Determine the Value of the Gradient Vector

the gradient of the scalar performance index are given. The only notation which is different from that used in Chapter III is

$$X_{P_i} = \frac{\partial X}{\partial P_i}, \quad Y_{P_i} = \frac{\partial Y}{\partial P_i}, \quad F_{P_i} = \frac{\partial F}{\partial P_i}$$

and

$$G_X = \left[\frac{\partial G}{\partial X_1}, \dots, \frac{\partial G}{\partial X_N} \right].$$

The first block of Figure 22 gives the proper initial conditions for the dynamical equations, the second block contains the dynamical equations which must be numerically integrated, and the third block contains the integral equation for each of the components of the gradient vector.

The sensitivity of the state vector with respect to initial condition ψ_i is X_{ψ_i} , and the sensitivity with respect to P_i is X_{P_i} . These sensitivities are determined as a function of time by solving the set of differential equations given in the second block of Figure 22. These equations are coupled with the equations for the basic dynamical system, and their mathematical development is given in Appendix D.

In Figure 23 the necessary equations for determining the elements of the matrix of second partial derivatives of the performance index are given. The only notation which is different from that used in Chapter III is

Initial Conditions and Parameter Values

$$X(t_0) = \begin{bmatrix} \psi \\ X_0 \end{bmatrix} \quad \begin{array}{l} \text{- guess} \\ \text{- known} \end{array}$$

$$X_{\psi_i} = \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \\ 0 \\ 0 \end{bmatrix} \quad \text{- row } i \quad i = 1, 2, \dots, K$$

$$X_{P_i} = 0 \quad i = 1, 2, \dots, M$$

$$X_{\psi_j \psi_i} = 0 \quad \begin{array}{l} i = 1, 2, \dots, K \\ j = 1, 2, \dots, K \end{array}$$

$$X_{P_j \psi_i} = 0 \quad \begin{array}{l} i = 1, 2, \dots, K \\ j = 1, 2, \dots, M \end{array}$$

$$X_{P_j P_i} = 0 \quad \begin{array}{l} i = 1, 2, \dots, M \\ j = 1, 2, \dots, M \end{array}$$

P = guess

Dynamical Equations

$$\frac{dX}{dt} = F(X, P, t)$$

$$\frac{dX_{\psi_i}}{dt} = F_X X_{\psi_i} \quad i = 1, 2, \dots, K$$

$$\frac{dX_{P_i}}{dt} = F_X X_{P_i} + F_{P_i} \quad i = 1, 2, \dots, M$$

$$dX_{\psi_j \psi_i} = F_X X_{\psi_j \psi_i} + \sum_{L=1}^N \left(\frac{\partial F_X}{\partial X_L} \frac{\partial X_L}{\partial \psi_j} \right) X_{\psi_i} \quad \begin{array}{l} i = 1, 2, \dots, K \\ j = 1, 2, \dots, K \end{array}$$

$$dX_{P_j \psi_i} = F_X X_{P_j \psi_i} + \sum_{L=1}^N \left(\frac{\partial F_X}{\partial X_L} \frac{\partial X_L}{\partial P_j} + \frac{\partial F_X}{\partial P_j} \right) X_{\psi_i} \quad \begin{array}{l} i = 1, 2, \dots, K \\ j = 1, 2, \dots, M \end{array}$$

$$\frac{dX_{P_j P_i}}{dt} = F_X X_{P_j P_i} + \sum_{L=1}^N \left(\frac{\partial F_X}{\partial X_L} \frac{\partial X_L}{\partial P_j} + \frac{\partial F_X}{\partial P_j} \right) X_{P_i} + \sum_{L=1}^N \left(\frac{\partial F_{P_j}}{\partial X_L} \frac{\partial X_L}{\partial P_j} \right) + F_{P_j P_i}$$

Elements of Matrix of Second Partial Derivatives of Scalar Performance Function

$$Y_{\psi_j \psi_i} = \int_{t_0}^{t_f} X_{\psi_i}^T G_{XX} X_{\psi_j} + G_X X_{\psi_j \psi_i} dt \quad \begin{array}{l} i = 1, 2, \dots, K \\ j = 1, 2, \dots, K \end{array}$$

$$Y_{P_j \psi_i} = \int_{t_0}^{t_f} X_{\psi_i}^T G_{XX} X_{P_j} + G_X X_{P_j \psi_i} dt \quad \begin{array}{l} i = 1, 2, \dots, K \\ j = 1, 2, \dots, M \end{array}$$

$$Y_{P_j P_i} = \int_{t_0}^{t_f} X_{P_i}^T G_{XX} X_{P_j} + G_X X_{P_j P_i} dt \quad \begin{array}{l} i = 1, 2, \dots, M \\ j = 1, 2, \dots, M \end{array}$$

Figure 23. Equations Required to Determine the Values for the Elements of the Matrix of Second Partial Derivatives of the Performance Index

$$X_{P_j \psi_i} = \frac{\partial X_{\psi_i}}{\partial P_j}, \quad X_{P_j P_i} = \frac{\partial X_{P_i}}{\partial P_j}, \quad F_{P_j P_i} = \frac{\partial F_{P_i}}{\partial P_j}$$

and

$$G_{XX} = \begin{bmatrix} \frac{\partial^2 G}{\partial X_1 \partial X_1} & \cdots & \frac{\partial^2 G}{\partial X_N \partial X_1} \\ \vdots & & \vdots \\ \frac{\partial^2 G}{\partial X_1 \partial X_N} & \cdots & \frac{\partial^2 G}{\partial X_N \partial X_N} \end{bmatrix}.$$

The mathematical development of the equations for determining the second-order sensitivity coefficients

($X_{\psi_j \psi_i}$, $X_{P_j \psi_i}$, and $X_{P_j P_i}$) is given in Appendix D.

Figures 21, 22, and 23 contain all equations which are needed for determining (1) the value of the performance index, (2) the gradient of the performance index, and (3) the matrix of second partial derivatives of the performance index. Hence, the method of seeking principal planes can be used as a direct method for determining a minimum point for the performance index.

The differential equations which must be solved to determine the second-order sensitivity coefficient are quite involved. The second-order sensitivity coefficients would be unnecessary if the second term in the equations for determining the elements of the matrix of second partial derivatives is truncated (see Figure 23). However, example five in Chapter II demonstrates that considerable care should be exercised before making such a truncation.

The method of seeking principal planes was used to work several example problems, and the results are presented in the following section.

Examples

The computational algorithm which was used for working these example problems is presented in Appendix F. The algorithm is very versatile, and it is designed so that the user need only supply the basic information.

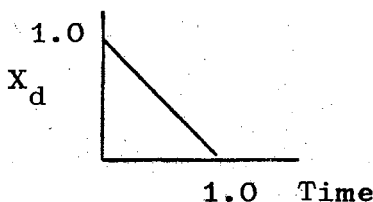
The algorithm makes extensive use of the digital computer's capability to generate partial derivatives, and this relieves the user of the responsibility for providing the equations for the partial derivatives.

Example 1

The first example worked was that of determining the proper initial condition and parameter value such that

$$\dot{X} = -PX \quad (4-5)$$

would have a dynamical response which fit the desired response, X_d ,



as close as possible. The performance index used was the standard integral error squared criterion,

$$Y = \int_0^{1.0} (X - X_d)^2 dt. \quad (4-6)$$

The computational effort required and other pertinent results and information for this problem are presented in Figure 24.

Example 2

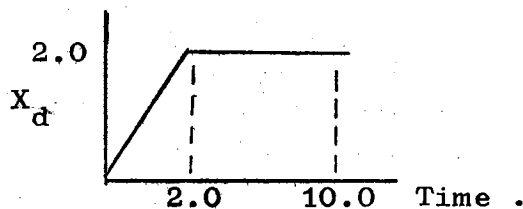
The mathematical model for this example was

$$\begin{aligned} \dot{X}_1 &= X_2 \\ \dot{X}_2 &= -P_1 X_1 - P_2 X_2 + 1.0. \end{aligned} \quad (4-7)$$

Once again the integral error squared criterion was used

$$Y = \int_0^{10} (X - X_d)^2 dt. \quad (4-8)$$

But the desired response which was used for this example was



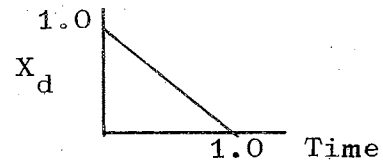
Difficulty had been encountered in previous attempts to work this parameter identification problem by using standard gradient techniques. The difficulty encountered was that of zigzagging back and forth across a valley with relatively insignificant changes in the parameters.

 Dynamical Equations

$$\dot{X} = -PX$$

Performance Index

$$Y = \int_0^1 (X - X_d)^2 dt$$



Number of Time Steps = 5

Initial Time = 0.0

Final Time = 1.0

Number of Free Initial Conditions = 1

Initial Condition Guess

$$X_1 = 1$$

Converged Initial Condition

$$X_1 = 1.0892$$

Initial Parameter Guess

$$P = 1.0$$

Converged Parameter Value

$$P = 1.8037$$

Converged After:

- 10 Evaluations of performance index
 - 3 Evaluations of gradient vector
 - 5 Evaluations of the matrix of second partial derivatives
-

Figure 24. Equations and Results for Example 1

But the method of seeking principal planes was able, with no difficulties, to solve this problem. The results are given in Figure 25. In Figure 26, the response of the system for the original parameter guess and for the converged parameter vector is presented. It can be seen that the converged response is considerably improved.

Example 3

This example is the same as Example 2 except that the initial conditions for X_1 and X_2 are left free. The results are presented in Figure 27.

Since this example has more free independent parameters than Example 2, it is reasonable to expect that the converged solution will more closely fit the desired response. Figure 28 shows that the previous statement is true.

Spool Valve Example

A fundamental component of many hydraulic systems is a spool valve such as is shown in Figure 29. In Dr. Bose's (6) thesis, it is shown that under certain circumstances the following mathematical model is reasonable:

$$\dot{X}_1 = X_2$$

$$\dot{X}_2 = -.36X_2 - .24X_1 - P_1X_1^3 - P_2X_1X_2 + 1.0.$$

Proper values for P_1 and P_2 need to be determined so that the spool valve will require a minimum amount of time to open and have a steady-state opening of approximately 1.0.

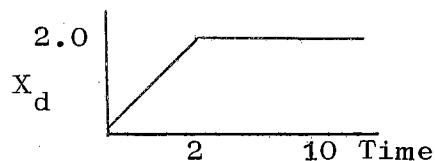
 Dynamical Equations

$$\dot{X}_1 = X_2$$

$$\dot{X}_2 = -P_1 X_1 - P_2 X_2 + 1.0$$

Performance Index

$$Y = \int_0^{10} (X - X_d)^2 dt$$



Number of Time Steps = 20

Initial Time = 0.0

Final Time = 10.0

Number of Free Initial
Conditions = None

Initial Condition Vector

$$X_1 = 0.0 \quad X_2 = 0.0$$

Initial Parameter Guess

$$P_1 = 1.0 \quad P_2 = 2.0$$

Converged Parameter Vector

$$P_1 = .53045 \quad P_2 = .67262$$

Converged After:

24 Evaluations of performance index

5 Evaluations of gradient vector

8 Evaluations of matrix of second partial
derivatives

Figure 25. Equations and Results for Example 2

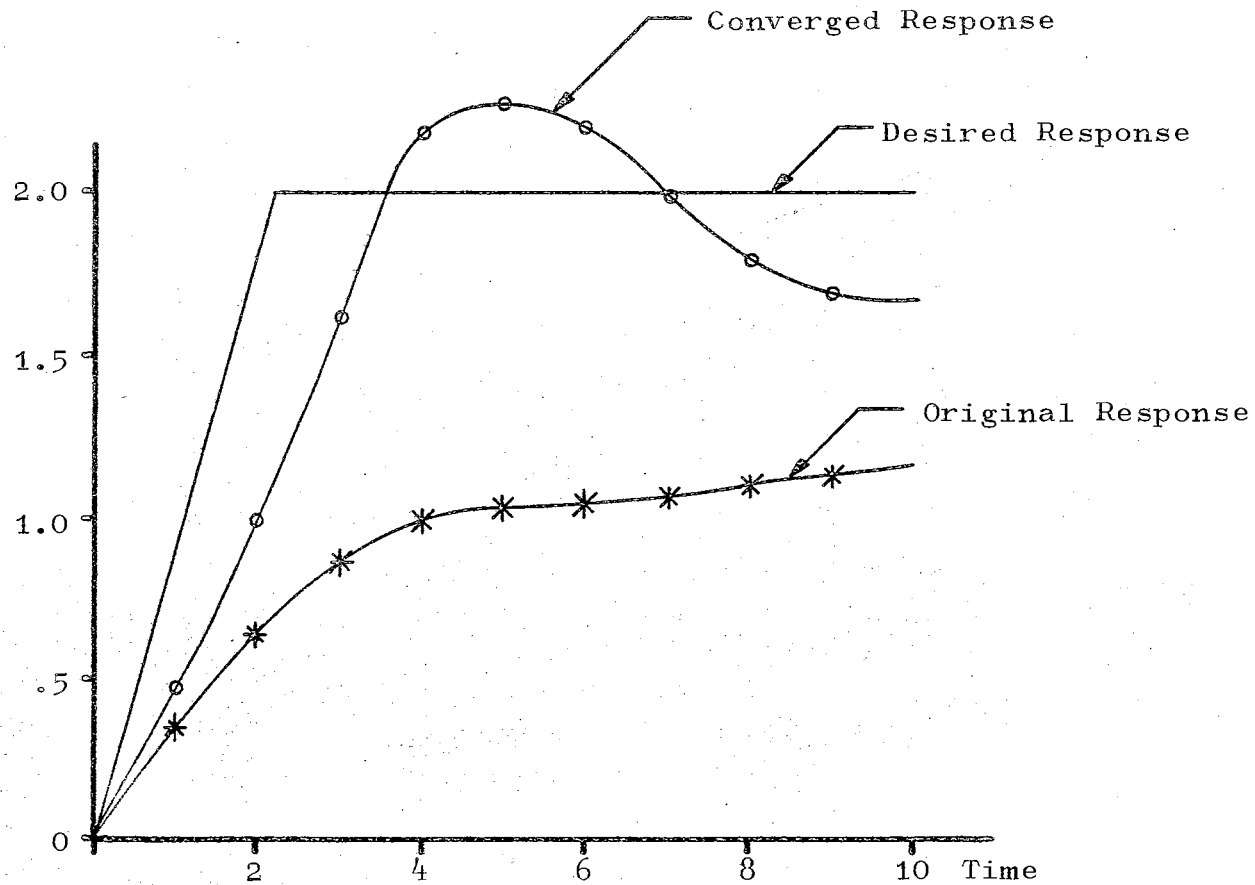


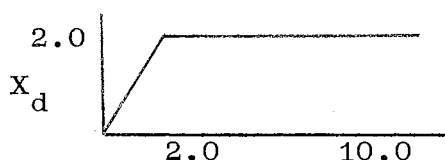
Figure 26. This Figure Shows the Response Improvement Which Was Obtained for $\ddot{Y} = -P_1 \dot{X} - P_2 X + 1.0$

 Dynamical Equations

$$\dot{X}_1 = X_2$$

$$\dot{X}_2 = -P_1 X_1 - P_2 X_2 + 1.0$$

Performance Index

$$Y = \int_0^{10} (X - X_d)^2 dt$$


Number of Time Steps = 20

Initial Time = 0.0

Final Time = 10.0

Number of Free Initial Conditions = 2

Initial Condition Guess

$$X_1 = 0.0 \quad X_2 = 0.0$$

Converged Initial Condition

$$X_1 = -.14634 \quad X_2 = 1.6947$$

Initial Parameter Guess

$$P_1 = 1.0 \quad P_2 = 2.0$$

Converged Parameter Vector

$$P_1 = .51136 \quad P_2 = 1.1786$$

Converged After:

38 Evaluations of the performance index

7 Evaluations of the gradient vector

11 Evaluations of the matrix of second
partial derivatives

Figure 27. Equations and Results for Example 3

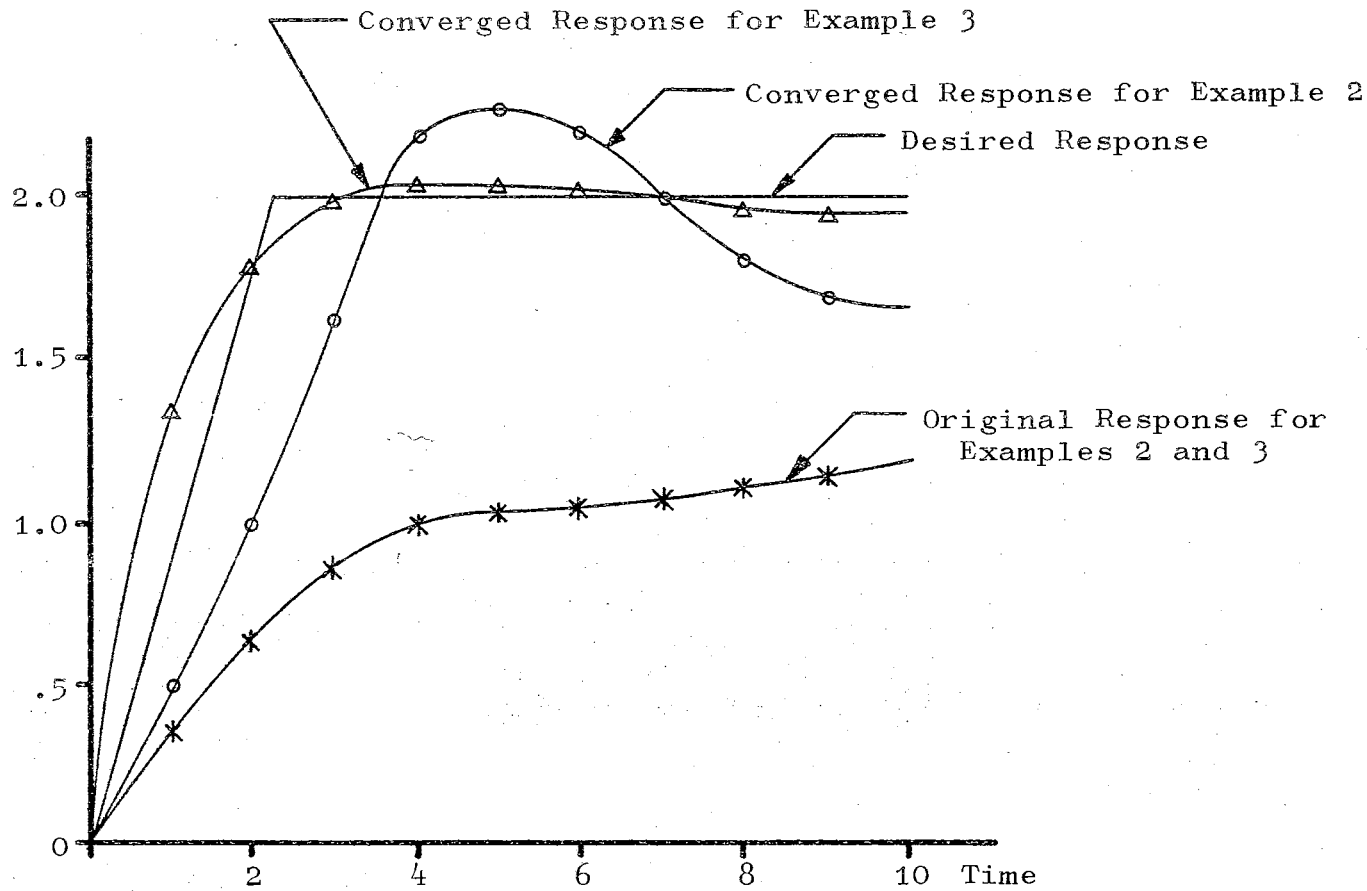


Figure 28. This Figure Shows That the Response for the Converged Solution of Example 3 is Considerably Better Than the Converged Solution Response of Example 2

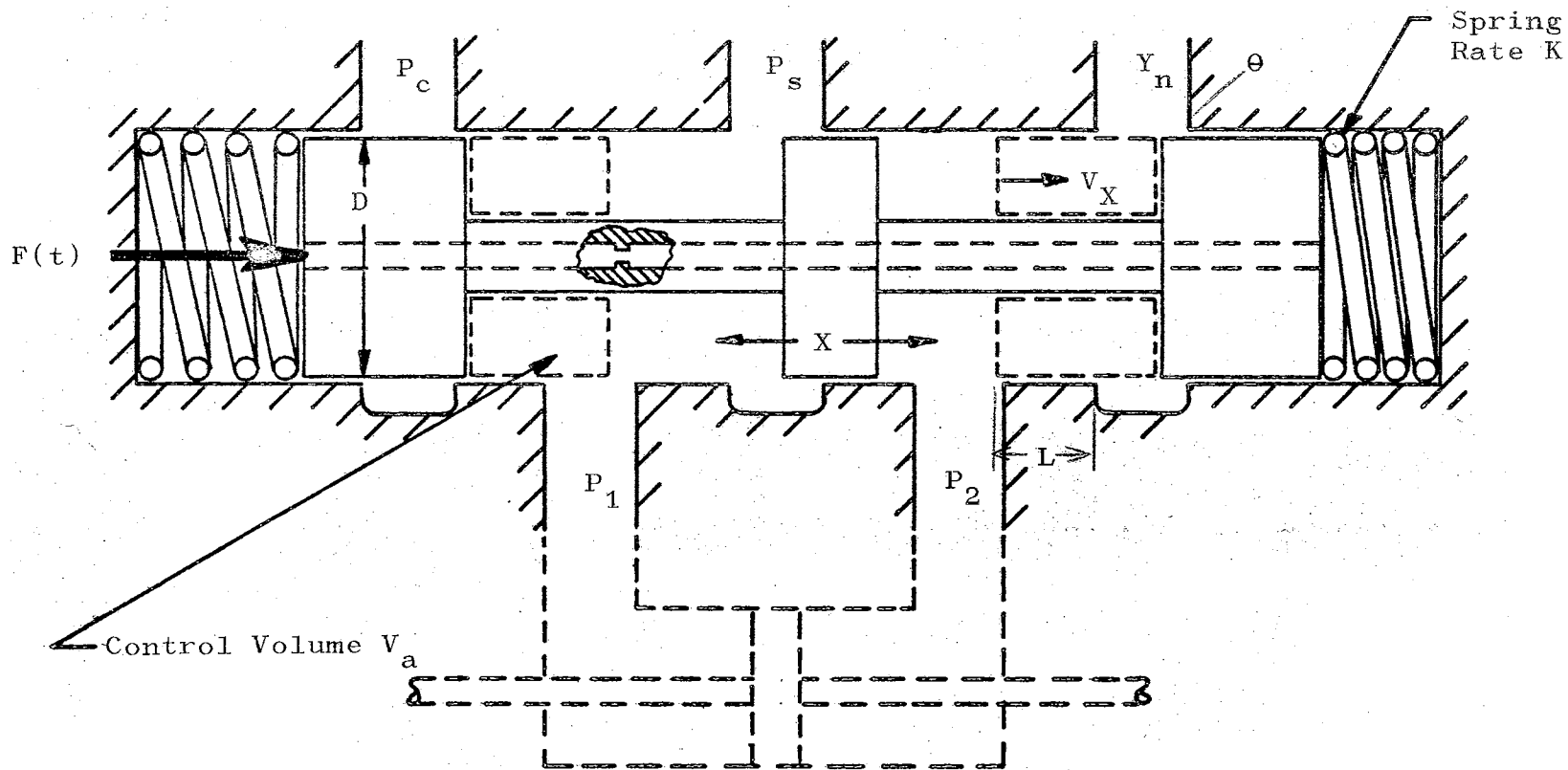
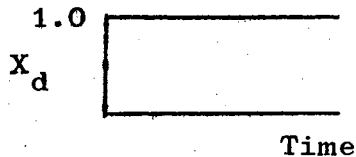


Figure 29. Hydraulic Spool Valve

The $P_1 X_1^3$ term in the equation represents a "hard" spring, and the $P_2 X_1 X_2$ term in the equation represents the unsteady flow force.

The desired response of the valve is that it instantaneously opens, i.e.,



The values of $P_1 = 0$, $P_2 = 0$ were chosen as the starting point for determining a minimum point of

$$Y = \int_0^{5.0} (X - X_2)^2 dt$$

by the method of seeking principal planes. The equations used and the obtained results are presented in Figure 30. In Figure 31 the original response and the converged solution response are presented. The improvement in the response is quite dramatic.

This chapter has shown that the method of seeking principal planes can, quite effectively, be directly applied to system identification or design problems. A variety of examples were worked and all converged with no difficulties.

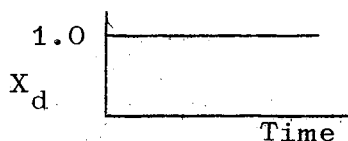
The method of seeking principal planes is effective for determining optimal parameters of dynamical systems. The examples worked in this chapter and Chapter III verify the preceding statement.

 Dynamical Equations

$$\dot{X}_1 = X_2$$

$$\dot{X}_2 = -.36 X_2 - .24 X_1 - P_1 X_1^3 - P_2 X_1 X_2 + 1.0$$

Performance Index

$$Y = \int_0^{5.0} (X - X_d)^2 dt$$


Number of Time Steps = 20

Initial Time = 0.0

Final Time = 5.0

Number of Free Initial
Conditions = None

Initial Condition Vector

$$X_1 = 0.0 \quad X_2 = 0.0$$

Initial Parameter Guess

$$P_1 = 0.0 \quad P_2 = 0.0$$

Converged Parameter Vector

$$P_1 = .86122 \quad P_2 = 1.3174$$

Converged After:

21 Evaluations of the performance index

3 Evaluations of gradient vector

15 Evaluations of matrix of second
partial derivatives

 Figure 30. Equations and Results for the
Spool Valve Example

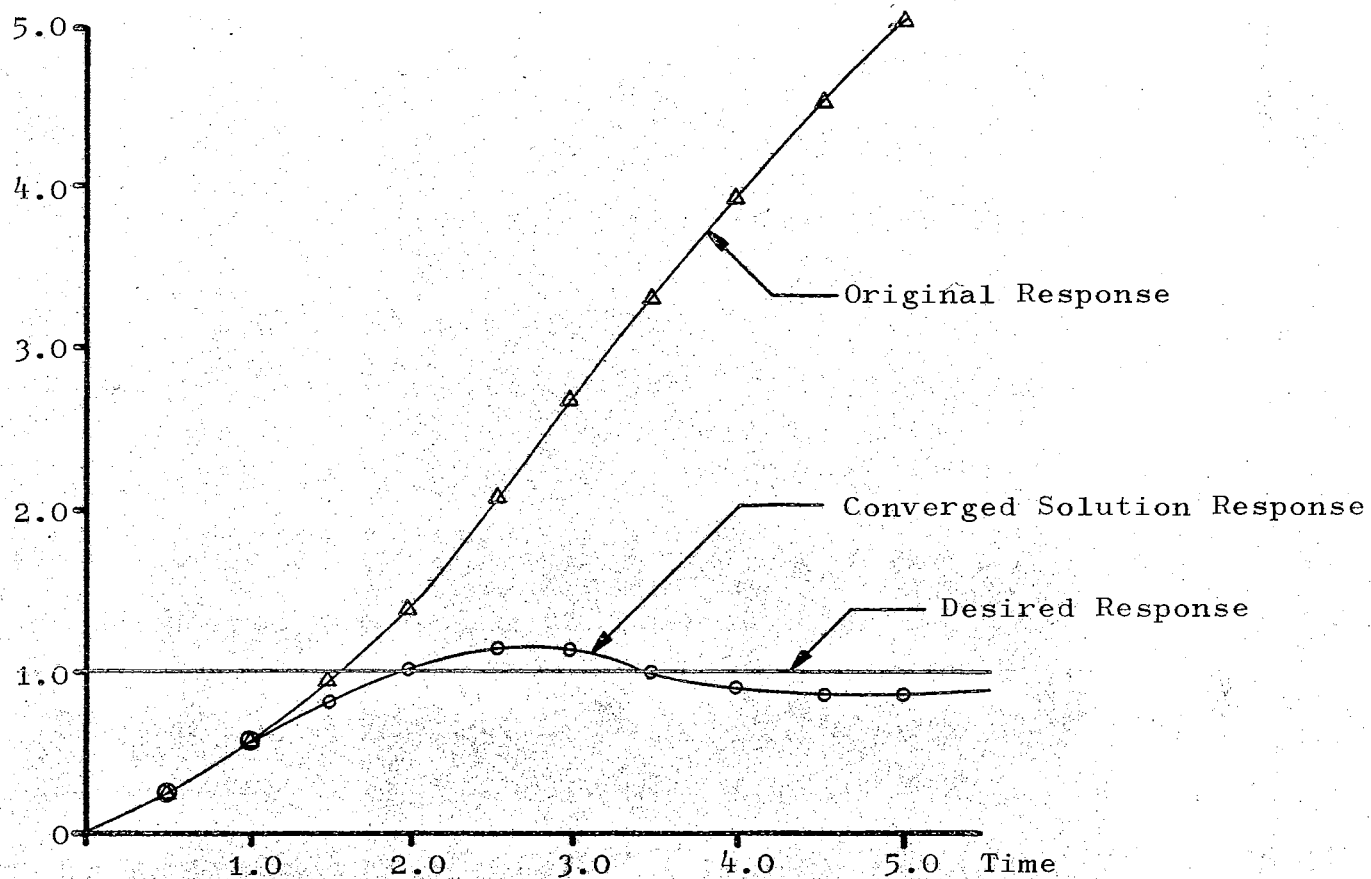


Figure 31. This Figure Shows the Improvement Which Was Obtained in the Spool Valve Response

However, all of these examples have all been continuous dynamical systems. If the dynamical system has discontinuities during the time period of interest, the problem becomes much more difficult. The following chapter deals with some of these problems and contains several proposals of methods for minimizing them.

CHAPTER V

DYNAMICAL SYSTEM DISCONTINUITIES:

PROBLEMS AND PROPOSALS

Problems Caused by Dynamical System Discontinuities

In the dynamical analysis of hydraulic control systems, the functional form of the right-hand side of the state vector model will sometimes change. The time at which the functional form changes will quite often depend upon the state vector. Two examples will be presented to clarify the preceding statements.

Figure 2 shows a hydraulic system which contains a poppet type relief valve. In Figure 32 a typical response for the position and velocity of the poppet is shown. The figure depicts a situation where the relief valve is dumping oil to the reservoir during the time interval of t_0 to t_1 . Since the valve is open during this time period, the functional form of the state model for the poppet will be governed by Newton's second law. At time t_2 the poppet hits the seat, and the functional form of the state model will abruptly change. This causes a discontinuity in the poppet velocity. At time t_2 the opening forces are larger

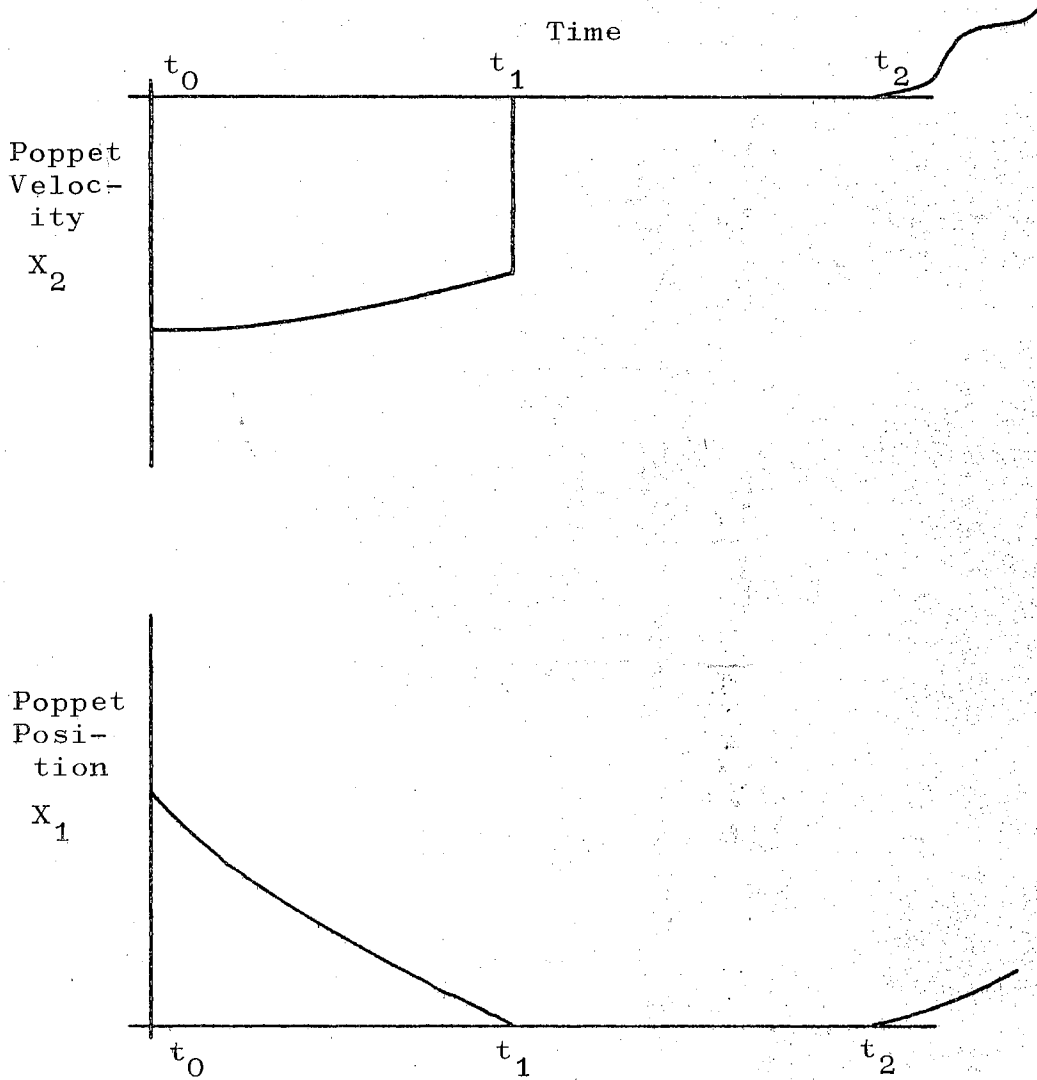


Figure 32. Response of Poppet's Velocity and Position

than the closing forces, and the functional form of the state model changes so that it is once again governed by Newton's Law.

The functional form of the state model for the spool valve shown in Figure 29 will depend upon the spool's position. If it is an overlapped valve, the mathematical model will depend upon whether the spool is open to the right, in its center position, or open to the left. And this provides another example of a dynamical system whose functional form of the right hand side of the state model depends upon the state vector.

The change in functional form of the right-hand side of the state vector model causes the following two problems to appear:

1. Difficulties are encountered in the numerical integration of the dynamical system equation. If a variable step size algorithm is employed, it will often (at points similar to that depicted at time t_1 in Figure 39) use such a small step size that very slow progress is made.
2. If the method of seeking principal planes is to be used on a parameter identification problem, it was stated in Chapter II that all of the third partial derivatives of the scalar performance function should be continuous. It is difficult if not impossible to

insure that such conditions are met at the points where the functional form of the dynamical equations change.

Proposals for Reducing the Problems Caused by Dynamical System Discontinuities

It may be possible to eliminate the second problem presented above by using techniques such as are presented in Lastman's Thesis (15). Lastman's basic approach is to expand the state vector in a special manner so that all of the state variables are continuous. This approach will not be simple, but it does provide one possible way for approaching the problem.

Zeiger (16) has recently presented a semiexhaustive search approach for solving the parameter identification problem presented in Chapter IV. The method presented by Zeiger requires only that the user be capable of numerically integrating the dynamical equations. Zeiger's approach becomes feasible for use on systems where the form of the dynamical equations change if the numerical integration can be performed without using too small a step size.

A method for avoiding the small step size problem will now be presented. A typical Runge Kutta numerical integration algorithm requires four evaluations of the right-hand side of the state model for each time step. The numerical integration of the differential equations which would provide the response shown in Figure 33 could be expected to

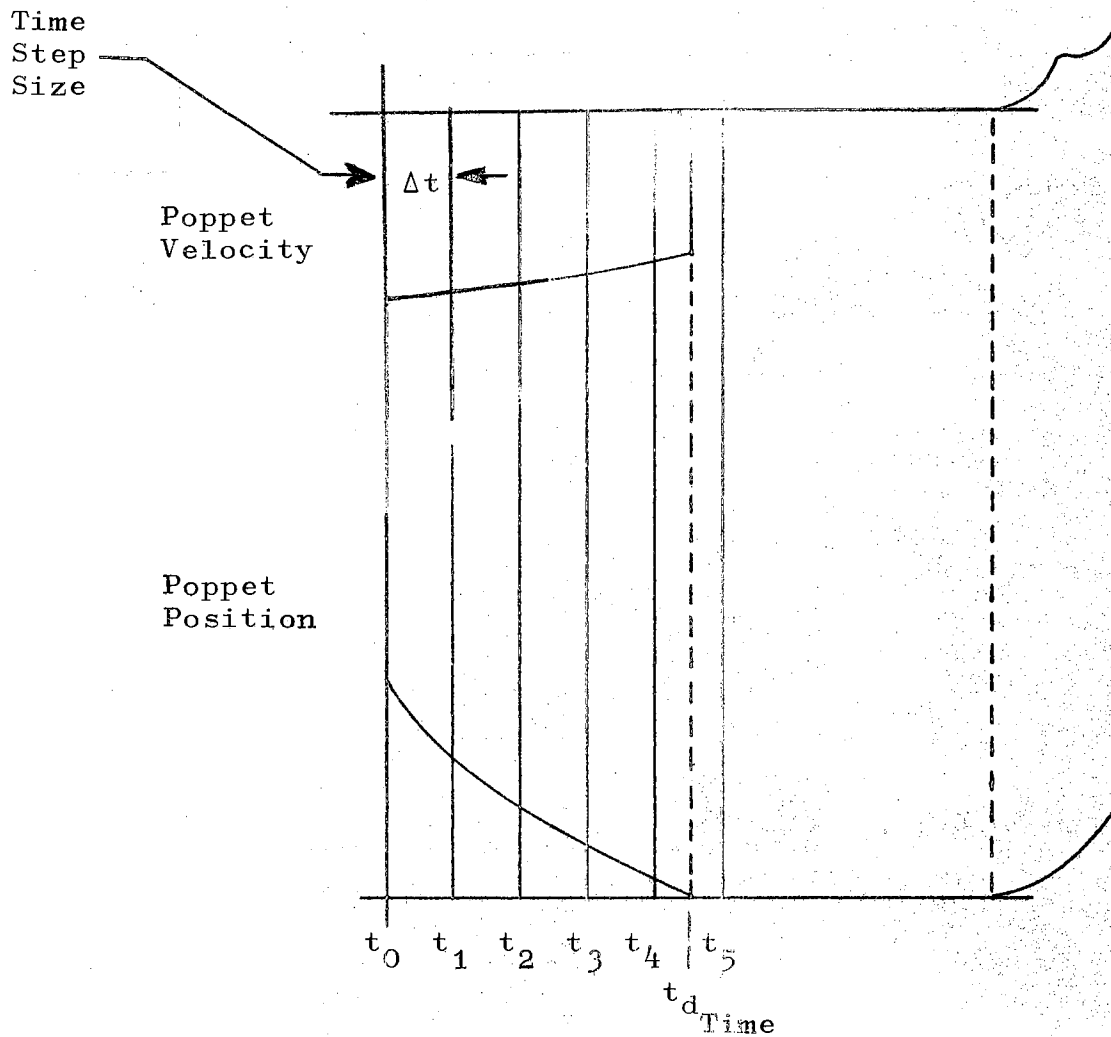


Figure 33. The Fifth Time Step Contains the Discontinuity Time, t_D

proceed smoothly during the first four time steps. But the functional form of the right-hand side of the state model will change during the fifth time step, and trouble will occur since the Runge Kutta numerical integration algorithm is based on the assumption that the functional form of the state model will not change,

If the precise time for the discontinuity, t_d , could be determined, and the value for the state vector at that time could be determined, the standard Runge Kutta Numerical integration procedure could be used to carry on from that point. One method for locating the time at which the discontinuity occurs, t_d , is to expand the state vector in a Taylor series. If the last time point at which the numerical integration was proceeding smoothly is used for the Taylor series expansion (t_4 in Figure 33), it will become

$$X(t_d) = X(t_4) + \left. \frac{dX}{dt} \right|_{t_4} (t_d - t_4) + \frac{1}{2} \left. \frac{d^2X}{dt^2} \right|_{t_4} (t_d - t_4)^2. \quad (5-1)$$

In the hypothetical examples of the poppet valve and the spool valve which were presented earlier in this chapter, the point at which the state model changed form was governed by one component of the state vector becoming equal to a particular value. For example, the functional form of the poppet valve equations change when the poppet position becomes equal to zero ($X_1 = 0$). The discontinuity time for the poppet example can be determined by truncating Equation (5-1) after its second term. The result is

$$t_d = t_4 \frac{-\frac{dX_1}{dt} \pm \sqrt{\left(\frac{dX_1}{dt}\right)^2 - 2 \left(\frac{d^2X_1}{dt^2}\right) (X_1(t_4) - X_1(t_d))}}{\frac{d^2X_1}{dt^2}}. \quad (5-2)$$

In Equation (5-2), the derivatives need to be evaluated at t_4 , and the value for $X_1(t_d)$ is zero for the poppet example. The equation for the first derivative is obtained from the state model, and it is

$$\left. \frac{dX_1}{dt} \right|_{t_4} = F_1(X(t_4), t_4). \quad (5-3)$$

The equation for the second derivative is obtained by differentiating Equation (5-3), then the result is

$$\frac{d^2X_1}{dt^2} = \left. \frac{\partial F_1}{\partial X} \right|_{(X(t_4), t_4)} \left. \frac{dX}{dt} \right|_{(X(t_4), t_4)} + \left. \frac{\partial F_1}{\partial t} \right|_{(X(t_4), t_4)}. \quad (5-4)$$

The state model for the system is

$$\left. \frac{dX}{dt} \right|_{(X(t_4), t_4)} = F(X(t_4), t_4). \quad (5-5)$$

Equations (5-3), (5-4), and (5-5) can now be substituted into Equation (5-2) to yield

$$t_d = t_4 \frac{-F_1 \pm \sqrt{F_1^2 - 2 \left(\frac{\partial F_1}{\partial X} F + \frac{\partial F_1}{\partial t} \right) [X_1(t_4) - X_1(t_d)]}}{\left(\frac{\partial F_1}{\partial X} F + \frac{\partial F_1}{\partial t} \right)}. \quad (5-6)$$

The discontinuity time can be determined from Equation (5-6). F_1 and all of the partial derivatives of F_1 in

Equation (5-6) must be evaluated at $(X(t_4), t_4)$.

Once the discontinuity time has been determined, the value for the state vector at that time can be determined by substituting Equations (5-4) and (5-5) into Equation (5-1) and truncating after two terms. The result is

$$X(t_d) = X(t_4) + F(t_d - t_4) + \left(\frac{\partial F}{\partial X} F + \frac{\partial F}{\partial t} \right) (t_d - t_4)^2. \quad (5-7)$$

Equations (5-6) and (5-7) appear to be rather complicated, but if the digital computer's capability for performing partial differentiation is used (see Appendix A), Equations (5-6) and (5-7) can be included in a Runge Kutta numerical integration algorithm which requires the user to provide very little additional information.

The steps which have been presented in this chapter are:

1. Use a standard Runge Kutta numerical integration algorithm until a point is reached at which the functional form of the differential equations changes.
2. Determine the precise time at which the equation functional form changes.
3. Determine the value of the state vector at the time where the equation functional form changes.
4. Return to step 1.

The steps which have been outlined in this chapter

should make the parameter identification procedure presented by Zeiger feasible for dynamical systems which have discontinuities.

CHAPTER VI

CONCLUSIONS AND RECOMMENDATIONS

Conclusions

The basic philosophy of the method of seeking principal planes is quite flexible. This is verified by the application in this research of the basic philosophy to three types of problems (1. algebraic minimization, 2. two-point boundary value problems, and 3. parameter identification of dynamical systems) within this thesis.

The method of seeking principal planes has the following desirable characteristics when applied to the problem of parameter identification of dynamical systems:

1. The method has excellent convergence characteristics when the parameter guess is close to an optimum point. This occurs since the method is a true second-order technique.
2. The method seems to be quite stable even if the original parameter guess is not close to an optimum parameter point, and it will quite often converge.
3. The method adjusts any specified parameters in the dynamical equations instead of adjusting only the coefficients.

4. The method of seeking principal planes does not require that the parameter identification problem first be reformulated into a two-point boundary value problem.
5. The desired response and the inputs for the dynamical equations can be presented in graphical form.
6. The method does not require the knowledge of the response of the entire state vector at all instants of time.
7. The method is not restricted to linear dynamical systems. It works well on parameter identification problems whose dynamical equations are non-linear.

The method of seeking principal planes has the following undesirable characteristics:

1. As presented in this thesis, limits have not been placed on the values which the parameters can assume. Sometimes the physics of a problem dictates that certain ranges of parameter values are unrealistic. Therefore, the computational algorithm could be improved by placing constraints on the allowable parameter values.
2. The method of seeking principal planes requires considerable computational effort since the second-order influence coefficients need

to be numerically integrated over the time period of interest.

Recommendations

The following specific recommendations are areas in which further work could be performed:

1. Constraints on the allowable ranges for the parameter values could be inserted into the computational algorithm.
2. The possibility of using hybrid computer facilities with the method of seeking principal planes for parameter identification should be investigated. This appears to be a very promising area.
3. The first and second-order sensitivity coefficients (X_{ψ_i} , X_{p_i} , $X_{\psi_j\psi_i}$, $X_{\psi_j\psi_i}$, and $X_{p_j p_i}$) might need to be scaled for some particular problems. Difficulties in this area were not encountered in any of the problems worked in this thesis.
4. The determination of convergence regions for several parameter identification problems would provide useful results for comparing the method of seeking principal planes with other procedures.
5. The proposals presented in Chapter V for minimizing the difficulties encountered when dynamical system discontinuities occur should

- be investigated.
6. The results presented in this thesis show that the method of seeking principal planes will work well for problems having up to five dependent variables. It would be interesting to investigate whether the procedure will work equally well in problems which have hundreds of independent variables.
 7. The method has promise of being a very powerful approach for determining the inverse of ill-conditioned matrices.
 8. For the optimal control of dynamical systems, one normally tries to find a continuous control which will cause the response of the dynamic system to minimize some specified performance index. Figure 34 illustrates that a continuous optimal control trajectory can be approximated by a series of constant control levels. Hence, the continuous optimal control of dynamical systems can be approximated as a parameter identification problem with the free parameters P_1 through P_7 as indicated in Figure 34.
 9. Kokotovic (17) has shown that the gradient vector for the parameter identification problem can be determined through the use of the adjoint differential equations. The advantage

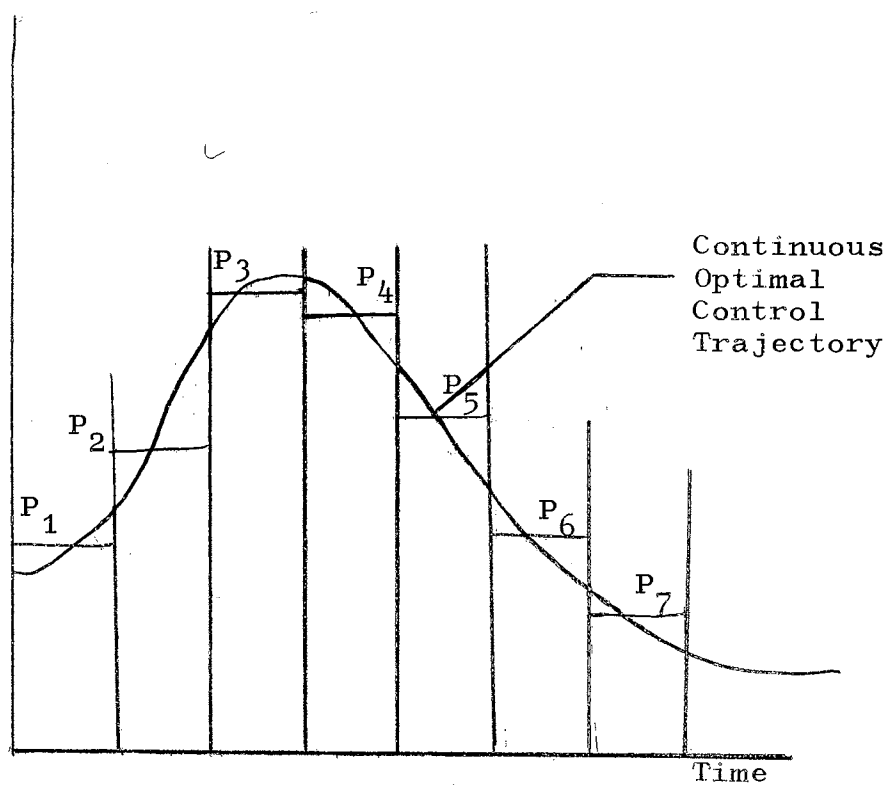


Figure 34. This Figure Illustrates That a Continuous Optimal Control Trajectory Can be Approximated by a Series of Constant Control Levels

of this approach is that the required computational effort remains feasible even when the number of parameters becomes large. If this approach can also be used for determining the matrix of second partial derivatives for the parameter identification problem, it may become quite feasible to use the method of seeking principal planes for the parameter identification problem even when a large number of parameters are involved.

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APPENDIX A

ANALYTIC PARTIAL DERIVATIVES OF ALGEBRAIC FUNCTIONS BY THE DIGITAL COMPUTER

In engineering and mathematical analysis, the need often arises to perform total or partial differentiation of an algebraic function. The basic rules which the mathematicians have established for differentiating an algebraic function are very systematic. In practice, the application of these rules to an arbitrary function often becomes very tedious and time consuming.

IBM has a compiler which is called FORMAC that will perform formal mathematical manipulations of mathematical functions. An integral part of the FORMAC compiler is the ability to differentiate most mathematical expressions. However, this program as described by Sammet and Bond (18) is available for only IBM computers operating under the PL/1 monitor.

Since the author did not have access to a FORMAC compiler, the author developed the algorithm given in this appendix. It will analytically differentiate most mathematical expressions which can be written in the Fortran IV language, and a listing is given at the end of this appendix. It is written in the Fortran IV language and can

be used on any computer which can process Fortran IV.

An algebraic function can contain two types of variables: dependent and independent variables. The value for a dependent variable cannot be determined unless the values of the particular independent variables upon which it depends are given first.

For a function which contains one independent variable and no dependent variables, the total derivative and partial derivative are identical.

If a function contains one independent variable and one or more dependent variables, the total derivative is determined by use of the chain rule. To utilize the chain rule, one must be able to calculate the partial derivative of the analytic function with respect to each of the dependent variables and with respect to the independent variable. Hence, if the partial derivatives of an algebraic function can be calculated, the total derivative can be determined by use of the chain rule. It is for this reason that the scope of this appendix is limited to the determination of analytical partial derivatives of algebraic functions.

Since the basic rules for calculating partial derivatives of algebraic functions are very systematic, the digital computer can be programmed to execute these rules. The following sections of this appendix will demonstrate one particular method for performing partial differentiation on the digital computer.

Operators and Operands Involved in Basic Algebraic Functions

The operators which this computational program will handle and their corresponding Fortran IV symbols are given in Table II.

It is convenient in the following pages to refer to any algebraic function which contains a single type operator as a basic algebraic function. It will be demonstrated in the following section that any analytic function can be decomposed into a series of basic algebraic functions.

Since each basic algebraic function has a single type of operator, it is reasonable to ask what constitutes an allowable operand and how many operands are required for each operator. There are three types of allowable operands for a basic algebraic function, and they are (1) a single constant, (2) a variable, or (3) an algebraic function. Categories one and two are actually special case of the third category. The first two categories are very important since they are the simplest algebraic functions known.

The addition and multiplication operators are variary operators since the number of operands depends upon the particular function being considered. The addition operator has one or more operands, and the multiplication operator has two or more operands. The power raising operator has two operands. The division and square root operations are treated within the computational program as a combination of multiplication and power raising. The rest of the operators

TABLE II
 OPERATORS AND FORTRAN IV SYMBOLS WHICH
 THE COMPUTATION PROGRAM WILL ACCEPT

Operator	Fortran, IV Symbol
Addition	+
Multiplication	*
Division	/
Power Raising	**
Subtraction	-
Exponentiation	EXP
Natural Logrithm	ALOG
Base 10 Logrithm	ALOG10
Sine	SIN
Cosine	COS
Tangent	TAN
Inverse Cosine	ARCOS
Inverse Sine	ARSIN
Inverse Tangent	ATAN
Hyperbolic Sine	SINH
Hyperbolic Cosine	COSH
Hyperbolic Tangent	TANH
Square Root	SQRT
Absolute Value	ABS
Cotangent	COTAN

in Table II are unary operators since they have only one operand.

Decomposing an Algebraic Function

In order to decompose an algebraic function which has been written in Fortran IV notation into a series of basic algebraic functions, it is necessary to utilize the standard Fortran IV order of computation. This hierarchy of operations is given in Table III. In the instances where the operations are of equivalent level, the operations are performed as they are encountered by proceeding from the left to the right through the function.

The decomposition of an algebraic function into a series of basic algebraic functions is best illustrated through the use of an example. It will be noted that the procedure uses the hierarchy of operations table extensively. The algebraic function whose equation is

$$(X(1)*X(2)+X(1))*SIN(X(2)) \quad (A-1)$$

will now be composed.

The hierarchy of operations table indicates that the first operation which must be performed is to remove the parenthesis which surround the subscripts of the variables. The algebraic function being considered can then be rewritten as

$$(X_1*X_2+X_1)*SIN(X_2). \quad (A-2)$$

TABLE III
HIERARCHY OF OPERATIONS

	Hierarchy
Remove parenthesis delimiting subscript	1st
Evaluate subfunction delimited by innermost parenthesis set by utilizing hierarchy steps three through six	2nd
Evaluation of Functions	3rd
Power Raising (**)	4th
Multiplication and Division (* and /)	5th
Addition and Subtraction (+ and -)	6th

The next step indicated by the hierarchy table is to evaluate the subfunction which is delimited by the innermost parenthesis set. The first innermost parenthesis set which is encountered in proceeding from the left to the right is the subfunction

$$X_1 * X_2 + X_1. \quad (A-3)$$

Hierarchy steps three through six are now performed on this subfunction. There are no function operators or power raising operators involved in the subfunction, and hierarchy steps three and four yield no results. The multiplication operator is involved; and this yields the first basic analytic function, F_1 . The equation for this basic analytic function is

$$F_1 = X_1 * X_2.$$

The first basic algebraic function is now substituted into Equation (A-3), and the subfunction becomes

$$F_1 + X_1. \quad (A-4)$$

The resulting subfunction contains only one operator and is defined as the second basic algebraic function, F_2 , where

$$F_2 = F_1 + X_1. \quad (A-5)$$

Equation (A-5) is the final form for the subfunction, and it is now substituted into the algebraic function being considered, Equation (A-2). The algebraic function becomes

$$F_2 * \text{SIN}(X_2). \quad (\text{A-6})$$

The hierarchy of operations table now indicates that the subfunction X_2 should now be evaluated. This subfunction is really a basic algebraic function with the implied operation of addition. Hence, the third basic algebraic function is

$$F_3 = + X_2. \quad (\text{A-7})$$

The substitution of Equation (A-7) into Equation (A-6) yields

$$F_2 * \text{SIN } F_3. \quad (\text{A-8})$$

Hierarchy step number three yields the next basic algebraic function which is

$$F_4 = \text{SIN } F_3. \quad (\text{A-9})$$

The substitution of Equation (A-9) into Equation (A-8) completes the reduction of the given algebraic function, Equation (A-1), to the basic algebraic function which is

$$F_2 * F_4. \quad (\text{A-10})$$

The results of decomposing the example function given in this section are summarized in Table IV, and it is noted that the algebraic function can be rewritten as a series of five basic algebraic functions.

TABLE IV

EXAMPLE OF DECOMPOSING AN ALGEBRAIC FUNCTION
TO A SERIES OF BASIC ALGEBRAIC FUNCTIONS

Algebraic Function Being Considered

$$(X(1)*X(2)+X(1)) * SIN(X(2))$$

Description as a Series of Basic Algebraic Functions

$$F_1 = X_1 * X_2$$

$$F_2 = F_1 + X_1$$

$$F_3 = + X_2$$

$$F_4 = SIN F_3$$

$$\text{Algebraic Function} = F_2 * F_4$$

Partial Derivatives of Basic Algebraic Functions

The partial derivatives for the basic algebraic functions are given in Table V. In this table the symbols U and V stand for algebraic functions; X_i stands for the variable X_i ; and the symbols U_{X_i} and V_{X_i} stand for the partial derivatives of U and V with respect to X_i .

The bases for the ability to perform partial differentiation on the digital computer of an algebraic function have now been formulated, and they are:

1. An algebraic function can be decomposed into a series of basic algebraic functions.
2. The partial derivatives for the basic algebraic functions are given in Table V.
3. The partial derivatives for an algebraic function can be obtained by the proper combination of the partial derivatives of the basic algebraic functions.

Representing an Algebraic Function by a String of Integers

It is convenient in the computational program to represent the algebraic function as a string of integers. This can easily be done since there are only nineteen allowable operators and only three types of operands for the algebraic functions under consideration.

In Table VI a number code has been set up for each of

TABLE V
PARTIAL DERIVATIVES OF BASIC
ALGEBRAIC FUNCTIONS

$$\frac{\partial (U + V)}{\partial X_i} = U_{X_i} + V_{X_i}$$

$$\frac{\partial (U * V)}{\partial X_i} = U_{X_i} * V + U * V_{X_i}$$

$$\frac{\partial (U ** V)}{\partial X_i} = V * U^{(V-1)} * U_{X_i} + U^V * (\text{LOG}_e U) * V_{X_i}$$

$$\frac{\partial (-U)}{\partial X_i} = - U_{X_i}$$

$$\frac{\partial \text{EXP}(U)}{\partial X_i} = \text{EXP}(U) U_{X_i}$$

$$\frac{\partial \text{ALOG}(U)}{\partial X_i} = U_{X_i} * U^{-1}$$

$$\frac{\partial \text{ALOG}_{10}(U)}{\partial X_i} = (\text{LOG}_{10} e) U_{X_i} * U^{-1}$$

$$\frac{\partial \text{SIN}(U)}{\partial X_i} = \text{COS}(U) U_{X_i}$$

$$\frac{\partial \text{COS}(U)}{\partial X_i} = - \text{SIN}(U) U_{X_i}$$

$$\frac{\partial \text{TAN}(U)}{\partial X_i} = U_{X_i} * \text{COS}^{-2}(U)$$

$$\frac{\partial \text{COTAN}(U)}{\partial X_i} = - U_{X_i} * \text{SIN}^{-2}(U)$$

$$\frac{\partial \text{ARSIN}(U)}{\partial X_i} = U_{X_i} * (1 - U^2)^{-\frac{1}{2}}$$

$$\frac{\partial \text{ARCOS}(U)}{\partial X_i} = - U_{X_i} * (1 - U^2)^{-\frac{1}{2}}$$

TABLE V (Continued)

$$\frac{\partial \text{ATAN} (U)}{\partial X_i} = U_{X_i} * (1 + U^2)^{-1}$$

$$\frac{\partial \text{SINH} (U)}{\partial X_i} = U_{X_i} * \text{COSH} (U)$$

$$\frac{\partial \text{COSH} (U)}{\partial X_i} = U_{X_i} * \text{SINH} (U)$$

$$\frac{\partial \text{TANH} (U)}{\partial X_i} = U_{X_i} * \text{COSH}^{-2} (U)$$

$$\frac{\partial \text{ABS} (U)}{\partial X_i} = U_{X_i} * U * \text{ABS}^{-1} (U)$$

TABLE VI¹
 NUMBER CODE USED TO REPRESENT
 ALGEBRAIC FUNCTION

Operator	Code Number	Operator	Code Number
+	1	TAN	10
*	2	ATAN	11
**	3	COTAN	12
-	4	ALOG	13
		ALOG10	14
EXP	5	SINH	15
SIN	6	COSH	16
ARSIN	7	TANH	17
COS	8	SQRT	18
ARCOS	9	ABS	19
	Operand	Code Number	
	Constant	51	
	Variable	52	
	Function	53	

¹The idea of using a number code to represent an algebraic function was first presented to the author by Stanley Wendt, a fellow graduate student.

the operators and operands.

It is possible to go directly from the description of the function as a series of basic algebraic functions to an integer string representation. This can be done in three simple steps:

1. The basic algebraic function representation is written as a row rather than as a column. The example given in Table IV then becomes

$$\begin{array}{cccccc}
 F_1 & F_2 & F_3 & F_4 & \text{Algebraic} & \\
 & & & & \text{Function} & \\
 \underbrace{X_1 * X_2}_{F_1} & \underbrace{F_1 + X_1}_{F_2} & \underbrace{+X_2}_{F_3} & \underbrace{\text{SIN } F_3}_{F_4} & \underbrace{F_2 * F_4}_{\text{Algebraic}} & \text{Function} \\
 & & & & & \text{Function}
 \end{array} \quad (A-11)$$

2. As an aid for distinguishing where each basic function begins, the operator is written first. Hence, Equation (A-11) is rewritten

$$\begin{array}{cccccc}
 F_1 & F_2 & F_3 & F_4 & \text{Algebraic} & \\
 & & & & \text{Function} & \\
 \underbrace{*X_1 X_2}_{F_1} & \underbrace{+F_1 X_1}_{F_2} & \underbrace{+X_2}_{F_3} & \underbrace{\text{SIN } F_3}_{F_4} & \underbrace{*F_2 F_4}_{\text{Algebraic}} & \text{Function} \\
 & & & & & \text{Function}
 \end{array} \quad (A-12)$$

3. The number code which is given in Table VI is now substituted into Equation (A-12). This results in an integer string representation for the algebraic function. The auxiliary integer string gives the subscripts for the operands.

	F_1	F_2	F_3	F_4	Algebraic Function
Integer String -	2 52 52	1 53 52	1 52	6 53	2 53 53
Subscripts -	1 2	1 1	2	3	2 4

(A-13)

Partial Derivatives of Algebraic Functions

Represented as an Integer String

In Table VII the partial derivatives for the basic algebraic functions are given. If either U or V in the table are independent of the variable X_i , a considerable amount of simplification can be performed since many of the terms in the resulting derivative are multiplied by zero.

The performance of this simplification can be done as the derivatives of the algebraic functions are being formed if one adopts a dependency notation. If a dot is placed above an operand, it is dependent upon X_i . If there is no dot above the operand, it is independent of X_i .

In Table VII the partial derivatives for the basic functions are written in the notation equivalent to that used in Equation (A-12). In this table U, V, W, and Z represent the operands. A dot placed above them indicates that they are dependent. The subscript X_i represents the partial derivative with respect to X_i .

The column labeled "operands involved" will be discussed in detail later.

The procedure for determining if an operand is

TABLE VII
PARTIAL DERIVATIVES WHICH UTILIZE
DEPENDENCY INFORMATION

	Operands Involved
$\frac{\partial (+\dot{U}VWZ)}{\partial X_i} = + U_{X_i} Z_{X_i}$	None
$\frac{\partial (*\dot{U}VWZ)}{\partial X_i} = \underbrace{* U_{X_i} VWZ}_{F_j} \underbrace{* UVWZ_{X_i}}_{F_{j+1}} + F_j F_{j+1}$	All if the number of dependent operands is greater than one. All except the dependent operand if there is only one dependent operand.
$\frac{\partial (**\dot{U}V)}{\partial X_i} = \underbrace{-1}_{F_j} \underbrace{+ VF_j}_{F_{j+1}} \underbrace{** UF_{j+1}}_{F_{j+2}} \text{ etc.}$ $* VF_{j+2} U_{X_i} ** UV \text{ LOG}_e U$ $* F_{j+4} F_{j+5} V_{X_i} + F_{j+3} F_{j+6}$	U, V
$\frac{\partial (**\dot{U}V)}{\partial X_i} = -1 + V F_j ** U F_{j+1}$ $* V F_{j+2} U_{X_i}$	U, V
$\frac{\partial (**\dot{U}V)}{\partial X_i} = ** UV \text{ LOG}_e U * F_j F_{j+1} V_{X_i}$	U, V
$\frac{\partial (-\dot{U})}{\partial X_i} = -U_{X_i}$	None
$\frac{\partial \text{EXP } \dot{U}}{\partial X_i} = \text{EXP } U * F_j U_{X_i}$	U
$\frac{\partial \text{ALOG } \dot{U}}{\partial X_i} = -1 ** U F_j * F_{j+1} U_{X_i}$	U

TABLE VII (Continued)

	Operands Involved
$\frac{\partial \text{ALOG}_{10} \dot{U}}{\partial X_i} = -1 ** U F_j + \text{LOG}_{10} e$ $* F_{j+1} F_{j+2} U_{X_i}$	U
$\frac{\partial \text{SIN} \dot{U}}{\partial X_i} = \text{COS} U * F_j U_{X_i}$	U
$\frac{\partial \text{COS} \dot{U}}{\partial X_i} = -1 \text{ SIN} U * F_j F_{j+1} U_{X_i}$	U
$\frac{\partial \text{TAN} \dot{U}}{\partial X_i} = -2 \text{ COS} U ** F_{j+1} F_j$ $* F_{j+2} U_{X_i}$	U
$\frac{\partial \text{COTAN} \dot{U}}{\partial X_i} = -1 -2 \text{ SIN} U ** F_{j+2} F_{j+1}$ $* F_j F_{j+3} U_{X_i}$	U
$\frac{\partial \text{ARSIN} \dot{U}}{\partial X_i} = -.50 + 2 ** U F_{j+1}$ $- F_{j+2} + 1 F_{j+3}$ $** F_{j+4} F_j * F_{j+5} U_{X_i}$	U
$\frac{\partial \text{ARCOS} \dot{U}}{\partial X_i} = -.50 + 2 ** U F_{j+1}$ $- F_{j+2} + 1 F_{j+3}$ $** F_{j+4} F_j * F_{j+5} U_{X_i}$ $- F_{j+6}$	U
$\frac{\partial \text{ATAN} \dot{U}}{\partial X_i} = -1 + 2 ** U F_{j+1} + 1 F_{j+2}$ $** F_{j+3} F_j * F_{j+4} U_{X_i}$	U

TABLE VII (Continued)

	Operands Involved
$\frac{\partial \text{SINH } \dot{U}}{\partial X_i} = \text{COSH } U * F_j U_{X_i}$	U
$\frac{\partial \text{COSH } \dot{U}}{\partial X_i} = \text{SINH } U * F_j U_{X_i}$	U
$\frac{\partial \text{TANH } \dot{U}}{\partial X_i} = -2 \text{ COSHU} ** F_{j+1} F_j$ $* F_{j+2} U_{X_i}$	U
$\frac{\partial \text{ABS } \dot{U}}{\partial X_i} = -1 \text{ ABSU} ** F_{j+1} F_j$ $* U F_{j+2} U_{X_i}$	U

dependent after the equation has been set up in a form analogous to Equation (A-12) involves three steps:

1. Steps two and three are performed on one basic function at a time starting from the left.
2. The dependency notation is set for the operand if
 - a. it is equal to X_i or
 - b. the operator for the basic function to which it refers is dependent.
3. The operator is defined to be dependent if any of its operands are dependent.

In Table VII there is a column which is labeled operands involved. Information in this column is used to determine which if any of the basic algebraic functions should be included in the equation for the partial derivative. This can be determined by a five-step process:

1. Steps two, three, and four are performed on one basic function at a time starting from the right side of the equation.
2. If the involvement notation for the operator has already been set, all of its operands are involved.
3. Even though the operator is not involved, the operands may still be involved as is indicated by the "operands involved" column of Table VII.
4. The operator of a basic function is defined

as being involved if an operand which refers to it is involved.

5. Only the basic functions whose operator has been designated as involved are included in the equation for the partial derivative.

The dependency and involvement information is used to keep the expression for the derivative of the function relatively free of unnecessary terms. The formal rules for setting up the equation for the derivative of a function will now be stated, and then an example problem will be worked.

In the rules which follow the subscript I refers to the number for the next basic function to be inserted into the derivative equation chain. N stands for the number of basic functions which are required for writing the derivative of the basic function being operated upon:

1. The equation is set up in a form analogous to Equation (A-12).
2. The operands which are dependent and the basic functions which are involved are determined by using the rules outlined previously.
3. An auxiliary chain is set up which contains the partial derivative of each of the operands.
4. The function which is being differentiated is operated upon one basic function at a time. The basic function at the extreme left of the

equation is considered first, and then one proceeds toward the right.

5. Is the basic function involved?

a. Yes. It is inserted into the derivative chain; I is set equal to $I + 1$; and one proceeds to step 6.

b. No. The following changes are performed on the portion of the equation chain and the auxiliary chain which lies to the right of the basic function which is being operated upon.

F_j is changed to F_{j-1} , and $\frac{\partial F_j}{\partial X_i}$ is changed to $\frac{\partial F_{j-1}}{\partial X_i}$ if j is greater than

I . One then proceeds to step 6.

6. Are any of the operands dependent?

a. Yes. The derivative for the basic function is inserted into the derivative chain.

The following changes are performed on the portion of the equation chain and the auxiliary chain which lie to the right of the basic function which

is being operated upon. F_j is changed to F_{j+N} and $\frac{\partial F_j}{\partial X_i}$ is changed to $\frac{\partial F_{j+N}}{\partial X_i}$ if

$j \geq I$. F_{I-1} is changed to F_{I-1+N} ;

$\frac{\partial F_{I-1}}{\partial X_i}$ is changed to $\frac{\partial F_{I-1+N}}{\partial X_i}$; I is set

equal to $I + N$; and one returns to

step 4.

b. No. One returns to step 4.

The example function whose derivative with respect to X_2 will be formed using the above rules is given by Equation (A-12). If a dot is placed above each operator and operand which is dependent, the function will appear as follows:

$$* \dot{X}_1 \dot{X}_2 + \dot{F}_1 X_1 + \dot{X}_2 \text{ SIN } \dot{F}_3 * \dot{F}_2 \dot{F}_4. \quad (\text{A-14})$$

If a \wedge is used to indicate involvement, the equation becomes

$$\begin{array}{c} \wedge \wedge \wedge \wedge \wedge \wedge \wedge \wedge \wedge \wedge \\ * \dot{X}_1 \dot{X}_2 + \dot{F}_1 X_1 + \dot{X}_2 \text{ SIN } \dot{F}_3 * \dot{F}_2 \dot{F}_4. \end{array} \quad (\text{A-15})$$

Hence, it is noted that all, except the final one, of the basic functions will appear in the equation for the derivative.

Step three is now performed and yields

$$\begin{array}{c} \wedge \wedge \wedge \wedge \wedge \wedge \wedge \wedge \wedge \wedge \\ * \dot{X}_1 \dot{X}_2 + \dot{F}_1 X_1 + \dot{X}_2 \text{ SIN } \dot{F}_3 * \dot{F}_2 \dot{F}_4 \end{array} \quad (\text{A-16})$$

$$0 \quad 1 \quad \frac{\partial F_1}{\partial X_2} \quad 0 \quad 1 \quad \frac{\partial F_3}{\partial X_2} \quad \frac{\partial F_2}{\partial X_2} \quad \frac{\partial F_4}{\partial X_2} \cdot$$

If steps five and six are performed on the first basic function of Equation (A-16), the equation which results for the first portion of the derivative is

$$\underbrace{* X_1 X_2}_{F_1} \quad \underbrace{* X_1 1}_{F_2} \quad (\text{A-17})$$

The command which the user must supply within his Fortran IV program in order to read the equation which is given on the data card is

```
CALL FORTIN(NAME).
```

In the previous statement, NAME is any subscripted or simple integer variable. The computation algorithm will assign an integer constant to this integer variable which is symbolic information for where the equation is stored.

Subroutine FORTIN changes the equation which the user supplies on a data card to an integer string similar to that given by Equation (A-13). The equation which is supplied on the data card must be contained in columns 7 through 72. The independent variables must be either X or Y, and they must be subscripted variables. Any proper Fortran IV equation which can be written by using the operators given in Table II, floating point constants, E type constants, integer constants, and the subscripted independent variables X or Y is allowable. If the equation is continued on more than one data card, a C must be placed in column 6 of every data card except the last one.

Subroutine PARDIF will determine the partial derivative for an equation, and the necessary command is

```
CALL PARDIF (NAME1, NAME2,N).
```

In the previous command NAME1 is the integer name for the equation whose partial derivative with respect to X(N) is

to be taken. The resulting equation is assigned the integer name NAME2.

Subroutine ISTORE stores the integer strings for every equation which is read in from data cards or generated within a program.

A function subprogram with the title

VAL (NAME, X)

has been supplied. Upon return from this function subprogram VAL will contain the value for the equation whose symbolic name is NAME when it is evaluated for independent variable values which have been supplied through X. The dimension statement DIMENSION X(50) must be provided in all programs which use function subprogram VAL.

A function subprogram with the title

DVAL (NAME, X)

has been supplied. Upon return from this function subprogram DVAL will contain the double precision value for the equation whose symbolic name is NAME when it is evaluated for the double precision independent variable values which have been supplied through X. The following statements must be provided in all programs which use function subprogram DVAL.

DIMENSION X(50)

DOUBLE PRECISION DVAL, X.

In Figure 35 an example program is supplied which determines the value for the equation

$$3.2 * X(1) ** X(2) - 4.2E02 * X(2) \quad (A-21)$$

when evaluated at

$$X(1) = 1.5$$

$$X(2) = -.72.$$

The partial derivative of the equation with respect to $X(2)$ is then determined and its value is evaluated at the point

$$X(1) = -23.0$$

$$X(2) = 7.2.$$

In Figure 36 an example program has been supplied for determining, evaluating, and writing all of the first and second partial derivatives for Equation (A-21).

```

0000000001111111112222222222333333333333444444444455555555556666666666
1234567890123456789012345678901234567890123456789012345678901234567890

```

```

      IMPLICIT INTEGER*2 (I-N)
      DIMENSION X(50)
100 FORMAT (E15.7)
C
C   READ THE EQUATION WHICH IS ON THE DATA CARD
C
      CALL FORTIN(IF)
      X(1)=1.5
      X(2)=-.72
C
C   DETERMINE AND WRITE THE VALUE FOR THE EQUATION EVALUATED AT
C   THE POINT X(1)=1.5   X(2)=-.72
C
      FVAL=VAL(IF,X)
      WRITE (6,100) FVAL
C
C   DETERMINE THE PARTIAL DERIVATIVE FOR THE EQUATION WITH RESPECT
C   TO X(2)
C
      J=2
      CALL PARDIF (IF,JPARD,J)
      X(1)=-23.0
      X(2)=-.72
C
C   DETERMINE AND WRITE THE PARTIAL DERIVATIVE FOR THE EQUATION
C   EVALUATED AT X(1)=-23.0   X(2)=-.72
C
      FPAR=VAL(JPARD,X)
      WRITE (6,100) FPAR
      CALL EXIT
      END

```

```

3.2*X(1)**X(2)-4.2E02*X(2)

```

Figure 35. Example of Calculating a Partial Derivative

```

00000000011111111112222222223333333333444444444455555555566
1234567890123456789012345678901234567890123456789012345678901

```

```

      IMPLICIT INTEGER*2 (I-N)
      DIMENSION X(50)
      DIMENSION IF1(2),IF2(2,2)
100  FORMAT (4E15,7)
      X(1)=1.0
      X(2)=2.0
      CALL FORTIN (IF)
      VALIF=VAL(IF,X)
      WRITE (6,100) VALIF
      DO 1 I=1,2
      CALL PARDIF (IF,IF1(I),I)
      VALIFI=VAL(IF1(I),X)
      WRITE (6,100) VALIFI
      DO 1 J=1,2
      CALL PARDIF (IF1(I),IF2(I,J),J)
      VALIF2=VAL(IF2(I,J),X)
      WRITE (6,100) VALIF2
1  CONTINUE
      END

```

```

3.2*X(1)**X(2)-4.2E02*X(2)

```

Figure 36. Example of Calculating First and Second Partial Derivatives

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A-24

00000000111111112222222222333333333344444444445555555555666666666677777777778
 12345678901234567890123456789012345678901234567890123456789012345678901234567890

```

SUBROUTINE FORTIN (NAME)                                001 006
C                                                         002
C   I - POSITION OF FIN BEING CHECKED                     003
C   J - POSITION OF NFIN BEING SET.                       004
C   L - POSITION OF NFIN WITHIN THE AUXILIARY FUNCTION    005
C         BEING CHECKED.                                 006
C   ALPH - VARIABLE USED TO DECODE THE ALPHAMERIC FORTRAN 4 INPUT 007
C         FUNCTION.                                       008
C   NFLOT - TOTAL LENGTH OF NFIN(1,J)                    009
C   NFIN(I,J)                                             010
C   NFIN(I,J) - INTEGER STRING FOR THE INPUT FUNCTION. J INDI- 011
C         CATES THE COLUMN BEING REFERED TO IN THE STRING. 012
C   NFIN(2,J) - THE SUBSCRIPT WHICH BELONGS TO OPERAND NFIN(1,J).013
C         IF NFIN(1,J) IS NOT AN OPERAND, THAN NFIN(2,J)=0.014
C   NFIN(I,J)                                             015
C   NFIN(1,J) - THE FUNCTION IN ITS FINAL DECODED FORM.   016
C   NFIN(2,J) - SUBSCRIPT WHICH GOES ALONG WITH NFIN(1,J). 017
C   NFUNTO - TOTAL LENGTH OF NFIN(1,J)                   018
C   C(I) - CONSTANT NUMBER I.                            019
C   NPARR - COLUMN OF RIGHT HAND PARENTHESIS.           020
C   NPARR - COLUMN OF LEFT HAND PARENTHESIS.           021
C   NAME - FUNCTION NAME.                                022
C   FIN - ALPHAMERIC FORTRAN 4 INPUT OF THE FUNCTION.   023
C   NC - CONSTANT NUMBER.                                024
C   NLEFT - NUMBER OF PLACES THE DECIMAL POINT IS TO THE LEFT 025
C         OF NUMERAL BEING CONSIDERED.                  026
C                                                         027
C   CODE FOR ALPH                                         028
C   1 1 21 A 35 D 029 009
C   2 2 22 B 36 P 030 010
C   3 3 23 C 37 Q 031 011
C   4 4 24 D 38 R 032 012
C   5 5 25 E 39 S 033 013
C   6 6 26 F 40 T 034 014
C   7 7 27 G 41 U 035 015
C   8 8 28 H 42 V 036 016
C   9 9 29 I 43 W 037 017
C   10 0 30 J 44 X 038 018
C   11 . 31 K 45 Y 039 019
C   12 + 32 L 46 Z 040 020
C   13 - 33 M 47 { 041 021
C   14 * 34 N 48 } 042 022
C   15 / 043 023
C   16 THROUGH 20 CORRESPOND TO BLANK 044 024
C                                                         045
C   CODE FOR NFIN                                         046
C   1 + 11 TAN 47 { 047 027
C   2 * 12 ATAN 48 } 048
C   3 / 13 ABS 50 INTEGER CONSTANT 049
C   4 ** 14 ALOG 51 FLOATING POINT CONSTANT 050
C   5 - 15 ALOGIO 52 VARIABLE 051
C   6 EXP 16 SING 53 AUX. FUNCTION 052 032
C   7 SIN 17 COSH 053 033
C   8 ARSIN 18 TANH 054
C   9 COS 19 COTAN 055

```

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000000000111111111122222222223333333333333333444444444455555555556666666666777777777788
 12345678901234567890123456789012345678901234567890123456789012345678901234567890

C	10	ARCOS	20	SQRT		056
C		THE FINAL CODE FOR NFUN IS THE SAME AS THE ABOVE EXCEPT THAT				057
C		3	(FLOATING POINT VALUE)**(FLOATING POINT VALUE)			058
C		4	(FLOATING POINT VALUE)**(INTEGER VALUE)			059
C		REMARKS				060
C		THE FORTRAN 4 FUNCTION THAT IS TO BE READ IN MUST BE WRITTEN				061
C		IN COLUMNS 7 THROUGH 72 OF THE DATA CARDS. COLUMN 6 MUST BE				062
C		BLANK IF THE FUNCTION IS TATALLY CONTAINED ON ONE CARD. IF THE				063
C		FUNCTION IS CONTINUED ON MORE THAN ONE CARD, THAN THE LAST CARD				064
C		MUST HAVE A BLANK IN COLUMN 6 AND EACH OF THE PREVIOUS CARDS				065
C		OF THE CONTINUED FUNCTION MUST HAVE A 'C' (FOR CONTINUATION) IN				066
C		COLUMN 6.				067
C		MAXL - MAXIMUM LENGTH OF INPUT FUNCTION (66 PER CARD).				068
C		IMPLICIT INTEGER*2 (I-N)				069
C		INTEGER*4 IC				070
C		DIMENSION ALPHA(48),CC(8),NFUN(2,MAXL),FIN(MAXL),NPARL(10)				071
C		DIMENSION ALPHA(48),NFUN(2,200),FIN(200),NPARL(10),CC(8),IC(2)				072
C		DATA CC(1),CC(2),CC(3),CC(4),CC(5),CC(6),CC(7),CC(8),NC1,NC2				073
C		10.0,.50,-.50,1.0,-1.0,2.0,-2.0,.43429 ,9.0/				074
C		DATA ALPHA/1H1,1H2,1H3,1H4,1H5,1H6,1H7,1H8,1H9,1H0,1H.,1H+,1H-,				075 039
C		11H*,1H/,1H ,1H ,1H ,1H ,1H ,1HA,1HB,1HC,1HD,1HE,1HF,1HG,1HH,				076 040
C		21HI,1HJ,1HK,1HL,1HM,1HN,1HO,1HP,1HQ,1HR,1HS,1HT,1HU,1HV,				077 041
C		31HW,1HX,1HY,1HZ,1H(/,1H)/				078 042
C		MAXFUN - MAXIMUM LENGTH OF ANY FUNCTION TO BE GENERATED.				079
C		COMMON /BLK1/ NFUN(2,MAXFUN),NFUNTO				080
C		COMMON /BLK1/ NFUN(2,300),NFUNTO				081
C		MAXC - MAXIMUM NUMBER OF CONSTANTS ALLOWED.				082
C		COMMON /BLK2/ C(MAXC),NC				083
C		COMMON /BLK2/ C(200),NC				084
C	100	FORMAT (5X,A1,66A1,8X)				085
C	101	FORMAT (40I3)				086 046
C	102	FORMAT (' AN IMPROPER FORTRAN 4 FUNCTION HAS BEEN SUPPLIED ON				087 047
C		THE DATA CARD')				088 048
C	103	FORMAT (' NFUN(1,J)=')				089 049
C	104	FORMAT (' NFUN(2,J)=')				090 050
C	105	FORMAT (' NAUXF(1,J)=')				091 051
C	106	FORMAT (' NAUXF(2,J)=')				092 052
C	107	FORMAT (' NFUN(1,J)=')				093 053
C	108	FORMAT (' NFUN(2,J)=')				094 054
C	109	FORMAT (' C(' ,15,')=' ,E15.7)				095 055
C		READ THE INPUT FUNCTION				096 056
C		II=1				097
C		NFTOT=66				098
C	90	READ (5,100) CONT,(FIN(I),I=II,NFTOT)				099
C		WRITE (6,100) (FIN(I),I=II,NFTOT)				100
C		IF (CONT.EQ.ALPH(20)) GO TO 91				101
C		II=NFTOT+1				102
C		NFTOT=NFTOT+66				103
C		GO TO 90				104
C	91	CONTINUE				105
C		SET CONSTANTS C(1) THROUGH C(8)				106
C		NC2=NC2+1				107
C		IF (NC2.GT.1) GO TO 8				108
C		NC=9				109
C		DO 6 I=1,8				110

80/80 LIST

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6	C(I)=CC(I)	111
8	CONTINUE	112
C	REMOVE THE BLANKS	113
	J=0	114
	DO 1 I=1,NFTOT	115
	IF (FIN(I).EQ.ALPH(16)) GO TO 1	116
	J=J+1	117
	FIN(J)=FIN(I)	118
1	CONTINUE	119
	NFTOT=J	120
C		121
C		122
C	CODE NFIN(1,J) AND NFIN(2,J)	123
C		124
C		125
	J=0	126
	IBASE =0	127
	I=1	128
	NLC=1	129
	NPARL(1)=0	130
	NFUNTO=0	131
2	CONTINUE	132
	J=J+1	133
	IF (I.GT.NFTOT) GO TO 50	134
	NFIN(2,J)=0	135
C	CHECK IF FIN(I) IS A VARIABLE	136
	IF (FIN(I).NE.ALPH(44).AND.FIN(I).NE.ALPH(45)) GO TO 4	137
	NFIN(1,J)=52	138
C	DETERMINE THE VALUE FOR THE SUBSCRIPT	139
	KK=I+2	140
	J=J+1	141
	IE=1	142
	NIC=1	143
	GO TO 41	144
C	CODE (145
	4 IF (FIN(I).NE.ALPH(47)) GO TO 5	146
	NFIN(1,J)=47	147
	NLC=NLC+1	148
	NPARL(NLC)=J	149
	I=I+1	150
	GO TO 2	151
C	CODE)	152
	5 IF (FIN(I).NE.ALPH(48)) GO TO 10	153
	I=I+1	154
	NFIN(1,J)=48	155
	GO TO 50	156
C	CODE +	157
	10 IF (FIN(I).NE.ALPH(12)) GO TO 11	158
	NFIN(1,J)=1	159
	I=I+1	160
	GO TO 2	161
C	CODE -	162
	11 IF (FIN(I).NE.ALPH(13)) GO TO 12	163
	NFIN(1,J)=5	164
	I=I+1	165

80/80 LIST

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	GO TO 2	166
C	CODE *	167
	12 IF (FIN(I).NE.ALPH(14)) GO TO 14	168
	NFIN(1,J)=2	169
C	CODE **	170
	13 I=I+1	171
	IF (FIN(I).NE.ALPH(14)) GO TO 2	172
	NFIN(1,J)=4	173
	I=I+1	174
	GO TO 2	175
C	CODE /	176
	14 IF (FIN(I).NE.ALPH(15)) GO TO 15	177
	NFIN(1,J)=3	178
	I=I+1	179
	GO TO 2	180
C	CODE EXP	181
	15 IF (FIN(I).NE.ALPH(25)) GO TO 21	182
	NFIN(1,J)=6	183
	I=I+3	184
	GO TO 2	185
	21 IF (FIN(I).NE.ALPH(39)) GO TO 24	186
	IF (FIN(I+1).NE.ALPH(37)) GO TO 22	187
C	CODE SORT	188
	NFIN(1,J)=20	189
	I=I+4	190
	GO TO 2	191
	22 IF (FIN(I+3).NE.ALPH(28)) GO TO 23	192
C	CODE SINH	193
	NFIN(1,J)=16	194
	I=I+4	195
	GO TO 2	196
C	CODE SIN	197
	23 NFIN(1,J)=7	198
	I=I+3	199
	GO TO 2	200
	24 IF (FIN(I).NE.ALPH(21)) GO TO 35	201
	IF (FIN(I+1).NE.ALPH(40)) GO TO 25	202
C	CODE ATAN	203
	NFIN(1,J)=12	204
	I=I+4	205
	GO TO 2	206
	25 IF (FIN(I+1).NE.ALPH(22)) GO TO 26	207
C	CODE ABS	208
	NFIN(1,J)=13	209
	I=I+3	210
	GO TO 2	211
	26 IF (FIN(I+1).NE.ALPH(38)) GO TO 28	212
	IF (FIN(I+2).NE.ALPH(39)) GO TO 27	213
C	CODE ARSIN	214
	NFIN(1,J)=8	215
	I=I+5	216
	GO TO 2	217
C	CODE ARCOS	218
	27 NFIN(1,J)=10	219
	I=I+5	220

80/80 LIST

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	GO TO 2	221
	28 IF (FIN(I+4).NE.ALPH(1)) GO TO 29	222
C	CODE ALOG10	223
	NFIN(1,J)=15	224
	I=I+6	225
	GO TO 2	226
C	CODE ALOG	227
	29 NFIN(1,J)=14	228
	I=I+4	229
	GO TO 2	230
	35 IF (FIN(I).NE.ALPH(23)) GO TO 38	231
	IF (FIN(I+2).NE.ALPH(40)) GO TO 36	232
C	CODE COTAN	233
	NFIN(1,J)=19	234
	I=I+5	235
	GO TO 2	236
	36 IF (FIN(I+3).NE.ALPH(28)) GO TO 37	237
C	CODE COSH	238
	NFIN(1,J)=17	239
	I=I+4	240
	GO TO 2	241
C	CODE COS	242
	37 NFIN(1,J)=9	243
	I=I+3	244
	GO TO 2	245
	38 IF (FIN(I).NE.ALPH(40)) GO TO 40	246
	IF (FIN(I+3).NE.ALPH(20)) GO TO 39	247
C	CODE TANH	248
	NFIN(1,J)=18	249
	I=I+4	250
	GO TO 2	251
C	CODE TAN	252
	39 NFIN(1,J)=11	253
	I=I+3	254
	GO TO 2	255
C	IE=1 INTEGER. IE=2 FLOATING POINT. IE=3 E TYPE RAISED TO A	256
C	POSITIVE POWER. IE=4 E TYPE RAISED TO NEGATIVE POWER.	257
	40 CONTINUE	258
	KK=I	259
	IE=1	260
	NIC=1	261
	41 NLEFT=0	262
	IC(NIC)=0	263
	DO 42 K=KK,NFTOT	264
	I=K	265
	IF (FIN(K).EQ.ALPH(11)) GO TO 43	266
	IF (FIN(K).EQ.ALPH(25)) GO TO 44	267
	IFIN=-1	268
	DO 93 M=1,9	269
	93 IF (FIN(K).EQ.ALPH(M)) IFIN=M	270
	IF (FIN(K).EQ.ALPH(10)) IFIN=0	271
	IF (IFIN.EQ.-1) GO TO 46	272
	NLEFT=NLEFT+I	273
	IC(NIC)=IC(NIC)*10+IFIN	274
	GO TO 42	275

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43	IE=2	276
	NLEFT=0	277
	NIC=NIC+1	278
	IC(NIC)=0	279
42	CONTINUE	280
	I=NFTOT+1	281
46	GO TO (48,47,49,49),IE	282
44	IE=3	283
	KK=I+2	284
	IF (FIN(I+1).EQ.ALPH(13)) GO TO 45	285
	IF (FIN(I+1).NE.ALPH(12)) KK=I+1	286
	GO TO 47	287
45	IE=4	288
47	RIC=IC(NIC)	289
	RICM=IC(NIC-1)	290
	C(NC)=RICM+RIC*10.0**(-NLEFT)	291
	WRITE (6,109) NC,C(NC)	292
	NFIN(1,J)=51	293
	NFIN(2,J)=NC	294
	NC=NC+1	295
	NIC=NIC-1	296
	IF (IE.EQ.2) GO TO 2	297
	GO TO 41	298
48	NFIN(1,J)=50	299
	NFIN(2,J)=IC(NIC)	300
	IF (NFIN(1,J-1).NE.52) GO TO 2	301
	J=J-1	302
	NFIN(2,J)=IC(NIC)	303
	I=I+1	304
	GO TO 2	305
49	ICCC=IC(NIC)	306
	IF (IE.EQ.4) ICCC=-ICCC	307
	C(NC-1)=C(NC-1)*10.0**ICCC	308
	NCM=NC-1	309
	WRITE (6,109) NCM,C(NCM)	310
	GO TO 2	311
50	NPARR=J	312
	J=NPARR(NLC)+1	313
	L=NPARR(NLC)	314
C		315
C	DEFINE FORTRAN 4 FUNCTIONS AS BASIC FUNCTIONS	316
C		317
C		318
C		319
58	L=L+1	320
	IF (L.EQ.NPARR) GO TO 61	320
	IF (NFIN(1,L).GT.20.OR.NFIN(1,L).LT.6) GO TO 60	321
	NFUNTO=NFUNTO+1	322
	NFUN(1,NFUNTO)=NFIN(1,L)	323
	NFUN(2,NFUNTO)=0	324
	NFUNTO=NFUNTO+1	325
	L=L+1	326
	NFUN(1,NFUNTO)=NFIN(1,L)	327
	NFUN(2,NFUNTO)=NFIN(2,L)	328
	IF (NFIN(1,L-1).NE.20) GO TO 62	329
	NFUN(1,NFUNTO-1)=3	330

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	NFUNTO=NFUNTO+1	331
	NFUN(1,NFUNTO)=51	332
	NFUN(2,NFUNTO)=2	333
	GO TO 59	334
62	IF (NFUN(1,L-1).NE.19) GO TO 59	335
C	CHANGE COTAN TO 1.0/TAN	336
	NFUN(1,NFUNTO-1)=11	337
	NFUNTO=NFUNTO+1	338
	IBASE=IBASE+1	339
	NFUN(1,NFUNTO)=4	340
	NFUN(2,NFUNTO)=0	341
	NFUNTO=NFUNTO+1	342
	NFUN(1,NFUNTO)=53	343
	NFUN(2,NFUNTO)=IBASE	344
	NFUNTO=NFUNTO+1	345
	NFUN(1,NFUNTO)=50	346
	NFUN(2,NFUNTO)=-1	347
59	IBASE=IBASE+1	348
	NFIN(1,J)=53	349
	NFIN(2,J)=IBASE	350
	J=J+1	351
	GO TO 58	352
60	NFIN(1,J)=NFIN(1,L)	353
	NFIN(2,J)=NFIN(2,L)	354
	J=J+1	355
	GO TO 58	356
61	NPARR=J	357
C		358
C	REMOVE ** OPERATOR AND DEFINE IT AS A BASIC FUNCTION	359
	L=NPARR(NLC)	360
	J=NPARR(NLC)+1	361
65	L=L+1	362
	IF (L.EQ.NPARR) GO TO 67	363
	IF (NFUN(1,L).NE.4) GO TO 66	364
	NFUNTO=NFUNTO+1	365
	NFUN(1,NFUNTO)=NFIN(1,L)	366
	NFUN(2,NFUNTO)=0	367
	NFUNTO=NFUNTO+1	368
	NFUN(1,NFUNTO)=NFIN(1,J-1)	369
	NFUN(2,NFUNTO)=NFIN(2,J-1)	370
	NFUNTO=NFUNTO+1	371
	L=L+1	372
	NFUN(1,NFUNTO)=NFIN(1,L)	373
	NFUN(2,NFUNTO)=NFIN(2,L)	374
	IF (NFUN(1,L).NE.50) NFUN(1,NFUNTO-2)=3	375
	IBASE=IBASE+1	376
	NFIN(1,J-1)=53	377
	NFIN(2,J-1)=IBASE	378
	GO TO 65	379
66	NFIN(1,J)=NFIN(1,L)	380
	NFIN(2,J)=NFIN(2,L)	381
	J=J+1	382
	GO TO 65	383
67	NPARR=J	384
C		385

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C	REMOVE THE / AND - OPERATIONS.	386
	L=NPARR(NLC)	387
76	L=L+1	388
	IF (L.EQ.NPARR) GO TO 69	389
	IF (NFUN(1,L).NE.5) GO TO 77	390
C	REMOVE THE * OPERATIONS AND DEFINE AS BASIC FUNCTIONS.	391
	NFUNTO=NFUNTO+1	392
	NFUN(1,NFUNTO)=NFUN(1,L)	393
	NFUN(2,NFUNTO)=0	394
	NFUNTO=NFUNTO+1	395
	L=L+1	396
	NFUN(1,NFUNTO)=NFUN(1,L)	397
	NFUN(2,NFUNTO)=NFUN(2,L)	398
	IBASE=IBASE+1	399
	NFIN(1,L-1)=1	400
	NFIN(1,L)=53	401
	NFIN(2,L)=IBASE	402
	GO TO 76	403
C	REMOVE / OPERATORS AND CHANGE TO *	404
77	IF (NFUN(1,L).NE.3) GO TO 76	405
	NFUNTO=NFUNTO+1	406
	NFUN(1,NFUNTO)=4	407
	NFUN(2,NFUNTO)=0	408
	NFUNTO=NFUNTO+1	409
	L=L+1	410
	NFUN(1,NFUNTO)=NFUN(1,L)	411
	NFUN(2,NFUNTO)=NFUN(2,L)	412
	NFUNTO=NFUNTO+1	413
	NFUN(1,NFUNTO)=50	414
	NFUN(2,NFUNTO)=-1	415
	IBASE=IBASE+1	416
	NFIN(1,L-1)=2	417
	NFIN(1,L)=53	418
	NFIN(2,L)=IBASE	419
	GO TO 76	420
C		421
C	REMOVE * OPERATORS AND DEFINE AS BASIC FUNCTIONS.	422
69	L=NPARR(NLC)	423
	J=NPARR(NLC)+1	424
70	L=L+1	425
	IF (L.GE.NPARR) GO TO 75	426
	IF (NFUN(1,L).NE.2) GO TO 74	427
	NFUNTO=NFUNTO+1	428
	NFUN(1,NFUNTO)=NFUN(1,L)	429
	NFUN(2,NFUNTO)=0	430
	NFUNTO=NFUNTO+1	431
	NFUN(1,NFUNTO)=NFUN(1,L-1)	432
	NFUN(2,NFUNTO)=NFUN(2,L-1)	433
71	L=L+1	434
	NFUNTO=NFUNTO+1	435
	NFUN(1,NFUNTO)=NFUN(1,L)	436
	NFUN(2,NFUNTO)=NFUN(2,L)	437
	L=L+1	438
	IF (L.EQ.NPARR) GO TO 72	439
	IF (NFUN(1,L).EQ.2) GO TO 71	440

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72	CONTINUE	441
	IBASE=IBASE+1	442
	NFIN(1,J-1)=53	443
	NFIN(2,J-1)=IBASE	444
	L=L-1	445
	GO TO 70	446
74	NFIN(1,J)=NFIN(1,L)	447
	NFIN(2,J)=NFIN(2,L)	448
	J=J+1	449
	GO TO 70	450
75	NPARR=J	451
		452
C	REMOVE THE + OPERATION AND DEFINE IT AS A BASIC FUNCTION.	453
C		454
79	L=NPARR(NLC)+1	455
	J=NPARR(NLC)	456
	IF (NFIN(1,L).EQ.1) L=L+1	457
	IF (NPARR-L.EQ.1.AND.J.NE.0) GO TO 81	458
	NFUNTO=NFUNTO+1	459
	NFUN(1,NFUNTO)=1	460
	NFUN(2,NFUNTO)=0	461
80	NFUNTO=NFUNTO+1	462
	NFUN(1,NFUNTO)=NFIN(1,L)	463
	NFUN(2,NFUNTO)=NFIN(2,L)	464
	L=L+2	465
	IF (L.LT.NPARR) GO TO 80	466
	IF (J.EQ.0) GO TO 95	467
	IBASE=IBASE+1	468
	NLC=NLC-1	469
	NFIN(1,J)=53	470
	NFIN(2,J)=IBASE	471
	GO TO 2	472
81	NLC=NLC-1	473
	NFIN(1,J)=NFIN(1,L)	474
	NFIN(2,J)=NFIN(2,L)	475
	GO TO 2	476
95	CONTINUE	477
	IBF=0	478
	III=1	479
196	I1=III	480
	I2=NFUNTO	481
	DO 198 I=I1,I2	482
	IF (NFUN(1,I).LE.20) IBF=IBF+1	483
	IF (NFUN(1,I).NE.1) GO TO 198	484
	IF (I+2.GT.NFUNTO) GO TO 199	485
	IF (NFUN(1,I+2).GT.20) GO TO 198	486
	NFS1=NFUN(1,I+1)	487
	NFS2=NFUN(2,I+1)	488
	NFUNTO=NFUNTO-2	489
	III=1	490
	DO 197 J=III,NFUNTO	491
	NFUN(1,J)=NFUN(1,J+2)	492
	NFUN(2,J)=NFUN(2,J+2)	493
	IF (NFUN(1,J).NE.53.OR.NFUN(2,J).LE.IBF) GO TO 201	494
	NFUN(2,J)=NFUN(2,J)-1	495
	GO TO 197	

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201	IF (NFUN(1,J).NE.53.OR.NFUN(2,J).NE.IBF) GO TO 197	496
	NFUN(1,J)=NFS1	497
	NFUN(2,J)=NFS2	498
197	CONTINUE	499
	IBF=IBF-1	500
	GO TO 196	501
198	CONTINUE	502
	GO TO 200	503
199	IF (NFUNTO.EQ.2.OR.NFUN(1,NFUNTO).NE.53) GO TO 200	504
	NFUNTO=NFUNTO-2	505
200	CONTINUE	506
	WRITE (6,107)	507
	WRITE (6,101) (NFUN(1,K),K=1,NFUNTO)	508
	WRITE (6,101) (NFUN(2,K),K=1,NFUNTO)	509
	I=1	510
	CALL ISTORE(NAME,I)	511
	RETURN	512
	END	513

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SUBROUTINE PARDIF (NAME1,NAME2,N)                                001  001
C   NFUN(I,J) - FUNCTION TO BE DIFFERENTIATED.                  002  002
C   NFUN(1,J) - OPERATOR, OPERAND STRING.                       003  003
C   NFUN(2,4) - SUBSCRIPTS FOR THE OPERANDS.                   004  004
C   NFUNTO - TOTAL LENGTH OF NFUN.                              005  005
C   NDERF(I,J) - DIFFERENTIAL OF THE FUNCTION                   006  006
C   NDERF(1,J) - OPERATOR, OPERAND STRING FOR DERIVATIVE.     007  007
C   NDERTO - TOTAL LENGTH OF NDERF                              008  008
C   NDEROP(1,J) - CONTAINS DEPENDENCY INFORMATION IF NFUN(I,J) IS 009
C   AN OPERATOR. CONTAINS A 0 IF THE OPERAND NFUN(I,J) IS NOT 010
C   DEPENDENT. CONTAINS THE DERIVATIVE OF THE OPERAND IF OPERAND 011
C   IS DEPENDENT.                                              012
C   NDEROP(2,J) - CONTAINS INVOLVEMENT INFORMATION IF NFUN(I,J) IS 013
C   AN OPERATOR. OTHERWISE IT CONTAINS THE SUBSCRIPT FOR      014
C   NDEROP(1,J).                                              015
C   IBASE(I) - CONTAINS THE COLUMN IN WHICH THE OPERATOR FOR BASIC 016
C   FUNCTION I IS LOCATED.                                      017
C   IMPLICIT INTEGER*2 (I-N)                                    018
C   DIMENSION NDERF(2,MAXFUN),NDEROP(2,MAXFUN)                 019
C   DIMENSION NDERF(2,600),NDEROP(2,600),IBASE(400)           020
C   COMMON /BLK1/ NFUN(2,MAXFUN),NFUNTO                        021
C   COMMON /BLK1/ NFUN(2,300),NFUNTO                            022
C   COMMON /BLK2/ CT(200),NC                                    023
100 FORMAT (' NDERF(1,J)=')                                     024  020
101 FORMAT (40I3)                                              025  021
102 FDRMAT (' NDERF(2,J)=')                                     026  022
103 FORMAT (' NFUN(1,J)=')                                       027  023
104 FORMAT (' NFUN(2,J)=')                                       028  024
105 FORMAT (' NDEROP(1,J)=')                                       029  025
106 FDRMAT (' NDEROP(2,J)=')                                       030  025
109 FDRMAT(4H NC=,I10,7H C(NC)=,E15.7)                          031
   I=2                                                         032
   CALL ISTORE (NAME1,I)                                         033
   NFUN(1,NFUNTO+1)=0                                           034
   NFUN(2,NFUNTO+1)=0                                           035
   NDEROP(1,NFUNTO+1)=0                                          036
   NDEROP(2,NFUNTO+1)=0                                          037
C   SET UP NDEROP WHICH CONTAINS THE PARTIAL DERIVITIVES OF EACH OF 038  032
C   THE OPERANDES IN THE NFUN CHAIN.                            039  033
C   ALSO SET DEPENDENCY INFORMATION.                             040
   I=0                                                         041
   DO 4 J=1,NFUNTO                                              042
     IF (NFUN(1,J).LE.20) GO TO 2                                043
     IF (NFUN(1,J).NE.53) GO TO 8                                044
     IF (NDEROP(1,IBASE(NFUN(2,J)))) .NE.0) GO TO 1            045
8   IF (NFUN(2,J).EQ.0) GO TO 3                                  046
     IF (NFUN(1,J).NE.52) GO TO 3                                047
     IF (NFUN(2,J).NE.N) GO TO 3                                048
     NDEROP(1,J)=51                                             049
     NDEROP(2,J)=4                                              050
     NDEROP(1,IBASE(I))=1                                       051
     GO TO 4                                                      052
1   NDEROP(1,J)=54                                             053
     NDEROP(2,J)=NFUN(2,J)                                       054  042
     NDEROP(1,IBASE(I))=1                                       055

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80/80 LIST

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	GO TO 4	056	
2	I=I+1	057	
	IBASE(I)=J	058	
3	NDEROP(1,J)=0	059	
	NDEROP(2,J)=0	060	
4	CONTINUE	061	
C	SET INVOLVEMENT INFORMATION	062	
	I=I+1	063	
	IBASE(I)=NFUNTO+1	064	
40	I=I-1	065	
	IF (I.EQ.0) GO TO 44	066	
	J=IBASE(I)	067	
	IF (NDEROP(1,J).EQ.0.AND.NDEROP(2,J).EQ.0) GO TO 40	068	
	NF=NFUN(1,J)	069	
	IF (NF.EQ.1.OR.NF.EQ.2.OR.NF.EQ.5) GO TO 42	070	
	J=J+1	071	
	IF (NFUN(1,J).NE.53) GO TO 41	072	
	NDEROP(2,IBASE(NFUN(2,J)))=1	073	
41	IF (NF.NE.3) GO TO 40	074	
	J=J+1	075	
	IF (NFUN(1,J).NE.53) GO TO 40	076	
	NDEROP(2,IBASE(NFUN(2,J)))=1	077	
	GO TO 40	078	
42	IF (NDEROP(2,J).EQ.0.AND.(NF.EQ.1.OR.NF.EQ.5)) GO TO 40	079	
	NTERMS=0	080	
	KK=IBASE(I)+1	081	
	KKK=IBASE(I+1)-1	082	
	DO 43 K=KK,KKK	083	
	IF (NDEROP(1,K).EQ.0) GO TO 48	084	
	NTERMS=NTERMS+1	085	
	L=K	086	
48	IF (NFUN(1,K).NE.53) GO TO 43	087	
	NDEROP(2,IBASE(NFUN(2,K)))=1	088	
43	CONTINUE	089	
	IF (NDEROP(2,IBASE(I)).EQ.1) GO TO 40	090	
	IF (NF.NE.2.OR.NTERMS.GT.1) GO TO 40	091	
	IF (NFUN(1,L).NE.53) GO TO 40	092	
	NDEROP(2,IBASE(NFUN(2,L)))=0	093	
	GO TO 40	094	
44	CONTINUE	095	
C		096	
C		097	
C		098	
	NDERTO=0	099	051
	IAUXDF=0	100	053
	I=0	101	
45	I=I+1	102	
	J=IBASE(I)	103	
	IF (J.GT.NFUNTO) GO TO 95	104	
C	RESET THE SUBSCRIPTS IF THE BASIC FUNCTION IS NOT INVOLVED.	105	
	IF (NDEROP(2,J).EQ.1) GO TO 46	106	
	KK=IBASE(I+1)	107	
	DO 9 K=KK,NFUNTO	108	
	IF (NFUN(1,K).NE.53) GO TO 9	109	
	IF (NFUN(2,K).LE.1AUXDF) GO TO 9	110	

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	NFUN(2,K)=NFUN(2,K)-1	111	
	IF (NDEROP(1,K).EQ.0) GO TO 9	112	
	NDEROP(2,K)=NDEROP(2,K)-1	113	
	9 CONTINUE	114	
	GO TO 47	115	
C	SET THE BASIC FUNCTION CHAIN INTO THE DERIVATIVE CHAIN.	116	058
46	NDERTO=NDERTO+1	117	
	NDERF(1,NDERTO)=NFUN(1,J)	118	
	NDERF(2,NDERTO)=NFUN(2,J)	119	
	IAUXDF=IAUXDF+1	120	
	JJ=J	121	
7	JJ=JJ+1	122	
	IF (NFUN(1,JJ).LE.20) GO TO 6	123	
	NDERTO=NDERTO+1	124	
	NDERF(1,NDERTO)=NFUN(1,JJ)	125	
	NDERF(2,NDERTO)=NFUN(2,JJ)	126	
	GO TO 7	127	
6	CONTINUE	128	
C	EXPAND THE DERIVATIVE CHAIN SO THAT IT INCLUDES THE PARTIAL	129	074
C	DERIVATIVE OF THE AUXILIARY FUNCTION PRESENTLY BEING CONSIDERED.	130	075
47	IF (NDEROP(1,J).EQ.0) GO TO 45	131	
	NF=NFUN(1,J)	132	076
5	GO TO (10,19,30,31,10,60,61,82,64,82,70,82,72,80,80,62,63,71),NF	133	
C	+ AND -	134	
10	NDERTO=NDERTO+1	135	
	NDERF(1,NDERTO)=NF	136	
	NDERF(2,NDERTO)=0	137	
	IDIFF=1	138	
	JJ=J	139	
11	JJ=JJ+1	140	
	IF (NFUN(1,JJ).LE.20) GO TO 1000	141	
	IF (NDEROP(1,JJ).EQ.0) GO TO 11	142	
	NDERTO=NDERTO+1	143	
	NDERF(1,NDERTO)=NDEROP(1,JJ)	144	
	NDERF(2,NDERTO)=NDEROP(2,JJ)	145	
	GO TO 11	146	
C	*	147	
19	NTERMS=0	148	
20	JJ=J	149	
26	JJ=JJ+1	150	
	IF (NDEROP(1,JJ).GT.1) GO TO 21	151	
	IF (NFUN(1,JJ).LE.20) GO TO 24	152	
	GO TO 26	153	
21	JJ=JJ-1	154	
	DO 22 K=J,JJ	155	
	NDERTO=NDERTO+1	156	
	NDERF(1,NDERTO)=NFUN(1,K)	157	
22	NDERF(2,NDERTO)=NFUN(2,K)	158	
	NDERTO=NDERTO+1	159	
	JJ=JJ+1	160	
	NDERF(1,NDERTO)=NDEROP(1,JJ)	161	
	NDERF(2,NDERTO)=NDEROP(2,JJ)	162	
	NDEROP(1,JJ)=0	163	
	NTERMS=NTERMS+1	164	
23	JJ=JJ+1	165	

80/80 LIST

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	IF (NFUN(1,JJ).LE.20) GO TO 20	166
	NDERTO=NDERTO+1	167
	NDFRF(1,NDERTO)=NFUN(1,JJ)	168
	NDERF(2,NDERTO)=NFUN(2,JJ)	169
	GO TO 23	170
24	NDERTO=NDERTO+1	171
	NDFRF(1,NDERTO)=1	172
	NDERF(2,NDERTO)=0	173
	IF (NTERMS.EQ.0) GO TO 26	174
	DO 25 K=1,NTERMS	175
	NDERTO=NDERTO+1	176
	NDERF(1,NDERTO)=53	177
25	NDERF(2,NDERTO)=IAUXDF+K	178
	IDIFF=NTERMS+1	179
	GO TO 1000	180
C	**	181
30	IDIFF=0	182
	IF (NDEROP(1,J+1).EQ.0) GO TO 35	183
	NDERTO=NDERTO+1	184
	NDERF(1,NDERTO)=1	185
	NDFRF(2,NDERTO)=0	186
	NDERF(1,NDERTO+1)=NFUN(1,J+2)	187
	NDERF(2,NDERTO+1)=NFUN(2,J+2)	188
	NDERTO=NDERTO+2	189
	NDERF(1,NDERTO)=51	190
	NDERF(2,NDERTO)=5	191
	NDERF(1,NDERTO+1)=3	192
	NDFRF(1,NDERTO+3)=53	193
	NDERF(2,NDERTO+3)=IAUXDF+1	194
	NDERF(2,NDERTO+5)=IAUXDF+2	195
	NDERF(1,NDERTO+6)=NFUN(1,J+2)	196
	NDERF(2,NDERTO+6)=NFUN(2,J+2)	197
	IDIFF=3	198
	GO TO 32	199
31	IDIFF=0	200
	IF (NDEROP(1,J+1).EQ.0) GO TO 35	201
	NDERF(1,NDERTO+1)=4	202
	NDERF(1,NDERTO+3)=50	203
	NDERF(2,NDERTO+3)=NFUN(2,J+2)-1	204
	IF (NDERF(2,NDERTO+3).EQ.0) GO TO 37	205
	NDERF(2,NDERTO+5)=IAUXDF+1	206
	NDERF(1,NDERTO+6)=51	207
	C(NC)=NFUN(2,J+2)	208
	WRITE (6,109) NC,C(NC)	209
	NC=NC+1	210
	NDERF(2,NDERTO+6)=NC-1	211
	IDIFF=2	212
32	NDERF(2,NDERTO+1)=0	213
	NDERF(1,NDERTO+2)=NFUN(1,J+1)	214
	NDFRF(2,NDERTO+2)=NFUN(2,J+1)	215
	NDERF(1,NDERTO+4)=2	216
	NDFRF(2,NDERTO+4)=0	217
	NDFRF(1,NDERTO+5)=53	218
	NDERF(1,NDERTO+7)=NDEROP(1,J+1)	219
	NDERF(2,NDERTO+7)=NDEROP(2,J+1)	220

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NDERT0=NDERT0+7	221
35 IF (NDEROP(1,J+2).EQ.0) GO TO 36	222
NDERF(1,NDERT0+1)=3	223
NDERF(2,NDERT0+1)=0	224
NDERF(1,NDERT0+2)=NFUN(1,J+1)	225
NDERF(2,NDERT0+2)=NFUN(2,J+1)	226
NDERF(1,NDERT0+2)=NFUN(1,J+2)	227
NDERF(2,NDERT0+2)=NFUN(2,J+2)	228
NDERF(1,NDERT0+3)=2	229
NDERF(2,NDERT0+3)=0	230
NDERF(1,NDERT0+4)=53	231
NDERF(2,NDERT0+4)=IAUXDF+IDIFF+1	232
NDERF(1,NDERT0+5)=51	233
NDERF(2,NDERT0+5)=9	234
NDERF(1,NDERT0+6)=NDEROP(1,J+2)	235
NDERF(2,NDERT0+6)=NDEROP(2,J+2)	236
NDERT0=NDERT0+6	237
IDIFF=IDIFF+2	238
36 IF (NDEROP(1,J+1).EQ.0.OR.NDEROP(1,J+2).EQ.0) GO TO 1000	239
NDERF(1,NDERT0+1)=1	240
NDERF(2,NDERT0+1)=0	241
NDERF(1,NDERT0+2)=53	242
NDERF(2,NDERT0+2)=IAUXDF+IDIFF	243
NDERF(1,NDERT0+3)=53	244
NDERF(2,NDERT0+3)=IAUXDF+IDIFF-2	245
NDERT0=NDERT0+3	246
IDIFF=IDIFF+1	247
GO TO 1000	248
37 IDIFF=1	249
NDERF(1,NDERT0+1)=1	250
NDERF(2,NDERT0+1)=0	251
NDERT0=NDERT0+2	252
NDERF(1,NDERT0)=NDEROP(1,J+1)	253
NDERF(2,NDERT0)=NDEROP(2,J+1)	254
GO TO 1000	255
C EXP	256
60 NDERF(1,NDERT0+1)=6	257
GO TO 65	258
C SIN	259
61 NDERF(1,NDERT0+1)=9	260
GO TO 65	261
C SINH	262
62 NDERF(1,NDERT0+1)=17	263
GO TO 65	264
C COSH	265
63 NDERF(1,NDERT0+1)=16	266
GO TO 65	267
C COS	268
64 NDERF(1,NDERT0+1)=7	269
65 NDERF(2,NDERT0+1)=0	270
NDERT0=NDERT0+2	271
NDERF(1,NDERT0)=NFUN(1,J+1)	272
NDERF(2,NDERT0)=NFUN(2,J+1)	273
IDIFF=1	274
IF (NF.EQ.9) GO TO 66	275

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	IF (NDEROP(1,J+1).EQ.51) GO TO 1000	276
66	NDERF(1,NDERTO+1)=2	277
	NDERF(2,NDERTO+1)=0	278
	NDERF(1,NDERTO+2)=53	279
	NDERF(2,NDERTO+2)=IAUXDF+1	280
	NDERTO=NDERTO+3	281
	NDERF(1,NDERTO)=NDEROP(1,J+1)	282
	NDERF(2,NDERTO)=NDEROP(2,J+1)	283
	IDIFF=2	284
	IF (NF.NE.9) GO TO 1000	285
	IF (NDEROP(1,J+1).EQ.51) GO TO 67	286
	NDERTO=NDERTO+1	287
67	NDERF(1,NDERTO)=51	288
	NDERF(2,NDERTO)=5	289
	GO TO 1000	290
C	TAN	291
70	NDERF(1,NDERTO+1)=9	292
	NDERF(2,NDERTO+5)=-2	293
	IDIFF=3	294
	GO TO 73	295
C	TANH	296
71	NDERF(1,NDERTO+1)=17	297
	NDERF(2,NDERTO+5)=-2	298
	IDIFF=3	299
	GO TO 73	300
C	ABS	301
72	NDERF(1,NDERTO+1)=13	302
	NDERF(2,NDERTO+5)=-1	303
	NDERF(1,NDERTO+9)=NFUN(1,J+1)	304
	NDERF(2,NDERTO+9)=NFUN(2,J+1)	305
	IDIFF=3	306
73	NDERF(2,NDERTO+1)=0	307
	NDERF(1,NDERTO+2)=NFUN(1,J+1)	308
	NDERF(2,NDERTO+2)=NFUN(2,J+1)	309
	NDERF(1,NDERTO+3)=4	310
	NDERF(2,NDERTO+3)=0	311
	NDERF(1,NDERTO+4)=53	312
	NDERF(2,NDERTO+4)=IAUXDF+1	313
	NDERF(1,NDERTO+5)=50	314
	NDERF(1,NDERTO+6)=2	315
	NDERF(2,NDERTO+6)=0	316
	NDERF(1,NDERTO+7)=NDEROP(1,J+1)	317
	NDERF(2,NDERTO+7)=NDEROP(2,J+1)	318
	NDERTO=NDERTO+8	319
	NDERF(1,NDERTO)=53	320
	NDERF(2,NDERTO)=IAUXDF+2	321
	IF (NF.EQ.13) NDERTO=NDERTO+1	322
	GO TO 1000	323
C	ALOG	324
80	NDERF(2,NDERTO+3)=-1	325
	NDERF(1,NDERTO+6)=NDEROP(1,J+1)	326
	NDERF(2,NDERTO+6)=NDEROP(2,J+1)	327
	IDIFF=2	328
	IF (NF.EQ.15) GO TO 81	329
	GO TO 85	330

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C	ALOG10	331
81	NDERF(1,NDERTO+7)=51	332
	NDERF(2,NDERTO+7)=8	333
	GO TO 85	334
C	AR SIN	335
82	NDERF(2,NDERTO+3)=2	336
	NDERF(1,NDERTO+6)=51	337
	NDERF(2,NDERTO+6)=5	338
	NDERF(1,NDERTO+10)=3	339
	NDERF(1,NDERTO+12)=51	340
	NDERF(2,NDERTO+12)=3	341
	IDIFF=5	342
	IF (NF.EQ.10) GO TO 83	343
	IF (NF.EQ.12) GO TO 84	344
	GO TO 85	345
C	ARCOS	346
83	NDERF(1,NDERTO+16)=51	347
	NDERF(2,NDERTO+16)=5	348
	GO TO 85	349
C	ATAN	350
84	NDERF(2,NDERTO+6)=4	351
	NDERF(1,NDERTO+10)=4	352
	NDERF(1,NDERTO+12)=50	353
	NDERF(2,NDERTO+12)=-1	354
85	NDERF(1,NDERTO+1)=4	355
	NDERF(2,NDERTO+1)=0	356
	NDERF(1,NDERTO+2)=NFUN(1,J+1)	357
	NDERF(2,NDERTO+2)=NFUN(2,J+1)	358
	NDERF(1,NDERTO+3)=50	359
	NDERF(1,NDERTO+4)=2	360
	NDERF(2,NDERTO+4)=0	361
	NDERF(1,NDERTO+5)=53	362
	NDERF(2,NDERTO+5)=1AUXDF+1	363
	NDERTO=NDERTO+6	364
	IF (NF.EQ.14) GO TO 1000	365
	IF (NF.NE.15) GO TO 86	366
	NDERTO=NDERTO+1	367
	GO TO 1000	368
86	NDERF(1,NDERTO+1)=1	369
	NDERF(2,NDERTO+1)=0	370
	NDERF(1,NDERTO+2)=53	371
	NDERF(2,NDERTO+2)=1AUXDF+2	372
	NDERF(1,NDERTO+3)=51	373
	NDERF(2,NDERTO+3)=4	374
	NDERF(2,NDERTO+4)=0	375
	NDERF(1,NDERTO+5)=53	376
	NDERF(2,NDERTO+5)=1AUXDF+3	377
	NDERF(1,NDERTO+7)=2	378
	NDERF(2,NDERTO+7)=0	379
	NDERF(1,NDERTO+8)=53	380
	NDERF(2,NDERTO+8)=1AUXDF+4	381
	NDERF(1,NDERTO+9)=NDEROP(1,J+1)	382
	NDERF(2,NDERTO+9)=NDEROP(2,J+1)	383
	NDERTO=NDERTO+9	384
	IF (NF.NE.10) GO TO 1000	385

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NDERTO=NDERTO+1	386
GO TO 1000	387
C CHANGE THE PARTIAL DERIVATIVE TO ITS PROPER AUXILIARY FUNCTION	388
C NUMBER. UPDATE THE AUXILIARY FUNCTION NUMBERS AND THE NDEROPT(2,	389
C JJ) NUMBERS.	390
1000 CONTINUE	391
KMAX=0	392
L=1	393
87 L=L+1	394
K=IBASE(L)	395
IF (K.EQ.NFUNTO+1) GO TO 90	396
KMAX=IBASE(L+1)	397
88 K=K+1	398
IF (K.FQ.KMAX) GO TO 87	399
IF (NFUN(1,K).NE.53) GO TO 88	400
IF (NFUN(2,K).NE.1AUXDF) GO TO 91	401
IF (NDEROP(1,K).NE.54) GO TO 88	402
NDEROP(1,K)=53	403
NDEROP(2,K)=NDEROP(2,K)+IDIFF	404
GO TO 88	405
91 IF (NFUN(2,K).LE.1AUXDF) GO TO 88	406
NFUN(2,K)=NFUN(2,K)+IDIFF	407
IF (NDEROP(1,K).NE.54) GO TO 88	408
NDEROP(2,K)=NDEROP(2,K)+IDIFF	409
GO TO 88	410
90 1AUXDF=1AUXDF+IDIFF	411
GO TO 45	412
95 IF (NDERTO.EQ.0) GO TO 97	413
DO 96 I=1,NDERTO	414
NFUN(1,I)=NDERF(1,I)	415
96 NFUN(2,I)=NDERF(2,I)	416
NFUNTO=NDERTO	417
GO TO 98	418
97 NFUN(1,1)=1	419
NFUN(2,1)=0	420
NFUNTO=2	421
NFUN(1,NFUNTO)=51	422
NFUN(2,NFUNTO)=1	423
98 CONTINUE	424
IBF=0	425
III=1	426
196 II=III	427
I2=NFUNTO	428
DO 198 I=11,12	429
IF (NFUN(1,I).LE.20) IBF=IBF+1	430
IF (NFUN(1,I).NE.1) GO TO 198	431
IF (I+2.GT.NFUNTO) GO TO 199	432
IF (NFUN(1,I+2).GT.20) GO TO 198	433
NFS1=NFUN(1,I+1)	434
NFS2=NFUN(2,I+1)	435
NFUNTO=NFUNTO-2	436
III=I	437
DO 197 J=III,NFUNTO	438
NFUN(1,J)=NFUN(1,J+2)	439
NFUN(2,J)=NFUN(2,J+2)	440

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IF (NFUN(1,J).NE.53.OR.NFUN(2,J).LE.IBF) GO TO 201	441	
NFUN(2,J)=NFUN(2,J)-1	442	
GO TO 197	443	
201 IF (NFUN(1,J).NE.53.OR.NFUN(2,J).NE.IBF) GO TO 197	444	
NFUN(1,J)=NFS1	445	
NFUN(2,J)=NFS2	446	
197 CONTINUE	447	
IBF=IBF-1	448	
GO TO 196	449	
198 CONTINUE	450	
GO TO 200	451	
199 IF (NFUNTO.EQ.2.OR.NFUN(1,NFUNTO).NE.53) GO TO 200	452	
NFUNTO=NFUNTO-2	453	
200 CONTINUE	454	
WRITE (6,105)	455	
WRITE (6,101) (NFUN(1,JJJ),JJJ=1,NFUNTO)	456	
WRITE (6,101) (NFUN(2,JJJ),JJJ=1,NFUNTO)	457	
I=1	458	
CALL ISTORE (NAME2,I)	459	
RETURN	460	488
END	461	489

80/80 LIST

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	FUNCTION DVAL(NAME,X)	001	
C	NFUN(I,J) - FUNCTION TO BE EVALUATED.	002	002
C	NFUNTO - TOTAL LENGTH OF NFUN	003	003
C	VALUE(I) - NUMERICAL VALUE OF AUXILIARY FUNCTION I.	004	004
	IMPLICIT INTEGER*2(I-N),REAL*8(A-H,O-Z)	005	
	REAL*4 C	006	
C	DIMENSION VALUE (MAXFUN/2),X(50)	007	
	DIMENSION VALUE(100),X(10)	008	
C	COMMON /BLK1/ NFUN(2,MAXFUN),NFUNTO	009	
	COMMON /BLK1/ NFUN(2,300),NFUNTO	010	
C	COMMON /BLK2/ C(MAXC),NC	011	
	COMMON /BLK2/ C(200),NC	012	
	I=2	013	
	CALL ISTORE (NAME,I)	014	
	NFUN(1,NFUNTO+1)=20	015	
	J=0	016	
	IAUXF=0	017	
50	J=J+1	018	
51	NF=NFUN(1,J)	019	
	IF (NFUN(1,J).EQ.20) GO TO 80	020	
	IAUXF=IAUXF+1	021	
	J=J+1	022	
	NOP=NFUN(1,J)-50	023	
	GO TO (52,53,54),NOP	024	
52	VAL1=C(NFUN(2,J))	025	
	GO TO 55	026	
53	VAL1=X(NFUN(2,J))	027	
	GO TO 55	028	
54	VAL1=VALUE(NFUN(2,J))	029	
55	GO TO (56,56,57,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18),NF	030	
56	VALUE(IAUXF)=VAL1	031	
57	J=J+1	032	
	NOP=NFUN(1,J)-50	033	
	IF (NOP.LT.1) GO TO 51	034	
	GO TO (58,59,60),NOP	035	
58	VAL2=C(NFUN(2,J))	036	
	GO TO (1,2,3),NF	037	
59	VAL2=X(NFUN(2,J))	038	
	GO TO (1,2,3),NF	039	
60	VAL2=VALUE(NFUN(2,J))	040	
	GO TO (1,2,3),NF	041	
1	VALUE(IAUXF)=VALUE(IAUXF)+VAL2	042	
	GO TO 57	043	
2	VALUE(IAUXF)=VALUE(IAUXF)*VAL2	044	
	GO TO 57	045	
3	VALUE(IAUXF)=VAL1**VAL2	046	
	GO TO 50	047	
4	J=J+1	048	
	VALUE(IAUXF)=VAL1**NFUN(2,J)	049	
	GO TO 50	050	
5	VALUE(IAUXF)=-VAL1	051	
	GO TO 50	052	
6	VALUE(IAUXF)=DEXP (VAL1)	053	
	GO TO 50	054	040
7	VALUE(IAUXF)=DSIN (VAL1)	055	

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GO TO 50	056	042
8 VALUE(IAXF)=DARSIN(VAL1)	057	
GO TO 50	058	044
9 VALUE(IAXF)=DCOS (VAL1)	059	
GO TO 50	060	046
10 VALUE(IAXF)=DARCOS(VAL1)	061	
GO TO 50	062	048
11 VALUE(IAXF)=DTAN (VAL1)	063	
GO TO 50	064	050
12 VALUE(IAXF)=DATAN (VAL1)	065	
GO TO 50	066	052
13 VALUE(IAXF)=DABS(VAL1)	067	
GO TO 50	068	054
14 VALUE(IAXF)=DLOG (VAL1)	069	
GO TO 50	070	056
15 VALUE(IAXF)=DLOG10(VAL1)	071	
GO TO 50	072	058
16 VALUE(IAXF)=DSINH (VAL1)	073	
GO TO 50	074	060
17 VALUE(IAXF)=DCOSH (VAL1)	075	
GO TO 50	076	062
18 VALUE(IAXF)=DTANH (VAL1)	077	
GO TO 50	078	064
80 DVAL=VALUE(IAXF)	079	
RETURN	080	
END	081	

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 1234567890123456789012345678901234567890123456789012345678901234567890

	FUNCTION VAL(NAME,X)	001	001
C	NFUN(I,J) - FUNCTION TO BE EVALUATED.	002	002
C	NFUNTO - TOTAL LENGTH OF NFUN	003	003
C	VALUE(I) - NUMERICAL VALUE OF AUXILIARY FUNCTION I.	004	004
	IMPLICIT INTEGER*2 (I-N)	005	
C	DIMENSION VALUE (MAXFUN/2),X(50)	006	
	DIMENSION VALUE(100),X(50)	007	
C	COMMON /BLK1/ NFUN(2,MAXFUN),NFUNTO	008	
	COMMON /BLK1/ NFUN(2,300),NFUNTO	009	
C	COMMON /BLK2/ C(MAXC),NC	010	
	COMMON /BLK2/ C(200),NC	011	
	I=?	012	
	CALL ISTORE (NAME,I)	013	
	NFUN(1,NFUNTO+1)=20	014	
	J=0	015	
	IAUXF=0	016	
50	J=J+1	017	
51	NF=NFUN(1,J)	018	
	IF (NFUN(1,J).EQ.20) GO TO 80	019	
	IAUXF=IAUXF+1	020	
	J=J+1	021	
	NOP=NFUN(1,J)-50	022	
	GO TO (52,53,54),NOP	023	
52	VAL1=C(NFUN(2,J))	024	
	GO TO 55	025	
53	VAL1=X(NFUN(2,J))	026	
	GO TO 55	027	
54	VAL1=VALUE(NFUN(2,J))	028	
55	GO TO (56,56,57,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18),NF	029	
56	VALUE(IAUXF)=VAL1	030	
57	J=J+1	031	
	NOP=NFUN(1,J)-50	032	
	IF (NOP.LT.1) GO TO 51	033	
	GO TO (58,59,60),NOP	034	
58	VAL2=C(NFUN(2,J))	035	
	GO TO (1,2,3),NF	036	
59	VAL2=X(NFUN(2,J))	037	
	GO TO (1,2,3),NF	038	
60	VAL2=VALUE(NFUN(2,J))	039	
	GO TO (1,2,3),NF	040	
1	VALUE(IAUXF)=VALUE(IAUXF)+VAL2	041	
	GO TO 57	042	
2	VALUE(IAUXF)=VALUE(IAUXF)*VAL2	043	
	GO TO 57	044	
3	VALUE(IAUXF)=VAL1**VAL2	045	
	GO TO 50	046	
4	J=J+1	047	
	VALUE(IAUXF)=VAL1**NFUN(2,J)	048	
	GO TO 50	049	
5	VALUE(IAUXF)=-VAL1	050	
	GO TO 50	051	
6	VALUE(IAUXF)=EXP (VAL1)	052	039
	GO TO 50	053	040
7	VALUE(IAUXF)=SIN (VAL1)	054	041
	GO TO 50	055	042

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```

0000000001111111112222222223333333334444444445555555556666666667777777778
1234567890123456789012345678901234567890123456789012345678901234567890
8 VALUE(IAUXF)=ARSIN (VAL1) 056 043
GO TO 50 057 044
9 VALUE(IAUXF)=COS (VAL1) 058 045
GO TO 50 059 046
10 VALUE(IAUXF)=ARCCOS (VAL1) 060 047
GO TO 50 061 048
11 VALUE(IAUXF)=TAN (VAL1) 062 049
GO TO 50 063 050
12 VALUE(IAUXF)=ATAN (VAL1) 064 051
GO TO 50 065 052
13 VALUE(IAUXF)= ABS(VAL1) 066
GO TO 50 067 054
14 VALUE(IAUXF)=ALOG (VAL1) 068 055
GO TO 50 069 056
15 VALUE(IAUXF)=ALOG10(VAL1) 070 057
GO TO 50 071 058
16 VALUE(IAUXF)=SINH (VAL1) 072 059
GO TO 50 073 060
17 VALUE(IAUXF)=COSH (VAL1) 074 061
GO TO 50 075 062
18 VALUE(IAUXF)=TANH (VAL1) 076 063
GO TO 50 077 064
80 VAL=VALUE(IAUXF) 078
RETURN 079
END 080

```

APPENDIX B

COMPUTATIONAL ALGORITHM FOR METHOD OF OF SEEKING PRINCIPAL PLANES

In this section a detailed explanation of a computational algorithm which utilizes the method of seeking principal planes is presented. A listing of this program is given at the end of this appendix. It should be pointed out that although this computational program at first hand appears to be rather complicated, the user need only supply the equation for the function being minimized in Fortran IV on a data card.

A flow chart for the method of seeking principal planes has been presented in Figure 37, and a detailed explanation of this flow chart will now be given.

The first two blocks of the flow chart presented in Figure 37 are self-explanatory. In the third block any available computational algorithm for determining eigenvalues of the symmetric matrix of second partial derivatives can be utilized. The number of positive eigenvalues will be denoted by P . Due to roundoff errors in the digital computer, if the matrix of second partial derivatives has a true eigenvalue equal to zero, the computational algorithm will probably not return an exact value of zero. Instead, the

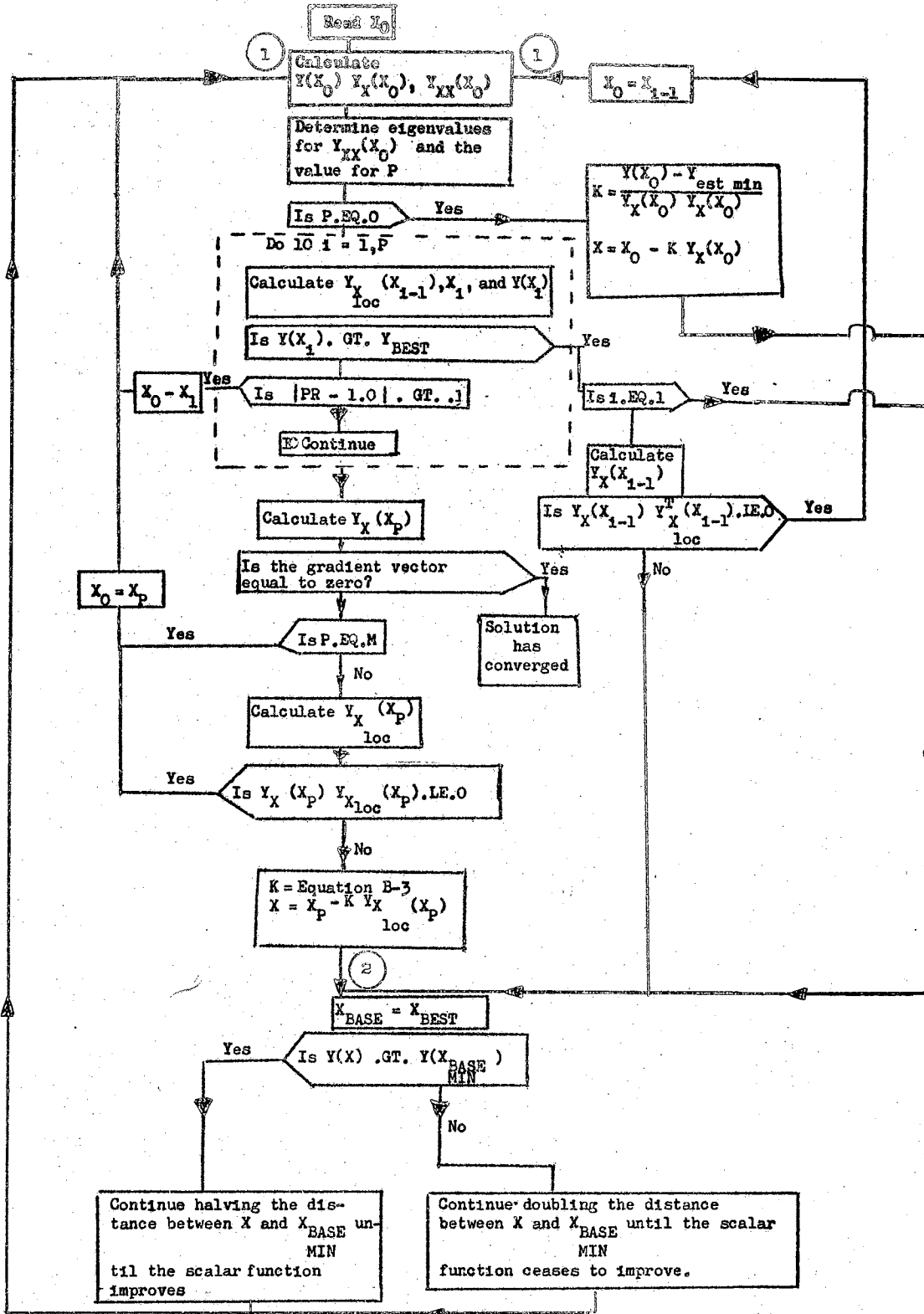


Figure 37. Flow Chart for Method of Seeking Principal Planes

value for the eigenvalue returned by the computational program might very likely be a small positive number. This difficulty is avoided by labeling an eigenvalue as zero if (1) it is positive, and (2) the value of the eigenvalue when multiplied by 10^6 is not larger than the largest eigenvalue.

The next block of the flow chart is a logic check to see if the number of positive eigenvalues, P , is equal to zero.

When the number of positive eigenvalues is zero, a linear search in the negative gradient direction for a minimum is performed. The location of this minimum need not be exact. The first problem which must be resolved in searching for the general area of this minimum is the magnitude of the initial step in the negative gradient direction. In the input data the user will provide an estimated minimum for the scalar function. The initial step used is such that if the gradient remained constant, then the scalar function would be reduced from its present value to the estimated minimum in one step. The resulting equations are:

$$K = \frac{Y(X_0) - Y_{\text{est min}}}{Y_X(X_0) \quad Y_X(X_0)^T} \quad (\text{B-1})$$

and

$$X = X_0 - K Y_X(X_0). \quad (\text{B-2})$$

If $Y(X_0)$ is already smaller than the estimated minimum, the algorithm is terminated, and a message which describes

why the algorithm was terminated is written. Otherwise, the algorithm continues to block 2. This is a block for determining the approximate minimum point for the scalar function along the predicted negative gradient direction, and it will now be described in detail.

The base point from which a minimum along the predicted negative gradient direction is being sought is called $X_{\text{BASE}}^{\text{MIN}}$. X_{BEST} is the value for the independent variable at the point where the smallest value for $Y(X)$ has thus far been obtained.

If the value for $Y(X)$ is greater than $Y(X_{\text{BEST}})$, the distance between X and $X_{\text{BASE}}^{\text{MIN}}$ is continually halved until a value for X is obtained such that $Y(X)$ is less than $Y(X_{\text{BASE}}^{\text{MIN}})$. X_0 is set equal to X and the algorithm returns to block 1.

If the value for $Y(X)$ is less than $Y(X_{\text{BASE}}^{\text{MIN}})$, the distance between X and $X_{\text{BASE}}^{\text{MIN}}$ is continually doubled until a point X is reached at which the scalar function ceases to improve. X_0 is set equal to the value of X at which $Y(X)$ was smallest, and the algorithm returns to block 1.

When the matrix of second partial derivatives has some positive eigenvalues, the algorithm proceeds into the iterative portion of the program which has been surrounded by a dotted line in Figure 37. This is the main part of the program, and it is within this area that the algorithm proceeds sequentially to the principal planes.

The subscript i is the iteration number and $i - 1$ refers

to the iteration just previous to the i^{th} iteration. The first block contained within the dotted lines indicates the calculation of (1) the gradient direction predicted by the truncated Taylor series at the point X_{i-1} , (2) the point, X_i , at which the predicted negative gradient intersects the desired principal plane, and (3) the magnitude of the scalar function evaluated at X_i .

When $Y(X_i)$ is greater than Y_{BEST} , it is desired to determine a new point such that the value of the scalar function is less than Y_{BEST} . Hence, the algorithm proceeds directly to block 2 if i is equal to 1.

If i is greater than 1 the direction being used in proceeding from point X_{i-1} to X_i is the gradient direction predicted by the truncated Taylor series. The predicted gradient direction will in general not be collinear with the true gradient direction. The value of the directional derivative along the predicted negative gradient direction will be negative (positive) if the dot product of the two gradient directions is positive (negative).

For the case of a positive directional derivative, the base point, X_0 , is set equal to X_{i-1} , and the algorithm returns to block 1 of the flow chart.

For the case of a negative directional derivative a minimum is determined along predicted negative gradient direction by going to block 2.

The next step within the iterative loop indicates the calculation of a performance ratio, PR. This performance

ratio is defined as

$$PR = \frac{Y(X_i) - Y(X_0)}{Y_{loc}(X_i) - Y(X_0)}$$

The reason for calculating the performance ratio is to determine if the point X_i is sufficiently close to the point X_0 so that the Taylor series approximation for the scalar function is accurate. If the truncated Taylor series described the function exactly at the point X_i , performance ratio would equal one.

When the absolute value of $(PR-1)$ is greater than .1, the Taylor series approximation is no longer very accurate. X_0 is then set equal to X_i and the algorithm returns to block 1 of the flow chart.

After P successful steps to the principle planes, a check is performed to determine if the scalar function has converged to a minimum. Hence, the next step after having completed the iterative loop is to calculate the true value of the gradient at X_p . If the absolute value of each component of the gradient is less than 10^{-8} , it is assumed that the true gradient is equal to zero; and the solution has converged.

The solution can converge even though the matrix of second partial derivatives has some zero eigenvalues. If this situation occurs, it may indicate that the minimum which has been located is not unique and that there are an infinite number of points located in the region of X_p that

have the same minimum value for the scalar function. An example of this type is presented in Chapter II. It is also possible for the scalar function to have a unique minimum at a point where the matrix of second partial derivatives has some zero eigenvalues. An example problem with this characteristic has also been worked in Chapter II.

The number of positive eigenvalues, P , is either equal to or less than the number of independent variables, M .

If P is equal to M , the base point, X_0 , is set equal to X_p ; and the algorithm returns to block 1 of the flow diagram.

When P is less than M , it is necessary to determine the sign of the directional derivative in the predicted negative gradient direction.

A positive directional derivative indicates that a better value for the scalar function cannot be obtained by going in the predicted negative gradient direction. The base point, X_0 , is set equal to X_p , and the algorithm returns to point 1 of the flow diagram.

A negative directional derivative indicates that a smaller value for the scalar function can be obtained by traveling in the predicted negative gradient direction.

The initial step size used is such that its distance is the same as the distance between the points X_0 and X_p . The magnitude for K and the equation for X then become

$$K^2 = \frac{[X_p - X_0]^T [X_p - X_0]}{Y_{X_{loc}}(X_p) Y_{X_{loc}}(X_p)^T} \quad (B-3)$$

and

$$X = X_P - K Y_{X_{loc}}(X_P). \quad (B-4)$$

The algorithm then proceeds to determine the approximate location of the minimum along this direction by going to block 2.

The computational algorithm for the method of seeking principal planes is composed of seven subroutines which are named SEEK, FCT, EIGEN, FORTIN, PARDIF, ISTORE, and DVAL.

The listings for subroutines SEEK, FCT, and EIGEN are given at the end of this appendix. The listings and descriptions of subroutines FORTIN, PARDIF, ISTORE, and DVAL are given in Appendix A.

A general flow chart for the subroutine SEEK is given in Figure 37.

The subroutine FCT is called by SEEK, and its purpose is to supply the values for the function, gradient, and matrix of second partial derivatives.

EIGEN is a subroutine which IBM provides through their Scientific Subroutine Package. This subroutine is used to determine the eigenvalues of the matrix of second partial derivatives.

Users Guide for the SEEK Algorithm

In order to use the SEEK algorithm, the user must supply the simple three card calling program which is given in Part A of Figure 38.

```

CALL    SEEK
CALL    EXIT
END

```

- A. Example of the calling program which is required for the SEEK algorithm.

```

Column -      5      1      1      2
First Data 2  0      5      0
Card          0.000

```

```

Column      5      1      1      2
Second      0      5      0
Data Card  100.0 * (X(2) - X(1) **2) **2 + (1.0 - X(1)) **2

```

- B. Data cards required to work the Rosenbrock curved valley problem using the SEEK algorithm.
-

Figure 38. Example Program for Determining the Minimum of an Algebraic Function

The SEEK algorithm requires two data cards.

The first data card has FORMAT (I5, D15.7) and contains the number of independent variables in column 5 and an estimate for the minimum of the function between columns 6 and 20.

The second data card must contain the right-hand side of the function which is to be minimized. It should be written in columns 7 through 72. If it is necessary to continue the equation onto more data cards, a C should be placed in column 6 of every one of the equation data cards except the last one.

The equation for Rosenbrock's curved valley is

$$Y = 100.0 * (X(2) - X(1) **2) **2 + (1.0 - X(1)) **2.$$

The data cards which are required for determining the minimum of this function are given in Part B of Figure 38.

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CALL SFEK	001
CALL EXIT	002
END	003
SUBROUTINE SFEK	004
C	005
C THIS PROGRAM WAS WRITTEN AND PROGRAMED BY DENNIS UNRUH AT THE	006
C DEPARTMENT OF MECHANICAL AND AEROSPACE ENGINEERING, OKLAHOMA STATE	007
C UNIVERSITY, STILLWATER, OKLAHOMA. JULY 1969	008
C	009
C DELFPR - THE PREDICTED DIFFERENCE BETWEEN THE VALUE OF F AT	010 0023
C THE AXIS PLAIN AND F AT THE BASE POINT.	011 0024
C DEN - SEE NUM/DEN.	012 0043
C DIRECT - IF THIS NUMBER IS POSITIVE, THAN THE PREDICTED	013 0038
C GRADIENT DIRECTION AND ACTUAL GRADIENT DIRECTION ARE WITHIN	014 0039
C 90 DEGREES OF EACH OTHER.	015 0040
C EIGVAL - EIGENVALUE VECTOR OF GX.	016 0037
C F - FUNCTION BEING MINIMIZED. F=F(X)	017 0015
C FBASF - VALUE OF F AT BASE POINT	018 0027
C FBEST - VALUE OF F AT BEST POINT.	019 0028
C FESMIN - ESTIMATED MINIMUM FOR THE SCALAR FUNCTION.	020
C G - GRADIENT VECTOR OF FUNCTION F. FOR EXAMPLE G(2)=PARTIAL F/	021 0016
C PARTIAL X(2).	022 0017
C GMAG - MAGNITUDE OF GRADIENT AFTER NPOS STEPS TO AXIS PLANES.	023
C GPRED - PREDICTED VALUE OF GRADIENT AT AXIS PLAIN.	024 0022
C GX - MATRIX OF SECONO PARTIALS OF F. I.E. GX(2,3)=PARTIAL G(2)	025 0018
C /PARTIAL X(3).	026 0019
C GXS - VECTOR WHICH CONTAINS GX IN SCIENTIFIC SUBROUTINE PACKAGE	027 0035
C SYMMETRIC STORAGE MODE.	028 0036
C N - THE NUMBER OF INDEPENDENT VARIABLES.	029
C NF - NUMBER OF TIMES F HAS BEEN CALCULATED.	030
C NG - NUMBER OF TIMES THE GRADIENT VECTOR HAS BEEN CALCULATED.	031
C NGX - NUMBER OF TIMES MATRIX GX HAS BEEN CALCULATED.	032
C NPOS - NUMBER OF POSITIVE EIGENVALUES.	033 0029
C NUM/DEN - THIS IS THE MAGNITUDE USED ON STEP NPOS+1 PROVIDED	034 0032
C NPOS SUCCESSFUL STEPS TO THE AXIS PLANES HAVE BEEN MADE. THIS	035 0033
C IS USED ONLY IF NNEG IS NOT ZERO.	036 0034
C NXMAX - MAXIMUM NUMBER OF INDEPENDENT VARIABLES.	037 0044
C PEKRAT - RATIO BETWEEN THE PREDICTED FUNCTION CHANGE AND THE	038 0025
C ACTUAL FUNCTION CHANGE.	039 0026
C R - DUMMY VARIABLE NEEDED FOR CALL STATEMENT OF EIGEN.	040 0045
C WORK - WORKING VARIABLE.	041 0046
C X - INDEPENDENT VARIABLE VECTOR.	042 0012
C XBAMIN - BASE POINT FROM WHICH A MINIMUM IS BEING SOUGHT BY A	043
C LINEAR SEARCH IN THE PREDICTED NEGATIVE GRADIENT DIRECTION.	044
C XBASF - THE VALUE OF THE INDEPENDENT VARIABLE VECTOR AT THE	045 0013
C BASE POINT.	046 0014
C XBEST - THE VALUE OF THE INDEPENDENT VARIABLE AT THE POINT	047 0020
C WHERE THE CALCULATED VALUE OF F WAS SMALLEST.	048 0021
C XNPOS - THE VALUE OF THE INDEPENDENT VARIABLE AFTER NPOS	049 0041
C SUCCESSFUL STEPS TO THE AXIS PLANES.	050 0042
C IMPLICIT INTEGER*2 (I-N),REAL*8 (A-H,O-Z)	051
C INTEGER*4 MM	052
C REAL*8 NUM,DEN,MAG	053
C NXMAX=10	054 0047
C DIMENSION X(NXMAX),G(NXMAX),XBEST(NXMAX),	055

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C	XBASE(NXMAX),GXS((NXMAX*(NXMAX+1))/2),R(1),EIGVAL(NXMAX),	056
C	GPRED(NXMAX),XBAMIN(NXMAX)	057
C	,GXSS(NXMAX*(NXMAX+1))/2)	058
	DIMENSION X(50),G(10),XBEST(10),XBASE(10),GXS(55),	059
	1R(1),EIGVAL(10),GPRED(10),XBAMIN(50)	060
	2,GXSS(55)	061
	COMMON /BLK3/ IF,IG(10),IGXS(55),N	062
100	FORMAT (8D15.7)	063 0052
101	FORMAT (' THE EIGENVALUE VECTOR IS')	064 0053
102	FORMAT (6H NPOS=,15)	065
103	FORMAT (4HONF=,15,4H NG=,15,5H NGX=,15)	066 0055
104	FORMAT (' INDEPENDENT VECTOR X IS')	067
105	FORMAT (3H F=,D15.7)	068 0057
106	FORMAT (' THE GRADIENT VECTOR IS')	069 0058
107	FORMAT (' GXS(I),I=1,IJMAX')	070
108	FORMAT (8H PERRAT=,D15.7)	071 0060
109	FORMAT (' THE SOLUTION HAS CONVERGED')	072 0061
110	FORMAT (8HODIRECT=,D15.7)	073 0062
111	FORMAT (7H FBEST=,D15.7)	074 0063
112	FORMAT (' THE VALUE OF X TO AXIS PLANE',15,' IS')	075 0064
113	FORMAT (' THE VALUE OF X AFTER HALVING IS')	076 0065
114	FORMAT (' THE VALUE OF X AFTER DOUBLING IS')	077 0066
115	FORMAT (15,D15.7)	078
116	FORMAT (' THE FUNCTION VALUE IS ALREADY LESS THAN YOUR PREDICTED	079
	IMINIMUM')	080
117	FORMAT (3H N=,15,8H FESMIN=,D15.7)	081
118	FORMAT (' GRADIENT EVALUATED AT XBAMIN')	082
	READ(5,115) N,FESMIN	083
	READ(5,100) (X(I),I=1,N)	084
	WRITE (6,117) N,FESMIN	085
	IJMAX=(N*(N+1))/2	086
	CALL FORTIN (IF)	087
	DO 35 I=1,N	088
	CALL PARDIF(IF,IG(I),I)	089
	DO 35 J=I,N	090
	IJ=((J-1)*J)/2+I	091
35	CALL PARDIF(IG(I),IGXS(IJ),J)	092
	NF=0	093 0067
	NG=0	094 0068
	NGX=0	095 0069
	I=1	096
	CALL FCT(X,F,G,GXS,NXMAX,I,NF,NG,NGX)	097
	WRITE (6,103) NF,NG,NGX	098 0071
	WRITE (6,104)	099 0072
	WRITE (6,100) (X(I),I=1,N)	100 0073
	WRITE (6,105) F	101 0074
	DO 1 I=1,N	102 0075
1	XBEST(I)=X(I)	103 0076
	FBEST=F	104 0077
2	I=2	105
	CALL FCT(X,F,G,GXS,NXMAX,I,NF,NG,NGX)	106
	WRITE (6,103) NF,NG,NGX	107 0079
	WRITE (6,106)	108 0082
	WRITE (6,100) (G(I),I=1,N)	109 0083
3	I=3	110

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 12345678901234567890123456789012345678901234567890123456789012345678901234567890

```

CALL FCT(X,F,G,GXS,NXMAX,I,NF,NG,NGX) 111
WRITE (6,103) NF,NG,NGX 112 0085
WRITE (6,107) 113 0088
WRITE (6,100) (GXS(I),I=1,IJMAX) 114
DO 5 I=1,N 115
5 XBASE(I)=X(I) 116
FBASE=F 117 0092
C 118 0093
C DETERMINE EIGENVALUES OF GX AND THE NUMBER NPOS. 119
C 120 0095
DO 7 J=1,IJMAX 121
7 GXSS(I)=GXS(I) 122
MMM=N 123
CALL EIGEN(GXSS,R,MMM,1) 124
DO 6 I=1,N 125 0101
II=(I*(I+1))/2 126 0102
6 EIGVAL(I)=GXSS(II) 127
NPOS=N 128 0105
DO 8 I=1,N 129 0106
IF (1.0D05*EIGVAL(I).GT.EIGVAL(1)) GO TO 8 130
NPOS=NPOS-1 131 0108
8 CONTINUE 132 0115
IF (EIGVAL(1).LE.0.0D0) NPOS=0 133
WRITE (6,101) 134 0117
WRITE (6,100) (EIGVAL(I),I=1,N) 135 0118
WRITE (6,102) NPOS 136
C 137
C IF NPOS IS EQUAL TO ZERO , A LINEAR SEARCH IS PERFORMED FOR A 138
C MINIMUM IN THE NEGATIVE GRADIENT DIRECTION. 139
C 140
IF (NPOS.NE.0) GO TO 52 141
DO 53 I=1,N 142
53 XBAMIN(I)=X(I) 143
NUM=FBEST-FESMIN 144
IF (NUM.LT.0.0D0) GO TO 30 145
DEN=0.0D0 146
DO 50 I=1,N 147
50 DEN=DEN+G(I)*G(I) 148
DO 51 I=1,N 149
51 X(I)=X(I)-(NUM/DEN)*G(I) 150
GO TO 23 151
C 152 0120
C DETERMINE VALUES FOR X TO THE SUCCESSIVE AXIS PLAINS. 153 0121
C 154 0122
52 DO 14 K=1,NPOS 155
DO 9 I=1,N 156 0123
GPRED(I)=G(I) 157 0124
DO 9 J=1,N 158 0127
IJ=((J-1)*J)/2+1 159
IF (J.EY.1) IJ=((I-1)*I)/2+J 160
9 GPRED(I)=GPRED(I)+GXS(IJ)*(X(J)-XBASE(J)) 161
DO 10 I=1,N 162 0129
10 X(I)=X(I)-GPRED(I)/EIGVAL(I) 163 0130
I=1 164
CALL FCT(X,F,G,GXS,NXMAX,I,NF,NG,NGX) 165

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80/80 LIST

B-14

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WRITE (6,103) NF,NG,NGX	166	0132
WRITE (6,112) K	167	0133
WRITE (6,100) (X(I),I=1,N)	168	0134
WRITE (6,105) F	169	0135
IF (F.GT.FBEST.AND.K.EQ.1) GO TO 41	170	
IF (F.GT.FBEST) GO TO 60	171	
C	172	0140
C CALCULATE PERRAT	173	0141
C	174	0142
DELFPR=0.0	175	0143
DO 13 I=1,N	176	0144
WORK=0.0	177	0145
DO 12 J=1,N	178	0146
IJ=((J-1)*J)/2+1	179	
IF (J.LT.1) IJ=((I-1)*I)/2+J	180	
12 WORK=WORK+GXS(IJ)*(X(J)-XBASE(J))	181	
13 DELFPR=DELFPR+(G(I))+.50*WORK*(X(I)-XBASE(I))	182	0148
PERRAT=(F-FBASE)/DELFPR	183	0149
WRITE (6,108) PERRAT	184	0150
IF (DABS(PERRAT-1.000).GT..100) GO TO 2	185	
DO 11 I=1,N	186	0137
11 XBEST(I)=X(I)	187	0138
FBEST=F	188	0139
14 CONTINUE	189	0152
DO 15 I=1,N	190	0154
GPRED(I)=G(I)	191	
DO 15 J=1,N	192	0156
IJ=((J-1)*J)/2+1	193	
IF (J.LT.1) IJ=((I-1)*I)/2+J	194	
15 GPRED(I)=GPRED(I)+GXS(IJ)*(X(J)-XBASE(J))	195	
I=2	196	
CALL FCT(X,F,G,GXS,NXMAX,I,NF,NG,NGX)	197	
WRITE (6,103) NF,NG,NGX	198	0159
WRITE (6,106)	199	0162
WRITE (6,100) (G(I),I=1,N)	200	0163
C	201	
C CHECK FOR CONVERGENCE.	202	
C	203	
DO 45 I=1,N	204	
IF (DABS(G(I)).GT.1.00-8) GO TO 46	205	
45 CONTINUE	206	
GO TO 33	207	
46 IF (NPOS.EQ.N) GO TO 3	208	
DIRECT=0.0	209	0164
DO 16 I=1,N	210	0165
16 DIRECT=DIRECT+G(I)*GPRED(I)	211	0166
WRITE (6,110) DIRECT	212	0167
IF (DIRECT.LE.0.0) GO TO 3	213	0168
NUM=0.0	214	0169
DEN=0.0	215	0170
DO 17 I=1,N	216	0171
NUM=NUM+(X(I)-XBASE(I))**2	217	0172
17 DEN=DEN+(GPRED(I))**2	218	0173
MAG=DSQRT(NUM/DEN)	219	
DO 18 I=1,N	220	0174

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18 X(I)=X(I)-MAG*GPRED(I) 221
C 222
C PERFORM A LINEAR SEARCH FOR A MINIMUM IN THE PREDICTED NEGATIVE 223
C GRADIENT DIRECTION. 224
C 225
I=1 226
CALL FCT(X,F,G,GXS,NXMAX,I,NF,NG,NGX) 227
WRITE (6,103) NF,NG,NGX 228 0178
WRITE (6,104) 229 0179
WRITE (6,100) (X(I),I=1,N) 230 0180
WRITE (6,105) F 231 0181
41 DO 42 I=1,N 232
42 XBAMIN(I)=XBEST(I) 233
IF (F.GT.FBEST) GO TO 23 234 0182
C 235
C CONTINUE DOUBLING THE DISTANCE UNTIL F CEASES TO BECOME BETTER. 236
C 237
19 DO 20 I=1,N 238 0183
20 XBEST(I)=X(I) 239 0184
FBEST=F 240 0185
DO 21 I=1,N 241 0186
21 X(I)=XBAMIN(I)+2.0*(X(I)-XBAMIN(I)) 242
I=1 243
CALL FCT(X,F,G,GXS,NXMAX,I,NF,NG,NGX) 244
WRITE (6,103) NF,NG,NGX 245 0189
WRITE (6,114) 246 0190
WRITE (6,100) (X(I),I=1,N) 247 0191
WRITE (6,105) F 248 0192
IF (F.LT.FBEST) GO TO 19 249 0193
DO 22 I=1,N 250 0194
22 X(I)=XBEST(I) 251 0195
F=FBEST 252 0196
GO TO 2 253 0197
C 254
C CONTINUE HALVING THE DISTANCE UNTIL F BECOMES BETTER. 255
C 256
23 DO 24 I=1,N 257 0198
24 X(I)=XBAMIN(I)+.50*(X(I)-XBAMIN(I)) 258
I=1 259
CALL FCT(X,F,G,GXS,NXMAX,I,NF,NG,NGX) 260
WRITE (6,103) NF,NG,NGX 261 0201
WRITE (6,113) 262 0202
WRITE (6,100) (X(I),I=1,N) 263 0203
WRITE (6,105) F 264 0204
IF (F.GT.FBEST) GO TO 23 265 0205
DO 25 I=1,N 266 0206
25 XBEST(I)=X(I) 267 0207
FBEST=F 268 0208
GO TO 2 269 0209
60 DO 61 I=1,N 270
61 XBAMIN(I)=XBEST(I) 271
I=2 272
CALL FCT(XBAMIN,F,G,GXS,NXMAX,I,NF,NG,NGX) 273
WRITE (6,103) NF,NG,NGX 274
WRITE (6,118) 275

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WRITE (6,100) (G(I),I=1,N)	276
DIRECT=0.0	277
DO 62 I=1,N	278
62 DIRECT=DIRECT+G(I)*GPRED(I)	279
WRITE (6,110) DIRECT	280
IF (DIRECT.GT.0.000) GO TO 23	281
DO 63 I=1,N	282
63 X(I)=XBAMIN(I)	283
GO TO 3	284
30 WRITE (6,116)	285
CALL EXIT	286
33 WRITE (6,109)	287
CALL EXIT	288 0241
RETURN	289 0242
END	290 0243
SUBROUTINE FCT(X,F,G,GXS,NXMAX,II,NF,NG,NGX)	291
IMPLICIT INTEGER*2 (I-N),REAL*8 (A-H,O-Z)	292
DIMENSION X(50),G(10),GXS(55)	293
COMMON /BLK3/ IF,IG(10),IGXS(55),N	294
GO TO (1,2,3),II	295 0247
1 NF=NF+1	296 0248
C	297 0249
C INSERT THE EQUATION FOR F AS A FUNCTION OF X.	298 0250
C	299 0251
F=DVAL(IF,X)	300
RETURN	301 0253
C	302 0254
C	303 0255
C	304 0256
C INSERT THE EQUATIONS FOR G IMMEDIATELY FOLLOWING THE STATEMENT	305 0257
C 2 NG=NG+1.	306 0258
2 NG=NG+1	307 0259
DO 4 I=1,N	308
4 G(I)=DVAL(IG(I),X)	309
RETURN	310 0264
C	311 0265
C INSERT THE EQUATIONS FOR GX IMMEDIATELY FOLLOWING THE STATEMENT	312 0266
C 3 NGX=NGX+1	313 0267
3 NGX=NGX+1	314 0268
DO 5 I=1,N	315
DO 5 J=I,N	316
IJ=((J-1)*J)/2+I	317
5 GXS(IJ)=DVAL(IGXS(IJ),X)	318
RETURN	319 0274
END	320 0275

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SUBROUTINE EIGEN(A,R,N,MV) EIGEN041
C EIGEN001
C ..... EIGEN002
C EIGEN003
C SUBROUTINE EIGEN EIGEN004
C EIGEN005
C PURPOSE EIGEN006
C COMPUTE EIGENVALUES AND EIGENVECTORS OF A REAL SYMMETRIC EIGEN007
C MATRIX EIGEN008
C EIGEN009
C USAGE EIGEN010
C CALL EIGEN(A,R,N,MV) EIGEN011
C EIGEN012
C DESCRIPTION OF PARAMETERS EIGEN013
C A - ORIGINAL MATRIX (SYMMETRIC), DESTROYED IN COMPUTATION. EIGEN014
C RESULTANT EIGENVALUES ARE DEVELOPED IN DIAGONAL OF EIGEN015
C MATRIX A IN DESCENDING ORDER. EIGEN016
C R - RESULTANT MATRIX OF EIGENVECTORS (STORED COLUMNWISE, EIGEN017
C IN SAME SEQUENCE AS EIGENVALUES) EIGEN018
C N - ORDER OF MATRICES A AND R EIGEN019
C MV- INPUT CODE EIGEN020
C 0 COMPUTE EIGENVALUES AND EIGENVECTORS EIGEN021
C 1 COMPUTE EIGENVALUES ONLY (R NEED NOT BE EIGEN022
C DIMENSIONED BUT MUST STILL APPEAR IN CALLING EIGEN023
C SEQUENCE) EIGEN024
C EIGEN025
C REMARKS EIGEN026
C ORIGINAL MATRIX A MUST BE REAL SYMMETRIC (STORAGE MODE=1) EIGEN027
C MATRIX A CANNOT BE IN THE SAME LOCATION AS MATRIX R EIGEN028
C EIGEN029
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED EIGEN030
C NONE EIGEN031
C EIGEN032
C METHOD EIGEN033
C DIAGONALIZATION METHOD ORIGINATED BY JACOBI AND ADAPTED EIGEN034
C BY VON NEUMANN FOR LARGE COMPUTERS AS FOUND IN 'MATHEMATICAL EIGEN035
C METHODS FOR DIGITAL COMPUTERS', EDITED BY A. KALSTON AND EIGEN036
C H.S. WILF, JOHN WILEY AND SONS, NEW YORK, 1962, CHAPTER 7 EIGEN037
C EIGEN038
C ..... EIGEN039
C DIMENSION A(1),R(1) EIGEN040
C EIGEN041
C ..... EIGEN042
C EIGEN043
C ..... EIGEN044
C IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE EIGEN045
C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION EIGEN046
C STATEMENT WHICH FOLLOWS. EIGEN047
C EIGEN048
C EIGEN049
C DOUBLE PRECISION A,R,ANORM,ANRMX,THR,X,Y,SINX,SINX2,COSX, EIGEN050
C 1 COSX2,SINCS,RANGE EIGEN051
C DOUBLE PRECISION A,R,ANORM,ANRMX,THR,X,Y,SINX,SINX2,COSX,
C 1 COSX2,SINCS,RANGE,DABS,DSQRT
C EIGEN052
C THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS EIGEN053

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C	APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS	EIGEN054
C	ROUTINE.	EIGEN055
C		EIGEN056
C	THE DOUBLE PRECISION VERSION OF THIS SUBROUTINE MUST ALSO	EIGEN057
C	CONTAIN DOUBLE PRECISION FORTRAN FUNCTIONS. SQRT IN STATEMENTS	EIGEN058
C	40, 68, 75, AND 78 MUST BE CHANGED TO DSQRT. ABS IN STATEMENT	EIGEN059
C	62 MUST BE CHANGED TO DABS. THE CONSTANT IN STATEMENT 5 SHOULD	EIGEN060
C	BE CHANGED TO 1.0D-12.	EIGEN061
C	EIGEN062
C		EIGEN063
C	GENERATE IDENTITY MATRIX	EIGEN064
C		EIGEN065
	5 RANGE=1.0D-12	
	IF(MV-1) 10,25,10	EIGEN066
10	IQ=-N	EIGEN067
	DO 20 J=1,N	EIGEN068
	IO=IO+N	EIGEN069
	DO 20 I=1,N	EIGEN070
	IJ=IQ+I	EIGEN071
	R(IJ)=0.0	EIGEN072
	IF(I-J) 20,15,20	EIGEN073
15	R(IJ)=1.0	EIGEN074
20	CONTINUE	EIGEN075
C		EIGEN076
C	COMPUTE INITIAL AND FINAL NORMS (ANORM AND ANORMX)	EIGEN077
C		EIGEN078
	25 ANORM=0.0	EIGEN079
	DO 35 I=1,N	EIGEN080
	DO 35 J=1,N	EIGEN081
	IF(I-J) 30,35,30	EIGEN082
30	IA=I+(J-J)/2	EIGEN083
	ANORM=ANORM+A(IA)*A(IA)	EIGEN084
35	CONTINUE	EIGEN085
	IF(ANORM) 165,165,40	EIGEN086
40	ANORM=1.414*DSQRT(ANORM)	
	ANRMX=ANORM*RANGE/FLOAT(N)	EIGEN086
C		EIGEN089
C	INITIALIZE INDICATORS AND COMPUTE THRESHOLD, THR	EIGEN090
C		EIGEN091
	IND=0	EIGEN092
	THR=ANORM	EIGEN093
45	THR=THR/FLOAT(N)	EIGEN094
50	L=1	EIGEN095
55	M=L+1	EIGEN096
C		EIGEN097
C	COMPUTE SIN AND COS	EIGEN098
C		EIGEN099
	60 MQ=(M*M-M)/2	EIGEN100
	LQ=(L*L-L)/2	EIGEN101
	LM=L+MQ	EIGEN102
62	IF(DABS(A(LM))-THR) 130,65,65	
65	IND=1	EIGEN104
	LL=L+LQ	EIGEN105
	MM=M+MQ	EIGEN106

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X=0.5*(A(LL)-A(MM))
68 Y=-A(LM)/DSQRT(A(LM)*A(LM)+X*X)
IF(X) 70,75,75
70 Y=-Y
75 SINX=Y/DSQRT(2.0*(1.0+(DSQRT(1.0-Y*Y))))
SINX2=SINX*SINX
78 COSX=DSQRT(1.0-SINX2)
COSX2=COSX*COSX
SINCS =SINX*COSX
C
C ROTATE L AND M COLUMNS
C
ILQ=N*(L-1)
IMQ=N*(M-1)
DO 125 I=1,N
IQ=(I+I-1)/2
IF(I-L) 80,115,80
80 IF(I-M) 85,115,90
85 IM=I+MQ
GO TO 95
90 IM=M+IQ
95 IF(I-L) 100,105,105
100 IL=I+LQ
GO TO 110
105 IL=L+IQ
110 X=A(IL)*COSX-A(IM)*SINX
A(IM)=A(IL)*SINX+A(IM)*COSX
A(IL)=X
115 IF(MV-1) 120,125,120
120 ILR=ILQ+I
IMR=IMQ+I
X=R(ILR)*COSX-R(IMR)*SINX
R(IMR)=R(ILR)*SINX+R(IMR)*COSX
R(ILR)=X
125 CONTINUE
X=2.0*A(LM)*SINCS
Y=A(LL)*COSX2+A(MM)*SINX2-X
X=A(LL)*SINX2+A(MM)*COSX2+X
A(LM)=(A(LL)-A(MM))*SINCS+A(LM)*(COSX2-SINX2)
A(LL)=Y
A(MM)=X
C
C TFSTS FOR COMPLETION
C
C TEST FOR M = LAST COLUMN
C
130 IF(M-N) 135,140,135
135 M=M+1
GO TO 60
C
C TEST FOR L = SECOND FROM LAST COLUMN
C
140 IF(L-(N-1)) 145,150,145
145 L=L+1
GO TO 55

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EIGEN107

EIGEN109

EIGEN110

EIGEN112

EIGEN114

EIGEN115

EIGEN116

EIGEN117

EIGEN118

EIGEN119

EIGEN120

EIGEN121

EIGEN122

EIGEN123

EIGEN124

EIGEN125

EIGEN126

EIGEN127

EIGEN128

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150	IF(IND-1) 160,155,160	EIGEN162
155	IND=0	EIGEN163
	GU TO 50	EIGEN164
C		EIGEN165
C	COMPARE THRESHOLD WITH FINAL NORM	EIGEN166
C		EIGEN167
160	IF(THK-ANRMX) 165,165,45	EIGEN168
C		EIGEN169
C	SORT EIGENVALUES AND EIGENVECTORS	EIGEN170
C		EIGEN171
165	IQ=-N	EIGEN172
	DO 185 I=1,N	EIGEN173
	IQ=IQ+N	EIGEN174
	LL=I+(I-1)/2	EIGEN175
	JQ=N*(I-2)	EIGEN176
	DO 185 J=1,N	EIGEN177
	JQ=JQ+N	EIGEN178
	MM=J+(J-J)/2	EIGEN179
	IF(A(LL)-A(MM)) 170,185,185	EIGEN180
170	X=A(LL)	EIGEN181
	A(LL)=A(MM)	EIGEN182
	A(MM)=X	EIGEN183
	IF(MV-1) 175,185,175	EIGEN184
175	DO 180 K=1,N	EIGEN185
	ILR=IQ+K	EIGEN186
	IMR=JQ+K	EIGEN187
	X=R(ILR)	EIGEN188
	R(ILR)=R(IMR)	EIGEN189
180	R(IMR)=X	EIGEN190
185	CONTINUE	EIGEN191
	RETURN	EIGEN192
	END	EIGEN193

APPENDIX C

CONDITIONS FOR CONVERGENCE OF GAUSS'S METHOD

The Newton-Raphson method as given by Equation (2-3) requires the computation of the entire matrix of second partial derivatives for the scalar function. This is a considerable amount of computational effort, and it would be desirable if the matrix of second partial derivatives could be approximated by a simpler equation.

Gauss's method does neglect some of the more complicated terms of the matrix of second partial derivatives. This can be seen by looking at Equations (2-42) and (2-43).

In this appendix the matrix of second partial derivatives is given by the sum of the symmetric matrices A and B.

$$Y_{XX} = A + B. \quad (C-1)$$

Gauss's equation can be obtained by neglecting the matrix B in Equation (C-1) and then substituting Equation (C-1) into Equation (2-3). The equation which results is

$$X_{i+1} - X_i = -A (X_i)^{-1} Y_X^T(X_i). \quad (C-2)$$

A matrix Q is now defined as

$$Q = A^{-1} B. \quad (C-3)$$

The conditions for convergence of Gauss's method will now be shown by a proof which is similar to one presented by Bekey and McGhee (19). The conclusions of this proof are:

1. Gauss's method will converge provided the starting point is sufficiently close to the extremum point, X_{EXT} , if all of the eigenvalues of the matrix $Q^T(X_{EXT}) Q(X_{EXT})$ are less than one.
2. Gauss's method will diverge from the extremum point, X_{EXT} , if all of the eigenvalues of the matrix $Q^T(X_{EXT}) Q(X_{EXT})$ are larger than one.
3. If some of the eigenvalues of $Q^T(X_{EXT}) Q(X_{EXT})$ are larger than one and some are smaller than one, no final conclusions are drawn.

At an extremum point the gradient vector must be 0, and the Taylor series expansion for the scalar function about the point X_{EXT} becomes

$$Y(X) = Y(X_{EXT}) + \frac{1}{2}[X - X_{EXT}]^T Y_{XX}(X_{EXT})[X - X_{EXT}] + (\text{higher order terms}). \quad (C-4)$$

The gradient of Equation (C-4) is

$$Y_X(X) = [X - X_{EXT}]^T Y_{XX}(X_{EXT}) + (\text{higher order terms}). \quad (C-5)$$

The substitution of Equation (C-1) into Equation (C-5) yields

$$Y_X(X) = [X - X_{EXT}]^T [A(X_{EXT}) + B(X_{EXT})] + (\text{higher order terms}). \quad (C-6)$$

The substitution of Equation (C-6) into Equation (C-2) yields

$$X_{i+1} - X_i = -A(X_i)^{-1} [A(X_{EXT}) + B(X_{EXT})][X_i - X_{EXT}] + (\text{higher order terms}). \quad (C-7)$$

The equations for each of the elements in the matrix $A(X_i)^{-1}$ could be expanded in a Taylor series about the point X_{EXT} provided that A is not singular within a neighborhood of the extremum point. This yields

$$A(X_i)^{-1} = A(X_{EXT})^{-1} + (\text{higher order terms in } X_i - X_{EXT}). \quad (C-8)$$

Equation (C-8) can now be substituted into Equation (C-7). Since only values of X within an infinitesimal region of X_{EXT} are being considered, the higher order terms can be neglected, and the equation which results is

$$X_{i+1} - X_i = -[I + A(X_{EXT})^{-1} B(X_{EXT})][X_i - X_{EXT}]. \quad (C-9)$$

Equation (C-3) is substituted into Equation (C-9), and the resulting equation is rearranged to yield

$$X_{i+1} - X_{EXT} = -Q(X_{EXT}) [X_i - X_{EXT}]. \quad (C-10)$$

The coordinate transformation

$$W = E^T [X_i - X_{EXT}] \quad (C-11)$$

is now introduced. In Equation (C-11), the matrix E is the eigenvector matrix of $Q^T(X_{EXT}) Q(X_{EXT})$. Athans and Falb (9) demonstrate that

$$E^T E = I \quad (C-12)$$

and

$$E^T Q^T(X_{EXT}) Q(X_{EXT}) E = \lambda. \quad (C-13)$$

In Equation (C-12), λ is the eigenvalue matrix.

From Equations (C-11) and (C-12), it follows that

$$W^T W = [X_i - X_{EXT}]^T [X_i - X_{EXT}]. \quad (C-14)$$

Equations (C-10) through (C-13) can be combined to yield

$$[X_{i+1} - X_{EXT}]^T [X_{i+1} - X_{EXT}] = W^T \lambda W. \quad (C-15)$$

If all of the eigenvalues are less than one, Equations (C-15) and (C-14) can be combined to yield

$$\begin{aligned} [X_{i+1} - X_{EXT}]^T [X_{i+1} - X_{EXT}] &= W^T \lambda W < W^T W \\ &= [X_i - X_{EXT}]^T [X_i - X_{EXT}]. \end{aligned} \quad (C-16)$$

Equation (C-16) is the mathematical statement for conclusion number one given at the start of this proof.

If all of the eigenvalues are greater than one, Equations (C-15) and (C-14) can be combined to yield

$$\begin{aligned} [X_{i+1} - X_{EXT}]^T [X_{i+1} - X_{EXT}] &= W^T \lambda W > W^T W \\ &= [X_i - X_{EXT}]^T [X_i - X_{EXT}]. \end{aligned} \quad (C-17)$$

Equation (C-17) is the mathematical statement for conclusion number two given at the start of this proof.

APPENDIX D

SENSITIVITY EQUATIONS FOR DYNAMICAL SYSTEMS

It is assumed that a mathematical model for the system has been formulated and written in state variable notation as

$$\dot{X} = F(X, P, t). \quad (D-1)$$

In the above equation, X is an N dimensional state vector, P is an M dimensional parameter vector, and t is the independent variable, time.

The initial condition vector is partitioned as

$$X(t_0) = \begin{bmatrix} \psi \\ X_0 \end{bmatrix} \begin{array}{l} \text{- free} \\ \text{- specified.} \end{array} \quad (D-2)$$

In the above equation, ψ is a K dimensional vector of free initial conditions, and X_0 is an $N-K$ dimensional vector of known initial conditions.

Equation (D-1) has been written as a total differential equation, but in actuality it should be a partial differential equation because the dependent variables, X , are functions of $K+M+1$ independent variables,

$$X = X(P_1, \dots, P_M, \psi_1, \dots, \psi_K, t).$$

Hence, Equation (D-1) becomes

$$\frac{\partial X}{\partial t} = F(X, P, t). \quad (D-3)$$

If the partial derivative of Equation (D-3) is taken with respect to P_i and the order of the partial derivatives reversed, the following is obtained

$$\frac{\partial X_{P_i}}{\partial t} = F_X X_{P_i} + F_{P_i} \quad i = 1, 2, \dots, M. \quad (D-4)$$

The notation used in Equation (D-4) is

$$X_{P_i} = \frac{\partial X}{\partial P_i} \quad (D-5)$$

$$F_{P_i} = \frac{\partial F}{\partial P_i} \quad (D-6)$$

$$F_X = \begin{bmatrix} \frac{\partial F_1}{\partial X_1} & \cdots & \frac{\partial F_1}{\partial X_N} \\ \vdots & & \vdots \\ \frac{\partial F_N}{\partial X_1} & \cdots & \frac{\partial F_N}{\partial X_N} \end{bmatrix}. \quad (D-7)$$

If the partial derivative of Equation (D-3) is taken with respect to ψ_i , and the order of the partial derivatives reversed, the following is obtained:

$$\frac{\partial X_{\psi_i}}{\partial t} = F_X X_{\psi_i} \quad i = 1, 2, \dots, K. \quad (D-8)$$

The additional notation used in Equation (D-8) is

$$X_{\psi_i} = \frac{\partial X}{\partial \psi_i}. \quad (D-9)$$

At time t_0 each of the initial conditions for the state variables is independent of the parameter guess. This yields,

$$X_{P_i} = 0; \quad i = 1, 2, \dots, M. \quad (D-10)$$

Since each of the free initial conditions is independent of the other initial conditions, one can conclude that

$$X_{\psi_i} = \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \\ 0 \end{bmatrix} \leftarrow \text{row } i, \quad i = 1, 2, \dots, K. \quad (D-11)$$

Equations (D-10) and (D-11) provide the initial conditions necessary for integrating Equations (D-4) and (D-8) forward in time from t_0 to t_f if a guess is made for the free portion of the initial condition given by Equation (D-2).

Equations (D-12) and (D-13) are generated by taking the partial derivative of Equations (D-4) and (D-8) with respect to P_j , and then reversing the order of the partial derivatives. Equations (D-14) and (D-15) are formed in a similar manner by taking the partial derivative with respect to ψ_j .

$$\frac{\partial X_{P_j P_i}}{\partial t} = F_X X_{P_j P_i} + \sum_{L=1}^N \left(\frac{\partial F_X}{\partial X_L} \frac{\partial X_L}{\partial P_j} + \frac{\partial F_X}{\partial P_j} \right) X_{P_i} +$$

$$+ F_{P_j P_i} + \sum_{L=1}^N \left(\frac{\partial F_{P_i}}{\partial X_L} \frac{\partial X_L}{\partial P_j} \right) \quad (D-12)$$

$$\frac{\partial X_{P_j \psi_i}}{\partial t} = F_X X_{P_j \psi_i} + \sum_{L=1}^N \left(\frac{\partial F_X}{\partial X_L} \frac{\partial X_L}{\partial P_j} + \frac{\partial F_X}{\partial P_j} \right) X_{\psi_i} \quad (D-13)$$

$$\begin{aligned} \frac{\partial X_{\psi_j P_i}}{\partial t} &= F_X X_{\psi_j P_i} + \sum_{L=1}^N \left(\frac{\partial F_X}{\partial X_L} \frac{\partial X_L}{\partial \psi_j} \right) X_{P_i} \\ &+ \sum_{L=1}^N \left(\frac{\partial F_{P_i}}{\partial X_L} \frac{\partial X_L}{\partial \psi_j} \right) \end{aligned} \quad (D-14)$$

$$\frac{\partial X_{\psi_j \psi_i}}{\partial t} = F_X X_{\psi_j \psi_i} + \sum_{L=1}^N \left(\frac{\partial F_X}{\partial X_L} \frac{\partial X_L}{\partial \psi_j} \right) X_{\psi_i} \quad (D-15)$$

The additional notation used in Equations (D-12) through (D-15) is

$$\begin{aligned} X_{P_j P_i} &= \frac{\partial X_{P_i}}{\partial P_j} & X_{P_j \psi_i} &= \frac{\partial X_{\psi_i}}{\partial P_j} \\ X_{\psi_j P_i} &= \frac{\partial X_{P_i}}{\partial \psi_j} & X_{\psi_j \psi_i} &= \frac{\partial X_{\psi_i}}{\partial \psi_j} \\ F_{P_j P_i} &= \frac{\partial F_{P_i}}{\partial P_j} \quad \text{etc.} \end{aligned}$$

The initial condition for Equations (D-12) through (D-15) is the zero vector since $X_{\psi_i}(t_0)$ and $X_{P_i}(t_0)$ remain constant regardless of how much the initial condition

vector and parameter vector change.

Equations (D-4), (D-8), and (D-12) through (D-15) provide the equations which can be integrated from time t_0 to t_f to provide values for the sensitivities of the state vector with respect to the free parameters.

APPENDIX E

COMPUTATIONAL ALGORITHM FOR SOLUTION OF TWO-POINT BOUNDARY VALUE PROBLEMS

In this appendix, a brief discussion of an algorithm for solving two-point boundary value problems by the method of seeking principal planes (TPSEEK) is presented. A listing of the algorithm is presented at the end of this appendix.

The TPSEEK algorithm is based upon the theoretical results which were presented in Chapters II and III.

The main program and subroutines TPSEEK, INPUT, SCAFACT, FCT, OUTF, and DRKF are listed at the end of this appendix. The subroutines FORTIN, PARDIF, DVAL, and ISTORE are also needed; and a description and listing of these subroutines has already been provided in Appendix A. The subroutine EIGEN is also needed, and it has been described and listed in Appendix B.

A brief description of each of the subroutines which are listed at the end of this appendix will now be provided.

Subroutine TPSEEK calculates the distance to each of the principal planes. It is basically the equivalent of the SEEK subprogram given in Appendix B for solving algebraic

minimization problems.

Subroutine INPUT is used for reading the input data from the data cards.

Subroutine SCAFCT evaluates the scalar function and the partial derivatives of the scalar function.

Subroutine DRKF is a fixed step size Runge Kutta numerical integration program.

Subroutine FCT provides the equations for the derivatives of the dynamical equations.

Subroutine OUTP prints the response of the dynamical equations.

Users Guide for the TPSEEK Algorithm

The user need only supply the appropriate data cards in order to use the TPSEEK algorithm.

The first data card has FORMAT (5I5) and contains the order of the dynamical system in columns 1 to 5, the number of free initial conditions in columns 6 to 10, the number of time steps between the print out of the dynamical response in columns 11 to 15, the number of steps to be used in the numerical integration in columns 16 to 20, and a one in column 25.

The second data card has FORMAT (3D15.7) and contains the initial time in columns 1 to 15, the final time in columns 16 to 30, and a zero in columns 31 to 45.

The state model must be set up so that the initial conditions of the first $N - N_{\text{FREE}}$ (N is the order of the

system, and N_{FREE} is the number of unknown initial conditions) state variables are known.

The third data card has FORMAT (5D15.7) and contains the initial conditions for the state vector. A guess is used for the unknown initial conditions.

The next N data cards contain the equations for the right-hand of the state model. The state variables must be denoted by $X(1)$ through $X(N)$. If the equations involve the independent variable, time; it must be denoted by $X(N+1)$. The equations must be written in columns 7 through 72. If it is necessary to continue an equation on more than one data card, a C should be placed in column 6 of every data card except the last data card associated with that equation. Column 6 of the last data card associated with a continued equation must be left blank.

The last data card contains the equation for the performance index, and the notation for writing this equation is presented in the previous paragraph.

The dynamical equations for a two-point boundary value problem presented by Birta and Trushel in IEEE Transactions on Automatic Control, Vol. AC-12, are presented in Figure 39. The convergence characteristics of the method of seeking principal planes are also presented in this figure.

The data cards which are necessary for this example are presented in Figure 40.

 Dynamical Equations

$$\dot{x}_1 = (1.0 - x_2^2) x_1 - x_2 - x_3/2.0$$

$$\dot{x}_2 = x_1$$

$$\dot{x}_3 = -2.0 x_1 - x_3 + x_3 x_2^2 - x_4$$

$$\dot{x}_4 = -2.0 x_2 + 2.0 x_1 x_2 x_3 + x_3$$

Scalar Performance Index

$$Y = x_3^2 + x_4^2$$

Initial Condition Guess

$$x_1 = 0.0 \quad x_2 = .10 \quad x_3 = 0.0 \quad x_4 = 0.0$$

Converged Initial Condition

$$x_1 = 0.0 \quad x_2 = .10 \quad x_3 = .081176 \quad x_4 = .66941$$

Initial Time = 0.0
 Final Time = 4.0
 Number of Steps = 40

Converged After:

10 Evaluations of the performance index
 2 Evaluations of the gradient vector
 7 Evaluations of the matrix of second
 partial derivatives

Figure 39. Results for the Birta and Trushel Example

COLUMN\	0	1	1	2	2	3	4	6
NUMBER	5	0	5	0	5	0	5	0
1st. Data Card	4	2	2	4	0	1		
2nd. Data Card		0.0D00		4.0D00		0.0D00		
3rd. Data Card		0.0D00		1.0D00		0.0D00		0.0D00
4th. Data Card	(1.0-X(2) **2)*X(1)-X(2)-X(3)/2.0							
5th. Data Card	X(1)							
6th. Data Card	-2.0*X(1)-X(3)+X(3)*X(2)**2-X(4)							
7th. Data Card	-2.0*X(2)+2.0*X(1)*X(2)*X(3)+X(3)							
8th Data Card	X(3)**2+X(4)**2							

Figure 40. Data Cards Required for the Birta and Trushel
Example in Chapter III

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CALL TPSEEK	001
CALL EXIT	002
END	003
SUBROUTINE TPSEEK	004
C PURPOSE	005
C DETERMINE THE BEST VALUES FOR THE PARAMETERS AND THE FREE	006
C INITIAL CONDITIONS BY THE METHOD OF SEEKING AXIS PLANES.	007
C	008
C THIS PROGRAM WAS WRITTEN AND PROGRAMED BY DENNIS UNRUH AT THE	009
C DEPARTMENT OF MECHANICAL AND AEROSPACE ENGINEERING, OKLAHOMA STATE	010
C UNIVERSITY, STILLWATER, OKLAHOMA. JULY 1969	011
C	012
C DELFPR - THE PREDICTED DIFFERENCE BETWEEN THE VALUE OF F AT	013 0023
C THE AXIS PLANE AND F AT THE BASE POINT.	014 0024
C DEN - SEE NUM/DEN.	015 0043
C DIRECT - IF THIS NUMBER IS POSITIVE, THAN THE PREDICTED	016 0038
C GRADIENT DIRECTION AND ACTUAL GRADIENT DIRECTION ARE WITHIN	017 0039
C 90 DEGREES OF EACH OTHER.	018 0040
C EIGVAL - EIGENVALUE VECTOR OF GX.	019 0037
C F - FUNCTION BEING MINIMIZED. F=F(X)	020 0015
C FBASE - VALUE OF F AT BASE POINT	021 0027
C FBEST - VALUE OF F AT BEST POINT.	022 0028
C FESMIN - ESTIMATED MINIMUM FOR THE SCALAR FUNCTION.	023
C G - GRADIENT VECTOR OF FUNCTION F. FOR EXAMPLE G(2)=PARTIAL F	024 0016
C PARTIAL X(2).	025 0017
C GMAG - MAGNITUDE OF GRADIENT AFTER NPOS STEPS TO AXES PLANES.	026
C GPRED - PREDICTED VALUE OF GRADIENT AT AXIS PLAIN.	027 0022
C GX - MATRIX OF SECOND PARTIALS OF F. I.E. GX(2,3)=PARTIAL G(2)	028 0018
C 7PARTIAL X(3).	029 0019
C GXS - VECTOR WHICH CONTAINS GX IN SCIENTIFIC SUBROUTINE PACKAGE	030 0035
C SYMMETRIC STORAGE MODE.	031 0036
C N - THE NUMBER OF INDEPENDENT VARIABLES.	032
C NF - NUMBER OF TIMES F HAS BEEN CALCULATED.	033
C NG - NUMBER OF TIMES THE GRADIENT VECTOR HAS BEEN CALCULATED.	034
C NGX - NUMBER OF TIMES MATRIX GX HAS BEEN CALCULATED.	035
C NPOS - NUMBER OF POSITIVE EIGENVALUES.	036 0029
C NUM/DEN - THIS IS THE MAGNITUDE USED ON STEP NPOS+1 PROVIDED	037 0032
C NPOS SUCCESSFUL STEPS TO THE AXIS PLAINS HAVE BEEN MADE. THIS	038 0033
C IS USED ONLY IF NNEG IS NOT ZERO.	039 0034
C NXMAX - MAXIMUM NUMBER OF INDEPENDENT VARIABLES.	040 0044
C PERRAT - RATIO BETWEEN THE PREDICTED FUNCTION CHANGE AND THE	041 0025
C ACTUAL FUNCTION CHANGE.	042 0026
C R - DUMMY VARIABLE NEEDED FOR CALL STATEMENT OF EIGEN.	043 0045
C WJRK - WORKING VARIABLE.	044 0046
C X - INDEPENDENT VARIABLE VECTOR.	045 0012
C XBAMIN - BASE POINT FROM WHICH A MINIMUM IS BEING SOUGHT BY A	046
C LINEAR SEARCH IN THE PREDICTED NEGATIVE GRADIENT DIRECTION.	047
C XBASE - THE VALUE OF THE INDEPENDENT VARIABLE VECTOR AT THE	048 0013
C BASE POINT.	049 0014
C XBEST - THE VALUE OF THE INDEPENDENT VARIABLE AT THE POINT	050 0020
C WHERE THE CALCULATED VALUE OF F WAS SMALLEST.	051 0021
C XNPOS - THE VALUE OF THE INDEPENDENT VARIABLE AFTER NPOS	052 0041
C SUCCESSFUL STEPS TO THE AXIS PLAINS.	053 0042
IMPLICIT INTEGER*2 (I-N),REAL*8 (A-H,O-Z)	054
INTEGER*4 MMM	055

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C		111	0095
	DO 7 I=1,IJMAX	112	
	7 GXSS(I)=GXS(I)	113	
	MMM=N	114	
	CALL EIGENT(GXSS,R,MMM,I)	115	
	DO 6 I=1,N	116	0101
	II=(I*(I+1))/2	117	0102
	6 EIGVAL(I)=GXSS(II)	118	
	NPOS=N	119	0105
	DO 8 I=1,N	120	0106
	IF (1.0005*EIGVAL(I).GT.EIGVAL(I)) GO TO 8	121	
	NPOS=NPOS-1	122	0108
	8 CONTINUE	123	0115
	IF (EIGVAL(I).LE.0.000) NPOS=0	124	
	WRITE (6,101)	125	0117
	WRITE (6,100) (EIGVAL(I),I=1,N)	126	0118
	WRITE (6,102) NPOS	127	
C		128	
C	IF NPOS IS EQUAL TO ZERO , A LINEAR SEARCH IS PERFORMED FOR A	129	
C	MINIMUM IN THE NEGATIVE GRADIENT DIRECTION.	130	
C		131	
	IF (NPOS.NE.0) GO TO 52	132	
	DO 53 I=1,N	133	
	53 XBAMIN(I)=X(I)	134	
	NUM=FBEST-FESMIN	135	
	IF (NUM.LT.0.000) GO TO 30	136	
	DEN=0.000	137	
	DO 50 I=1,N	138	
	50 DEN=DEN+G(I)*G(I)	139	
	DO 51 I=1,N	140	
	51 X(I)=X(I)-(NUM/DEN)*G(I)	141	
	GO TO 23	142	
C		143	0120
C	DETERMINE VALUES FOR X TO THE SUCCESSIVE AXIS PLANES.	144	0121
C		145	0122
	52 DO 14 K=1,NPOS	146	
	DO 9 I=1,N	147	0125
	GPRED(I)=G(I)	148	0126
	DO 9 J=1,N	149	0127
	IJ=((J-1)*J)/2+1	150	
	IF (J.LT.1) IJ=((I-1)*I)/2+J	151	
	9 GPRED(I)=GPRED(I)+GXS(IJ)*(X(IJ)-XBASE(IJ))	152	
	DO 10 I=1,N	153	0129
	10 X(I)=X(I)-GPRED(I)/EIGVAL(K)	154	0130
	I=1	155	
	CALL SCAFACT(X,F,G,GXS,I)	156	
	NF=NF+1	157	
	WRITE (6,103) NF,NG,NGX	158	0132
	WRITE (6,112) K	159	0133
	WRITE (6,100) (X(I),I=1,N)	160	0134
	WRITE (6,105) F	161	0135
	IF (F.GT.FBEST.AND.K.EQ.1) GO TO 41	162	
	IF (F.GT.FBEST) GO TO 60	163	
C		164	0140
C	CALCULATE PERRAT	165	0141

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C		166	0142
	DELFPF=0.0	167	0143
	DO 13 I=1,N	168	0144
	WORK=0.0	169	0145
	DO 12 J=1,N	170	0146
	IJ=((J-1)*J)/2+1	171	
	IF (J.LT.I) IJ=((I-1)*I)/2+J	172	
12	WORK=WORK+GXS(IJ)*(X(J)-XBASE(J))	173	
13	DELFPF=DELFPF+(G(I)+.50*WORK)*(X(I)-XBASE(I))	174	0148
	PERRAT=(F-FBASE)/DELFPF	175	0149
	WRITE (6,108) PERRAT	176	0150
	IF (DABS(PERRAT-1.000).GT..100) GO TO 3	177	
	DO 11 I=1,N	178	0137
11	XBEST(I)=X(I)	179	0138
	FBEST=F	180	0139
14	CONTINUE	181	0152
	DO 15 I=1,N	182	0154
	GPRED(I)=G(I)	183	
	DO 15 J=1,N	184	0156
	IJ=((J-1)*J)/2+1	185	
	IF (J.LT.I) IJ=((I-1)*I)/2+J	186	
15	GPRED(I)=GPRED(I)+GXS(IJ)*(X(J)-XBASE(J))	187	
	I=2	188	
	CALL SCAFACT(X,F,G,GXS,I)	189	
	NG=NG+1	190	
	WRITE (6,103) NF,NG,NGX	191	0159
	WRITE (6,106)	192	0162
	WRITE (6,100) (G(I),I=1,N)	193	0163
C		194	
C	CHECK FOR CONVERGENCE.	195	
C		196	
	DO 45 I=1,N	197	
	IF (DABS(G(I)).GT.1.0D-8) GO TO 46	198	
45	CONTINUE	199	
	GO TO 33	200	
46	IF (NPOS.EQ.N) GO TO 3	201	
	DIRECT=0.0	202	0164
	DO 16 I=1,N	203	0165
16	DIRECT=DIRECT+G(I)*GPRED(I)	204	0166
	WRITE (6,110) DIRECT	205	0167
	IF (DIRECT.LE.0.0) GO TO 3	206	0168
	NUM=0.0	207	0169
	DEN=0.0	208	0170
	DO 17 I=1,N	209	0171
	NUM=NUM+(X(I)-XBASE(I))**2	210	0172
17	DEN=DEN+(GPRED(I))**2	211	0173
	MAG=DSQRT(NUM/DEN)	212	
	DO 18 I=1,N	213	0174
18	X(I)=X(I)-MAG*GPRED(I)	214	
		215	
C		216	
C	PERFORM A LINEAR SEARCH FOR A MINIMUM IN THE PREDICTED NEGATIVE	217	
C	GRADIENT DIRECTION.	218	
C		219	
	I=1	219	
	CALL SCAFACT(X,F,G,GXS,I)	220	

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NF=NF+1	221
WRITE (6,103) NF,NG,NGX	222 0178
WRITE (6,104)	223 0179
WRITE (6,100) (X(I),I=1,N)	224 0180
WRITE (6,105) F	225 0181
41 DO 42 I=1,N	226
42 XBAMIN(I)=XBEST(I)	227
IF (F.GT.FBEST) GO TO 23	228 0182
C	229
C CONTINUE DOUBLING THE DISTANCE UNTIL F CEASES TO BECOME BETTER.	230
C	231
19 DO 20 I=1,N	232 0183
20 XBEST(I)=X(I)	233 0184
FBEST=F	234 0185
DO 21 I=1,N	235 0186
21 X(I)=XBAMIN(I)+2.0*(X(I)-XBAMIN(I))	236
I=1	237
CALL SCAFCT(X,F,G,GXS,I)	238
NF=NF+1	239
WRITE (6,103) NF,NG,NGX	240 0189
WRITE (6,114)	241 0190
WRITE (6,100) (X(I),I=1,N)	242 0191
WRITE (6,105) F	243 0192
IF (F.LT.FBEST) GO TO 19	244 0193
DO 22 I=1,N	245 0194
22 X(I)=XBEST(I)	246 0195
F=FBEST	247 0196
GO TO 3	248
C	249
C CONTINUE HALVING THE DISTANCE UNTIL F BECOMES BETTER.	250
C	251
23 DO 24 I=1,N	252 0198
24 X(I)=XBAMIN(I)+.50*(X(I)-XBAMIN(I))	253
I=1	254
CALL SCAFCT(X,F,G,GXS,I)	255
NF=NF+1	256
WRITE (6,103) NF,NG,NGX	257 0201
WRITE (6,113)	258 0202
WRITE (6,100) (X(I),I=1,N)	259 0203
WRITE (6,105) F	260 0204
IF (F.GT.FBEST) GO TO 23	261 0205
DO 25 I=1,N	262 0206
25 XBEST(I)=X(I)	263 0207
FBEST=F	264 0208
GO TO 3	265
60 DO 61 I=1,N	266
61 XBAMIN(I)=XBEST(I)	267
I=2	268
CALL SCAFCT(XBAMIN,F,G,GXS,I)	269
NG=NG+1	270
WRITE (6,103) NF,NG,NGX	271
WRITE (6,118)	272
WRITE (6,100) (G(I),I=1,N)	273
DIRECT=0.0	274
DO 62 I=1,N	275

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62	DIRECT=DIRECT+G(I)*GPRED(I)	276
	WRITE (6,110) DIRECT	277
	IF (DIRECT.GT.0.000) GO TO 23	278
	DO 63 I=1,N	279
63	X(I)=XBAMIN(I)	280
	GO TO 3	281
30	WRITE (6,116)	282
	CALL EXIT	283
33	WRITE (6,109)	284
	CALL EXIT	285 0241
	RETURN	286 0242
	END	287 0243
	SUBROUTINE INPUT(X,FESMIN)	288
	IMPLICIT INTEGER*2(I-N),REAL*8(A-H,O-Z)	289
C	PURPOSE	290
C	READ DATA CARDS.	291
C	DATA CARD ONE CONTAINS NSYS,NFREE,NPAR,NWRITE,NSTEP,NOPT	292
C	DATA CARD TWO CONTAINS PRMT(1),PRMT(2),FESMIN	293
C	DATA CARD THREE CONTAINS THE INITIAL CONDITION GUESS FOR	294
C	COMPONENTS 1 THROUGH NSYS OF Y.	295
C	DATA CARD FOUR CONTAINS THE INITIAL GUESS FOR THE PARAMETERS.	296
C	IF NPAR=0 LEAVE THIS DATA CARD OUT.	297
C	THE SYSTEM EQUATIONS ARE ENTERED ON CARDS 5 THROUGH NSYS+4.	298
C	THE EQUATION FOR THE INTEGRAL OF THE SCALAR PERFORMANCE INDEX	299
C	IS ENTERED ON THE LAST DATA CARD.	300
C	IF NOPT=1 EQUATIONS ARE ENTERED ON DATA CARDS. IF NOPT=2 EQUATION	301
C	ARE ENTERED ON DATA CARDS AND THEIR SYMBOLIC FORM IS PUNCHED.	302
C	IF NOPT=3 EQUATIONS ARE ENTERED IN SYMBOLIC FORM.	303
	DIMENSION X(10)	304
	COMMON /GENER/ NSYS,NFREE,NFIXED,NSYSP1	305
	COMMON /INFC/ IF(10),IFX(10,10),IFXXS(10,55)	306
	COMMON /INOU/ NWRITE	307
	COMMON /SCIN/ YI(10),PRMT(5),IG,IGX(10),IGXXS(55)	308
100	FORMAT (3D15.7)	309
101	FORMAT (5D15.7)	310
102	FORMAT (10I5)	311
103	FORMAT (' NSYS,NFREE,NWRITE,NSTEP,NOPT')	312
104	FORMAT (' PRMT(1) PRMT(2) FESMIN')	313
106	FORMAT (5(15,F10.5))	314
108	FORMAT (' INITIAL CONDITION USED')	315
110	FORMAT (' IF(' ,14,')=')	316
111	FORMAT (' IFX(' ,214,')=')	317
112	FORMAT (' IFXXS(' ,214,')=')	318
113	FORMAT (' IG=')	319
114	FORMAT (' IGX(' ,14,')=')	320
115	FORMAT (' IGXXS(' ,14,')=')	321
	READ (5,102) NSYS,NFREE,NWRITE,NSTEP,NOPT	322
	WRITE (6,103)	323
	WRITE (6,102) NSYS,NFREE,NWRITE,NSTEP,NOPT	324
	READ(5,101) PRMT(1),PRMT(2),FESMIN	325
	WRITE (6,104)	326
	WRITE (6,100) PRMT(1),PRMT(2),FESMIN	327
	READ(5,101) (YI(I),I=1,NSYS)	328
	WRITE (6,108)	329
	WRITE (6,100) (YI(I),I=1,NSYS)	330

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NFIXED=NSYS-NFREE	331
NSYSP1=NSYS+1	332
RNSTEP=NSTEP	333
PRMT(3)=(PRMT(2)-PRMT(1))/RNSTEP	334
DO 3 I=1,NFREE	335
II=NFIXED+I	336
3 X(I)=YI(II)	337
IF (NDPT.EQ.3) GO TO 20	338
DO 7 L=1,NSYS	339
WRITE (6,110) I	340
CALL FORTIN(IF(I))	341
DO 7 K=1,NSYS	342
WRITE (6,111) I,K	343
CALL PARDIF(IF(I),IFX(I,K),K)	344
DO 7 J=1,K	345
JK=((K-1)*K)/2+J	346
WRITE (6,112) I,JK	347
7 CALL PARDIF(IFX(I,K),IFXXS(I,JK),J)	348
WRITE (6,113)	349
CALL FORTIN (IG)	350
DO 8 J=1,NSYS	351
WRITE (6,114) J	352
CALL PARDIF(IG,IGX(J),J)	353
DO 8 I=1,J	354
IJ=((J-1)*J)/2+I	355
WRITE (6,115) IJ	356
8 CALL PARDIF(IGX(J),IGXXS(IJ),I)	357
IF (NDPT.EQ.1) RETURN	358
I=3	359
CALL ISTORE (NAME,I)	360
RETURN	361
20 I=4	362
CALL ISTORE (NAME,I)	363
RETURN	364
END	365
SUBROUTINE SCAFCT (X,F,G,GXS,ILOG)	366
PURPOSE	367
C SETS UP THE INITIAL CONDITIONS FOR THE DYNAMICAL EQUATIONS.	368
C EVALUATES THE SCALAR PERFORMANCE FUNCTION,ITS GRADIENT, AND	369
C ITS MATRIX OF SECOND PARTIAL DERIVATIVES.	370
IMPLICIT INTEGER*2 (I-N),REAL*8 (A-H,O-Z)	371
INTEGER*4 NTOTAL,IHLF	372
DIMENSION X(10),G(10),GXS(55),Y(210),DERV(210),AUX(210)	373
1,GX(10),GXXS(55),B(10),Z(50)	374
COMMON /GENER/ NSYS,NFREE,NFIXED,NSYSP1	375
COMMON /SCIN/ YI(10),PRMT(5),IG,IGX(10),IGXXS(55)	376
COMMON /SCFCOU/ ILOGIC	377
EXTERNAL FCT,OUTP	378
DATA NDIFTO /0/	379
100 FORMAT (' NDIFTO=',I5)	380
ILOGIC=ILOG	381
IF (NFIXED.EQ.0) GO TO 4	382
DO 1 I=1,NFIXED	383
1 Y(I)=YI(I)	384
4 DO 2 I=1,NFREE	385

80/80 LIST

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	II=I+NFIXED	386
2	Y(II)=X(I)	387
	GO TO (10,20,30), ILOGIC	388
C		389
C	DETERMINE THE VALUE FOR THE SCALAR PERFORMANCE FUNCTION, F.	390
C		391
10	NTOTAL=NSYS	392
	NDIFTO=NDIFTO+NTOTAL	393
	WRITE (6,100) NDIFTO	394
	CALL DRKF(PRMT,Y,DERY,NTOTAL,IHLF,FCT,OUTP,AUX)	395
	GO TO 40	396
C		397
C	DETERMINE THE VALUE FOR THE GRADIENT OF THE SCALAR PERFORMANCE	398
C	FUNCTION, G.	399
C		400
20	NTOTAL=(NFREE+1)*NSYS	401
	DO 21 I=NSYSPI,NTOTAL	402
21	Y(I)=0.0	403
	DO 22 I=1,NFREE	404
	II=NSYS*I+NFIXED+I	405
22	Y(II)=1.0	406
	NDIFTO=NDIFTO+NTOTAL	407
	WRITE (6,100) NDIFTO	408
23	CALL DRKF(PRMT,Y,DERY,NTOTAL,IHLF,FCT,OUTP,AUX)	409
	GO TO 40	410
C		411
C	DETERMINE THE VALUES FOR THE ELEMENTS OF THE MATRIX OF SECOND	412
C	PARTIAL DERIVATIVES OF THE SCALAR PERFORMANCE FUNCTION.	413
C		414
30	NTOTAL=(1+NFREE+((NFREE+1)*NFREE)/2)*NSYS	415
	DO 31 I=NSYSPI,NTOTAL	416
31	Y(I)=0.0	417
	DO 32 I=1,NFREE	418
	II=NSYS*I+NFIXED+I	419
32	Y(II)=1.0	420
	NDIFTO=NDIFTO+NTOTAL	421
	WRITE (6,100) NDIFTO	422
33	CALL DRKF(PRMT,Y,DERY,NTOTAL,IHLF,FCT,OUTP,AUX)	423
40	DO 41 I=1,NSYS	424
41	Z(I)=Y(I)	425
	IF (ILOGIC.EQ.2) GO TO 42	426
	F=DVAL(IG,Z)	427
	IF (ILOGIC.EQ.1) RETURN	428
42	DO 43 I=1,NSYS	429
43	GX(I)=DVAL(IGX(I),Z)	430
	DO 44 I=1,NFREE	431
	G(I)=0.0	432
	DO 44 J=1,NSYS	433
	JJ=I*NSYS+J	434
44	G(I)=G(I)+GX(J)*Y(JJ)	435
	IF (ILOGIC.EQ.2) RETURN	436
	DO 50 J=1,NSYS	437
	DU 50 I=1,J	438
	IJ=((I-1)*J)/2+I	439
50	GXXS(IJ)=DVAL(IGXXS(IJ),Z)	440

80/80 LIST

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DO 52 J=1,NFREE ..... 441
DO 51 LI=1,NSYS ..... 442
B(LI)=0.0 ..... 443
DO 51 LJ=1,NSYS ..... 444
LIJ=((LJ-1)*LJ)/2+LI ..... 445
IF (LJ.LT.LI) LIJ=((LI-1)*LI)/2+LJ ..... 446
LJJ=J*NSYS+LJ ..... 447
51 B(LI)=B(LI)+GXXS(LIJ)*Y(LJJ) ..... 448
DO 52 I=1,J ..... 449
IJ=((J-1)*J)/2+I ..... 450
GXS(IJ)=0.0 ..... 451
DO 52 K=1,NSYS ..... 452
KK=I*NSYS+K ..... 453
KKK=(NFREE+IJ)*NSYS+K ..... 454
52 GXS(IJ)=GXS(IJ)+Y(KK)*B(K)+GX(K)*Y(KKK) ..... 455
RETURN ..... 456
END ..... 457
SUBROUTINE FCT(T,Y,DERY) ..... 458
C PURPOSE ..... 459
C SUPPLYS THE EQUATIONS FOR THE DYNAMICAL SYSTEM. ..... 460
IMPLICIT INTEGER*2(I-N),REAL*8 (A-H,O-Z) ..... 461
DIMENSION Y(210),DERY(210),Z(50),FX(10,10),FXXS(10,55), ..... 462
IB(10,10) ..... 463
COMMON /GENER/ NSYS,NFREE,NFIXED,NSYSP1 ..... 464
COMMON /INFC/ IF(10),IFX(10,10),IFXXS(10,55) ..... 465
COMMON /SCFCOU/ ILOGIC ..... 466
DO 1 I=1,NSYS ..... 467
1 Z(I)=Y(I) ..... 468
Z(NSYSP1)=T ..... 469
C ..... 470
C DETERMINE THE VALUES FOR THE DERIVATIVE OF THE BASIC SYSTEM. ..... 471
C ..... 472
10 DO 11 I=1,NSYS ..... 473
11 DERY(I)=DVAL(IF(I),Z) ..... 474
IF (ILOGIC.EQ.1) RETURN ..... 475
C ..... 476
C DETERMINE THE VALUES FOR THE DERIVATIVES OF THE FIRST ORDER ..... 477
C INFLUENCE COEFFICIENTS. ..... 478
20 DO 21 I=1,NSYS ..... 479
DO 21 J=1,NSYS ..... 480
21 FX(I,J)=DVAL(IFX(I,J),Z) ..... 481
DO 22 I=1,NSYS ..... 482
DO 22 J=1,NFREE ..... 483
IJ=J*NSYS+I ..... 484
DERY(IJ)=0.0 ..... 485
DO 22 K=1,NSYS ..... 486
JK=J*NSYS+K ..... 487
22 DERY(IJ)=DERY(IJ)+FX(I,K)*Y(JK) ..... 488
IF (ILOGIC.EQ.2) RETURN ..... 489
C ..... 490
C DETERMINE THE DERIVATIVES FOR THE SECOND ORDER INFLUENCE ..... 491
C COEFFICIENTS. ..... 492
C ..... 493
DO 25 I=1,NSYS ..... 494
DO 25 K=1,NSYS ..... 495

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80/80 LIST

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	DD 25 J=1,K	496
	JK=((K-1)*K)/2+J	497
25	FXXS(I,JK)=DVAL(IFXXS(I,JK),Z)	498
	DD 32 J=1,NFREE	499
	DD 30 LI=1,NSYS	500
	DD 30 LJ=1,NSYS	501
	B(LI,LJ)=0.0	502
	DD 30 LK=1,NSYS	503
	JJ=J*NSYS+LK	504
	LJLK=((LK-1)*LK)/2+LJ	505
	IF (LK.LT.LJ) LJLK=((LJ-1)*LJ)/2+LK	506
30	B(LI,LJ)=B(LI,LJ)+Y(JJ)*FXXS(LI,LJLK)	507
	DD 32 I=1,J	508
	DD 32 K=1,NSYS	509
	IJ=((J-1)*J)/2+1	510
	KK=(NFREE+IJ)*NSYS+K	511
	DERY(KK)=0.0	512
	DD 32 L=1,NSYS	513
	LL=(NFREE+((J-1)*J)/2+1)*NSYS+L	514
	LLL=I*NSYS+L	515
32	DERY(KK)=DERY(KK)+FX(K,L)*Y(ILL)+B(K,L)*Y(LLL)	516
	RETURN	517
	END	518
	SUBROUTINE OUTP(T,Y,DERY,IHLF,NTOTAL,PRMT)	519
C	PURPOSE	520
C	WRITE THE SYSTEM RESPONSE AFTER EVERY NWRITE STEPS OF NUMERICAL	521
C	INTEGRATION. NUMERICALLY INTEGRATE THE INTEGRAL EQUATIONS BY	522
C	USING THE TRAPAZOID RULE.	523
	IMPLICIT INTEGER*2(I-N),REAL*8 (A-H,O-Z)	524
	INTEGER*4 IHLF,NTOTAL	525
	DIMENSION Y(210),DERY(210),PRMT(5)	526
	COMMON /GENER/ NSYS,NFREE,NFIXED,NSYSPI	527
	COMMON /INOU/ NWRITE	528
	COMMON /SCFCOU/ ILOGIC	529
100	FORMAT (1H0,D15.7)	530
101	FORMAT (8D15.7)	531
	GO TO (10,20,30),ILOGIC	532
10	NINT=1	533
	GO TO 35	534
20	NINT=1+NFREE	535
	GO TO 35	536
30	NINT=1+NFREE+((NFREE+1)*NFREE)/2	537
35	IF (I.EQ.PRMT(1)) GO TO 41	538
	IF (I.GT.PRMT(2)-PRMT(3)/2.0) GO TO 41	539
	IF (ILOGIC.GT.1) RETURN	540
	IF (NCOUNT.EQ.NWRITE) GO TO 41	541
	NCOUNT=NCOUNT+1	542
	RETURN	543
C		544
C	RESET NCOUNT AND WRITE OUT THE VALUES AT THIS TIME.	545
C		546
41	NCOUNT=1	547
	WRITE (6,100) T	548
	DD 42 I=1,NINT	549
	JJ=(I-1)*NSYS+1	550

80/80 LIST

E-15

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II=1*NSYS	551
42 WRITE (6,101) (Y(J),J=JJ,II)	552
RETURN	553
END	554

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```

SUBROUTINE DRKF (PRMT,Y,DERY,NDIM,IHLF,FCT,OUTP,AUX)
C
C ..... DRKGS001
C DRKGS002
C DRKGS003
SUBROUTINE DRKF
C
C PURPOSE DRKGS005
C TO SOLVE A SYSTEM OF FIRST ORDER ORDINARY DIFFERENTIAL DRKGS006
C EQUATIONS WITH GIVEN INITIAL VALUES. DRKGS007
C DRKGS008
C DRKGS009
C USAGE DRKGS010
C CALL DRKF (PRMT,T,DERY,NDIM,IHLF,FCT,OUTP,AUX)
C PARAMETERS FCT AND OUTP REQUIRE AN EXTERNAL STATEMENT. DRKGS012
C DRKGS013
C DESCRIPTION OF PARAMETERS DRKGS014
C PRMT - DOUBLE PRECISION INPUT AND OUTPUT VECTOR WITH DRKGS015
C DIMENSION GREATER THAN OR EQUAL TO 5, WHICH DRKGS016
C SPECIFIES THE PARAMETERS OF THE INTERVAL AND OF DRKGS017
C ACCURACY AND WHICH SERVES FOR COMMUNICATION BETWEEN DRKGS018
C OUTPUT SUBROUTINE (FURNISHED BY THE USER) AND DRKGS019
C SUBROUTINE DRKGS. EXCEPT PRMT(5) THE COMPONENTS DRKGS020
C ARE NOT DESTROYED BY SUBROUTINE DRKGS AND THEY ARE DRKGS021
C PRMT(1)- LOWER BOUND OF THE INTERVAL (INPUT), DRKGS022
C PRMT(2)- UPPER BOUND OF THE INTERVAL (INPUT), DRKGS023
C PRMT(3)- INITIAL INCREMENT OF THE INDEPENDENT VARIABLE DRKGS024
C (INPUT), DRKGS025
C PRMT(4)- DUMMY PARAMETER WHICH NEED NOT BE SPECIFIED SINCE
C IT IS NOT USED IN THIS SUBROUTINE. IT IS LEFT
C OVER FROM DRKGS. SEE REMARKS GIVEN BELOW
C PRMT(5)- NO INPUT PARAMETER. SUBROUTINE DRKGS INITIALIZES DRKGS032
C PRMT(5)=0. IF THE USER WANTS TO TERMINATE DRKGS033
C SUBROUTINE DRKGS AT ANY OUTPUT POINT, HE HAS TO DRKGS034
C CHANGE PRMT(5) TO NON-ZERO BY MEANS OF SUBROUTINE DRKGS035
C OUTP. FURTHER COMPONENTS OF VECTOR PRMT ARE DRKGS036
C FEASIBLE IF ITS DIMENSION IS DEFINED GREATER DRKGS037
C THAN 5. HOWEVER SUBROUTINE DRKGS DOES NOT REQUIRE DRKGS038
C AND CHANGE THEM. NEVERTHELESS THEY MAY BE USEFUL DRKGS039
C FOR HANDING RESULT VALUES TO THE MAIN PROGRAM DRKGS040
C (CALLING DRKF ) WHICH ARE OBTAINED BY SPECIAL
C MANIPULATIONS WITH OUTPUT DATA IN SUBROUTINE OUTP. DRKGS042
C Y - DOUBLE PRECISION INPUT VECTOR OF INITIAL VALUES DRKGS043
C (DESTROYED). LATERON Y IS THE RESULTING VECTOR OF DRKGS044
C DEPENDENT VARIABLES COMPUTED AT INTERMEDIATE DRKGS045
C POINTS X. DRKGS046
C DERY - DERY IS THE VECTOR OF
C DERIVATIVES, WHICH BELONG TO FUNCTION VALUES Y AT DRKGS050
C INTERMEDIATE POINTS X. DRKGS051
C NDIM - AN INPUT VALUE, WHICH SPECIFIES THE NUMBER OF DRKGS052
C EQUATIONS IN THE SYSTEM. DRKGS053
C IHLF - DUMMY PARAMETER WHICH NEED NOT BE SPECIFIED SINCE
C IT IS NOT USED IN THIS SUBROUTINE. IT IS LEFT
C OVER FROM DRKGS. SEE REMARKS GIVEN BELOW
C FCT - THE NAME OF AN EXTERNAL SUBROUTINE USED. THIS DRKGS061
C SUBROUTINE COMPUTES THE RIGHT HAND SIDES DERY OF DRKGS062
C THE SYSTEM TO GIVEN VALUES X AND Y. ITS PARAMETER DRKGS063

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80/80 LIST

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C LIST MUST BE X,Y,DERY. SUBROUTINE FCT SHOULD DRKGS064
 C NOT DESTROY X AND Y. DRKGS065
 C OUTP - THE NAME OF AN EXTERNAL OUTPUT SUBROUTINE USED. DRKGS066
 C ITS PARAMETER LIST MUST BE X,Y,DERY,IHLF,NDIM,PRMT. DRKGS067
 C NONE OF THESE PARAMETERS (EXCEPT, IF NECESSARY, DRKGS068
 C PRMT(5),...) SHOULD BE CHANGED BY
 C SUBROUTINE OUTP. IF PRMT(5) IS CHANGED TO NON-ZERO, DRKGS070
 C SUBROUTINE DRKGS IS TERMINATED. DRKGS071
 C AUX - DOUBLE PRECISION AUXILIARY VECTOR STORAGE WITH
 C NDIM ROWS. DRKGS074
 C REMARKS DRKGS075
 C THE PROCEDURE TERMINATES AND RETURNS TO CALLING PROGRAM, IF DRKGS076
 C (1) SUBROUTINE OUTP HAS CHANGED PRMT(5) TO NON-ZERO.
 C (2) INITIAL INCREMENT IS EQUAL TO 0 OR HAS WRONG SIGN DRKGS080
 C (3) THE WHOLE INTEGRATION INTERVAL IS WORKED THROUGH, DRKGS082
 C THIS PROGRAM IS A REVISION OF THE SSP PROGRAM DRKGS. IT
 C USES A FIXED STEP SIZE FOR ALL STEPS EXCEPTING PERHAPS THE
 C LAST STEP WHICH WILL BE ADJUSTED TO HIT THE DESIRED
 C FINAL TIME EXACTLY. THE CALL STATEMENTS HAVE ALL BEEN LEFT
 C WITH THE SAME PARAMETERS AS IN DRKGS.
 C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED DRKGS084
 C THE EXTERNAL SUBROUTINES FCT(X,Y,DERY) AND DRKGS085
 C OUTP(X,Y,DERY,IHLF,NDIM,PRMT) MUST BE FURNISHED BY THE USER. DRKGS086
 C DRKGS087
 C DRKGS088
 C METHOD DRKGS089
 C EVALUATION IS DONE BY MEANS OF FOURTH ORDER RUNGE-KUTTA DRKGS090
 C FORMULAE IN THE MODIFICATION DUE TO GILL.
 C TO GET FULL FLEXIBILITY IN OUTPUT, AN OUTPUT SUBROUTINE DRKGS099
 C MUST BE FURNISHED BY THE USER. DRKGS100
 C FOR REFERENCE, SEE DRKGS101
 C RALSTON/WILF, MATHEMATICAL METHODS FOR DIGITAL COMPUTERS, DRKGS102
 C WILEY, NEW YORK/LONDON, 1960, PP.110-120. DRKGS103
 C DRKGS104
 C DRKGS105
 C DRKGS106
 C DRKGS108
 C DRKGS109
 C DIMENSION Y(1),DERY(1),AUX(1),A(4),B(4),C(4),PRMT(1)
 C DOUBLE PRECISION PRMT,Y,DERY,AUX,A,B,C,X,XEND,H,AJ,BJ,CJ,R1,R2
 C X=PRMT(1) DRKGS115
 C XEND=PRMT(2) DRKGS116
 C H=PRMT(3) DRKGS117
 C PRMT(5)=0.00 DRKGS118
 C CALL FCT(X,Y,DERY) DRKGS119
 C DRKGS120
 C ERROR TEST DRKGS121
 C IF (H*(XEND-X)) 40,40,2
 C DRKGS123
 C PREPARATIONS FOR RUNGE-KUTTA METHOD DRKGS124
 C A(1)=.500 DRKGS125
 C A(2)=.2923932188134524800 DRKGS126
 C A(3)=1.707106781186547500 DRKGS127

80/80 LIST

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A(4)=.15666666666666667D0 DRKGS128
B(1)=2.00 DRKGS129
B(2)=1.00 DRKGS130
B(3)=1.00 DRKGS131
B(4)=2.00 DRKGS132
C(1)=.5D0 DRKGS133
C(2)=.29289321881345248D0 DRKGS134
C(3)=1.7071067811865475D0 DRKGS135
C(4)=.5D0 DRKGS136
C DRKGS137
C PREPARATIONS OF FIRST RUNGE-KUTTA STEP DRKGS138
  DO 3 I=1,NDIM DRKGS139
3 AUX(I)=0.00
  IEND=0 DRKGS148
C DRKGS149
C DRKGS150
C START OF A RUNGE-KUTTA STEP DRKGS151
4 IF((X+H-XEND)*H)7,6,5 DRKGS152
5 H=XEND-X DRKGS153
6 IEND=1 DRKGS154
C DRKGS155
C RECORDING OF INITIAL VALUES OF THIS STEP DRKGS156
7 CALL OUTP(X,Y,DERY,IREF,NDIM,PRMT) DRKGS157
  IF (PRMT(5).NE.0.D0) GO TO 40
C DRKGS161
C DRKGS162
C START OF INNERMOST RUNGE-KUTTA LOOP DRKGS163
  J=1 DRKGS164
10 AJ=A(J) DRKGS165
  BJ=B(J) DRKGS166
  CJ=C(J) DRKGS167
  DO 11 I=1,NDIM DRKGS168
  R1=H*DERY(I) DRKGS169
  R2=AJ*(R1-BJ*AUX(I))
  Y(I)=Y(I)+R2 DRKGS171
  R2=R2+R2+R2 DRKGS172
11 AUX(I)=AUX(I)+R2-CJ*R1
  IF(J-4)12,15,15 DRKGS174
12 J=J+1 DRKGS175
  IF(J-3)13,14,13 DRKGS176
13 X=X+.5D0*H DRKGS177
14 CALL FCT(X,Y,DERY) DRKGS178
  GOTO 10 DRKGS179
C DRKGS180
C END OF INNERMOST RUNGE-KUTTA LOOP DRKGS181
15 CALL FCT(X,Y,DERY)
30 IF (IEND) 4,4,41
41 CALL OUTP(X,Y,DERY,IHLF,NDIM,PRMT)
40 RETURN DRKGS262
  END DRKGS263

```

APPENDIX F

COMPUTATIONAL ALGORITHM FOR PARAMETER IDENTIFICATION OF DYNAMICAL SYSTEMS

In this appendix a brief discussion of an algorithm for identifying the parameters of a dynamical system by the method of seeking principal planes (PRSEEK) is presented. A listing of the algorithm is presented at the end of this appendix.

The PRSEEK algorithm is based upon the theoretical results which were presented in Chapters II and IV.

The Main program and subroutines TPSEEK, INPUT, SCAFACT, FCT, and OUTP are listed at the end of this appendix. The subroutines FORTIN, PARDIF, DVAL, and ISTORE are also needed, and a description and listing of these subroutines has already been provided in Appendix A. The subroutine EIGEN is also needed, and it has been described and listed in Appendix B. The subroutine DRKF is also needed and it has been described and listed in Appendix E.

A brief description of each of the subroutines which are listed at the end of this appendix will now be provided.

Subroutine PRSEEK calculates the distance to each of the principal planes. It is basically the equivalent of the SEEK subprogram given in Appendix B for solving algebraic

minimization problems.

Subroutine INPUT is used for reading the input data from the data cards.

Subroutine SCAFCT evaluates the scalar function and the partial derivatives of the scalar function.

Subroutine FCT provides the equations for the derivatives of the dynamical equations.

Subroutine OUTP prints the response of the dynamical equations.

Users Guide for the PRSEEK Algorithm

The user need only supply the appropriate data cards in order to use the PRSEEK algorithm.

The first data card has FORMAT (5I5) and contains the order of the dynamical system in columns 1 to 5, the number of free initial conditions in columns 6 to 10, the number of free parameters in columns 11 to 15, the number of time steps between the print out of the dynamical response in columns 16 to 20, and the number of steps to be used in the numerical integration in columns 21 to 25.

The second data card has FORMAT (3D15.7) and contains the initial time in columns 1 to 15, the final time in columns 16 to 30, and an estimate for the minimum of the performance index in columns 31 to 45.

The state model must be set up so that the initial conditions of the first $N - N_{\text{FREE}}$ (N is the order of the system, and N_{FREE} is the number of unknown initial conditions)

state variables are known.

The third data card has FORMAT (5D15.7) and contains the initial conditions for the state vector. A guess is used for the unknown initial conditions.

The fourth data card has FORMAT (5D15.7) and contains a guess for the values of the parameters which are to be adjusted.

The next N data cards contain the equations for the right-hand side of the state model. The state variables must be denoted by $X(1)$ through $X(N)$. The parameters are denoted by $X(N+1)$ through $X(N+N_{\text{PAR}})$. (N_{PAR} is the number of parameters free to be adjusted.) The independent variable, time, is denoted by $X(N+N_{\text{PAR}}+1)$. The equations must be written in columns 7 through 72. If it is necessary to continue an equation on more than one data card, a C should be placed in column 6 of every data card except the last data card associated with that equation. Column 6 of the last data card associated with a continued equation must be left blank.

The last data card contains the equation for the integrand of the performance index, and the notation for writing this equation is presented in the previous paragraph.

The dynamical equations and convergence characteristics for the spool valve system identification problem which was presented in Chapter IV are given in Figure 41.

The data cards which are necessary for working this

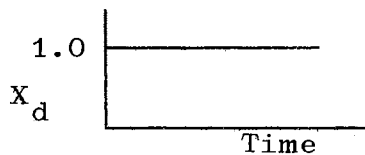
example are presented in Figure 42.

 Dynamical Equations

$$\dot{X}_1 = X_2$$

$$\dot{X}_2 = -.36 X_2 - .24 X_1 - P_1 X_1^3 - P_2 X_1 X_2 + 1.0$$

Performance Index

$$Y = \int_0^{5.0} (X - X_d)^2 dt$$


Number of Time Steps = 20

Initial Time = 0.0

Final Time = 5.0

Number of Free Initial Conditions = None

Initial Condition Vector

$$X_1 = 0.0 \quad X_2 = 0.0$$

Initial Parameter Guess

$$P_1 = 0.0 \quad P_2 = 0.0$$

Converged Parameter Vector

$$P_1 = .86122 \quad P_2 = 1.3174$$

Converged After:

21 Evaluations of the performance index

3 Evaluations of gradient vector

15 Evaluations of matrix of second partial derivatives

Figure 41. Equations and Results for the Spool Valve Example

COLUMN NUMBER	0	1	1	2	2	3	4
	5	0	5	0	5	0	5
1st. Data Card	2	0	2	2	20		
2nd. Data Card		0.0D00			5.0D00		0.0D00
3rd. Data Card		0.0D00			0.0D00		
4th. Data Card		0.0D00			0.0D00		
5th. Data Card		X(2)					
6th. Data Card		$-.36 * X(2) - .24 * X(1) - X(3) * X(1) ** 3 - X(4) * X(1) * X(2) + 1.0$					
7th. Data Card		$(X(1) - 1.0) ** 2$					

Figure 42. Data Cards Required for the Spool Valve Example in Chapter IV

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F-5

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 1234567890123456789012345678901234567890123456789012345678901234567890

CALL PRSEEK	001
CALL EXIT	002
END	003
SUBROUTINE PRSEEK	004
C PURPOSE	005
C DETERMINE THE BEST VALUES FOR THE PARAMETERS AND THE FREE	006
C INITIAL CONDITIONS BY THE METHOD OF SEEKING AXES PLANES.	007
C	008
C THIS PROGRAM WAS WRITTEN AND PROGRAMED BY DENNIS UNRUH AT THE	009
C DEPARTMENT OF MECHANICAL AND AEROSPACE ENGINEERING, OKLAHOMA STATE U	010
C UNIVERSITY, STILLWATER, OKLAHOMA. JULY 1969	011
C	012
C DELFPR - THE PREDICTED DIFFERENCE BETWEEN THE VALUE OF F AT	013 0023
C THE AXIS PLANE AND F AT THE BASE POINT.	014 0024
C DEN - SEE NUM/DEN.	015 0043
C DIRECT - IF THIS NUMBER IS POSITIVE, THEN THE PREDICTED	016 0038
C GRADIENT DIRECTION AND ACTUAL GRADIENT DIRECTION ARE WITHIN	017 0039
C 90 DEGREES OF EACH OTHER.	018 0040
C EIGVAL - EIGENVALUE VECTOR OF GX.	019 0037
C F - FUNCTION BEING MINIMIZED. F=F(X)	020 0015
C FBASE - VALUE OF F AT BASE POINT	021 0027
C FBEST - VALUE OF F AT BEST POINT.	022 0028
C FESMIN - ESTIMATED MINIMUM FOR THE SCALAR FUNCTION.	023
C G - GRADIENT VECTOR OF FUNCTION F. FOR EXAMPLE G(2)=PARTIAL F/	024 0016
C PARTIAL X(2).	025 0017
C GMAG - MAGNITUDE OF GRADIENT AFTER NPOS STEPS TO AXIS PLANES.	026
C GPRD - PREDICTED VALUE OF GRADIENT AT AXIS PLAIN.	027 0022
C GX - MATRIX OF SECOND PARTIALS OF F. I.E. GX(2,3)=PARTIAL G(2)	028 0018
C /PARTIAL X(3).	029 0019
C GXS - VECTOR WHICH CONTAINS GX IN SCIENTIFIC SUBROUTINE PACKAGE	030 0035
C SYMMETRIC STORAGE MODE.	031 0036
C N - THE NUMBER OF INDEPENDENT VARIABLES.	032
C NF - NUMBER OF TIMES F HAS BEEN CALCULATED.	033
C NG - NUMBER OF TIMES THE GRADIENT VECTOR HAS BEEN CALCULATED.	034
C NGX - NUMBER OF TIMES MATRIX GX HAS BEEN CALCULATED.	035
C NPOS - NUMBER OF POSITIVE EIGENVALUES.	036 0029
C NUM/DEN - THIS IS THE MAGNITUDE USED ON STEP NPOS+1 PROVIDED	037 0032
C NPOS SUCCESSFUL STEPS TO THE AXIS PLAINS HAVE BEEN MADE. THIS	038 0033
C IS USED ONLY IF NNEG IS NOT ZERO.	039 0034
C NXMAX - MAXIMUM NUMBER OF INDEPENDENT VARIABLES.	040 0044
C PERRAT - RATIO BETWEEN THE PREDICTED FUNCTION CHANGE AND THE	041 0025
C ACTUAL FUNCTION CHANGE.	042 0026
C R - DUMMY VARIABLE NEEDED FOR CALL STATEMENT OF EIGEN.	043 0045
C WORK - WORKING VARIABLE.	044 0046
C X - INDEPENDENT VARIABLE VECTOR.	045 0012
C XBAMIN - BASE POINT FROM WHICH A MINIMUM IS BEING SOUGHT BY A	046
C LINEAR SEARCH IN THE PREDICTED NEGATIVE GRADIENT DIRECTION.	047
C XBASE - THE VALUE OF THE INDEPENDENT VARIABLE VECTOR AT THE	048 0013
C BASE POINT.	049 0014
C XBEST - THE VALUE OF THE INDEPENDENT VARIABLE AT THE POINT	050 0020
C WHERE THE CALCULATED VALUE OF F WAS SMALLEST.	051 0021
C XNPOS - THE VALUE OF THE INDEPENDENT VARIABLE AFTER NPOS	052 0041
C SUCCESSFUL STEPS TO THE AXIS PLAINS.	053 0042
IMPLICIT INTEGER*2 (I-N),REAL*8 (A-H,O-Z)	054
INTEGER*4 MMM	055

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C		111 0095
	DO 7 I=1, IJMAX	112
	7 GXSS(I)=GXS(I)	113
	MMM=N	114
	CALL EIGENT(GXSS,R,MMM,I)	115
	DO 6 I=1,N	116 0101
	II=(I*(I+1))/2	117 0102
	6 EIGVAL(II)=GXSS(II)	118
	NNEG=N	119 0104
	NPOS=N	120 0105
	DO 8 I=1,N	121 0106
	IF (1.0005*EIGVAL(I).GT.EIGVAL(II)) GO TO 8	122
	NPOS=NPOS-1	123 0108
	8 CONTINUE	124 0115
	IF (EIGVAL(I).LE.0.000) NPOS=0	125
	WRITE (6,101)	126 0117
	WRITE (6,100) (EIGVAL(I),I=1,N)	127 0118
	WRITE (6,102) NPOS	128
		129
C	IF NPOS IS EQUAL TO ZERO , A LINEAR SEARCH IS PERFORMED FOR A	130
C	MINIMUM IN THE NEGATIVE GRADIENT DIRECTION.	131
C		132
	IF (NPOS.NE.0) GO TO 52	133
	DO 53 I=1,N	134
	53 XBAMIN(I)=X(I)	135
	NUM=FBEST-FESMIN	136
	IF (NUM.LT.0.000) GO TO 30	137
	DEN=0.000	138
	DO 50 I=1,N	139
	50 DEN=DEN+G(I)*G(I)	140
	DO 51 I=1,N	141
	51 X(I)=X(I)-(NUM/DEN)*G(I)	142
	GO TO 23	143
C		144 0120
C	DETERMINE VALUES FOR X TO THE SUCCESSIVE AXIS PLAINS.	145 0121
C		146 0122
	52 DO 14 K=1,NPOS	147
	DO 9 I=1,N	148 0125
	GPRED(I)=G(I)	149 0126
	DO 9 J=1,N	150 0127
	IJ=((J-I)*J)/2+I	151
	IF (J.LT.I) IJ=((I-1)*I)/2+J	152
	9 GPRED(I)=GPRED(I)+GXS(IJ)*(X(IJ)-XBASE(IJ))	153
	DO 10 I=1,N	154 0129
	10 X(I)=X(I)-GPRED(I)/EIGVAL(K)	155 0130
	I=1	156
	CALL SCAFCT(X,F,G,GXS,I)	157
	NF=NF+1	158
	WRITE (6,103) NF,NG,NGX	159 0132
	WRITE (6,112) K	160 0133
	WRITE (6,100) (X(I),I=1,N)	161 0134
	WRITE (6,105) F	162 0135
	IF (F.GT.FBEST.AND.K.EQ.1) GO TO 41	163
	IF (F.GT.FBEST) GO TO 60	164
C		165 0140

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C	CALCULATE PERRAT	166	0141
C		167	0142
	DELFPF=0.0	168	0143
	DO 13 I=1,N	169	0144
	WORK=0.0	170	0145
	DO 12 J=1,N	171	0146
	IJ=((J-1)*J)/2+1	172	
	IF (J.LT.I) IJ=((I-1)*I)/2+J	173	
	12 WORK=WORK+GXS(IJ)*(X(J)-XBASE(J))	174	
	13 DELFPF=DELFPP+(G(I)+.50*WORK)*(X(I)-XBASE(I))	175	0148
	PERRAT=(F-FBASE)/DELFPP	176	0149
	WRITE (6,108) PERRAT	177	0150
	IF (DABS(PERRAT-1.000).GT..100) GO TO 3	178	
	DO 11 I=1,N	179	0137
	11 XBEST(I)=X(I)	180	0138
	FBEST=F	181	0139
	14 CONTINUE	182	0152
	DO 15 I=1,N	183	0154
	GPRED(I)=G(I)	184	
	DO 15 J=1,N	185	0156
	IJ=((J-1)*J)/2+1	186	
	IF (J.LT.I) IJ=((I-1)*I)/2+J	187	
	15 GPRED(I)=GPRED(I)+GXS(IJ)*(X(J)-XBASE(J))	188	
	I=2	189	
	CALL SCAFCT(X,F,G,GXS,I)	190	
	NG=NG+1	191	
	WRITE (6,103) NF,NG,NGX	192	0159
	WRITE (6,106)	193	0162
	WRITE (6,100) (G(I),I=1,N)	194	0163
C		195	
C	CHECK FOR CONVERGENCE.	196	
C		197	
	DO 45 I=1,N	198	
	IF (DABS(G(I)).GT.1.0D-8) GO TO 46	199	
	45 CONTINUE	200	
	GO TO 33	201	
	46 IF (NPOS.EQ.N) GO TO 3	202	
	DIRECT=0.0	203	0164
	DO 16 I=1,N	204	0165
	16 DIRECT=DIRECT+G(I)*GPRED(I)	205	0166
	WRITE (6,110) DIRECT	206	0167
	IF (DIRECT.LE.0.0) GO TO 3	207	0168
	NUM=0.0	208	0169
	DEN=0.0	209	0170
	DO 17 I=1,N	210	0171
	NUM=NUM+(X(I)-XBASE(I))**2	211	0172
	17 DEN=DEN+(GPRED(I))**2	212	0173
	MAG=DSORT(NUM/DEN)	213	
	DO 18 I=1,N	214	0174
	18 X(I)=X(I)-MAG*GPRED(I)	215	
C		216	
C	PERFORM A LINEAR SEARCH FOR A MINIMUM IN THE PREDICTED NEGATIVE	217	
C	GRADIENT DIRECTION.	218	
C		219	
	I=1	220	

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CALL SCAFCT(X,F,G,GXS,I)	221
NF=NF+1	222
WRITE (6,103) NF,NG,NGX	223 0178
WRITE (6,104)	224 0179
WRITE (6,100) (X(I),I=1,N)	225 0180
WRITE (6,105) F	226 0181
41 DO 42 I=1,N	227
42 XBAMIN(I)=XBEST(I)	228
IF (F.GT.FBEST) GO TO 23	229 0182
C	230
C CONTINUE DOUBLING THE DISTANCE UNTIL F CEASES TO BECOME BETTER.	231
C	232
19 DO 20 I=1,N	233 0183
20 XBEST(I)=X(I)	234 0184
FBEST=F	235 0185
DO 21 I=1,N	236 0186
21 X(I)=XBAMIN(I)+2.0*(X(I)-XBAMIN(I))	237
I=1	238
CALL SCAFCT(X,F,G,GXS,I)	239
NF=NF+1	240
WRITE (6,103) NF,NG,NGX	241 0189
WRITE (6,114)	242 0190
WRITE (6,100) (X(I),I=1,N)	243 0191
WRITE (6,105) F	244 0192
IF (F.LT.FBEST) GO TO 19	245 0193
DO 22 I=1,N	246 0194
22 X(I)=XBEST(I)	247 0195
F=FBEST	248 0196
GO TO 3	249
C	250
C CONTINUE HALVING THE DISTANCE UNTIL F BECOMES BETTER.	251
C	252
23 DO 24 I=1,N	253 0198
24 X(I)=XBAMIN(I)+.50*(X(I)-XBAMIN(I))	254
I=1	255
CALL SCAFCT(X,F,G,GXS,I)	256
NF=NF+1	257
WRITE (6,103) NF,NG,NGX	258 0201
WRITE (6,113)	259 0202
WRITE (6,100) (X(I),I=1,N)	260 0203
WRITE (6,105) F	261 0204
IF (F.GT.FBEST) GO TO 23	262 0205
DO 25 I=1,N	263 0206
25 XBEST(I)=X(I)	264 0207
FBEST=F	265 0208
GO TO 3	266
60 DO 61 I=1,N	267
61 XBAMIN(I)=XBEST(I)	268
I=2	269
CALL SCAFCT(XBAMIN,F,G,GXS,I)	270
NG=NG+1	271
WRITE (6,103) NF,NG,NGX	272
WRITE (6,118)	273
WRITE (6,100) (G(I),I=1,N)	274
DIRECT=0.0	275

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DO 62 I=1,N	276
62 DIRECT=DIRECT+G(I)*GPRED(I)	277
WRITE (6,110) DIRECT	278
IF (DIRECT.GT.0.000) GO TO 23	279
DO 63 I=1,N	280
63 X(I)=XBAMIN(I)	281
GO TO 3	282
30 WRITE (6,116)	283
CALL EXIT	284
33 WRITE (6,109)	285
CALL EXIT	286 0241
RETURN	287 0242
END	288 0243
SUBROUTINE INPUT(X,FESMIN)	289
IMPLICIT INTEGER*2(I-N),REAL*8(A-H,D-Z)	290
C PURPOSE	291
C READ DATA CARDS.	292
C DATA CARD ONE CONTAINS NSYS,NFREE,NPAR,NWRITE,NSTEP	293
C DATA CARD TWO CONTAINS PRMT(1),PRMT(2),FESMIN	294
C DATA CARD THREE CONTAINS THE INITIAL CONDITION GUESS FOR	295
C COMPONENTS 1 THROUGH NSYS OF Y.	296
C DATA CARD FOUR CONTAINS THE INITIAL GUESS FOR THE PARAMETERS.	297
C IF NPAR=0 LEAVE THIS DATA CARD OUT.	298
C THE SYSTEM EQUATIONS ARE ENTERED ON CARDS 5 THROUGH NSYS+4.	299
C THE EQUATION FOR THE INTEGRAL OF THE SCALAR PERFORMANCE INDEX	300
C IS ENTERED ON THE LAST DATA CARD.	301
DIMENSION X(10)	302
COMMON /GENER/ NSYS,NFREE,NPAR,NFPNP,NFIXED,NSPNP,NSYSPI	303
COMMON /INFC/ IF(10),IFX(10,10),IFXXS(10,55)	304
COMMON /INOU/ IG,IGX(10),IGXXS(55),NWRITE	305
COMMON /SCIN/ YI(10),PRMT(5)	306
COMMON /IDFCSC/ P(5)	307
100 FORMAT (8D15.7)	308
101 FORMAT (5D15.7)	309
102 FORMAT (10I5)	310
103 FORMAT (' NSYS,NFREE,NPAR,NWRITE,NSTEP')	311
104 FORMAT (' PRMT(1) PRMT(2) FESMIN')	312
106 FORMAT (5(I5,F10.5))	313
108 FORMAT (' INITIAL CONDITION USED')	314
109 FORMAT (' PARAMETER VECTOR')	315
110 FORMAT (' IF(' ,I4,')=')	316
111 FORMAT (' IFX(' ,2I4,')=')	317
112 FORMAT (' IFXXS(' ,2I4,')=')	318
113 FORMAT (' IG=')	319
114 FORMAT (' IGX(' ,I4,')=')	320
115 FORMAT (' IGXXS(' ,I4,')=')	321
READ(5,107) NSYS,NFREE,NPAR,NWRITE,NSTEP	322
WRITE (6,103)	323
WRITE (6,102) NSYS,NFREE,NPAR,NWRITE,NSTEP	324
READ(5,101) PRMT(1),PRMT(2),FESMIN	325
WRITE (6,104)	326
WRITE (6,100) PRMT(1),PRMT(2),FESMIN	327
READ(5,101) (YI(I),I=1,NSYS)	328
WRITE (6,108)	329
WRITE (6,100) (YI(I),I=1,NSYS)	330

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IF (NPAR.EQ.0) GO TO 2	331
READ (5,101) (P(I),I=1,NPAR)	332
WRITE (6,109)	333
WRITE (6,101) (P(I),I=1,NPAR)	334
2 NFPNP=NFREE+NPAR	335
NFIXED=NSYS-NFREE	336
NSPNP=NSYS+NPAR	337
NSYSP1=NSYS+1	338
RNSTEP=NSTEP	339
PRMT(3)=(PRMT(2)-PRMT(1))/RNSTEP	340
IF (NFREE.EQ.0) GO TO 4	341
DO 3 I=1,NFREE	342
II=NFIXED+I	343
3 X(I)=YI(II)	344
4 IF (NPAR.EQ.0) GO TO 6	345
DO 5 I=1,NPAR	346
II=NFREE+I	347
5 X(II)=P(I)	348
6 DO 7 I=1,NSYS	349
WRITE (6,110) I	350
CALL FORTIN(IF(I))	351
DO 7 K=1,NSPNP	352
WRITE (6,111) I,K	353
CALL PARDIF(IF(I),IFX(I,K),K)	354
DO 7 J=1,K	355
JK=((K-1)*K)/2+J	356
WRITE (6,112) I,JK	357
7 CALL PARDIF(IFX(I,K),IFXXS(I,JK),J)	358
WRITE (6,113)	359
CALL FORTIN(IG)	360
DO 8 J=1,NSYS	361
WRITE (6,114) J	362
CALL PARDIF(IG,IGX(J),J)	363
DO 8 I=1,J	364
IJ=(I*J)/2+1	365
WRITE (6,115) IJ	366
8 CALL PARDIF(IGX(J),IGXXS(IJ),I)	367
RETURN	368
END	369
SUBROUTINE FCT(T,Y,DERY)	370
C PURPOSE	371
C SUPPLYS THE EQUATIONS FOR THE DYNAMICAL SYSTEM.	372
IMPLICIT INTEGER*2(I-N),REAL*8 (A-H,O-Z)	373
DIMENSION Y(210),DERY(210),Z(50),FX(10,10),FXXS(10,55),	374
1B(10,10),C(10)	375
COMMON /GENER/ NSYS,NFREE,NPAR,NFPNP,NFIXED,NSPNP,NSYSP1	376
COMMON /INFC/ IF(10),IFX(10,10),IFXXS(10,55)	377
COMMON /SCFCOU/ ILOGIC	378
COMMON /IOFCSC/ P(5)	379
DO 1 I=1,NSYS	380
1 Z(I)=Y(I)	381
IF (NPAR.EQ.0) GO TO 3	382
DO 2 I=1,NPAR	383
II=NSYS+I	384
2 Z(II)=P(I)	385

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3	II=NSYS+NPAR+1	386
	Z(II)=T	387
C		388
C	DETERMINE THE VALUES FOR THE DERIVITIVE OF THE BASIC SYSTEM.	389
C		390
10	DO 11 I=1,NSYS	391
11	DERY(I)=DVAL(IF(I),Z)	392
	IF (ILOGIC.EQ.1) RETURN	393
C		394
C	DETERMINE THE VALUES FOR THE DERIVITIVES OF THE FIRST ORDER	395
C	INFLUENCE COEFFICIENTS.	396
20	DO 21 I=1,NSYS	397
	DO 21 J=1,NSYS	398
21	FX(I,J)=DVAL(IFX(I,J),Z)	399
	DO 22 I=1,NSYS	400
	DO 22 J=1,NFPNP	401
	IJ=J*NSYS+I	402
	DERY(IJ)=0.0	403
	DO 22 K=1,NSYS	404
	JK=J*NSYS+K	405
22	DERY(IJ)=DERY(IJ)+FX(I,K)*Y(JK)	406
	IF (NPAR.EQ.0) GO TO 24	407
	DO 23 J=1, NPAK	408
	DO 23 I=1,NSYS	409
	IJ=(NFREE+J)*NSYS+I	410
	II=NSYS+J	411
23	DERY(IJ)=DERY(IJ)+DVAL(IFX(I,II),Z)	412
24	IF (ILOGIC.EQ.2) RETURN	413
C		414
C	DETERMINE THE DERIVITIVES FOR THE SECOND ORDER INFLUENCE	415
C	COEFFICIENTS.	416
C		417
	DO 25 I=1,NSYS	418
	DO 25 K=1,NSPNP	419
	DO 25 J=1,K	420
	JK=((K-1)*K)/2+J	421
25	FXXS(I,JK)=DVAL(IFXXS(I,JK),Z)	422
	DO 32 J=1,NFPNP	423
	DO 30 LI=1,NSYS	424
	DO 30 LJ=1,NSYS	425
	B(LI,LJ)=0.0	426
	IF (J.LE.NFREE) GO TO 26	427
	JJ=NSYS+J-NFREE	428
	LJJJ=((JJ-1)*JJ)/2+LJ	429
	B(LI,LJ)=FXXS(LI,LJJJ)	430
26	CONTINUE	431
	DO 30 LK=1,NSYS	432
	JJ=J*NSYS+LK	433
	LJLK=((LK-1)*LK)/2+LJ	434
	IF (LK.LT.LJ) LJLK=((LJ-1)*LJ)/2+LK	435
30	B(LI,LJ)=B(LI,LJ)+Y(JJ)*FXXS(LI,LJLK)	436
	DO 32 I=1,J	437
	IF (J.LE.NFREE.OR.I.LE.NFREE) GO TO 33	438
	DO 31 K=1,NSYS	439
	JJ=NSYS+J-NFREE	440

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      II=NSYS+I-NFREE                                441
      IIJJ=((JJ-1)*JJ)/2+II                          442
      C(K)=FXXS(K,IIJJ)                              443
      DO 31 LI=1,NSYS                                444
      LII=((II-1)*II)/2+LI                          445
      IF (LI.GT.II) LII=((LI-1)*LI)/2+II           446
      LIJ=J*NSYS+LI                                  447
31    C(K)=C(K)+FXXS(K,LII)*Y(LIJ)                 448
33    CONTINUE                                       449
      DO 32 K=1,NSYS                                  450
      IJ=((J-1)*J)/2+I                               451
      KK=(NFPNP+IJ)*NSYS+K                          452
      DERY(KK)=0.0                                   453
      IF (J.GT.NFREE.AND.I.GT.NFREE) DERY(KK)=C(K) 454
      DO 32 L=1,NSYS                                  455
      LL=(NFPNP+((J-1)*J)/2+I)*NSYS+L             456
      LLL=L*NSYS+L                                   457
32    DERY(KK)=DERY(KK)+FX(K,L)*Y(LL)+B(K,L)*Y(LLL) 458
      RETURN                                         459
      END                                           460
      SUBROUTINE SCAFCT (X,F,G,GXS,ILOG)            461
C     PURPOSE                                       462
C     SETS UP THE INITIAL CONDITIONS FOR THE DYNAMICAL EQUATIONS. 463
C     EVALUATES THE SCALAR PERFORMANCE FUNCTION, ITS GRADIENT, AND 464
C     ITS MATRIX OF SECOND PARTIAL DERIVATIVES. 465
      IMPLICIT INTEGER*2 (I-N),REAL*8 (A-H,O-Z)    466
      INTEGER*4 NTOTAL,IHLF                         467
      DIMENSION X(10),GI(10),GXS(55),Y(210),DERY(210),AUX(210) 468
      COMMON /GENER/ NSYS,NFREE,NPAR,NFPNP,NFIXED,NPNP,NSYSPI 469
      COMMON /SCOU/ GRAL(21)                        470
      COMMON /SCIN/ YI(10),PRMT(5)                 471
      COMMON /SCFCOU/ ILOGIC                        472
      COMMON /IOFCSC/ P(5)                         473
      EXTERNAL FCT,OUTP                             474
      DATA NDIFTO /0/                              475
100   FORMAT (' NDIFTO=',I5)                      476
      ILOGIC=ILOG                                   477
      IF (NFIXED.FQ.0) GO TO 4                      478
      DO 1 I=1,NFIXED                               479
1     Y(II)=YI(I)                                   480
4     IF (NFREE.EQ.0) GO TO 3                      481
      DO 2 I=1,NFREE                               482
      II=I+NFIXED                                  483
2     Y(II)=X(I)                                    484
3     IF (NPAR.EQ.0) GO TO 6                      485
      DO 5 I=1,NPAR                                 486
      II=NFREE+I                                    487
5     P(II)=X(II)                                  488
6     GO TO (10,20,30), ILOGIC                    489
C
C     DETERMINE THE VALUE FOR THE SCALAR PERFORMANCE FUNCTION, F. 491
C
C
10   NTOTAL=NSYS                                   492
      NOIFTO=NDIFTO+NTOTAL                         493
      WRITE (6,100) NDIFTO                         494
      495

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	CALL DRKF (PRMT, Y, DERY, NTOTAL, IHLF, FCT, OUTP, AUX)	496
	F=GRAL(1)	497
	RETURN	498
C		499
C	DETERMINE THE VALUE FOR THE GRADIENT OF THE SCALAR PERFORMANCE	500
C	FUNCTION, G.	501
C		502
	20 NTOTAL=(NFPNP+1)*NSYS	503
	DO 21 I=NSYSPI,NTOTAL	504
	21 Y(I)=0.0	505
	IF (NFREE.EQ.0) GO TO 23	506
	DO 22 I=1,NFREE	507
	II=NSYS*I+NFIXED+I	508
	22 Y(II)=1.0	509
	NDIFTO=NDIFTO+NTOTAL	510
	WRITE (6,100) NDIFTO	511
	23 CALL DRKF (PRMT, Y, DERY, NTOTAL, IHLF, FCT, OUTP, AUX)	512
	DO 24 I=1,NFPNP	513
	24 G(I)=GRAL(I+1)	514
	RETURN	515
C		516
C	DETERMINE THE VALUES FOR THE ELEMENTS OF THE MATRIX OF SECOND	517
C	PARTIAL DERIVATIVES OF THE SCALAR PERFORMANCE FUNCTION.	518
C		519
	30 NTOTAL=(1+NFPNP+((NFPNP+1)*NFPNP)/2)*NSYS	520
	DO 31 I=NSYSPI,NTOTAL	521
	31 Y(I)=0.0	522
	IF (NFREE.EQ.0) GO TO 33	523
	DO 32 I=1,NFREE	524
	II=NSYS*I+NFIXED+I	525
	32 Y(II)=1.0	526
	NDIFTO=NDIFTO+NTOTAL	527
	WRITE (6,100) NDIFTO	528
	33 CALL DRKF (PRMT, Y, DERY, NTOTAL, IHLF, FCT, OUTP, AUX)	529
	F=GRAL(1)	530
	DO 34 J=1,NFPNP	531
	G(J)=GRAL(J+1)	532
	DO 34 I=1,J	533
	IJ=(I+J-1)*J/2+I	534
	II=NFPNP+1+IJ	535
	34 GX(IJ)=GRAL(II)	536
	RETURN	537
	END	538
	SUBROUTINE OUTP(I, Y, DERY, IHLF, NTOTAL, PRMT)	539
C	PURPOSE	540
C	WRITE THE SYSTEM RESPONSE AFTER EVERY NWRITE STEPS OF NUMERICAL	541
C	INTEGRATION. NUMERICALLY INTEGRATE THE INTEGRAL EQUATIONS BY	542
C	USING THE TRAPAZOID RULE.	543
	IMPLICIT INTEGER*2(I-N), REAL*8 (A-H, O-Z)	544
	INTEGER*4 IHLF, NTOTAL	545
	DIMENSION Y(210), DERY(210), Z(50), GRAN(21), GRANPR(21),	546
	IGX(10), GXXS(55), B(10), PRMT(5)	547
	COMMON /GENER/ NSYS, NFREE, NPAR, NFPNP, NFIXED, NSPNP, NSYSPI	548
	COMMON /SCOU/ GRAL(21)	549
	COMMON /INOU/ IG, IGX(10), IGXXS(55), NWRITE	550

80/80 LIST

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 1234567890123456789012345678901234567890123456789012345678901234567890

COMMON /SCFCOU/ ILOGIC	551
COMMON /IOFCSC/ P(5)	552
100 FORMAT (1H0,D15.7)	553
101 FORMAT (8D15.7)	554
102 FORMAT ('* THE INTEGRAL VECTOR IS')	555
DO 1 I=1,NSYS	556
1 Z(I)=Y(I)	557
IF (NPAR.EQ.0) GO TO 3	558
DO 2 I=1,NPAR	559
II=NSYS+I	560
2 Z(II)=P(II)	561
3 II=NSYS+NPAR+1	562
Z(II)=T	563
C	564
C SET UP THE VALUE FOR THE INTEGRAN OF THE SCALAR PERFORMANCE	565
C FUNCTION.	566
GRAN(I)=DVAL(IG,Z)	567
NINT=1	568
IF (ILOGIC.EQ.1) GO TO 30	569
C	570
C SET UP THE VALUES FOR THE INTEGRAN OF THE GRADIENT OF THE SCALAR	571
C PERFORMANCE FUNCTION.	572
C	573
DO 10 I=1,NSYS	574
10 GX(I)=DVAL(IGX(I),Z)	575
NINT=NFPNP+1	576
DO 11 I=2,NINT	577
GRAN(I)=0.0	578
DO 11 J=1,NSYS	579
JJ=(I-1)*NSYS+J	580
11 GRAN(I)=GRAN(I)+GX(J)*Y(JJ)	581
IF (ILOGIC.EQ.2) GO TO 30	582
C	583
C SET UP THE VALUES FOR THE INTEGRAN OF THE MATRIX OF SECOND	584
C PARTIAL DERIVITIVES OF THE SCALAR FUNCTION.	585
C	586
DO 20 J=1,NSYS	587
DO 20 I=1,J	588
IJ=((J-1)*J)/2+1	589
20 GXXS(IJ)=DVAL(IGXXS(IJ),Z)	590
DO 22 J=1,NFPNP	591
DO 21 LI=1,NSYS	592
B(LI)=0.0	593
DO 21 LJ=1,NSYS	594
LIJ=((LJ-1)*LJ)/2+LI	595
IF (LI.LT.LI) LIJ=((LI-1)*LI)/2+LJ	596
LJJ=J*NSYS+LJ	597
21 B(LI)=B(LI)+GXXS(LIJ)*Y(LJJ)	598
DO 22 I=1,J	599
IJ=((J-1)*J)/2+I	600
II=1+NFPNP+IJ	601
GRAN(II)=0.0	602
DO 22 K=1,NSYS	603
KK=I*NSYS+K	604
KKK=(NFPNP+IJ)*NSYS+K	605

80/80 LIST

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 1234567890123456789012345678901234567890123456789012345678901234567890

22	GRAN(I)=GRAN(I)+Y(KK)*B(K)+GX(K)*Y(KKK)	606
	NINT=1+NFPNP+((NFPNP+1)*NFPNP)/2	607
30	IF (T.EQ.PKMT(1)) GO TO 36	608
	DO 34 I=1,NINT	609
	GRAL(I)=GRAL(I)+.50*(GRAN(I)+GRANPR(I))*(T-TPR)	610
34	GRANPR(I)=GRAN(I)	611
	TPR=T	612
	IF (T.EQ.PRMT(2)) GO TO 41	613
	IF (NCOUNT.EQ.NWRITE) GO TO 41	614
	NCOUNT=NCOUNT+1	615
	RETURN	616
36	DO 37 I=1,NINT	617
	GRAL(I)=0.0	618
37	GRANPR(I)=GRAN(I)	619
	TPR=T	620
C		621
C	RESET NCOUNT AND WRITE OUT THE VALUES AT THIS TIME.	622
C		623
41	NCOUNT=1	624
	WRITE (6,100) T	625
	DO 42 I=1,NINT	626
	JJ=(I-1)*NSYS+1	627
	II=I*NSYS	628
42	WRITE (6,101) (Y(J),J=JJ,II)	629
	WRITE (6,102)	630
	WRITE (6,101) (GRAL(I),I=1,NINT)	631
	RETURN	632
	END	633

VITA 3

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Doctor of Philosophy

Thesis: DETERMINATION OF OPTIMAL PARAMETERS FOR DYNAMICAL SYSTEMS

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