CONTINUOUS MONITORING OF DISSOLVED OXYGEN CONCENTRATION AND TEMPERATURE AT MULTIPLE DEPTHS IN A RESERVOIR

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By

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Thesis Approved:

Thesis Adviser

Dean of the Graduate College

PREFACE

The objectives of the present study were to design, construct, and test an apparatus for continuous recording of physicochemical parameters and to determine the value of data collected from several reservoir depths for primary production studies.

Dr. Troy C. Dorris served as major adviser. Drs. Jerry Wilhm and Louis P. Varga served on the advisory committee and criticized the manuscript. Dr. Rex L. Eley made many helpful suggestions with regard to analysis of the data, Doug Carter assisted with the drawings, and Gary K. Rice helped with field work, mechanical maintenance, and computer programming. The typing of the final manuscript was done by Mrs. Gary Rice. I am grateful for the kind assistance of all these people.

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CHAPTER I

INTRODUCTION

A reservoir is a complex system of interacting physical, chemical, and biological forces influenced by meteorological phenomena (Mackenthun and Ingram, 1967). Like any other ecosystem the reservoir has structure and function, nutrient cycling, and energy flow. If the input and output of physical, chemical, biological, and meteorological factors can be measured; a model can be made that will permit a general prediction of future trends in reservoirs.

Physical, chemical, and meteorological parameters in reservoirs are more easily measured on a continuous basis than are the biological parameters they influence. The evaluation of a continuous physicochemical sampling program of a reservoir is the objective of this study.

Keystone Reservoir, completed and filled by April, 1965, is located just west of Tulsa in north-central Oklahoma. It is a mainstream reservoir constructed by the U. S. Army Corps of Engineers for hydroelectric power generation, flood control, recreation, and control of the Arkansas River navigation system. It is formed by the confluence of the Arkansas and Cimarron Rivers 3.2 km upstream from the dam site (Figs. 1 and 2). Surface area of the reservoir at normal power pool level (220 m Mean Sea Level) is 10,648 ha with a storage capacity of about 8.2 X 10⁸ m³. The two rivers and smaller tributary streams drain large semi-arid plains in southeastern Colorado, southern Kansas, and northern Oklahoma



LOCALITY OF KEYSTONE RESERVOIR

100 60 0 20 km

Figure 1



ω

 $(192,970 \text{ km}^2)$.

Incoming waters contain variable concentrations of dissolved and suspended inorganic and organic solids. It has been found that the turbid and salt-heavy water of the Cimarron River produces a density current which underflows the clearer and lighter water of the Arkansas River except during mixing by flood waters. However, the Cimarron River contributes only about 17% of the total inflow. During the summer months pronounced thermal and chemical stratification exists (Eley, 1967, 1970).

Continuous monitoring of physicochemical variables can provide immediate data for water quality determinations and aid in the establishment of a predictive mathematical reservoir model. An adequate model can be made if variables such as temperature, oxygen, light and nutrients, which control the distribution of organisms, and turbidity and chemical balances, which influence sedimentation are included (Nicholls and Logan, 1966). In order to make detailed stratification analyses and provide for the most efficient reservoir operation data are also needed on wind, evaporation, quality and quantity of inflow, reservoir topography, circulation, and currents (Leifeste and Popkin, 1968).

It has long been recognized that grab samples are not adequate for detailed oxygen evaluation (Okun, Lamb, and Wells, 1963; Frey, 1967). Recent improvements of <u>in situ</u> oxygen probes and recording devices permit continuous operation with minimal servicing. Ragone and Peters (1967) described the use of continuous oxygen recorders on rafts in reservoir spillways. Operators controlled outflow to prevent anoxic conditions and fish kills below the dams. Leifeste and Popkin (1968) used a pump, hose, and small chamber that contained sensors for measuring temperature, conductance and dissolved oxygen on several Texas

reservoirs but without a continuous sampling procedure.

Reservoirs with a high volume turnover, such as Keystone, are kept in a state of low successional maturity by runoff of nutrients from crop lands and urban and natural pollution fed into them (Margalef, 1968). Organic and inorganic nutrients are important in determining biological fluctuations in reservoirs. Continuous recording of ionic chemical species may aid in establishing the extent of transfer of biologically important nutrients through the density gradients of reservoirs (Okun and Weiss, 1963). Other possible predictions from recording ionic species include increases in turbidity, formation of sludge deposits, increases in toxic chemicals, changes to extreme acidity or alkalinity, and production of undesirable aquatic growths (Mackenthun and Ingram, 1967).

Ionic probes must be highly selective and sensitive to low concentrations. Improvement of specific ion electrodes is progressing rapidly particularly for use in laboratory applications. Field application of these electrodes at multiple depths and with continuous recording will make possible much more refined reservoir models.

Monitoring of rapidly changing water conditions has been limited to a few meteorological and chemical parameters and not often continuously or at multiple depths (Okun and Weiss, 1963; Oglesby and Weiss, 1963; Leifeste and Popkin, 1968; and Welch, 1969). Some researchers have obtained data by extending sensing probes to the depths they wished to measure (Pamatmat and Banse, 1969; Eley, 1970). However, most workers have found it acceptable to pump water to a convenient location (Strickland, 1961; Weiss and Oglesby, 1963; Keyser, 1965; Margalef, 1968; and Welch, 1969). Pumping to a central location was found to be a convenient method for the present study since it permitted the use of a single set of sensing probes. Depths were monitored in sequence and simultaneous multiple depth sampling was sacrificed for monetary reasons with minimal loss of data.

CHAPTER II

DESCRIPTION OF THE STUDY AREA

A sampling station was established 130 m upstream from the Keystone Reservoir Dam. Depth of the water at normal power pool level was 19.7 m. Depth during the study varied from 18.5 to 20.5 m because of variable river inflow and discharge through the dam.

Sampled depths were 0.5, 3, 6, 12, and 18 m. Oxygen and temperature were measured every hour at each depth. Oxygen and temperature depth profiles were measured more or less continuously form July 24, 1968, to November 27, 1968. Data from the five measured depths were used to calculate values for each meter of the water column. Sampled depths were closer together in the euphotic zone where more rapid oxygen change was expected than in the relatively stable hypolimnion.

Information on rainfall, river inflow, reservoir depth, and sunlight duration and intensity was provided as daily averages by the Tulsa District Corps of Engineers and the U. S. Weather Bureau, Tulsa, Oklahoma.

The water at three substations 200 m apart near the sampler was homogeneous in respect to stratification, depth, currents, and metabolic activity.

CHAPTER III

METHODS AND MATERIALS

A. Construction of the Floating Sampler

The sampling station was constructed on a raft floated by polystyrene foam logs (Fig. 3). All hoses and fittings were black polyvinyl chloride of 20 mm inside diameter. One hose from each depth connected directly to a solenoid-actuated valve. Water from one depth at a time passed through the valve, a copper tubing manifold, a pump, and into an airtight plexiglas tub which contained the probes (Fig. 4). After flowing through the sampling tub the water was pumped away from the float to minimize mixing with the sample water (Fig. 5).

B. Sampling Control and Recording

An electromechanical controller was constructed to switch the sample depths and to control the probe sequence at each depth. During sampling at each depth the water flushed through the sampling tub for 9 min while the probes equilibrated. Each probe reading was recorded for 30 sec on a Rustrak strip-chart recorder before the controller switched to the next probe. Any depth sequence desired could be monitored.

C. Temperature Sensing

Figure 3. View of Floating Sampler

Top View

Figure 4. Sampling Tub Dimensions in cm

Figure 5. Block Diagram of Sampling Apparatus

H

The temperature sensor was a shielded, corrosion-proof, plasticcased thermistor. The thermistor gave a linear response of reduced resistance with increase in temperature. Calibration was accomplished by measuring the millivolt drop across the thermistor over a temperature range of 0 to 35 C as measured by a precision mercury thermometer accurate to \pm 0.1 C.

D. Measurement of Oxygen

The oxygen sensor consisted of silver and lead electrodes encased in a porcelain cylinder. The oxygen sensor was placed near the water inlet of the sampling tub to attain the required water current of 30 cm \sec^{-1} over its surface.

The potential produced by oxygen reaction with the electrodes was linear, but probe sensitivity was temperature dependent and changed with time. The sensor was recalibrated after membrane renewal every 2 weeks. For calibration the sensitivity coefficient (γ) was obtained from the ratio of sensor voltage output to oxygen concentration (Equation 1).

(1)
$$Y = \frac{mv}{[O_2] \text{ in g m}^{-3}}$$

Air saturated water was used in calibration (Hutchinson, 1957; Yaakov and Kaplan, 1969). The sensitivity coefficient applied to sensor output gave oxygen concentration of sample water(Equation 2).

(2)
$$[O_2]$$
 of sample water = $\frac{mv}{\gamma}$

Functions determined by computer for temperature and oxygen sensor calibrations were made part of a computer conversion program by which millivolt output was converted to degrees C and g 0_2 m⁻³.

Oxygen, temperature, time, and oxygen saturation values output by the conversion program were used in a diurnal oxygen curve analysis program modified from Eley (1970). This program used changes in dissolved oxygen over a 24 hour period, summed for the water column, to calculate gross primary production (Pg), community respiration (Rt), net primary production (Pn = Pg - Rt), Pg/Rt ratio, and diffusion into and out of the reservoir.

Appendix A is a reproduction of the raw data conversion program. Appendix B contains an example of converted data. Appendix C contains representative oxygen curve data and graphs.

E. Operation of the Sampler

Monitoring of oxygen and temperature at several depths with a single set of sensors necessitated a sequential procedure. However, all temperature and oxygen values were considered as having been obtained at the beginning of each hour. Rates of change at the surface were greatest and were measured first. Changes at the bottom were almost negligible because of lack of photosynthetic activity and nearly anoxic conditions and were measured nearly an hour later.

During the 5 months the sampler was in operation, over 100 days of complete data from midnight to midnight was recorded. As many as 21 successive days of recorded data was obtained. A total of 64 days were analyzed for primary production.

F. Data Gathering - Possible Errors

The greatest sources of error in the oxygen curve method are caused by horizontal movement of water masses of different metabolic history and improper estimation of the reaeration constant (Eley, 1970). Further errors enter when oxygen is not measured at sufficiently frequent depths.

Vertical mixing of oxygen is known to occur. Errors in measurement may arise from mixing of water in the thermocline and from interflows. Vertical currents and mixing patterns were not considered in this study.

Seiches of about 6 hour periods were evident from oxygen and temperature recordings at the 12 m depth during summer months. Seiches were created whenever there was high-volume, short-duration outflow. Corrections for seiches could not be incorporated in the primary productivity program since total depths involved were not determined.

Horizontal currents resulted from river inflows and drawdown for hydroelectric power generation and have been described for Keystone Reservoir (Falls, 1969; Eley, 1970).

CHAPTER IV

COMMUNITY METABOLISM

A. Sampling Assumptions and Validity

One station was used partly on the assumption that valid estimates of community metabolism could be made for the immediate vicinity of the sampler whenever water of uniform metabolic history was measured over a 24 hour period (Eley, 1970). He found no significant differences in community metabolism among three to six substations 200 m apart in four areas of the Cimarron River Arm of Keystone Reservoir. Monitored data obtained in the present study when little outflow for power generation occurred was accurate as shown by comparison with grab sample data and the data provided better estimates of production and respiration than on days of high outflow.

Oxygen and temperature data selected from five depths were multiplied by appropriate depth factors for transformation to surface area basis and compared with the data from every meter for production and respiration estimates (Table I). Calculated oxygen changes were compared to observed changes (Table I). A test for paired samples was used to determine the significance level the estimates of Pg, Rt, and Pg/Rt could be considered equivalent. The significance level for Pg was $\alpha = 0.40$, for Rt $\alpha = 0.40$, and for Pg/Rt $\alpha = 0.30$. Calculated changes in net oxygen production were significantly different from

TABLE I

Pg, Rt, AND Pg/Rt RATIOS FROM DATA TAKEN FROM EVERY METER AND FROM FIVE DEPTHS, Pg, Rt AND NET 0₂ CHANGE IN g 0₂ m⁻² day⁻¹ (ORIGINAL DATA IS FROM ELEY, 1970)

Date	Cimarror River Station	n km Above Dam	E Pg	very Mete Rt	r Pg/Rt	Calculated Net 0 ₂ Change	Fi Pg	ve Depths Rt	Pg/Rt	Calculated Net O ₂ Change	Observed Net O ₂ Change
9/24/66	II	28.0	38.49	45.53	0.90	- 7.04	52.15	58.19	0.90	- 6.04	- 6.00
12/17/66	II	28.0	14.28	4.08	3.50	10.20	11.21	2.77	4.05	8.44	3.40
6/4/67	II	28.0	48.69	39.53	1.23	5.16	43.50	39.40	1.16	4.10	- 7.70
8/1/66	III	17.4	9.35	40.01	0.23	-30.74	0.73	20.34	0.04	-19.61	- 9.80
12/17/66	III	17.4	36.40	12.51	2.91	23.89	43.68	13.39	3.26	30.29	25.10
6/4/67	III	17.4	26.05	18.78	1.39	7.27	28.65	26.93	1.06	1.72	4.80
8/1/66	IV	4.8	21.33	15.12	1.41	6.21	18.03	8.34	2.16	9.69	13.10
12/17/66	IV	4.8	21.88	8.77	2.49	13.11	25.39	11.12	2.28	14.27	7.90
6/4/67	IV	4.8	27.78	30.99	0.90	- 3.21	29.83	32.01	0.93	- 2.18	2.30

observed changes with one exception. Presence of currents at stations along the Cimarron River Arm probably caused the differences. The same method of comparison was used on data from Lake Atitlan, Guatemala by Dorris (unpublished). Agreement existed between observed and calculated net oxygen changes within 0.5 mg liter⁻¹ in nineteen of twenty-seven diurnal production studies. In Lake Atitlan no detectable currents exist and the water column is considerably deeper than that of Keystone Reservoir.

The significant differences between data from five depths and every meter in Pg, Rt, Pg/Rt, and net oxygen changes indicate that more depths should be sampled, perhaps at least at every 2 m. The assumption must also be met that to account for horizontal currents, water of similar metabolic history must be measured over each 24 hour period.

B. Advantage of more Frequent Sampling

More frequent sampling permits greater detail in analyzing oxygen rates of change (Fig. 6). Predawn rates of change progressively increased in Fig. 6 B, but no change occurred in a 5.5 hour period in Fig. 6 A. Infrequent sampling produced estimates with too large positive rates of change and too small negative rates of change. As a result, computed estimates of Pg, Rt, Pn, and Pg/Rt were different between the two sets of data. More frequent sampling permits a more precise picture of rates of change and corresponding production and respiration estimates are more accurate.

C. Production and Respiration Estimates

The correlation coefficient between Pg and Rt was 0.85. The ratio

Figure 6. Comparison of Oxygen Rate of Change Curves from Sampler Data (24 Data Points, Bottom) and from Grab Samples (12 Data Points, Top) for July 27, 1968, in g O₂ m⁻² day⁻¹

between Pg and Rt was generally considerably less than 1.0 (Fig. 7) and averaged 0.63. The ratio approached 1.0 on only one occasion when Pg was high during a period of clear days in August (Table II). The low ratios indicate that this area of the reservoir was heterotrophic as defined by Odum (1959). This condition is caused by the oxidation of large quantities of organic matter.

Pg and solar intensity were related by: Pg = 0.158 S (Fig. 8) after assuming 15% error and forcing through the origin. A straight line was used because a direct relationship exists between light quanta absorbed and oxygen evolved (Rabinowitch and Govindjee, 1965).

Community metabolism at the dam was compared with data from Eley (1970). Pg, Rt, and Pg/Rt were significantly different from the down-stream station (Table III).

D. Differences in Community Metabolism between Clear Days and Cloudy Days

Higher Pg and Rt generally occurred on the clear days (Fig. 9). Minimum Pg occurred on July 26 when solar radiation was at its maximum and inhibiting (Table II). Maximum Pg occurred when solar radiation was 661 g cal cm⁻² day⁻¹, indicating that this intensity did not seem to be inhibitory, although Hannan (1967) said that 647 g cal cm⁻² day⁻¹ was inhibitory to macrophytes. When solar radiation was high ($\bar{x} = 650$ g cal cm⁻² day⁻¹) for 30 clear days, Pg was high. It appeared that the optimum photosynthetic activity occurred at a solar radiation of between 660 and 690 g cal cm⁻² day⁻¹ since intensity as high as 692 g cal cm⁻² day⁻¹ from a single observation seemed to be inhibitory. During 26 cloudy days solar radiation ($\bar{x} = 337$ g cal cm⁻² day⁻¹)

TABLE II

DAILY Pg, Rt, Pn, Pg/Rt, SOLAR INTENSITY (S), EFFICIENCY (F), AND WEATHER (* = CLEAR DAYS, # = PARTLY CLOUDY DAYS, AND - = CLOUDY DAYS)

(1968)	(g Og	2 m ⁻² day-	1)	P g/ Rt	% (g	cal c	m ⁻² day ⁻¹)
Date	Pg	Rt	Pn		F	S	Weather
7-25 7-26 7-27 7-28 7-29 7-30	59.27 5.01 78.42 54.50 25.16 48.48	63.13 43.63 103.07 84.17 45.52 75.93	- 3.85 - 38.61 - 24.65 - 29.67 - 20.37 - 27.45	0.94 0.11 0.76 0.65 0.55 0.64	3.41 0.25 4.10 4.91 1.31 4.04	607 692 669 388 472 420	# * # #
8-2 8-3 8-4 8-5 8-6 8-7 8-8 8-9	84.65 104.79 103.47 99.55 116.60 125.75 151.08 83.67	115.70 130.11 104.98 111.15 101.65 144.56 184.31 114.71	- 31.05 - 25.31 - 1.52 - 11.60 14.95 - 18.81 - 33.23 - 31.04	0.73 0.81 0.99 0.90 1.15 0.87 0.82 0.73	4.35 5.42 5.53 5.47 6.69 7.99 4.53	680 676 654 636 610 657 661 648	* * * * * * *
8 - 13	28.56	70.63	- 42.07	0.40	3.69	270	-
8-14	17.02	39.98	- 22.96	0.43	1.93	308	-
8-17 8-18 8-19 8-20 8-21 8-22 8-23 8-24 8-25	71.11 60.29 61.48 67.11 76.31 45.29 92.27 54.85 98.94	130.33 148.30 105.71 124.72 100.76 76.04 258.13 128.85 179.06	- 59.22 - 88.01 - 44.23 - 57.60 - 24.46 - 30.75 -165.87 - 74.00 - 80.12	0.55 0.41 0.58 0.54 0.76 0.60 0.36 0.43 0.55	4.39 4.58 3.53 3.65 4.26 2.53 5.32 4.57 8.97	566 460 643 626 625 607 422 386	
8-27	150.27	205.66	- 55.39	0.73	11.17	471	80
8-28	16.12	113.29	- 97.17	0.14	2.64	214	66
8-29	69.04	123.06	- 54.03	0.56	22.58	107	68
8-30	49.47	84.43	- 34.95	0.59	11.54	150	68
9 -1	49.35	65.16	- 15.81	0.76	2.75	627	*
9 - 2	30.40	54.43	- 24.03	0.56	2.12	503	
9 - 3	67.14	100.17	- 33.03	0.67	6.27	375	*
9-17	57.35	58.80	- 1.46	0.98	3.97	505	-

TABLE II (CONTINUED)

(1968)	(g O	2 m ⁻² day-	¹)	P g/ Rt	% (g ca	al cm ⁻² d	ay ⁻¹)
Date	Pg	Rt	Pn		F	S We	ather
9-19 9-20 9-21 9-22 9-23 9-24 9.25 9-26 9-27 9-28 9-27 9-28 9-29 9-30 10-1 10-2 10-3 10-4 10-5 10-6 10-7 10-8 10-9	22.79 12.04 51.46 27.65 35.08 27.36 42.71 28.20 67.13 121.46 48.86 68.40 104.30 43.89 89.89 25.99 31.58 84.62 55.43 76.32 42.52	37.18 29.56 74.05 46.01 54.65 27.69 51.10 50.71 83.03 137.47 67.06 117.63 138.06 59.54 97.22 46.56 50.32 106.90 72.47 94.81 69.75	- 14.39 - 17.51 - 22.59 - 18.36 - 19.57 - 0.33 - 8.39 - 22.51 - 15.90 - 16.01 - 18.21 - 49.23 - 33.77 - 15.65 - 7.33 - 20.57 - 18.73 - 22.28 - 17.04 - 18.49 - 27.22	0.61 0.41 0.69 0.60 0.64 0.99 0.84 0.56 0.81 0.73 0.58 0.73 0.58 0.74 0.92 0.56 0.63 0.79 0.56 0.63 0.79 0.56 0.63 0.79 0.61	$1.48 \\ 0.86 \\ 4.27 \\ 2.03 \\ 4.61 \\ 10.88 \\ 2.73 \\ 1.88 \\ 4.50 \\ 8.24 \\ 3.35 \\ 5.16 \\ 9.24 \\ 3.35 \\ 5.16 \\ 9.24 \\ 3.17 \\ 6.32 \\ 2.19 \\ 9.53 \\ 6.14 \\ 4.10 \\ 21.20 \\ 3.29 \\ \end{bmatrix}$	538 491 422 547 266 848 522 5516 5526 5525 510 453 496 1162 4726 4162 4726 453 453	* _ # * * * * * * * * * * * -
10–12	98.89	144.66	- 45.77	0.68	15.45	224	-
10–13	29.54	60.47	- 30.93	0.49	2.61	396	
10–14	48.65	115.44	- 66.79	0.42	3.99	427	
10–15	23.32	49.07	- 25.75	0.48	3.52	232	
10 - 26	87.71	112.82	- 25.11	0.78	7.38	416	⊹
10 - 27	20.16	46.79	- 26.63	0.43	1.67	422	
11-22 11-23 11-24 11-25	77.54 8.87 13.57 26.71	111.91 78.54 118.46 57.43	- 34.38 - 69.67 -104.90 - 30.72	0.69 0.11 0.11 0.47	6.78 0.78 1.43 3.58	400 350 331 261	* - *
MEAN	59.48	93.71	- 34.23	0.63	5.27	459	

TABLE III

MEAN Pg, Rt, Pg/Rt, AND EFFICIENCY (F) FOR CIMARRON RIVER STATIONS AND DAM - Pg AND Rt IN g O₂ m⁻² day⁻¹, F IN % (DATA FOR STATIONS I-IV IS FROM ELEY, 1970)

Station	km above dam	Pg	Rt	Pg/Rt	F
I	38.7	11.3 ***	11.0 ***	1.02 &	1.97
II	28.0	27.4 ***	22.3 ***	1.22 *	3.87
III	17.4	38.6 **	41.0 *	0.94	6.35
IV	4.8	49.1 **	54.1 ***	0.91 ***	8.23
dam	0.13	59.5	93.7	0.63	5.27

Asterisks indicate significant differences between means. ***($\alpha = .01$), **($\alpha = .05$), *($\alpha = .10$), $\otimes(\alpha = .15$).

.

Pg and Rt During 6 Cloudy or Partly Cloudy Days and 8 Consecutive Clear Days

appeared to be limiting or was less than optimal for photosynthetic activity. The difference in productivity between clear and cloudy days was 41% as estimated by the following:

$$\frac{\overline{x} Pg (clear days) - \overline{x} Pg (cloudy days)}{\overline{x} Pg (clear days)} X 100 = \% difference$$

Hannan (1967) found that cloudy days were only 52% as productive as clear days. He also found that low light intensity had no obvious effect on community respiration, but that respiration was reduced under conditions of high light intensity. In Keystone Reservoir under low light intensity of cloudy days productivity was reduced considerably more than was respiration (Table IV). High light intensity did not inhibit algal productivity or reduce respiration with the exception of inhibition on July 26.

E. Efficiency of Production

Efficiency of photosynthetic production (Table II) was calculated from solar radiation and Pg according to a formula modified from Oswald (1957):

$$F = \frac{(3500) Pg (100)}{(10,000) S}$$

where F is percent efficiency, Pg is g $0_2 \text{ m}^{-2} \text{ day}^{-1}$, S is solar radiation in g cal cm⁻² day⁻¹, 10,000 is a factor to convert m² to cm², and 3500 is the number of cal of solar radiation required to produce 1 g of oxygen according to Kraus (1956).

Mean efficiency for cloudy days was 5.93% while that for clear

|--|

MEAN Pg, Rt, Pn, AND Pg/Rt FOR 30 CLEAR DAYS AND 26 CLOUDY DAYS Pg, Rt, AND Pn IN g 0 m⁻² day⁻¹

parameter	clear days		cloudy days	
x Pg	78.36	***	46.42	
x Rt	106.03	*	89.00	
x Pn	- 27.67	**	- 42.58	
x Pg/Rt	0.75	***	0.53	

Asterisks indicate significant differences between means. ***($\alpha = .005$), **($\alpha = .01$), *($\alpha = .05$).

days was 5.52%. These values were not significantly different at $\alpha = .01$. It appears that under conditions of less than optimal light and lower photosynthetic activity on cloudy days, the algae are able to compensate for low light intensity and be as efficient with less solar energy as on clear days. The correlation between photosynthetic efficiency and light intensity was -0.46 (Fig. 10).

F. Effects of a Flood on Community Metabolism

On August 19, 1968, a large inflow of both Arkansas and Cimarron River water occurred. Before the flood the hypolimnion contained about 1.0 g O_2 m⁻³ (Fig. 11). Salt-heavy flood water of the Cimarron River was well-oxygenated as was interflowing Arkansas River water. The flood increased oxygen content of the entire water column. Stratification was not disrupted. Over a 15 day period the hypolimnion again almost became anoxic. Surface oxygen generally decreased during the first 11 days. A sharp increase in surface oxygen and decrease in oxygen at 18 m occurred during days 11-14, probably caused by a sharp reduction in outflow which allowed a build-up of oxygen at the surface from production and decrease in the hypolimnion from respiration.

No distinct pattern in Pg, Rt, or Pg/Rt could be observed during the flood period (Fig. 12). The great Rt values 4 to 8 days after the flood are indicative of a large amount of allochthonous organic material deposited in the reservoir.

Figure 10. Linear Regression of S and F through September 30, 1968

Figure 11. Oxygen and Temperature at Surface and 18 m as a Result of Flooding on August 19, 1968 (Double Line at Bottom Indicates Periods of Cloudiness)

• 30

CHAPTER V

CONCLUSION

Pumping water to a central location was an acceptable sampling technique and was convenient since it permitted the use of a single set of sensing probes.

At least every 2 m vertically should be monitored. Sample depths should be more frequent in the euphotic zone than in the relatively stable hypolimnion for primary production studies by the diurnal oxygen curve method. The feasibility of using oxygen curve analyses is limited by currents in reservoirs. A complex sampling program which incorporates tracing water masses when interflowing and underflowing currents exist must be developed in order to apply the diurnal oxygen curve dependably.

More frequent sampling during each 24 hour period permitted greater detail in analyzing oxygen rates of change for primary production. One sample every hour appeared to give good results.

At Keystone Reservoir Dam high Pg and low Pg/Rt indicated that much organic matter was being oxidized. Pg and Rt were highly correlated (r = 0.85). Mixing of Arkansas and Cimarron River water increased Pg and Rt and reduced the Pg/Rt ratio and efficiency at the dam as compared to four stations on the Cimarron River Arm. The large increase in Rt and decrease in Pg/Rt was probably due to a much larger amount of organic material carried by the Arkansas River than the Cimarron River.

Higher Pg and Rt occurred on clear days. It appeared that the optimum photosynthetic activity occurred at a solar radiation of between 660 and 690 g cal cm⁻² day⁻¹ since intensity as high as 692 g cal cm⁻² day⁻¹ was inhibitory. During cloudy days light was limiting or less than optimal for photosynthetic activity. Under low light on cloudy days productivity was reduced considerably more than respiration.

Efficiency of production between clear and cloudy days was not significantly different. On cloudy days the algae were able to compensate for low light intensity and were as efficient with less solar energy as on clear days.

Flooding oxygenated all water strata but did not always disrupt thermal stratification. It took 15 days after a flood for the hypolimnion to again become anoxic. No distinct patterns in Pg, Rt, or Pg/Rt were observed during the flood period. Great Rt values after the flood are indicative of large amounts of allochthonous organic matter deposited in the reservoir.

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APPENDIX A

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REPRODUCTION OF CONVERSION PROGRAM

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THIS PROGRAM CALCULATES OZ CONCENTRATION AND TEMPERATURE FROM RUSTRAK STRIP
      CHART RECORDER DATA READ IN AS LINE NUMBERS ON CHART PAPER PRODUCED BY THE
      RESERVOIR CONTINUOUS MONITORING SYSTEM, RECALIBRATION OF PROBES AND OF
Bottom Depth Constant is done automatically as the data is converted, the
Only requirement being that all necessary data be present and that each
      DATA SET BE IN CHRONOLOGIGAL ORDER.
  SURFACE SATURATION AND 02 CONCENTRATIONS ARE SUMMED OVER THE WATER COLUMN
  FOR FURTHER UTILIZATION BY PERIPHERAL PROGRAMS.
OUTPUT IS RECORDED ON MAGNETIC TAPE UNIT 4 AND PRINTED IN TABULAR FORM.
DIMENSION ITIME(24), TEMP(24,5), O2(24,5), ZERO(24,5), CON(5),
#HUTCH(36,10), PSAT(24), SUM(24), MONTH(24), IDAY(24), IYEAR(24),
    #CON5(200), RINTCP(200), SLOPE(200), IYEARX(200), MONTHX(200),
    +IDAYX(200), ITIMEX(200), IYEARC(200), MONTHC(200), IDAYC(200),
     + ITIMEC (200), NPROBE (200), 1X2(200), IT IMEA (200), IC2(200), ITIMEB (200)
      COMMON WORD (6)
  1 FORMAT (10(F4.2, 4X))
2 FORMAT (313, 2X, 14, 5(F5.1, F4.1, F4.1))
3 FORMAT (F3.2,46X,312,14,20X,11)
3 FORMAT (F3.2,46X,312,14,20X,11)

4 FORMAT (8X, E13.6, 3X, E13.6,6X,312,14,21X,12,3X,14)

8 FORMAT('1',T60, 'DATE', 14, '/', 12, '/', 12 // 8X, '0.5 M', 4X,

*'3.0 M', 4X, '6.0 M', 4X, '12.0 M', 3X, '18.0 M', 5X, '0.5 M',

*'3.0 M', 3X, '6.0 M', 3X, '12.0 M', 3X, '18.0 M', 13X,

*'SURFACE' / 1X, 'TIME', 2X, 'TEMP11', 2X, 'TEMP[21', 2X,

*'TEMP[3]+, 2X, 'TEMP[4]', 2X, 'TEMP[5]', 5X, '02(1)', 3X, '02(2)',

*3X, '02(3)', 3X, '02(4)',4X, '02(5)', 3X, 'SUM 02', 4X,

*SATURATION'/ ( 1X, 14, F8.2, F9.2, F9.2, F9.2, F9.2, F11.2,

*F8.2, F8.2, F8.2, F8.2, F9.2, F11.2]]

22 FORMAT (1X,T61,'CON(5) DATA'////35X,'CON(5)',46X,'TIME CODE'//

*(36X,F4.2,47X,312,14)]
    *(36X,F4.2,47X,312,14))
23 FORMAT (11, 154, 02 PROBE GALIBRATION DATA'////38X, INTERCEPT),
+8X, SLOPE', 12X, TIME', 6X, PROBE NO. //(35X, E13.6, 3X, E13.6, 5X, 312)
    +14,5X,13))
24 FORMAT (////* DIURNAL IS COMPLETE*)
25 FORMAT (* CON(5) CHANGED TO*,F5.2,* AT*,I5)
26 FORMAT (* CON(5) EQUALS *,F5.2,* AT*,I5)
28 FORMAT (* O2 PROBE NO.*,I3,* BEING USED AT*,I5)
30 FORMAT (1 02 PROBE CHANGED TO NO. 13, 13, 141, 15)
51 Format (1 ****CAPACITY OF ARRAY NOT ENOUGH TO STORE CALIBRATION DA
                      READ 200 DATA CARDS')
   +TA/
52 FORMAT (3(2A3,4X))

53 FORMAT (14,313/(14,12F6.2))

54 FORMAT (F5.2)

55 FORMAT (F5.2)

57 FORMAT (1-MORE THAN 10 CONS VALUES PER DAY * * * PROGRAM TERMINATE
    (+03
59 FORMAT (1X)
60 FORMAT (15)
61 FORMAT (215)
63 FORMAT (1-MORE THAN 10 02 PROBES PER DAY * * * PROGRAM TERMINATED!
    13
72 FORMAT (13)
73 FORMAT
                            (F5.2,15)
74 FORMAT
                         12151
      REVIND &
      NCARD=0
  READ ALPHABETIC CHARACTERS INTO COMMON FOR SUBROUTINE TIMCHK
      READ (5,52) (WORD(1),1=1,6)
  READ IN HUTCHIN'S SATURATION TABLE
```

```
READ BOTTOM DEPTH CONSTANTS (CON5)
C (C
        DO 20 1 = 1,200
        READ (5,3) CONS(1), IYEARC(1), MONTHC(1), IDAYC(1), ITIMEC(1), ISIG
        IF (ISIG .EQ. 9) GO TO 9
 C
      CHECK DEPTH CONSTANT DATA FOR TIME CODE ERRORS
     20 CALL TIMCHK (IYEARC(I), MONTHC(I), IDAYC(I), ITIMEC(I), I, 1)
        GO TO 50
      9 NC = 1-1
 C
      LIST CONS DATA
        WRITE (6,22) (CONS(I), IVEARC(I), MONTHC(I), IDAYC(I), ITINEC(I),
       +1 = 1,NC)
 С
      READ 02 PROBE CALIBRATION DATA
        DO 21 I = 1,200
        READ (5,4) RINTCP(I), SLOPE([), IYEARX(I), MONTHX(I), IDAYX(I),
       *ITIMEX(I),NPROBE(I),ISIG
        IF (ISIG .EQ. 9) GO TO 10
      CHECK D2 PROBE DATA FOR TIME CODE ERRORS
 C
     21 CALL TIMCHK (IVEARX(I), MONTHX(I), IDAYX(I), ITIMEX(I), 1, 3)
        GO TO 50
     10 NX = 1-1
      WRITE OZ PROBE DATA
 C
        WRITE (6,23) (RINTCP(I), SLOPE(I), IVEARX(I), MONTHX(I), IDAYX(I),
       #ITIMEX(I),NPROBE(I),I=1,NX)
 C
      INITIALIZE VARIABLES
        DATA CON(11, CON(2), CON(3), CON(4)/1.75, 3.25, 4.50, 6.00/, ISTOP, ICL,
       GIX1, IX4, MCON5, MO2/0, 2, 2, 1, 1, 1/, IC2(1), IX2(1)/1, 1/
        CON(5) + CON5(1)
     15 I = 0
     31 NCUN5 # 0
        NO2 = 0
     13 Î.+ Î+Î
 C
      READ RUSTRAK DATA
        READ (B,2,END+17) HONTH(I), [DAY(I), IYEAR(I), ITIME(I), (TEMP(I,J),
       +02(1, J), ZERO(1, J), J=1, 5)
        NCARD#NCARD+1
 ¢.
      CHECK RUSTRAK DATA FOR TIME CODE ERRORS
        CALL TINCHK (IYEAR(I), MONTH(I), IDAY(I), ITIME(I), NGARD, 5)
     35 ISIG * 0
        NS16 . 0
      IF DATA IS FOR A DIFFERENT DAY, STORE IT AND FINISH CALCULATIONS FOR THE DAY
IF (IDAYII) .NE. IDAYIII) GO TO 16
CHANGE BOTTOM DEPTH CONSTANT IF TIME CODE OF RUSTRAK DATA IS .GE. TIME CODE
 C.
 C
        OF NEXT CONS VALUE
 C
     32 IF LICE .GT. NOT GO TO 11
     IF (IYEAR(1)-IYEARC(ICI)) 11,42,45
42 IF (MONTH(1)-MONTHC(ICI)) 11,43,45
     43 1F (1047(1)-1047(1)(1)) 11,44,45
     44 IF (ITIMELII-ITIMEC(ICI)) 11,45,45
45 IF (ISIG .EQ. O) NCON5 = NCON5+1
CON(5) = CON5(IC1)
        IC2(NCON5) = IC1
         ITIMEBIICI) = ITIME(I)
        IC1 = IC1+1
ISIG = 1
      CHANGE OF PROBE CALIBRATION IF TIME CODE OF RUSTRAK DATA IS .GE. TIME CODE
OF NEXT OF PROBE CALIBRATION
C
 С.
        60. 10 32
```

11 IF (1X1 .GT. NX) GO TO 12 IF (IYEAR(I)-IYEARX(1X1)) 12,38,39 38 IF (MONTH(1)-MONTHX(IX1)) 12,40,39 40 IF (IDAY(1)-IDAYX(IX1)) 12,41,39 41 IF (ITIME(I)-ITIMEX(IX1)) 12,39,39 39 IF (NSIG .EQ. 0) ND2 = NO2+1 IX2(NO2) = IX1 ITIMEA(1X1) = ITIME(1) IX4 = IX1IX1 = IX1+1NSIG = 1INDICATE IF CONS OR OZ WAS NOT CHANGED DURING THE DAY C GO TO LL 12 IF (NCON5 .EQ. 0) GO TO 46 IF (I .EQ. 1) MCON5 = IC2(NCON5) 46 IF (NO2 .EQ. 0) GO TO 36 IF (I .EQ. 1) MO2 = IX2(NO2) CQNVERT RUSTRAK DATA TO TEMP. IN DEG. C AND 02 CONC. IN MG/L D2 C APPROX. EQUAL TO GRAM/(CUBIC METER) 02 C 36 DO 5 J = 1, 5TEMP(I,J) = (ZERO(I,J) - TEMP(I,J)) + 28.0 + (-0.0669758) + 55.61325 O2(1,J) = (ZERU(1,J) - D2(1,J))+28.0/(SLOPE(1X4)+TEMP(1,J)+RINTCP *([X4}) C USING HUTCHINSON'S TABLE CALCULATE % SAT. OF SURFACE WATER (PSAT) K = INT(TEMP(I,1)) + 1L = INT(TEMP(I,1)+10.0001) - (K -1)+10 + 1 6 PSAT(I) = 02(I,1)/(HUTCH(K,L)+1.03) SUM D2 CONC. TO GET (G D2)/(SQ. M LAKE SURFACE) С SUM(1) = 0.0007J = 1,57 SUM(1) = 02(1, J) + CON(J) + SUM(1) IF 24 RUSTRAK DATA CARDS WEREN'T READ, READ ANOTHER ONE C IF (ISTOP .EQ. 1) GO TO 84 IF (I .NE. 24) GO TO 13 84 N=1 GO TO 18 16 N = I - 1C WRITE CALCULATED DATA ONTO TAPE WITH ITS TIME CODE 18 WRITE (4,53) N. [YEAR(1), MONTH(1), IDAY(1), (ITIME(M), (TEMP(M,J), &J=1,5),(02(M,J),J=1,5),SUN(M),PSAT(M),N=1,N) С PAD UNUSED TAPE RECORDS WITH BLANKS M=24-N IF (M .EQ. 0) GD TO 66 DO 67 MPAD=1.M 67 WRITE (4.59) WRITE CONS VALUES USED FOR THE DAY ONTO TAPE 66 WRITE (4,54) CONS(MCONS) C NCOKNT=0 IF (NCONS .EQ. 0) GO TO 48 LIMITED TO 10 CONS VALUES PER DAY C IF (NCON5 .GT. 10) GD TO 56 DU 83 M+1.NCON5 IC3=1C2(M) IF (1C3 .EQ. MCON5) GO TO 83 NCOKNT = NCOKNT+1 **83 CONTINUE** WRITE NUMBER OF TIMES OZ PROBES WERE CHANGED DURING THE DAY C WRITE (4,72) NCOKNT

```
DO 47 M=1,NCON5
       IC3 = IC2(M)
       IF (IC3 .EQ. MCON5) GD TO 47
       WRITE (4,55) CONS(IC3), ITIMEB(IC3)
    47 CONTINUE
       GD TD 49
    48 IF (IC1 .EQ. 2) MCON5 = IC2(1)
       WRITE (4,72) NCOKNT
GO TO 27
   49 MCON5 = IC2(NCON5)
C PAD UNUSED TAPE RECORDS WITH BLANKS
    27 M=10-NCOKNT
   IF (M .EQ. 0) GD TO 49
DO 58 MPAD=1,M
58 WRITE (4,59)
WRITE 02 PROBE CALIBRATION NUMBERS USED FOR THE DAY ONTO TAPE
C
       WRITE (4,60) NPROBE(MO2)
       NO2KNT=0
    IF (NO2 .EQ. 0) GO TO 34
LIMITED TO IO NPROBE VALUES PER DAY
IF (NO2 .GT. 10) GO TO 62
C
       DO 82 M=1,NO2
        1X3=1X2(M)
       IF (1X3 .EQ. MO2) GO TO 82
       NO2KNT=NO2KNT+1
    B2 CONTINUE
C
   WRITE NUMBER OF TIMES OZ PROBES WERE CHANGED DURING THE DAY
       WRITE (4,72) NO2KNT
DO 33 M#1,NO2
        IX3 = IX2(M)
        IF (1X3 .EQ. MO2) GO TO 33
       WRITE (4,61) NPROBE(1X3), ITIMEA(1X3)
    33 CONTINUE
    GO TO 37
34 IF (1x1 .Eq. 2) MO2 = 1x2(1)
WRITE (4,72) NO2KNT
       GO TO 29
    37 MO2 = 1X2(NO2)
    PAD UNUSED TAPE RECORDS WITH BLANKS
С
    29 M=10-NO2KNT
       1F IM .EQ. 01 GO TO 37
DO 64 MPAD=1.M
64 WRITE (4,59)
C N.EQ. I WHEN 24 VALUES/DAY WERE CALCULATED (COMPLETE DIURNAL)
IF (ISTOP .EQ. 1) GQ TO 69
IF (N.EQ. 1) GQ TO 15
     TRANSFER STORED VALUES FOR THE NEXT DAY INTO DATA POSITION ONE OF EACH
С
                                                                    RESPECTIVE ARRAY
С
       IDAY(1) = IDAY(1)
MONTH(1) = MONTH(1)
                                                                                       Ъp
       IYEAR(1) = IYEAR(1)
       ITIME(1) = ITIME(I)
       \begin{array}{l} 00 & 19 \\ TEMP(1,J) = TEMP(1,J) \end{array}
      02(1,J) = 02(1,J)
   19 \ ZERO(1,J) = ZERO(1,J)
C INITIALIZE VARIABLES AND GO BACK TO BEGINNING
 uur, t≓ t
```

```
NCON5=0
       NU2=0
    GO TO 35
17 IF (I .EQ. 1) GO TO 69
       ISTOP = 1
    GO TO 35
WRITE ERRORS DETECTED BY PROGRAM AND TERMINATE (SEE RESPECTIVE FORMATS FOR
C
· C
    50 WRITE (6,51)
       STOP
    56 WRITE (6,57)
       STOP
    62 WRITE (6,63)
       STOP
    69 ENDFILE 4
       REWIND 4
     AT THIS POINT ALL DATA IS CALCULATED AND ON TAPE, THE REMAINING STATEMENTS
С
       READ BACK THE TAPE DATA AND PRODUCE PRINTED OUTPUT
C
    81 READ (4,53,END=76) N, IYEAR(1), MONTH(1), IDAY(1), (ITIME(M),
      &(TEMP[M, J), J=1,5), (02(M, J), J=1,5), SUM(M), PSAT(M), M=1, N)
     SKIP BLANK RECORDS
С
       M=24-N
       IF (M .EQ. 0) GO TO 77
       DO 70 MPAD=1.M
    70 READ 14,591
    77 WRITE(6,8)MONTH(1), IDAY(1), IYEAR(1), (ITIME(M), (TEMP(M,J),
      GJ=1,5),(02(M,J),J=1,5),SUM(M),PSAT(M),M=1,N)
       IF(N .EQ. 24)WRITE (6.24)
    READ AND WRITE CONS VALUE USED AT FIRST READING
C
       READ (4,54) CON5(1)
                                 ,ITIME(1)
       WRITE (6,26) CON5(1)
     READ AND WRITE CONS VALUES CHANGED DURING THE DAY AND THE TIME THEY WERE
С
       CHANGED
С
       READ (4,72) NOOKNT
       IF (NCOKNT .EQ. 0) GO TO 79
       READ (4,73) (CDN5(IC3),ITIMEB(IC3),IC3=1,NCC
WRITE (6,25)(CON5(IC3),ITIMEB(IC3),IC3=1,NCOKNT)
                          (CON5(IC3), IT IMEB(IC3), IC3=1, NCOKNT)
° C
     SKIP BLANK RECORDS
    79 M=10-NCOKNT
       IF (M .EQ. 0) GO TO 80
DO 71 MPAD=1+M
    71 READ (4,59)
    READ AND WRITE OZ PROBE NUMBER USED AT FIRST READING
C
    80 READ (4,60) NPROBE(1)
       WRITE (6,28) NPROBE(1) ,ITIME(1)
     READ AND WRITE OZ PROBE NUMBERS CHANGED DURING THE DAY AND THE TIME THEY
C
       WERE CHANGED
C
       READ (4,72) NO2KNT
       IF (NO2KNT .EQ. 0) GO TO 78
READ (4,74) (NPROBE(IX3)
                        (NPROBE(IX3), ITIMEA(IX3), IX3=1, NO2KNT)
       WRITE (6,30)(NPROBE(IX3),ITIMEA(IX3),IX3=1,N02KNT)
    SKIP BLANK RECORDS
C
    78 M=10-N02KNT
       DO 75 MPAD=1.M
    75 READ (4,59)
    GO TO B1
76 REWIND 4
       STOP
```

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SUBROUTINE TIMCHK (IYEAR, MONTH, IDAY, ITIME, I, IX)
      SUBPROGRAM TO CHECK DATA FOR PROPER TIME SEQUENCING AND GROSS TIME ERRORS
 C
         CUMMON WORD (6)
         IN=1-1
         IY = IX + 1
Ċ
         CHECK FOR UNREALISTIC TIME DATA
         IF ((IYEAR .LT. 68) .OR. (IYEAR .GT.70)) GD TO 17

IF ((MONTH .LT. 1) .OR. (MONTH .GT. 12)) GO TO 17

IF ((IDAY .LT. 1) .OR. (IDAY .GT. 31)) GO TO 17

IF ((ITIME .LT. 0000) .OR. (ITIME .GT. 2400)) GO TO 17

IF ((ITIME .LT. 0000) .OR. (ITIME .GT. 2400)) GO TO 17
         IF (1 .EQ. 1) GO TO 2
CHECK FOR PROPER TIME SEQUENCE
 C
         IF ((YEAR.LT.IYEARX) GO TO 13
IF (MONTH.LT.MONTHX) GO TO 6
      5 IF (IDAY.LT.IDAYX) GO TO 4
     10
         IF (ITIME.LE.ITIMEX) GO TO 12
         GO TO 2
       6 ASSIGN 5 TO N
      8 IF (IYEAR.GT.IYEARX) GO TO N. (5,2)
         GO TO 13
       4 ASSIGN 10 TO M
         MZ=10
     15 IF (MONTH.GT.MONTHX) GO TO N, (10,2)
         ASSIGN 10 TO N
         IF (MZ .EQ. 2) ASSIGN 2 TO N
         GO TO 8
     12 IF (IDAY.GT.IDAYX) GO TO 2
         MZ=2
         ASSIGN 2 TO M
         GO TO 15
      2 IYEARX=IYEAR
         MONTHX=MONTH
         IDAYX=IDAY
         ITIMEX=ITIME
         RETURN
     WRITE MESSAGES AND TERMINATE
13 WRITE(6,7)[N,MONTHX,IDAYX,IYEARX,ITIMEX,I,MONTH,IDAY,IYEAR,ITIME,
 С
        *(WORD(IW),IW=IX,IY)
       7 FORMATE -- ERROR DETECTED WHILE COMPARING CARD', 19, 10X, 313, 16/26X,
        ** WITH CARD . 19, 10X, 313, 16, 10X, 2A31
         STOP
     17 WRITE (6,18) I.MUNTH, IDAY, IYEAR, ITIME, (WORD(IW), IW=1X, IY)
     18 FORMAT ( +- UNREALISTIC DATA ENCOUNTERED ON CARD + 18,10X,313,16,10X,
        *2A3)
         STOP
         END
```

APPENDIX B

REPRESENTATIVE CONVERTED DATA

FINE Remetal Remetal <thremetal< th=""> <thremetal< th=""> <threme< th=""><th></th><th>* * 0</th><th>3.0 8</th><th>E 0~9</th><th>12-0 H</th><th>18-0 N</th><th>0.5 H</th><th>9.0 H</th><th>₽.0 H</th><th>12.0 H</th><th>18.0 M</th><th>•</th><th>SURFAC</th></threme<></thremetal<></thremetal<>		* * 0	3.0 8	E 0~9	12-0 H	18-0 N	0.5 H	9.0 H	₽.0 H	12.0 H	18.0 M	•	SURFAC
100 28.42 27.46 27.41 26.42 9.05 7.57 7.57 7.57 7.57 7.55 1.07 0.25 86.47 200 28.40 27.41 26.42 9.02 7.57 7.48 1.07 0.25 86.47 500 28.40 27.41 26.42 9.02 7.56 7.48 1.07 0.25 86.47 500 28.42 27.41 26.42 7.43 1.07 0.25 81.47 1.07 0.25 81.47 0.25	FENE	(C) dealer	TEMPS 2)	RE LIGHT	1 TO AN BL	FENPES1	02(1)	02421	02431	02 (4)	02451	SCM D2	SATURA
200 28.47 27.18 27.41 26.42 9.02 7.75 7.44 1.46 6.25 61.44 700 28.40 27.18 27.41 26.47 9.02 7.45 1.47 0.25 61.44 600 28.40 27.41 27.41 27.41 27.41 27.41 27.41 27.45 1.47 0.25 61.44<	100	24-42	28-23	27.48	27-30	26-92	9-25	1.57	EE E	1.63	0.25	86.77	1.17
700 28-80 28-80 27-86 77-81 2	200	28-42	27.86	28.61	27-41	28-92	9.02	1.75	7.58	1-48	0.25	ET. +8	1.14
400 28.61 27.46 27.46 27.41 2	300	28.80	28.05	27.96	27-11	26-13	9.06	1.54	7.43	1-07	0-25	81-44	1-15
500 28.23 28.05 77.11 2	004	29-61	27.06	27.86	27-41	27-11	61.19	1.83	7.35	1-64	0.25	85-67	1.16
600 28.23 28.98 27.48 26.92 77.89 8.60 7.61 1.07 0.08 82.11 700 28.422 27.457 27.41 26.92 27.43 8.71 8.60 7.63 0.25 0.25 0.25 0.25 0.25 0.16 7.64 900 27.457 28.412 26.92 27.411 27.41 8.71 8.60 7.95 0.25 0.25 0.25 0.25 0.25 0.41 0.16 7.64 1100 29.481 28.412 26.451 27.48 8.71 8.60 7.45 0.25 0.25 0.25 0.42 0.41 0.16 7.64 0.16 7.54 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.41 0.16 7.64 0.16 7.54 0.25	500	28-23	28.05	26.05	27-11	27-11	96.49	7.38	7.30	1.15	0.25	81.40	-1-18
700 24.23 28.42 27.06 27.11 27.41 6.05 8.15 7.43 0.33 0.16 7.64 900 27.45 27.45 27.41 26.47 26.47 8.15 1.25 0.25	600	28-23	28.98	812	26-92	27.30	8. 60	B. 00	7-61	1-07	0-08	82.13	1.08
900 26.45 27.67 27.11 26.17 6.13 6.20 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.26 0.25 0.26 0.25 0.26 0.25 0.26 0.25 0.26 0.25 0.26 0.25 0.26 0.25 0.26 0.25 0.26 <th0.26< th=""> <th0.26< th=""> 0.26 <t< td=""><td>001</td><td>28.23</td><td>2.9-62</td><td>22.86</td><td>27.11</td><td>27-11</td><td>8-05</td><td>8.15</td><td>7.43</td><td>0.33</td><td>0-16</td><td>76.80</td><td>1.01</td></t<></th0.26<></th0.26<>	001	28.23	2.9-62	22.86	27.11	27-11	8-05	8.15	7.43	0.33	0-16	76.80	1.01
900 27.86 27.67 28.61 26.92 27.36 8.11 8.60 7.95 0.25 0.26 90.85 11000 29.41 28.25 28.412 26.92 27.34 9.27 9.23 8.20 0.41 0.45 0.25 99.47 1200 29.41 28.41 26.47 10.63 9.47 0.45 0.45 0.45 0.45 0.45 99.47 1200 29.41 28.42 27.48 27.48 27.48 27.48 27.46 27.48 27.46 27.48 27.46 27.46 27.48 27.46 27.46 27.46 27.46 27.46 27.46 27.46 27.46 27.46 27.46 27.47 10.47 0.49 0.41 74.5 91.47	000	28-42	E2-02	27.67	27.11	26.13	8-31	8-28	8.20	0.25	· 0. 25	81.09	1.05
1000 20-61 28-42 26-55 26-92 9-27 9-23 0-75 0-75 0-25 89-90 1100 29-37 29-37 9-50 9-37 9-50 0-41 0.15 0-25 89-90 1200 29-47 27-48 27-48 27-48 27-48 9-50 9-37 0-80 0.41 0.16 90-40 1300 29-47 27-48 27-48 27-48 27-48 27-47 9-50 9-47 0-80 0.41 0.16 90-40 97-41 97-47	006	27-96	ZT-67	28-61	26.92	RE-12	8.71	860	7.95	0.25	0.08	80.85	1.09
1100 29,30 28,80 28,80 28,40 27,41 27,44 9,50 9,37 8,90 0,41 0,16 90,40 1200 29,417 28,42 21,46 27,46 27,47 10,65 9,96 8,47 0,69 0,25 95,44 1300 29,47 28,42 21,48 27,46 26,47 10,65 10,50 8,47 0,69 0,25 95,47 1400 29,47 27,46 27,46 26,42 10,65 10,50 8,47 0,69 0,41 97,57 1500 39,47 28,42 27,46 26,42 10,65 10,50 8,47 0,13 9,11 94,57 1600 39,46 21,46 27,10 26,42 11,05 9,41 0,17 9,161 94,57 94,57 94,17 94,19 94,16	1000	20-61	28-23	28-42	26-55	26.92	9.27	6° 23	8.23	0.75	0.25	89.01	1.17
1200 29.17 29.46 28.60 27.51 10.63 9.96 8.21 0.80 0.25 99.96 1300 29.42 27.46 27.47 10.55 10.56 8.51 1.05 0.40 0.25 99.76 1500 28.46 27.46 27.46 27.46 27.46 27.46 27.46 27.46 27.46 27.46 27.46 27.46 27.47 0.41 0.40 0.43 91.67 1600 38.46 27.46 27.46 26.42 10.56 10.56 10.57 0.40 0.33 91.67 1600 38.46 27.46 27.46 26.42 10.57 10.56 10.40 0.33 91.67 1600 39.47 7.81 10.57 10.57 10.57 0.41 96.91 1700 27.46 27.46 26.42 11.07 9.47 7.43 0.31 1800 27.46 27.47 26.57 10.57 10.57 0.40 0.31 86.42 1900 30.41 27.46 27.46 27.46 27.46 27.46 27.47 24.94 2000 30.41 27.46 27.46 27.46 27.46 27.46<	1100	29+ 36	28-80	28-80	27-22	27.48	9.50	9.37	8.90	0.41	0.16	9040	121
1300 29,92 29,47 28,47 10,50 8,47 0,69 0,25 96,47 1600 28,42 27,46 27,47 0,47 0,40 0,43 0,41 97,57 94,61 17,94 0,40 0,41 97,57 94,61 17,94 0,40 0,40 0,40 0,41 97,57 94,61 17,94 94,61 14,94 0,40 0,41 94,61 <	1200	29-17	29.36	28-80	27-67	27-11	10.63	9.96	8.21	0-80	0.25	93.94	1.35
1400 28.42 29.55 27.36 27.30 10.43 10.50 8.15 1.05 0.41 97.35 1500 39.46 28.45 27.36 26.92 10.65 10.33 7.43 0.17 0.13 91.61 1600 30.47 26.05 27.46 26.92 10.65 10.33 7.43 0.17 0.17 91.61 1700 30.47 26.05 21.30 26.92 11.05 9.49 1.43 0.17 0.17 91.61 1700 39.47 28.61 27.86 27.30 26.35 11.05 9.49 7.43 0.57 0.01 86.57 1900 29.48 27.30 26.35 10.98 9.27 7.43 0.33 0.17 64.03 1900 30.48 28.46 27.30 26.35 10.98 9.27 7.43 0.33 0.17 64.03 2000 30.48 28.45 27.30 26.45 11.05 9.47 7.43 0.34 65.64 2000 30.48 28.42 27.30 26.45 11.65 9.47 7.51 0.33 0.17 64.03 2000 30.48 28.45 27.30 <t< td=""><td>1300</td><td>2992</td><td>29. 73</td><td>28.42</td><td>2 7.48</td><td>26-73</td><td>10-52</td><td>10.36</td><td>8.47</td><td>0.69</td><td>0.25</td><td>96.78</td><td>1.36</td></t<>	1300	2992	29. 73	28.42	2 7.48	26-73	10-52	10.36	8.47	0.69	0.25	96.78	1.36
1500 38.86 29.92 26.92 10.65 10.36 7.83 0.40 0.33 91.61 1600 39.47 26.92 10.65 10.36 7.83 0.40 0.33 91.61 1700 29.47 26.92 10.94 9.69 7.45 0.57 0.17 9.47 1700 29.47 26.92 11.05 9.49 7.45 0.57 0.17 94.92 1900 29.47 26.42 11.05 9.49 7.45 0.33 0.41 85.26 1900 29.47 27.86 27.30 26.45 11.05 9.47 7.51 0.33 0.34 85.64 1900 30.41 27.86 27.30 26.43 10.78 9.47 0.33 0.34 85.64 2000 30.41 27.46 27.30 26.43 10.78 9.47 0.33 0.34 85.64 2100 30.40 28.45 27.46 27.46 27.46 27.49 0.23 0.17 84.40 2100 30.40 28.45 11.67 8.47 1.45 0.46 0.49 2100 30.46 28.45 27.46 27.49 27.49 0.23 </td <td>1400</td> <td>28-42</td> <td>29.55</td> <td>27-86</td> <td>27.48</td> <td>27.30</td> <td>10-43</td> <td>1050</td> <td>8.15</td> <td>1.05</td> <td>0.41</td> <td>6E-16</td> <td>1.39</td>	1400	28-42	29.55	27-86	27.48	27.30	10-43	1050	8.15	1.05	0.41	6E-16	1.39
1600 30.47 28.05 27.86 27.30 26.92 10.94 9.69 7.43 0.73 0.17 89.21 1700 29.92 28.61 27.86 27.31 26.92 11.05 9.49 7.35 0.57 0.08 66.53 1800 29.42 27.86 27.30 26.55 11.05 9.40 7.35 0.33 0.34 65.64 1900 30.48 27.30 26.55 11.05 9.40 7.45 0.33 0.34 65.64 2000 30.48 27.30 26.55 10.07 8.47 7.51 0.33 0.17 84.51 2100 30.40 28.65 27.30 26.73 10.78 8.47 7.51 0.33 0.01 84.51 2100 30.40 28.65 27.30 26.73 10.78 8.46 0.33 0.01 84.51 2100 30.40 28.66 27.30 26.73 10.16 8.67 7.45 0.23 0.03 84.51 2100 30.40 28.66 27.30 26.92 10.16 8.57 7.43 0.03 8.01 7.45 0.40 8.06 8.65 2100 30.41	1 500	30+96	29.92	27+86	27.48	26.92	10.65	10.38	7.83	0++0	0.33	91.67	1.30
1700 29.92 28.64 27.16 27.11 26.92 11.27 9.19 7.35 0.57 0.08 86.53 1800 27.82 28.80 27.86 21.30 26.35 11.05 9.06 7.43 0.33 0.34 85.84 1900 30.11 27.86 21.30 26.55 10.98 9.27 7.29 0.33 0.17 84.91 2000 30.30 28.23 27.66 27.30 26.73 10.78 8.97 7.51 0.33 0.01 84.41 2100 30.30 28.23 27.66 27.30 26.73 10.18 8.68 7.45 0.24 0.08 85.44 2200 30.30 28.23 27.66 27.30 26.92 10.18 8.68 7.45 0.24 0.08 85.44 2200 30.30 28.42 27.36 27.39 26.92 10.11 8.68 7.45 0.24 0.08 82.61 2300 30.31 28.42 27.39 26.92 10.77 10.73 8.70 7.35 0.40 0.08 82.61 2400 30.31 28.42 27.39 26.92 10.77 0.07 8.70 7.35 0.24 0.09 82.61 2400 30.31 28.42 27.39 26.92 10.77 0.73 8.70 7.35 0.40 0.08 82.61 2400 30.31 28.42 27.39 26.92 10.77 10.33 8.70 7.35 0.40 0.28 0.25 90.24	1 600	14-06	26-05	27.86	2 T. 30	26.92	10.94	9.69.	7.43	0.73	0-17	89.27	1.42
1800 74.92 26.86 21.30 26.36 11.05 9.06 7.43 0.33 0.34 85.96 1909 30.41 27.86 21.30 26.45 10.96 9.27 7.53 0.33 0.17 84.97 2000 30.46 27.30 26.73 10.96 8.27 7.51 0.33 0.17 84.97 2000 30.46 27.30 26.73 10.78 8.77 7.51 0.33 0.08 84.17 2100 30.40 27.30 26.73 10.16 8.57 12.51 0.24 0.17 84.97 2100 30.40 27.30 26.73 10.16 8.57 12.45 0.24 0.17 84.97 2100 30.40 28.61 27.50 26.73 10.16 8.67 7.45 0.24 0.17 84.97 2200 30.40 28.67 10.617 8.67 10.43 8.261 9.25 90.25 2300 30.11 28.42 27.30 26.47 10.71 8.77 1.45 0.24 0.24 2400 30.11 28.42 10.81 8.77 1.45 0.25 90.25 2700 30.10	1 700	26-62	28-61	27.86	27.14	26-92	24.27	9.19	7.35	0.57	0.08	8.6.53	1.45
1900 30.11 27.86 28.42 27.30 26.55 10.98 9.27 7.29 0.33 0.17 84.93 2000 30.49 28.05 27.86 27.30 26.73 10.78 8.97 7.51 0.33 9.08 84.18 2100 30.30 28.23 27.48 27.30 26.73 11.14 8.68 7.45 0.25 0.17 83.45 2200 31.05 28.42 27.36 27.51 26.92 10.81 8.57 7.35 0.40 0.08 82.61 2300 30.31 28.42 27.35 27.39 26.92 10.43 8.70 7.35 0.40 0.08 82.61 2400 30.11 28.42 27.39 26.97 10.43 8.70 7.45 1.45 0.25 90.24	1.800	20-62	2880	27+86	27.30	26-36	11.05	90-09	7.43	0.33	0-34	85.84	1.42
2000 30.46 28.05 27.46 27.30 26.73 10.78 8.97 7.51 0.33 9.08 84.18 2100 30.30 28.23 27.46 27.30 26.73 11.14 8.68 7.45 0.24 0.17 83.44 2200 31.05 28.42 27.46 27.35 26.92 10.81 8.57 7.35 0.40 0.08 82.61 2300 30.30 30.30 28.42 27.39 26.92 10.71 8.70 7.13 1.45 0.25 90.24 2400 30.11 28.42 27.30 26.73 10.43 8.70 7.15 1.48 0.25 90.24	0061	30+11	27.86	28-42	27.30	2655	10.98	5.2.6	7.429	0.33	0.17	84.93	1.42
2100 30.30 28.23 21.44 21.30 26.73 11.14 8.68 7.45 0.24 0.24 0.17 83.45 2200 31.05 28.41 27.86 27.45 26.92 10.81 8.57 7.35 0.40 0.08 82.61 2300 30.30 30.30 28.42 27.39 26.92 10.77 8.70 7.13 1.48 0.25 90.28 2400 30.11 28.42 27.30 26.73 10.43 8.70 7.45 1.38 0.25 90.28	2000	30.48	28-05	27-86	27.30	C1 92	10.78	- B. 97	7-51	0.33	0.08	81-18	1.40
2200 31.05 28.61 27.86 27.61 26.92 10.61 8.57 7.35 0.40 0.08 82.67 2308 30.30 28.42 28.42 27.39 26.92 10.77 8.70 7.13 1.63 0.25 90.24 2400 30.11 28.42 27.30 26.73 10.47 8.70 7.45 1.38 0.25 90.34	2 E00	DIE TO'E	28+23	21-40	27-30	26.13	11-14	8-68	7.45	0-24	0.17	63.49	3.044
2308 30.30 28.42 (28.42 (28.42) 26.92 (2.14) 10.17 (8.70) 4.13 (1.63) 0.25 90.24 240 30.11 (24.45) 1.63 (0.25 90.24	2 2:00	31.05	28-61	27.96	27.67	26-92	10-01	8.57	1.35	0-+0	0.08	82.67	1.41
2400 2401 1851 24450 1001 1001 2613.001 1001 261430 1001 26143 1001 1001 1001 1001 1001 1001 1001 1	2 300	30-30	28-42	24-42	21-30	26-92	10-17	8-70	E1.F	L-63	0.25	90.24	4-39
	24:00	30.11	24-42	24 82	27-30	26.73	10-83	01 -8	1911	1.38	0.25	0606	1.60

DATE 7/25/68

DEURNAL IS CONTETE

CONTSI EQUALS 4.98 47 IG

D2 PEODE NO. 2 BEING USED AT

APPENDIX C

REPRESENTATIVE OXYGEN CURVE DATA

۰.

VALUES ADJUS	STED ACCORDI	NG TO CLASSI3,2)		and the second
RESPIRATION	LINE BEGINS	AT 6.60 HOURS	AND ENDS AT	21.00HOURS
				a transformer and the

TIME	INTERVAL	RATE	
0.0	1.00	-0+25	•
1.00	1.00	-3.03	
2.00	1.00	-1.25	· .
3.00	1.00	-0.93	
4.00	1.00	-2-35	
5.00	1.60	-0.33	
6.60	0.40	-1-43	
7.00	1.00	-1-04	
8.00	1.00	2.15	
9+00	1.00	8.95	
10.00	1.00	5.59	
11.00	1.00	-1-90	
12.00	1.00	-5.85	
13.00	1.00	0.55	
14.00	1.00	1.67	
15.00	1.00	1.91	
16.00	1.00	0.07	
17.00	1.00	3.87	
18.00	1.00	13.76	
19.00	1.00	0.64	
20.00	1.00	-2.51	
21.00	1.00	-10.25	
22.00	1.00	-10-25	
23.00	1.00	2-13	
GROSS PROD =	103.47	6 DF 02/M++2/	24HR
TOTAL RESP =	104-98	G DF 02/M##2/	24HR
NET PROD	-1.52	G OF 02/M##2/	24 HR
PROD/RESP =	0+99		1. A.

BIFFUSION-OUT = DIFFUSION-IN =	3.55 -0.0	G DF	02/#**2/24	HR
			·	

DIFFUSION CONSTANT (K) = -1.00 SUPPLIED FOR ENTIRE SET

PRODARESP =	0.87	0.0.02			DIFFUSION C
TOTAL RESP =	144.56	G DF 02	/4++2/24HR		DIFFUS ION-I
	125.75	6 05 07	/***?/?4HE	•	O FEUSION-O
23.00	1.00	-3,99			
22.00	1.00	-9-92			
21-00	1.00	-9+92			
20.00	1.00	-0-38			
19.00	1.00	-3-47			the set of the set of the
18.00	1.00	-0.67	an National Astronomy	÷ .	
17.00	1.00	0.04			
16-00	1.00	2.85			
15.00	1.00	-5.43	and the second		
14.00	1.00	3.77			
13.00	1.00	15.85			
12.00	1.00	3-17			
11.00	1.00	23.36			
	1.000	2410	· · · · · · · · · · · · · · · · · · ·		- 1.2 Control (1997)

DIFFUSION-OUT +	0.16	G OF	02/#++2/24HR			
DIFFUSION-IN =	3-23	G OF	02/H##2/24HR			
DIFFUSION CONSTANT	- (K)	∵ = -1.	.00 SUPPLIED	FOR	ENTIRE	SET

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· • •

	0.0	1.00	-0+04
	1.00	1.00	-10.35
	2.00	1-00	-5.94
	3.00	1.00	-1.90
	4.00	1.00	-4.57
	5.00	1.63	-3.02
	6.63	0-37	-3.76
A second	7.00	1.00	-4.54
	8.00	1.00	-1.78
191	9.00	1.00	-0.79
	10.00	1.00	7.18
	11.00	1.00	23.36
	12.00	1.00	3-17
	13.00	1.00	15.85
	14.00	1.00	3.77
	15.00	1.00	-5.43
	16-00	1.00	2.85
	17.00	1.00	0.04
	18.00	1.00	-0-67
	19.00	1.00	-3.47
	20.00	1.00	-0-38
	21-00	1.00	-9.97
	72.00	1.00	-9-97
	23.00	1.00	-3.99
GRUSS	PRODE	125.75	6 OF 02/H#
TOTAL	RESP =	144.56	G DF 02/M+

TIME INTERVAL RATE

. 1.00

. .

VALUES ADJUSTED ACCORDING TO CLASSI3.29 RESPIRATION LINE REGINS AT 6.63 HOURS AND ENDS AT 21.00HOMRS

APPENDIX C (CONTINUED)

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CONTINUE	
NDIX C	
Hada I I I I I I I I I I I I I I I I I I I	
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	CONTINUED
	\sim
	U
•	APPENDIX

t, D ENDS NU CLASSIC DA RESPERATION LINE BECRNS AT

12-80HOURS

<u>53</u>

PLEE FOR

-2/24

6 OF 02/H -1-00

10.0

DEFFUSION CONSTANT 4K1

VALUES ADJUSTED ACCORDING TO CLASS(1,2) RESPIRATION LINE BEGINS AT 9.00 HOURS AND ENDS AT 20. OOHOURS

. . . .

	TIME	INTERVAL	RATE	. •
	0.0	1.00	2.51	
	i.00	1.00	-1.35	
	2.00	1.00	-0.97	
	3.00	1.00	-0.14	
	4.00	1.00	-2.39	
	5.00	1.00	-1.72	
	6.00	1.00	-0.24	
	7.00	1.00	-3.54	÷
	8.00	1.00	-10.40	
	9.00	1.00	6.91	
	10.00	1.00	3.46	
	11.00	1.00	-1.90	
	12.00	1.00	6.27	
	13.00	1.00	-0.72	
	14.00	1.00	0.94	
	15.00	1.00	4.11	
	16.00	1.00	-1.71	
	17.00	1.00	1.31	
	18.00	1.00	2.93	
	19.00	1.00	-1.76	
	20.00	1.00	-2-33	
	21-00	1.00	-0.94	
	22.00	1.00	-3-14	
	23.00	1.00	-0-02	
$\{ i_1, i_2, \dots, i_n \}$				
GROS	S PR.00 =	89.89	G OF 02/M##2/24	HR
TOTA	L RESP =	97.22	G OF 02/###2/2	HR.
NET	PR00 =	-7.33	G OF 02/M##2/24	HR.
PROD	/RESP =	0.92		

DIFFUSION-OUT	#	1.77	G	OF	02/#**2	2/24HR	
D1FFUSION-IN	# 111	-0.0	G	OF	.02/#**2	2/24HR	
				-			

DIFFUSION CONSTANT (K) = -1.00 SUPPLIED FOR ENTIRE SET

VITA

Allen Ray Faust

Candidate for the Degree of

Master of Science

Thesis: CONTINUOUS MONITORING OF DISSOLVED OXYGEN CONCENTRATION AND TEMPERATURE AT MULTIPLE DEPTHS IN A RESERVOIR

Major Field: Zoology

Biographical:

- Personal Data: Born in Clinton, Oklahoma, January 11, 1945, the son of Jacob S. and Elvira L. Faust.
- Education: Graduated from Midwest City High School, Midwest City, Oklahoma, in 1963; received the Bachelor of Science Degree, Oklahoma State University, Stillwater, Oklahoma, May, 1967, with a major in Zoology; completed requirements for Master of Science Degree in May, 1972, at Oklahoma State University.
- Professional Experience: Undergraduate research assistant, Cooperative Fishery Unit, Oklahoma State University, 1967; graduate research assistant for Reservoir Research Center, Oklahoma State University, June, 1967 January, 1969; biomedical research technician, U. S. Army Aeromedical Research Laboratory, Fort Rucker, Alabama, April, 1969 November, 1970; graduate research assistant for Reservoir Research Center, Oklahoma State University, January, 1971 May, 1972.
- Member: American Society of Limnology and Oceanography, American Society of Ichthyology and Herpetology, Phi Sigma Society, American Institute of Biological Sciences, Water Pollution Control Federation, Red Rose.

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