## A BASIC EVALUATION OF THE URANIUM POTENTIAL OF THE MORRISON FORMATION OF NORTHWESTERN CIMARRON COUNTY, OKLAHOMA, AND ADJOINING AREAS OF NEW MEXICO AND COLORADO

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PREFACE

Exploration for uranium on the Southern Great Plains has had very limited success in the past. Exposures of the Morrison Formation in the Dry Cimarron River Valley are centrally located in a region which has few other good exposures. Observations and relationships from these exposures were used to project trends of potential uranium mineralization into areas with limited outcrops.

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## CHAPTER I

ABSTRACT

The undifferentiated Morrison was deposited on an alluvial plain by braided and meandering streams as well as fresh-water lakes. Thicker accumulations of Morrison sediment are found above or closely associated with changes in basement provinces and Precambrian faults. Sediment transport and deposition were controlled by structures associated with faulting. The major alluvial systems shifted to the east along the Oklahoma-New Mexico border during deposition of the upper Morrison.

In the mineralized samples, uranium has a high positive correlation with titanium, lead, strontium and magnesium, as well as a high negative correlation with manganese. The uranium was closely related to carbonaceous material. The localities of mineralization were controlled by low permeability and other stratigraphic conditions.

The areas which contain the highest probability for uranium mineralization are associated with the thicker Morrison sections. These areas form two trands. One is located along a line from Clayton, New Mexico, to Kenton, Oklahoma. The other is located parallel to the Sierra Grande Uplift and slightly east of the crest of the structure.

## INTRODUCTION

Recent changes in energy awareness and the resulting economic conditions have caused an increase in exploration for new uranium reserves. The undifferentiated Morrison of the Southern Great Plains has received limited exploration activity since the mid-nineteen fifties. During that time localized high concentrations of uranium have been found in northeastern New Mexico and southeastern Colorado. The limited success has been due at least in part to poor exposures of the potential host rock.

Exploration efforts in this region should begin with an understanding of the geologic conditions present during and subsequent to deposition of the Morrison. The area of this investigation is located in Cimarron County, Oklahoma, T4-6N, R1-2ECM and Union County, New Mexico, T30-32N, R29-37E (Fig. 1). This area is located between the two previously mentioned areas of known mineralization. The Morrison Formation in this area was found to contain two stratigraphic horizons of uranium enrichment.

Purpose and Methodology

The study was undertaken to evaluate the potential uranium enrichment in the Morrison of the Southern High Plains and to predict areas for future possible exploration. Known evidence which suggested

Fig. 1.-Index map of study area.
a possibility of mineralization included:

1. higher-than-normal uranium in ground water and surface water of the area;
2. reported localized "hot spots" in the Morrison south of the study area in Harding, Mora, San Miguel, and Quary Counties, New Mexico;
3. localized concentrations of uranium in the study area reported by Baldwin and Muehlberger (1959) and Zeller et al. (1976);
4. reported concentration of uranium north of the study area in Bent County, Colorado;
5. the reported presence of organic material in the formation; and
6. the reported favorable depositional environments of the Morrison in northeastern New Mexico, which are similar to those of Laguna and Ambrosia Lake districts of west-central New Mexico.

Several methods of investigation were used to evaluate the formation. Reconnaissance of the area was conducted by a carborne radiometric survey using a scintillometer and a gamma-ray spectrometer. Uranium concentrations reported from the literature and by ranchers in the area were investigated, as well as random samples of the Morrison outcrops. Stratigraphic sections of the sample localities were made at the time of sampling.

Samples were analyzed by several quantitative and qualitative methods. Thin sections were made of selected samples and analyzed on a Nuclide Luminoscope, as well as under plane-polarized light. The clay fraction was analyzed using $x$-ray diffraction to determine the mineralogic composition. Seventy samples were analyzed for uranium by Skyline Labs, Inc., Denver, Colorado, using a Galvanek-Morrison-type
fluorometer. These samples were selected from 140 samples which were analyzed for 16 additional cations using a Perkin-Elmer 403 double-beam atomic-absorption spectrophotometer.

## Previous Investigations

There have been several previous investigations in the area which have dealt with the Morrison Formation. Lee $(1901,1902)$ traced the Morrison from its type locality near Morrison, Colorado, into northeastern New Mexico and southeastern Colorado. Stanton (1905) discussed the relationship of the formation with the Lower Cretaceous beds of southern Colorado. Rothrock (1925) and DeFord (1927) described the areal geology of Cimarron County, Oklahoma.

The stratigraphy of Cimarron County was revised by Stovall (1938, 1943). Cooley (1955) described the stratigraphy and structures in the Dry Cimarron River Valley in Union County, New Mexico. Mankin (1958) discussed the regional geology of northeastern New Mexico, and concentrated on a mapping area in northern Harding County, New Mexico. West (1978) discussed a stratigraphic problem in the lower Morrison of Cimarron County, near Kenton, Oklahoma.

The geology and ground water conditions of Cimarron County, were described by Schoff (1943). The ground water resources of Cimarron County, were also shown in Irwin and Morton (1969) and Sapik and Goemaat (1973). Baldwin and Mueh1berger (1959), Baldwin and Bushman (1957), and Cooper and Davis (1967) discussed the geology and ground water of Union County, New Mexico. McLaugh1in (1954) described the geology and ground water resources of Baca County, Colorado.

Several geologic guidebooks have been published for the region.

These include oklahoma City Geological Society (1956), Kansas Geological Society (1934), Panhande Geological Society (1955), Mueh1berger et al. (1967), Kelley and Trauger (1972), and Foster et al. (1972).

Finch (1972) and the United States Atomic Energy Commission (1970) have described the known uranium occurrences in northeastern New Mexico. Landis (1960) discussed the uranium content of ground and surface water in the region.

Finch et al. (1975) compiled an extensive bibliography dealing with uranium and related subjects for eastern New Mexico and western Texas, and nearby areas of Oklahoma, Colorado, and Kansas. Zeller et al. (1976) presented a regional reconnaissance of the uranium potential of the great plains of Kansas, Colorado, and adjoining areas.

A helicopter-borne radiometric survey using a scintillometer was conducted in the area in late May, 1955 , extending 23 miles west from the Oklahoma-New Mexico state line to Peacock Canyon. The survey reported localized "hotspots" near the clastic plugs of Triassic age but no reported mineralization in the Morrison. Mr. Roy David, the president of Allied Helicopter Company of Tulsa, Oklahoma, reported that no maps or data of the survey were retained when economic deposits were not found (Dautenhahn, 1978).

## STRATIGRAPHIC FRAMEWORK

The generalized Mesozoic stratigraphic section (Table I) of northeastern New Mexico, and nearby areas of Oklahoma and Colorado, includes several formations that are not found throughout the region. This is due in some cases because of nondeposition and in others because of post-depositional erosion of the units.

The Dockum Group records the Triassic Period. Baldwin and Muehlberger (1959) have divided the Dockum into the Sheep Pen Sandstone, the Sloan Canyon Formation, the Travesser Formation and the Baldy Hill Formation, in descending order. This division of the Dockum is recognized only in the Dry Cimarron River Valley of Union County, New Mexico.

The Jurassic Period is represented by the Exeter Sandstone and the Morrison Formation. The Exeter is probably equivalent to the Entrada Sandstone and the Ocate Sandstone (Baldwin and Muehlberger, 1959; Bachman, 1953; and Wood et al., 1953). The Morrison Formation is divided in Union County (Baldwin and Muehlberger, 1959), into the Brown-Silt Member which is the basal section and above which is undifferentiated Morrison except for an "agate bed" approximately ten feet above the basal member.

The Cretaceous is represented by the Dakota Group, the Benton Group, and the Niobrara Formation, in ascending order. The Dakota Group is composed of the Purgatoire Formation, which includes the lower

TABLE I

MESOZOIC STRATIGRAPHY WITHIN THE STUDY AREA


Cheyenne Sandstone Member and upper Kiowa Shale Member, and the Dakota Formation. The Carlile Shale and Niobrara Formation are not found in Oklahoma, but are present in Baca County, Colorado and in Union County, New Mexico.

## Regional Stratigraphy of the Morrison

Cross (1894) was the first to use the name "Morrison", for beds exposed near Pikes Peak. E1dridge (1896) defined the Morrison Formation with a type section near Morrison, Colorado. Lee (1902) followed the Morrison exposures into northeastern New Mexico and southeastern Colorado. During this work, he reported the persistant "agate bed" found in the lower part of the formation. Stanton (1905) discussed the age and correlation of the formation in southern Colorado.

Rothrock (1925) described the areal geology of Cimarron County, Oklahoma, and stated that the eastern limit of the formation was in the western part of the county. DeFord (1927) corrected Rothrock by reporting the Morrison exposures and eastern limit of the formation in Cimarron County, as being north of Boise City (T5N, R6ECM). Stovall (1939,1943) established evidence of a major unconformity between the Morrison and Lower Cretaceous formations northeast of Kenton, Oklahoma, in northwestern Cimarron County.

Waldschmidt and LeRoy redefined the type section in 1944 to an area two miles north of the town of Morrison. Their new type section (Table II) is divided into six units according to lithology. These are:

1. Sandstone and Shale Unit-76.5 feet thick, lavender, marroon, and greenish-gray shales and light gray sandstones;
2. Red Shale Unit-36.75 feet thick, maroon, gray, lesser
greenish-gray shales and light gray to buff sandstones;
3. Gray Shale and Sandstone Unit-51.5 feet thick, gray and bluishgray shales and sandstones and limestones present, lower 8 feet contains vertebrate fossils;
4. Gray Clay and Limestone Unit-49.75 feet thick, gray clay beds and limestones;
5. Gray and Red Shale Unit-55.6 feet thick, gray and reddish-gray silty shales and limestones;
and
6. Basa1 Sandstone Unit-7 feet thick.

Freeman and Hilpert (1957) defined the Morrison Formation in the Laguna mining district in central New Mexico, as being composed of the Recapture, Westwater Canyon, and Brushy Basin Members (Table II). They also described a sandstone underlying the Dakota Formation and overlying the Brushy Basin Member, which they informally called the Jackpile sandstone bed of the Brushy Basin Member. F1esch (1975) has suggested that the Jackpile be named a formal member of the Morrison Formation in this area, based on his work and that of others mapping in the area. ${ }^{1}$

Squyres (1970) described the Brushy Basin Member of west-central New Mexico, as similar to sediments in the upper section of the undifferentiated Morrison of the Colorado Front Range. Flesch (1974, p. 189) states,

[^0]TABLE II

MORRISON STRATIGRAPHY OF THE TYPE SECTION, LAGUNA DISTRICT, AND THE STUDY AREA


The Brushy Basin consists of gray-green and red-brown, montmorillonitic claystone ( $69 \%$ of measured thicknesses), yellow to tan, iron oxide stained, well indurated arkosic arenites ( $29 \%$ ), which contain conglomerate seams and clay galls, thin brown-gray micrite beds (2\%), and trace amounts or red-brown, very thin, dense volcanic ash (?) beds.

Craig et al. (1955) described the undifferentiated Morrison as having a lithology and depositional environment similar to the Brushy Basin Member in western Colorado and northwest New Mexico.

## Local Stratigraphy of the Morrison

In northeastern New Mexico, the thickness of the Morrison ranges from $0-500^{+}$feet. It is composed of variegated shales, lenticular sandstones, and lacustrine limestones. An informal subdivision of the Morrison for purposes of discussion in this report is shown in Table II. In the study area the basal member of the Morrison, the Brown-silt Member (Baldwin and Muehlberger, 1959), is equivalent to the unit Cooley (1955) termed the Wanakah Formation. Mankin (1958) did not divide the Morrison but described the lower Morrison as generally being reddish brown silty shale. Cooley (1955) described the Brown-silt interval as being 80 feet thick in Colfax County, New Mexico, (Woods et al., 1953) and thinning progressively to the east. Cooley interpretated the measured section of the Morrison by Stovall (1938) at Labrier Butte in Cimarron County, as containing the Brown-silt Member in the lower 8 feet of the section. The member is brown to tan and is graygreen at some localities. In the Dry Cimarron River Valley west of Guy Monocline, gypsum is present in the member but is absent to the east of the structure.

Cooley concluded that the Brown-silt Member was conformable above
the Exeter Sandstone and suggested an interfingering relationship between the lower Brown-silt units and upper Exeter. This relationship can be seen in the Dry Cimarron River Valley just west of the Guy Monocline and south of Bueyeros (Baldwin and Muehlberger, 1959). Near Las Vegas, New Mexico, the Morrison overlies the Todilto Formation (Mankin, 1958). The Todilto also separates the Entrada and Morrison in west central New Mexico.

The "agate bed" was considered by Ogden (1954) to be a time stratigraphic marker throughout the Rocky Mountain area. The bed is composed of clear, red, and blue nodular chalcedony generally found about 10 feet above the Brown-silt Member. The best exposures are found near Guy, New Mexico (Ba1dwin and Mueh1berger, 1959). Stovall (1938) did not identify the bed as being in Cimarron County, however, McLaugh1in (1954) noted its presence in Baca County, Colorado.

Stovall (1938), Cooley (1955), and West (1978) describe the middle Morrison as being composed of shales and limestones which are pale olive gray to green in color. The upper Morrison contains red, brown, and maroon shales with more sandstone and fewer limestones near the top of the unit. Mankin (1958) and Cooley (1955) describe a well developed sandstone in the middle Morrison in the area east and along the trend of the Sierra Grande Uplift.

In the Kenton area, the Morrison is composed of the middle (limestones and gray green shales) and the upper (sandstones and maroon shales) sections. The middle Morrison contains a pelletoidal limestone which is the best stratigraphic marker in the region (West, 1978), because the "agate bed" has not been found.

Volcanic ash beds are better developed in the upper part of the
formation throughout the area (Mankin, 1958). Volcanic ash has, however, been noted in the lower middle Morrison in the Dry Cimarron River Valley (Cooley, 1955) and near Bueyeros (Mankin, 1958).

Stovall (1938) reported the Morrison in Cimarron County, as unconformably underlying the Purgatoire Formation. To the west, at Flathead Canyon, in Union County, the contact is disconformable (Cooley, 1955). In Colfax County, the Morrison conformably underlies the Cretaceous units (Wood et al., 1953). In areas where sandstones of the upper Morrison are overlain disconformably or concordantly by the Cheyenne Sandstone, it is difficult to determine the boundary between the formations (Baldwin and Muehlberger, 1959; Cooley, 1955).

Finch (1972) describes an overlapping of the lower Morrison by the middle Morrison near Tucumcari, New Mexico. This is also shown in the Dry Cimarron Valley by the Brown-silt Member thinning to the east. The gypsum beds found in the lower part of the member are missing east of Guy Monocline. North of Boise City, the Brown-silt Member and the greenish gray shales and limestones are not present. The measured sections in this area by Stovall (1938) contain only the upper Morrison of maroon shales and sandstones. Near Las Vegas, the Morrison has as overstepping relationship with the underlying Todilto Limestone. In Baca County, the Lower Cretaceous formations overstep the Morrison (McLaughlin, 1954). These observations serve to illustrate the conclusion that as the late Jurassic sedimentary basin was filled the upper units covered the lower units and extended further to the east.

## STRUCTURAL FRAMEWORK

The major structural features which were influential during Morrison deposition in the study area were the Sierra Grande Uplift, Las Animas Arch, and Apishapa Uplift. To the west and south of the area the Mogollon Rim, Pedernal Uplift, Las Vegas Basin, Raton Basin, Tucumcari Basin, and the Umcompahgre Uplift were of importance (Fig. 2). All of the structures were partially or completely covered during the late Paleozoic, but continued to influence sedimentation through the Jurassic. The Mogollon Rim south of Gallup, New Mexico, is thought to be the source area for the "western" Morrison (Flesch, 1975).

The Bravo Dome in Hartley County, Texas, Clapham Anticline and Pasamonte Anticline in Union County, New Mexico, were smaller structures which were prominent during deposition of the Morrison. In the Dry Cimarron Valley the Guy Monocline and an unnamed smaller anticline in T29N, R35E (Winchester, 1934) were of importance.

Schoenfelt (1934) described a small anticline with a northeast trend in Baca County, Colorado (T35S, R49W). In Union County, New Mexico, T31N, R36E Winchester (1934) and Bates (1942) denoted a similar anticlinal structure. Stovall's (1943) stratigraphic section of the Morrison Formation was measured on the southeast limb of a pre-Cretaceous fold located near the Three Corners area north of Kenton, Oklahoma. Scott (1968) located a similar monocline in $\mathrm{S}^{\frac{1}{2}, ~ T 34 S, ~ R 49 W ~}$


Fig. 2.-Generalized tectonic setting during the Late Jurassic for northeastern New Mexico and southeastern Colorado. Letters indicate towns referred to in the text.
in Baca County. These four locations are considered to be sections of a continuous structure, which for purposes of this report will be named the Three Corners Monocline. This structure is the most likely reason for the changes in direction of the basalt flow in Section 6, T31N, R37E.

Similar continuity can be seen between the Tecolote Monocline (Scott, 1968), located in T33-34S, R51W Baca County, and the unnamed structure in T 29 N , R 35 E in Union County. The basalt flow also changes direction as it crosses the trend of this structure. The Baltillo Creek Monocline T34S, R53W may also be an extention of Guy Monocline by similar association. Continuity between the two structures is suggested by the structural maps by $S \operatorname{cott}$ (1968) and Baldwin and Muehlberger (1959). The structure map of the Mississippian surface by Anderman (1961) suggests that trends of the Guy and Tecolote Monoclines extend northeastward and converge to the Mustang Creek Monocline.

Amplitudes of the folds are largest on Guy Monocline and decrease progressively to the eastern structure at Three Corners. These monoclinal terraces associated with the eastern slope of the Sierra Grande Uplift have an eastern boundary developed along Precambrian faults and a western boundary developed along late Pennsylvanian faults (Martin, 1965).

The geologic map of the Precambrian and the major faults in northeastern New Mexico are shown in Fig. 3 (Foster et al., 1972). Structures in the study area and in southeastern Colorado, are shown in Fig. 4. The north-south fault in Union County (Fig. 3) is thought to be connected with the Freezeout Creek Fault (Kleindopf et al., 1972) by a fault along the Clapham Anticline. To the north, the Freezeout Creek


Fig. 3.-Precambrian provinces and faults for northeastern New Mexico, modified after Foster et al. (1972).


Fig. 4.-Structural map of the study area. Dots indicate known uranium mineralization localities.

Fault extends into the Ute Pass Fault in the saddle between the Sierra Grande Uplift and the Las Animas Arch. Thus the eastern and northern boundaries of the biotite granite of the Sierra Grande Uplift probably have a fault contact with the rhyolite and granite basement units to the east and north. Foster et al. (1972) interprets the basement complex as being tilted fault blocks and gives several lines of evidence to support this interpretation. The similarity between the fault patterns in San Miguel, Quay, and Quadalupe Counties, New Mexico, and the generalized basement provinces (Fig. 3) suggests that the faults may be associated with the basement province boundaries.

The location of the Freezeout Creek Fault could not be determined with any degree of certainty near Clayton, New Mexico, because of limited data. The fault may be associated with the boundary between the basement rocks (Fig. 3) which trends northeast-southwest, or the fault may extend through the panhandle volcanic terrane along a northsouth trend near the Oklahoma-New Mexico state line.

Martin (1965) shows upper Pennsylvanian faulting in the western part of the monoclinal terrace (Fig. 4). Post-Exeter faulting with the same trend can be seen on the Tecolote Monocline in Union County. The faulting along the western boundary of the monoclinal terrace is not associated with movement in the basement rocks and is therefore of less magnitude than the faulting along the eastern boundary.

## CHAPTER V

SEDIMENTOLOGY OF THE MORRISON

The Morrison in the study area is composed of variegated shales, limestones, and sandstones. The formation was deposited blanket like on an alluvial plain by meandering and braided streams separated by freshwater lakes. The micritic lacustrine beds are better developed along the eastern region of the depositional basin and in areas of maximum sedimentation (Mankin, 1958). The sandstones of the middle Morrison are generally lenticular in shape and grade vertically into shales. They have sharp erosional lower and lateral contacts, and are very discontinuous. Outcrop exposures are generally measured in tens or hundreds of feet. Two strong sandstone developments occurred within the Morrison, one in the middle Morrison and one in the upper Morrison. The latter is better developed than the first and contains slightly coarser sediment (Mankin, 1958). These sandstones are best exposed near Kenton, Oklahoma, Stead, New Mexico, and west of the Guy Monocline in Union County, New Mexico.

The thinner, less well developed sandstones contain medium and small scale crossbedding and horizontal bedding. Tabular crossbedding is better developed than trough crossbedding. These thinner sandstones were deposited by meandering stream systems.

The thicker sandstones contain massive and horizontal bedding along with medium scale trough and tangential crossbedding. Granular
and pebble conglomeratic beds containing clay galls are also present. Grading within individual cross laminae can often be found. A slight decrease in size of the crossbeds upward within genetic units can be seen at some locations. These thicker sandstone units were deposited by braided stream systems.

The well developed upper Morrison sandstone near Kenton, Oklahoma, was deposited in a structural trough just east of the Three Corners Monocline. Field observations suggests pre-, syn-, and post-Morrison development of the Monocline and related trough. The paleocurrent data from the upper Morrison sandstones show a $N 47^{\circ}$ E trend (Fig. 5), which is very similar to the trend of the Three Corners Monocline. Well log data suggests that the thicker Morrison development is confined to a trough extending from near Stead, New Mexico, to the ColoradoOklahoma border north of Kenton (Fig. 6). The trough is thought to be controlled by tilted block-faulted basement. McLaughlin (1954) reports not finding any evidence to suggest a thicker Morrison section in Baca County. The thinning of the Morrison section to the north and the divergence of the Precambrian faults to the north suggests that the depositing streams were less confined in that direction.

The isopach map of the Morrison Formation in northeastern New Mexico (Fig. 6), shows several generalized trends in deposition. There is a remarkable similarity between Fig. 6 and the map of the basement provinces and faults (Fig. 3). The thicker Morrison section in T15-17N, R30-32E is bounded on two sides by faults near a change in basement terrains. The thicker section in T19-22N, R24-26E is flanked on both sides by the basement faults trending along the axis of the Sierra Grande Uplift. Mankin (1972) states that the Morrison shows a general


Fig. 5.-Rose diagram of current directions in sandstones of the upper Morrison from the Kenton area.


Fig. 6.-Isopach map of the Morrison Formation of northeastern New Mexico, modified after Mankin (1958). Dots indicate known uranium mineralization localities.
thinning across the axis of the uplift. Roberts et al. (1976) show a similar thinning of the formation across the axis of the structure near Des Moines in Union County. The thicker section in the Las Vegas Basin is also located along major faults and changes in basement terrain. The Raton Basin may also have developed similar thick Morrison sections to the west of the Sierra Grande Uplift in western Colfax County (Roberts et al., 1976 and Baltz, 1965). The Tucumeari Basin, Clapham Anticline, and the monoclinal terrace received very limited sediment during deposition of the Morrison.

Mankin (1958) describes the source area for the Morrison in northeastern New Mexico, as being to the west and northwest because of an increase in grain size, feldspar and apatite content in that direction. Several authors have described the paleocurrent directions within the Westwater Canyon Sandstone, the Brushy Basin Shale, and Jackpile Sandstone Members of the "western" Morrison as being in an east or northeasterly direction. These authors include Flesch (1975), Brookins (1975), Schlee and Moench (1961), and Rackley (1976). During late Morrison deposition, sedimentation was controlled by a structural trough possibly between the Uncompahgre Uplift in Colorado and northern New Mexico and the Pedernal Uplift to the south (Fig. 2). A similar drainage pattern during Early Cretaceous is shown by McGookey et al. (1972).

## CHAPTER VI

## PET'ROGRAPHY

Petrographic analysis was conducted on 25 thin sections from the middle and upper Morrison. These samples were collected near Kenton, Oklahoma, and represent a vertical sequence of the Morrison from the area (Table III). Stratigraphic positioning of the samples was possible because of work by West (1978).

The grain size ranges from silt (<4.0 ) to pebble (>-4.0 ) . The mean grain size for the sandstones is approximately $3.5 \phi$ to $3.0 \phi$ or upper very fine. An overall coarsening upward sequence is present, with the pebbles only being found in the upper samples.

The sorting ranges from very poorly sorted to well sorted. The lower section, which is composed of samples NM-2 to NM-17 of Table III, is moderately sorted. The best sorting is found in the middle of the section (samples MR-1 to MR-11) which is the beginning of the upper Morrison and is predominantly sandstone. The sorting of the upper most samples (PA-22 to $\mathrm{AB}-4$ ) is poor to very poor because of an introduction of a coarser mode.

The roundness ranges from angular to well rounded with a mean of subround. The roundness increases upward through the section. In the upper Morrison several samples contained angular and well rounded detrital grains. Mankin (1958) contributes this to two source areas.

The foregoing descriptions reflect changes in the depositional

TABLE III
PETROGRAPHIC ANALYSIS OF THE MIDDLE AND UPPER MORRISON FORMATION

| Terrigenous |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sample |  |  |  | Sedimentary | Igneous Rock |  |  |  |
| Number | Quartz | Chert | Feldspar | Rock Fragments | Fragments | Zircon | Tourmaline | Apatite |
| $A B-4$ | 64 | 20 | 6 | <2 | <2 | $<1$ | $<1$ | -- |
| $A B-45$ | 49 | 5 | 5 | --† | -- | <1 | <1 | -- |
| $A B-43$ | 35 | tr* | tr | 56 | <4 | tr | tr | -- |
| AB-44 | 24 | 15 | 1 | -- | -- | 1 | 1 | -- |
| PA-15 | 13 | 86 | 1 | -- | -- | -- | -- | -- |
| PA-3 | 86 | 10 | 2 | -- | -- | 1 | 1 | -- |
| PA-23 | 3 | -- | tr | -- | -- | -- | -- | -- |
| PA-22 | 34 | tr | tr | 40 | -- | -- | tr | -- |
| MR-11 | 78 | 14 | tr | -- | -- | tr | tr | -- |
| MR-10 | 87 | 3 | 2 | -- | -- | tr | -- | -- |
| MJ-7 | 76 | <1 | 3 | -- | -- | tr | tr | tr |
| MR-8 | 77 | 3 | tr | -- | -- | tr | tr | -- |
| MR-6 | 89 | 1 | tr | -- | -- | tr | tr | -- |
| MR-4 | 62 | 5 | 3 | -- | -- | tr | tr | -- |
| MR-2 | 63 | 5 | 2 | -- | -- | tr | tr | -- |
| MR-1 | 87 | 2 | 1 | -- | -- | -- | tr | -- |
| NM-17 | 32 | 2 | 2 | -- | -- | tr | -- | tr |
| NM-15 | 20 | 3 | 3 | -- | -- | tr | -- | -- |
| NM-13 | 17 | 5 | 3 | 15 | -- | tr | tr | tr |
| NM-12 | 25 | tr | 1 | -- | -- | -- | tr | tr |
| NM-10 | 25 | 4 | 3 | -- | -- | -- | tr | -- |
| NM-8 | 37 | tr | 2 | -- | -- | tr | tr | tr |
| NM-5 | 20 | 5 | 5 | -- | -- | tr | tr | tr |
| NM-3 | <1 | - | -- | -- | -- | -- | -- | -- |
| NM-2 | 33 | 6 | 11 | -- | -- | tr | tr | -- |

TABLE III (Continued)

| Terrigenous |  |  |  | Cement |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sample <br> Number | $\begin{aligned} & \text { Biotite } \\ & \text { (mica) } \end{aligned}$ | Hematite | Pyrite | Carbonate | Quartz | Opal | Chalcedony | Clay |
| AB-4 | -- | tr | -- | -- | -- | 5 | -- | -- |
| $A B-45$ | tr | tr | -- | -- | -- | -- | 40 | tr |
| $A B-43$ | tr | tr | -- | -- | -- | 4 | -- | tr |
| AB-44 | -- | tr | -- | -- | -- | 60 | -- | -- |
| PA-15 | -- | tr | - -- | -- | -- | -- | -- | -- |
| PA-3 | -- | tr | -- | -- | - | 30 | -- | tr |
| PA-23 | -- | tr | tr | 97 | -- | - | -- | -- |
| PA-22 | -- | tr | -- | 25 | - | -- | tr | -- |
| MR-11 | -- | tr | -- |  | 7 | -- | -- | tr |
| MR-10 | -- | tr | -- | 4 | -- | 4 | -- | tr |
| MJ-7 | -- | tr | -- | 13 | 12 | -- | -- | tr |
| MR-8 | -- | tr | -- | 14 | 16 | -- | -- |  |
| MR-6 | -- | tr | -- | -- | 9 | -- | -- | tr |
| MR-4 | -- | tr | -- | 23 | -- | -- | 7 | -- |
| MR-2 | tr | tr | -- | 30 | -- | -- | -- | tr |
| MR-1 | -- | tr | -- | tr | 3 | - | 6 | tr |
| NM-17 | tr | tr | 1 | 20 | - | 43 | -- | -- |
| NM-15 | -- | tr | 4 | -- | -- | 55 | -- | -- |
| NM-13 | -- | tr | -- | -- | -- | 60 | -- | -- |
| NM-12 | -- | tr | tr | 64 | -- | -- | -- | -- |
| NM-10 | 1 | tr | tr | 65 | - | -- | -- | -- |
| NM-8 | 1 | tr | -- | 55 | -- | -- | -- | -- |
| NM-5 | -- | tr | -- | 30 | -- | -- | -- | -- |
| NM-3 | -- | tr | tr | 99 | -- | - | -- | -- |
| iNM-2 | tr | tr | -- | 50 | -- | tr | - | -- |

*Trace recorded.
$\dagger$ Not detectable.
environments and the energy of the transporting media. The lower samples were deposited in freshwater lakes and by low-energy meandering streams. The middle samples were from an environment with better sorting which suggests that the energy was sufficient to carry away the fines but was not strong enough to transport the coarser material found higher in the section. Sedimentation was predominately by braided streams. The upper samples show an increase in grain size and rounding and are very poorly sorted. These were deposited by braided streams which had higher energy than the streams of the middle unit.

## Mineralogy

Quartz is the most abundant mineral found in the Morrison Formation. The middle braided stream interval has the highest percentage of quartz. This is due to a smaller proportion of chert and chalcedony as is found in the upper $1 / 3$ of the formation. The quartz occurs as plain and undulose extinction. Overgrowths of quartz are found in most slides, but are better developed upward in the sequence.

Feldspar occurs as orthoclase, microcline, and a small plagioclase fraction. The amount ranges from $<1 \%$ to $22 \%$ of the detrital assemblage. The percentage decreases upward thought the section except for the very coarse mode at the top of the sampled interval which contains granitic rock fragments. These results follow Mankin's analysis which suggested a decrease in feldspar content upward in the formation and to the east in Oklahoma. Overgrowths of authigenic feldspar were not found in any of the samples, although they have been reported in the Morrison. Sedimentary and igneous rock fragments were in several samples. The granitic rock fragments were only found in the coarser samples at the
top of the stratigraphic section. The sedimentary rock fragments were present at several horizons. These are rounded fragments of micrite, opal, and chalcedony. The upper coarse mode contains pebbles which were once algal micrites from the lacustrine deposits of the middle Morrison and which have been altered to opal and chalcedony (Fig. 7). Detrital chert has the most pronounced distribution of any mineral in the study area. The lower $2 / 3$ of the formation has approximately $3 \%$ chert per slide. Chert represents about $10 \%$ of each sample in the upper $1 / 3$ of the formation.

Anhedral crystals of ziron, tourmaline, and hematite are present in most of the samples. No significant changes in distribution for these minerals were found. Altered cubes of pyrite, distorted flakes of biotite, and anhedral and euhedral apatite were found preferentially distributed in the lower half of the formation.

The limestones examined represent freshwater lake deposits. Green-algae (Dasycladacean?), Charophytes, thin walled ostracodes, cryptalgal structures, and fecal pellets were found. Scholle (1978) describes Charophytes and thin walled ostrasodes as freshwater fauna. These are also present in the opal-chalcedony pebbles of the coarser upper samples. The pelletoidal limestone (Fig. 8) was used by West (1978) to correlate the Morrison beds in the Kenton area. The persistent redevelopment of lacustrine environments near the New MexicoOklahoma border suggests continuous subsidence along the Freezeout Creek Fault trend during Morrison deposition.

Cement

The most common cementing agents found in the thin section were


Fig. 7.-Algal limestone altered to opal and chalcedony, ( $0.7 \times 0.5 \mathrm{~mm} ; ~ p l a n e-p o l a r i z e d ~ l i g h t)$.


Fig. 8.-Pelletoidal limestone from the middle Morrison near Kenton, Oklahoma; pellets (P), calcite (Ca), ( $0.7 \times 0.5 \mathrm{~mm}$; crossed nicols).
calcite, quartz, opal and chalcedony. Kaolinite, hematite, and siderite were present in several slides but were of lesser importance as cement. In most samples more than one cement was present. Calcite occurs both as sparite and micrite. Sparite is more often the carbonate cement present in sandstones and micrite is present predominately in the lacustrine limestones. The silica minerals are the predominate cementing agent in the study area. Quartz occurs as quartz overgrowths. Chalcedony is found as fiberous radiating crystals. Opal is generally an amorphous groundmass. Floating contacts between detrital grains are often present when calcite, opal, or chalcedony are the cements (Fig. 9 and 10).

The vertical distribution of the cements fluctuated with changes in depositional environments. Carbonate cements dominate the middle Morrison. This changes to a silica rich cement as the lower sandstones and limestones are replaced by the better developed meandering streams near the top of the middle Morrison. The better sorted braided stream deposits of the upper section are cemented by silicas, carbonates, and authigenic clays. The poorly sorted sediments near the top of the stratigraphic section are cemented almost exclusively by silicas.

Several diagenetic relationships can be seen in the cementing material. In the sandstones overgrowths of quartz were the first cement present. It is found along grain boundaries or encircling the entire grain. Calcite was next and is found corroding the overgrowths and detrital grains. The lesser cements of hematite, siderite, and clays are found with interrelationships with calcite and is thought to have been developed about the same time. Opal and chalcedony are a third generation cement developed after calcite. These relationships are


Fig. 9.-Floating contacts between detrital grains in calcite cement; calcite (Ca), quartz (Q), ( $0.7 \times 0.5 \mathrm{~mm}$; crossed nicols).


Fig. 10.-Floating contacts between detrital grains in chalcedony cement; chalcedony (Ch), ( $0.7 \times 0.5 \mathrm{~mm}$; crossed nicols).
illustrated by Fig. 11 which shows micrite replaced by chalcedony and Fig. 12 of a corroded quartz grain encompassed by opal cement. Fig. 13 clearly illustrates the three generations of cement. A second sequence of calcite cement is found filling fractures which occur within the cemented rock (Fig. 14).

The increase in silica minerals, both in the cement and the detrital fraction, upward in the section suggest a more alkaline environment. Kruskopf (1967, p. 115) states that, "Any solution in contact with silicate minerals cannot long remain appreciably acid, and if contact is continued, the solution must eventually become alkaline." The following reaction illustrates this very well:

$$
4 \mathrm{KAlSi}_{3} \mathrm{O}_{8}+22 \mathrm{H}_{2} \mathrm{O} \rightarrow 4 \mathrm{~K}^{+}+4 \mathrm{OH}^{-}+\mathrm{Al}_{4} \mathrm{Si}_{4} \mathrm{O}_{10}(\mathrm{OH})_{8}+8 \mathrm{H}_{4} \mathrm{SiO}_{4} .
$$

Mankin (1958) reports an increase in volcanic activity during late Morrison deposition. The alteration of volcanic ash is thought to be the major contributor of the silica.

The $\left[K^{+}\right]$would be increased by this means if the volcanic ash were of an acidic origin. Changes in alkalinity and $\left[\mathrm{K}^{+}\right]$are the major reasons for fluctuations in illite and mixed-layer illite-montmorillonite development. Therefore, the clay mineral composition is associated with the volcanic ash composition and its subsequent alteration. The following chapter discusses the clay mineralogy of the Morrison.


Fig. 11.-Micrite replaced by chalcedony; micrite (M), chalcedony (Ch), ( $2.5 \times 1.7 \mathrm{~mm}$; plane-polarized light).


Fig. 12. -Quartz grain corroded by calcite in an opal cement; opal (Op), calcite (Ca), quartz (Qz), (0.7 X 0.5 mm ; crossed micols).


Fig. 13.-Three generations of cement; detrital quartz (Qd), quartz overgrowths (Qo), calcite (Ca), chalcedony (Ch), ( $0.19 \times 0.13 \mathrm{~mm}$; crossed nicols).


Fig. 14.-Calcite filled fractures; (2.5 X 1.7 mm ; cathodoluminescence).

## CHAPTER VII

## CLAY MINERALOGY

The clay mineralogy of the undifferentiated Morrison has been determined by Keller (1953) and Mankin (1958). The former described the clay minerals found in the new type section for the Morrison (Waldschmidt and LeRoy, 1944). The latter determined the clay mineral content of northeastern New Mexico.

Mankin's analysis of the Morrison divides the formation into two units according to the clay mineral content (Fig. 15). The lower unit is composed of montmorillonite, illite, and lesser amounts of kaolinite. The clay minerals of the upper unit, from his report, were kaolinite and a mixed-layer clay of montmorillonite-illite.

In this study 25 clay samples were collected from selected locations and stratigraphic positions. The analysis was conducted using a Philips-Norelco diffractometer. Untreated slides were first x-rayed and then treated with ethylene glycol for 24 hours to determine expansion properties. The samples were then heated for one hour at $500^{\circ} \mathrm{C}$ and reanalyzed. Methods described by Grim (1968) and Carroll (1970) were used in the clay mineral identification. The results are shown in Table IV. Sample set "F" was collected at Section 31, T31N, R33E (Mankin's, Dry Cimarron section and Cooley's, Pipeline Canyon section). This sample set was taken to determine the change in defraction patterns described by the previous investigation and to observe the


Fig. 15.-Fence diagram showing the distribution of clay mineral suites in northeastern New Mexico, modified after Mankin (1958).

TABLE IV
CLAY MINERAL COMPOSITION OF THE MORRISON FORMATION OF THE DRY CIMARRON RIVER VALLEY*

| Sample <br> Number | Kaolinite | Illite | Illite- <br> Montmorillonite <br> (mixed-1ayer) | Montmorillonite |
| :---: | :---: | :---: | :---: | :---: |
| A-1 | 66 | 25 | 9 | -- |
| A-2 | 50 | 32 | 18 | -- |
| A-3 | 37 | 33 | 30 | -- |
| A-4 | 35 | 32 | 33 | -- |
| A-5 | 21 | 36 | 43 | -- |
| A-6 | 21 | 35 | 44 | -- |
| A-7 | 15 | 60 | 25 | -- |
| A-8 | 10 | 26 | 64 | -- |
| A-9 | 42 | 13 | 45 | -- |
| A-10 | 65 | 23 | 12 | -- |
| B-1 | 14 | 33 | 53 | -- |
| B-2 | 57 | 9 | 34 | -- |
| B-3 | 45 | 9 | 46 | -- |
| C-1 | 78 | 3 | 18 | -- |
| C-2 | 62 | 13 | 25 | -- |
| C-3 | 22 | 26 | 52 | -- |
| C-4 | -- | 47 | 53 | -- |
| D-1 | -- | 75 | 25 | -- |
| E-1 | -- | 46 | 54 | -- |
| E-2 | -- | 60 | 40 | -- |
| F-1 | 5 | 81 | -- | 14 |
| F-2 | 7 | 66 | -- | 27 |
| F-3 | 3 | 8 | -- | 89 |
| F-4 | 3 | 47 | -- | 22 |
| F-5 | 40 | 42 | -- | 18 |

*Values present in the samp1e are in percent
stratigraphic position of the change.
The remaining samples were collected from the middle and upper Morrison near Kenton, Oklahoma. Sets "A" and "B" are a vertical sequence of Stovall's Labrier Butte and upper Morrison section. Sets "C", "D", and "E" were taken at outcrops which had higher than normal scintillometer readings.

The illite in both units is thought to be of the lMd type. The x-ray diffraction pattern is a poorly crystalline peak at a $10 A^{\circ}$. The montmorillonite in the lower unit expands to $17 A^{\circ}$ from $12 A^{\circ}$ when glycolated. The amount of kaolinite increases upward in the formation. The kaolinite is generally well crystalline, however poorly crystalline kaolinite was found in several samples. The mixed-layer clays have variable expansion characteristics according to the amounts of illite and montmorillonite present. The heated slides revealed no chlorite present.

The clay minerals which were present in the Kenton area were kaolinite, illite, and a mixed-layer illite-montmorillonite. The illite present exceeded the amount of mixed-layer clay in much of the lower middle Morrison of the area (Table IV). The illite content approximately equaled the mixed-layer clay in the upper units until kaolinite is the dominate clay mineral near the top of the section. In the lower part of the section, where illite is better developed, kaolinite also has better crystallinity and a higher concentration.

The change in clay mineral suites at the Dry Cimarron section occurs approximately 65 feet above the basal Morrison section. No evidence was found to suggest the occurrence of the lower clay mineral zone in Cimarron County. Therefore, it is doubtful that the basal

Morrison extends as far east as the Oklahoma-New Mexico border.
The regional analysis (Fig. 15) by Mankin (1958) suggests that the thicker Morrison sections in Harding and San Migue1 Counties, New Mexico, are the result of a thicker lower clay mineral zone. The upper unit was deposited with a relatively uniform thickness in the area. The thick Morrison section in Cimarron County, composed entirely of the upper clay mineral suite, is unique when compared to the uniform thicknesses observed to the southwest. This data supports the conclusion that the lower Morrison was overlapped by the upper Morrison and that much of the sediment transport shifted to the east of the monoclinal terrace during late Morrison deposition.

The foregoing conclusions should be considered only as general stratigraphic relationships. Since illite and montmorillonite are very susceptible to their geochemical environments (e.g. [ $\mathrm{K}^{+}$] as well as acid concentrations), each location has had different influences to produce the clay mineral suites present. Carroll and Starkey (1971) and Huang and Keller (1971) have demonstrated that selective clay minerals are more soluable in different types of acids. Generally, in an acidic environment, montmorillonite is more readly dissolved than illite, and kaolinite is more stable than either of the other two clays.

## CHAPTER VIII

## GEOCHEMISTRY

The samples for elemental analysis were prepared by crushing the samples in a ceramic jaw crusher and then pulverizing in a Spec Ball Mill using tungsten carbide balls and chamber. The samples were then seived to less than 80 mesh.

Elemental concentrations were determined for vanadium, cobalt, nickel, lead, copper, chromium, molydenum, iron, magnesium, strontium, zinc, titanium, silver, manganese, cadmium, and calcium. The samples were prepared by digesting 1 gm of sample in 20 ml of aqua regia ( $75 \%$ hydrocloric acid and $25 \%$ nitric acid). The solution was allowed to digest the rock for 24 hours; 6 hours of which the sample was heated to $100^{\circ} \mathrm{F}$. The resulting solution was filtered and then $1 \%$ lanthanum chloride was added. Each sample was then diluted to 50 ml with distilled water. Elemental analysis was conducted on 140 samples. Uranium concentrations were determined in 70 selected samples by Skyline Labs, Inc., Denver, Colorado. The results are presented in Appendix A.

Statistical Methods

A basic assumption used in analyzing the data was that different geochemical conditions were active in the different types of rocks (sandstones, shales, chert, and limestones). These varying conditions include Eh, pH , cation exchange capacity, and permeability. Therefore,
the raw data was divided into discrete populations according to lithology. A second assumption used in analyzing the data was that the populations were normally distributed.

Trace elements occur in nature with normal, gamma, or lognormal distributions (Krumbein and Graybill, 1965). The Kolmogorov-Smirnov test (Conover, 1971) was used to determine the type of distribution each element had within each population. The test compared the distribution of an element with a normal distribution. A maximum difference between the two distributions was computed. This $D_{\text {max }}$ value was compared to a critical value determined by the number of observations in the population and an acceptable level of statistical significance ( $\alpha=0.05$ ). The elements were found to be lognormally distributed in each lithology. Log base 10 was used for the transformation. The amount of each sample which did not go into solution (Resid) was found to be normally distributed.

A plot of uranium verses each of the elements by lithology revealed two discrete populations for uranium within the shale and limestone groups (e.g. Fig. 16). One population appeared to have normal background uranium concentrations and the other anomalously high uranium concentrations. A value of 100 ppm was chosen to delineate the boundary between the two groups. Further statistical analysis of the high uranium subgroup within the limestone group was not possible because only one observation was present.

Correlation matrices were calculated for each lithology and subgroup (Appendix B). A summary of the statistically significant correlations $(\alpha=0.05)$ from Appendix $B$ is presented in Table $V$.

Factor analysis (Morrison, 1967) was, also, conducted for each


TABLE V

## SUMMARY OF STATISTICALLY SIGNIFICANT CORRELATIONS


lithology and subgroup. This method of analysis was used to determine which elements were being influenced by the same geochemical factors. A second normality evaluation using the Lilliefors test was conducted prior to the factor analysis. The Lilliefors is a more conservative test for normality than the Kolmogorov-Smirnov test, because the empirical distribution function is obtained from a normalized sample and is unadjusted in the Kolmogorov-Smirnov test (Conover, 1971). Eigen values of 1.0 or greater were considered significant.

Results and Discussion

The correlation coefficients discussed below will be considered as follows:

$$
\begin{aligned}
<0.50 & =\text { low correlation } \\
0.50-0.65 & =\text { moderate correlation } \\
0.66-0.80 & =\text { high correlation } \\
0.81-1.00 & =\text { very high correlation. }
\end{aligned}
$$

Krauskopf (1956), Day (1963), Garre1s and Christ (1965), and Röster and Lange (1972), were used in the interpretation of the results.

High Uranium Shale

These samples were found in Section 3, T5N, R1ECM. Unlike most shales found within the Morrison sequence these samples were taken from an organic fissile shale. The depositional sequence was determined to be a lacustrine environment located on the down thrown side of the Freezeout Creek Fault, onto which a coarse conglomeratic sandstone was deposited. The organic rich shale was developed after the sandstone deposition ceased. Since the shale has a very localized
development, it is thought to have deposited as a peat bog with limited ground water circulation. The basal Cheyenne Sandstone was deposited directly above the shale. The contact between the two formations was found to be several feet lower at this location than in the surrounding area. The trend is thought to follow the paleocurrent direction (Fig. 5) and to have persisted into the Early Cretaceous deposition. Petrified wood fragments found in the basal Cheyenne are thought to have been confined to the subsiding area where the initial marine transgression would have taken place. A similar occurrence marking the Jurassic-Cretaceous boundary is found west of the monoclinal terrace near Folsom.

The association of uranium with carbonate forming cations (calcium, strontium, and magnesium) suggest that precipitation may have taken place as sexivalent uranium carbonate solutions were brought into reducing conditions. The correlation matrix and factor analysis revealed that uranium has a high correlation with titanium and lead (Fig. 17) and a high negative correlation with manganese. Many of the trace elements were transported as a $\mathrm{HCO}_{3}{ }^{-}$or $\mathrm{CO}_{3}{ }^{-}$complex and precipitation occurred principally as sulfides, oxides, and carbonates.

Low Uranium Shale

These samples represent the remaining analysis conducted on shales. The samples were gathered from the middle and upper Morrison near Kenton, Oklahoma.

The uranium is thought to have precipitated as a silicate in a slightly alkaline environment. Uranium has a high correlation coefficient with residual and moderate to high negative correlations were

LEAD VERSUS URANIUM FOR HIGH URANIUM SHALE NORMALIZED DATA BY LOG TRANSFORMATION SYMBOL IS VALUE OF CODE


Fig. 17.-Plot of urnaium versus lead for mineralized shale.
found between uranium and cadmium, manganese, strontium, silver, and calcium.

Chert

These samples were collected from Section 3, T5N, R1ECM. Field evidence suggests the chert was interbedded with the fresh water limestone located below the high uranium shale. The chert unit could be recognized over much of the SE $\frac{1}{4}$ of Section 3 by higher scintillometer readings. The unit forms a resistant layer to erosion and caps many of the lower hills in the $S E \frac{1}{4}$ of the section. The coarse sandstone located between the high uranium shale and the interbedded limestone and chert is also cemented by opal and chalcedony. King and Merriam (1969) suggest the origin of the "agate bed" may be due to devitrification of tuffaceous material. The increase in volcanic ash upward in the Morrison sequence (Mankin, 1958) would account for the increase in opal and chalcedony cement in the upper Morrison. Smith et al. (1970) have examined the organic content of cherts and have determined two ways in which fatty acids can be retained in chert. . The organic molecule may be enclosed within the chert matrix during deposition of the chert or the low permeability of chert (7-660 $\mu \mathrm{d}$ ) may prove to be impervious to the large organic molecules. Both of these mechanisms are thought to have been important at this locality.

The correlation matrix shows high correlations between uranium and iron, vanadium and molybdenum. Factor analysis also indicates a strong relationship between these minerals. The association of these minerals is most likely found in the organic material which Smith et al. (1970) termed "free fatty acids" found on the outer surface of the chert.

## Sandstone

The sandstone samples were collected from the middle and upper Morrison near Kenton, Oklahoma. Random samples from the thick Morrison section west of the monoclinal terrace (Fig. 6) are also included in the sandstone analysis.

The correlation matrix for sandstone contains many low and moderate correlations which were considered significant by the parameters previously selected $(\alpha=0.05)$. This relationship is created by a high variance within the population being analyzed. Subdivision of the population by different geologic parameters (e.g. stratigraphic position, cement, or grain size) did not lower the variance significantly. Therefore, the high variance may be a physical characteristic of the Morrison sandstones. This may reflect permeability of the sandstone, deposition in an alkaline-oxidizing environment (Squyres, 1970), or cation exchange capacity of the clays.

The sandstone correlation matrix shows uranium has a low positive correlation with nickel and molybdenum and a low negative correlation with residual. A moderate correlation between uranium and chromium is also shown.

## Limestone

The limestone samples were collected from the interbedded limestone and chert described previously and from the middle Morrison located along New Mexico State Highway 18 Section 18, T30N, R37E. Petrographic analysis has shown the samples were deposited in lacustrine environments.

The correlation matrix and factor analysis revealed no significant associations between uranium and any of the other elements. The limestone sample which had an anomalously high uranium reading also contained organic material which was visible in hand specimen and pyrite cubes which were visible in thin-section. The uranium was closely associated with the organic material and not as previously reported (Zeller et al., 1976) in the dark brown coating on the weathered surface.

## CHAPTER IX

## URANIUM POTENTIAL

The Morrison Formation in the study area contains several factors which are considered favorable criteria when exploring for sandstone uranium deposits (Grutt, 1972). The formation was deposited on an alluvial plain. The sandstone content increases upward in the section. The grain size increases in the upper Morrison sandstones and is often poorly sorted. Volcanic ash content also increases upward in the section. The sediment is interpreted as having had a source area composed of granite and sedimentary rock (Mankin, 1958). Structural dip is generally less than $5^{\circ}$ to the east. Paleocurrent data and an increase in grain size to the west suggest a sediment source associated with or similar to that for known uranium mineralization.

The investigation by Landis (1969) of the uranium content of ground and surface water for the area showed consistantly higher than normal concentrations for the samples closely associated with the Morrison. The highest readings were from near Kenton (Section 4, T5N, R1ECM), north of Boise City (Section 5, T5N, R5ECM), near Folsom (Section 28, T31N, R29E and Section 12, T31N, R31E), and in Las Animas County, Colorado (Section 34, T28S, R51W). The results of the ground water survey suggest that mineralization is more likely along the crest of the Sierra Grande Up1ift and east of the Freezeout Creek Fault near Kenton. This is in agreement with the results of the
helicopter-borne radiometric survey flown in the area.
Localized "hot spots". were reported (Baldwin and Mueh1berger, 1959) near the northwest corner of T29N, R33E. The area contained higher than normal background scintillometer readings, but a thick soil profile prevented the location of any mineralization. The reported "hot spots" along Tramperos Creek are thought to be associated with the Morrison. A specific location or strata was not determined.

Finch (1972), Baldwin and Muehlberger (1959), and the United States Atomic Energy Commission (1970) report that most of the known uranium occurrences are associated with petrified wood. Mineralization is also found with dinosaur bones, coaly shale, and carbonaceous trash. Squyres (1970) contributes the origin of the humate material in the "western" Morrison to oxidation and leaching of Jurassic plant material. He also discussed several lines of evidence which suggest a limited migration of the organic material after leaching.

Mankin (1958) observed that lacustrine limestones occurred most often with thick Morrison section and increased to the east. Cooley (1955) and Baldwin and Muehiberger (1959) have shown that sandstone development is confined to the area west of the Guy Monocline in the Dry Cimarron River Valley. It is suggested this is the result of depositional conditions rather than post-Morrison erosion. These areas were probably relatively low throughout much of the Morrison deposition. Therefore, such areas would be probable locations for plant growth and decay, as well as, accumulation of humate masses.

The preceding interrelationships suggest that uranium mineralization might be more likely in areas of subsidence during Morrison deposition. Schlee and Moench (1961) attribute similar circumstances to
the Jackpile Sandstone near Lahuna, New Mexico. The locations of known uranium mineralization are shown in Fig. 4 and Fig. 6. Most of these locations are associated with thick Morrison sequences. The isopach map (Fig. 6) shows two trends of thick Morrison development.

## The Kenton-Clayton Trend

The southern limit of the trend is located in the area of T 16 N , R31E which has a Morrison section of 516 feet. The region also has two locations of known uranium mineralization (Fig. 4). Near Stead, New Mexico, (T21-22N, R34-35E) Baldwin and Mueh1berger (1959) mapped a thick upper Morrison sandstone in the area, as well as reported localized "hot spots" along Tramperos Creek. The Herndon No. 1 Mock we11 located in NW $\frac{1}{4}$, Section 25 , T27N, R36E contains a Morrison section which is over 500 feet thick. The Morrison in the study area near Kenton, Oklahoma, contains 467 feet of section and two horizons of mineralization.

A comparison of Fig. 3 with Fig. 4 and Fig. 6 clearly illustrates that the trend of thicker Morrison sections are located parallel to mafor faults. Emphasis should be placed on the fact that it is not known if the subsidence along the faults is related to movement of the faults or compaction of sediment along the trends.

Since McLaugh1in (1954) did not find the thick Morrison section in western Baca County, the Jurassic stream systems may have been less confined or may have changed direction of the major drainage pattern away from the fault trends. Anderman (1961) and MacLachlan (1972) show a northeast trending trough which extends from $\mathrm{T} 35, \mathrm{R} 49 \mathrm{~W}$ to T28S, R43W and persisted from Mississippian through Jurassic
sedimentation. McKee et al. (1956) suggests that sandstone development continues in this direction.

## The Sierra Grande Trend

The southern part of the trend is the thick Morrison section found in T19-22N, R24-26E. Two locations of known uranium mineralization are associated with this area. The thick section is probably fault controlled (Fig. 3 and Fig. 6).

In the study area, the Morrison has a maximum thickness of 360 feet. One "hot spot" is reported in the northwest corner of T 29 N , R33E. Water samples from the Dry Cimarron Fiver contained 42 ppb (Section 28, T31N, R29E) and 23 ppb (Section 12, T31N, R31E). Background radiation readings on the scintillometer at the first location were 120-150 cps (average background $\simeq 60 \mathrm{cps}$ ). Two of the grab samples from this location contained significantly higher than background uranium concentrations but not anomalous (34 and 24 ppm ).

The northern limit of the trend is located in Bent County, Colorado. The area contains two known locations of mineralization (Finch, 1967). These are located in T27S, R53W and T27S, R51W. A water sample from the Cheyenne Sandstone (T28S, R51W) contained 50 ppb uranium. It is quite possible that chemical conditions in the upper Morrison might influence those in the lower Cheyenne aquifer. The thickness of the Morrison is not known for this area.

These three isolated exposures are thought to represent a continuous trend because the thicker Morrison of the exposures are bounded on the west by a thin Morrison along the axis of the Sierra Grande Uplift (Roberts et al., 1976, and Baltz, 1965). The Morrison thins to
the east of the trend on the monoclinal terrace. Therefore, the trend is projected into an area to the north in which the thickness is not known.

## The Monoclinal Terrace

The monoclinal terrace is situated between the Kenton-Clayton and Sierra Grande trends. The region is thought to have less potential for uranium mineralization than the areas to the east and west, which were described above. The monoclinal terrace contains no known uranium "hotspots" in the Morrison. The water samples from the Dry Cimarron River (Union County) and Carrizo Creek (Baca County) on the monoclinal terrace contained only background uranium concentrations. The radiometric survey located two small "hot spots" in the upper Dockum.

The locations are associated with the "clastic Plugs" (Parker, 1933) which are found where the Dry Cimarron River and its tributaries have exposed the upper Dockum on the monoclinal terrace (T31-32N, R33-37E). It is not known if these cylindrical structures were intruded from below and have the Baldy Hill Formation as a source or were collapse features and had the Jurassic formations as a source. Therefore, a comparison between the "clastic plugs" and Woodrow breccia pipe (Laguma District) should not be made at this time.

The boundaries of the monoclinal terrace in New Mexico and Oklahoma, are Precambrian faults on the east and Pennsylvanian faults on the west (Fig. 4). The southern limit is the Clapham Anticline in Union County.

The boundaries of the monoclinal terrace are less well defined in southeastern Colorado. The area in Fig. 4 between the Mustang Creek

Monocline and the Pennsylvanian fault (T29-32S, R51W) may be on the Sierra Grande trend or the monoclinal terrace. The area between the Precambrian faults (T27-34S, R49W) may be on the Kenton-Clayton trend or the monoclinal terrace. Additional information concerning the thickness and uranium content of the Morrison in these areas is needed.

## CHAPTER X

## CONCLUSIONS

## Summary

The principal conclusions of this study are as follows:

1) The Morrison was deposited on an alluvial plain which was composed of braided and meandering streams. Lacustrine limestones are found throughout the Morrison stratigraphic sequence and often redevelop in the same geographic area.
2) The grain size and feldspar content of the formation decrease from west to east across northeastern New Mexico into Oklahoma.
3) The clay mineralogy of the Morrison near Kenton, Oklahoma, was composed of kaolinite, illite, and a mixed-layer illite-montmorillonite. The clay minerals are equivalent to the assemblage previously reported (Mankin, 1958) for the middle and upper Morrison of New Mexico. Therefore, it is doubtful if the basal Morrison extends into Oklahoma from Union County, New Mexico.
4) It was found that the diagenetic sequence within the cements was quartz overgrowths, followed by calcite with lesser amounts of hematite, siderite, and clays, followed by chalcedony and opal replacing calcite, followed by a second generation of calcite cement.
5) The grain size of the upper Morrison is much larger than that of
the lower and middle Morrison. Some of the larger pebbles are undoubtedly reworked Morrison.
6) Sediment transport and deposition shifted to the east during late Morrison deposition.
7) Paleocurrent data from the middle and upper Morrison near Kenton, Oklahoma, have the same direction as the trend of the Three Corners Monocline. Therefore, sediment transport and deposition were structurally influenced.
8) Locations which have thicker Morrison sequences are closely related to changes in basement province and/or basement faults.
9) The monoclinal terrace, located along the eastern limits of the Sierra Grande Uplift, has little potential for uranium mineralization.
10) The Sierra Grande trend and Kenton-Clayton trend have the greatest potential for uranium mineralization.
11) Uranium has a very high correlation with titanium in the mineralized samples, a high correlation with lead, strontium, and magnesium, and a high negative correlation with manganese.
12) The uranium was closely associated with organic material which had been preserved by stratigraphic and low permeability barriers.
13) Future areas of study should include:
a) The Morrison in Baca and Las Animas Counties, Colorado;
b) The Morrison in the Raton Basin, Colfax County, New Mexico;
c) The relationship between the undifferentiated Morrison of the Front Range and the "western" Morrison.

## Recommendations

Exploratory drilling should first be conducted along the KentonClayton trend. This hypothesis is based on the following:

1) Volcanic activity increased during deposition of the upper Morrison.
2) Sedimentation shifted to the east during late Morrison deposition.
3) Precambrian faulting and Paleozoic structures strongly influenced the sedimentation.
4) Structural influence is more clearly seen along the KentonClayton trend than along the Sierra Grande trend because of more outcrop exposures.
5) Known uranium mineralization is closely associated with the upper Morrison along the Kenton-Clayton trend.

The southern half of the Kenton-Clayton trend from T21N, R34E to T27N, R36E in New Mexico and the Late Paleozoic trough in Baca County, Colorado, which Anderman (1961) and MacLachlan (1972) locate in T35S, R49W and T28S, R43W should be evaluated first. This trend is down the paleoslope from known uranium "hot spots" and extends into the area of mineralization described by Zeller et al. (1976). The northern part of the Sierra Grande trend should also be evaluated from the Dry Cimarron River Valley near Folsom, New Mexico, to Bent County, Colorado. The southern limits of the Sierra Grande and Kenton-Clayton trends are considered to have less potential for uranium mineralization because of previous exploration activity in those areas.

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APPENDIXES

APPENDIX A

GEOCHEMICAL ANALYSIS OF THE MORRISON FORMATION

GEOCHEMICAL ANALYSIS OF THE MORRISON FORMATION-----ELEMENTAL CONCENTRATIONS IN PPM, RESIDUAL IN GM

| OBS | SAMPLE | code |  |  | LOC |  | $u$ | PB | TI | FE | 2N | CU | MN | CR | NI | CO | mo | $v$ | CD | SR | AG | CA | MG | RESID |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | PA-1 | A | SE | SEC 3 | T5N | RIECM | 6.0 | 10 | 25 | 950 | 7.0 | 3.5 | 51.0 | 1 | 2 | 15 | 5 | 15.0 | 0.5 | 5.0 | 0.1 | 1000 | 135 | 0.8874 |
| 2 | PA-2 | B | SE | SEC3 | T5N | RIECM | 9.0 | 15 | 50 | 7000 | 19.5 | 8.0 | 215.0 | 1 | 2 | 10 | 5 | 30.0 | 0.5 | 15.0 | 0.5 | 1000 | 760 | 0.8664 |
| 3 | PA-4 | D | SE | SEC3 | T5N | RIECM | 28.0 | 25 | 50 | 3900 | 10.5 | 11.5 | 1650.0 | 1 | 10 | 10 | 10 | 45.0 | 5.0 | 175.0 | 3.5 | 56500 | 930 | 0.4243 |
| 4 | PA-6 | F | SE | SEC3 | T5N | R1ECM | - | 10 | 20 | 1675 | 10.0 | 7.5 | 10.0 | 1 | 2 | 2 | 10 | 7.5 | 1.0 | 5.0 | 0.5 | 500 | 515 | 0.8519 |
| 5 | PA-8 | H | SE | SEC3 | T5N | RIECM | 70.0 | 10 | 20 | 3925 | 12.5 | 8.0 | 36.5 | 1 | 2 | 2 | 10 | 35.0 | 1.0 | 10.0 | 1.0 | 2000 | 915 | 0.7323 |
| 6 | PA-11 | K | SE | SEC3 | T5N | R1ECM | 24.0 | 25 | 20 | 9400 | 19.5 | 10.0 | 96.5 | 1 | 10 | 45 | 15 | 45.0 | 1.0 | 10.0 | 1.0 | 750 | 510 | 0.8050 |
| 7 | PA-14 | N | SE | SEC3 | T5N | R1ECM | 0.5 | 10 | 20 | 700 | 10.0 | 9.5 | 24.5 | 1 | 2 | 5 | 5 | 15.0 | 1.5 | 5.0 | 0.5 | 500 | 370 | 0.8858 |
| 8 | PA-15 | 0 | SE | SEC3 | T5N | R1ECM | 80.0 | 15 | 25 | 15300 | 22.0 | 8.0 | 101.0 | 1 | 10 | 25 | 60 | 85.0 | 2.0 | 20.0 | 0.5 | 2750 | 565 | 0.8490 |
| 9 | PA-16 | P | SE | SEC3 | T5N | RIECM | 7.0 | 20 | 20 | 9100 | 27.5 | 8.5 | 197.5 | 1 | 2 | 10 | 10 | 20.0 | 1.5 | 15.0 | 0.5 | 1000 | 1070 | 0.9000 |
| 10 | MR-12 | L | NW | SEC 3 | T5N | RIECM | 3.0 | 5 | 20 | 1500 | 7.0 | 6.0 | 10.5 | 1 | 2 | 20 | 5 | 5.0 | 0.5 | 7.5 | 0.5 | 250 | 310 | 0.9122 |

- LITHO=LIMESTONE GP=LOW U
GBS SAMPLE CODE LOC U PB TI FE ZN CU MN CR NI CO MO V CD SR AG CA MG RESID

| 11 | PA-5 | E | SE | SEC 3 | T5N | RIECM |  | 30 | 50 | 2400 | 9.0 | 9.5 | 1975.0 | 1 | 2 | 5 | 10 | 20.0 | 5.0 | 305 | . | 6500 | 1410 | 0.2948 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | PA-23 | W | SW | SEC 3 | T5N | RIECM |  | 30 | 20 | 925 | 7.0 | 10.5 | 2750.0 | 5 | 10 | 25 | 10 | 20.0 | 6.5 | 335 | 5.0 | 75000 | 1020 | 0.0654 |
| 13 | PA-30 | X | SE | SEC 2 | T5N | RIECM |  | 20 | 20 | 11600 | 54.0 | 7.5 | 186.0 | 1 | 5 | 15 | 10 | 30.0 | 2.0 | 70 | 2.0 | 24000 | 1210 | 0.7511 |
| 14 | NM-2 | B | NE | SEC18 | T30N | R37E | 0.5 | 15 | 20 | 10600 | 30.5 | 7.5 | 1060.0 | 1 | 2 | 5 | 25 | 10.0 | 3.5 | 205 | 2.5 | 31000 | 3750 | 0.6320 |
| 15 | NM | D | NE | SEC18 | T30N | R37E | 7.0 | 15 | 20 | 11100 | 47.5 | 14.5 | 210.5 | 1 | 2 | 5 | 45 | 12.5 | 2.5 | 215 | 1.5 | 19000 | 2875 | 0.7805 |
| 16 | NM- | E | NE | SEC 18 | T30N | R37E | 15.0 | 20 | 20 | 4350 | 12.5 | 9.0 | 975.0 | 5 | 2 | 5 | 10 | 10.0 | 4.0 | 310 | 2.5 | 28500 | 1525 | 0.6051 |
| 17 | NM-8 | G | NE | SEC18 | T30N | R37E | 8.0 | 15 | 20 | 9000 | 34.0 | 5.0 | 330.0 | 1 | 2 | 10 | 2 | 10.0 | 1.5 | 105 | 1.0 | 14000 | 11750 | 0.7834 |
| 18 | NM-9 | H | NE | SEC18 | T30N | R37E | 3.0 | 20 | 20 | 9700 | 30.0 | 10.5 | 550.0 | 5 | 2 | 10 | 2 | 20.0 | 2.0 | 105 | 1.5 | 20500 | 11000 | 0.7137 |
| 19 | NM-10 | I | NE | SEC18 | T30N | R37E | 5.0 | 35 | 20 | 15400 | 40.0 | 10.0 | 1985.0 | 5 | 5 | 15 | 2 | 20.0 | 4.0 | 170 | 3.0 | 37000 | 7250 | 0.4569 |
| 20 | NM-12 | K | NE | SEC18 | T30N | R37E | 0.5 | 40 | 20 | 21700 | 64.5 | 13.0 | 1750.0 | 10 | 15 | 20 | 5 | 15.0 | 4.0 | 145 | 3.0 | 36000 | 4000 | 0.4961 |
| 21 | NM-15 | N | NE | SEC18 | T30N | R37E | 4.0 | 20 | 20 | 10100 | 37.5 | 10.0 | 100.0 | 1 | 5 | 5 | 2 | 5.0 | 1.0 | 25 | 1.0 | 12000 | 940 | 0.8066 |



| OBS | SAMPLE | Code |  |  |  | LOC | $u$ | PB | TI | FE | 2N | cu | MN | CR | NI | CO | MD | $v$ | CD | SR | AG | CA |  | RESID |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 35 | AB-49 | W | NE | SEC 3 | T5N | RIECM | - | 5.0 | 20 | 2450 | 12.0 | 8.5 | 133.0 | 1 | 2 | 5 | 5 | 15.0 | 1.5 | 2.5 | 0.5 | 500 | 290 | 0.9459 |
| 36 | AB-50 | X | NE | SEC 3 | T5N | RIECM | . | 5.0 | 20 | 1675 | 7.0 | 6.0 | 9.0 | 1 | 2 | 5 | 5 | 10.0 | 1.0 | 2.5 | 0.1 | 250 | 180 | 0.9638 |
| 37 | PA-3 | C | SE | SEC3 | I5N | RIECM | 13.0 | 15.0 | 20 | 1675 | 12.5 | 6.5 | 29.5 | 1 | 2 | 5 | 10 | 15.0 | 1.0 | $5 \pm 0$ | 0.5 | 250 | 255 | 0.9066 |
| 38 | PA-7 | G | SE | SEC 3 | T5N | RIECM | . | 10.0 | 20 | 1750 | 13.0 | 8.0 | 21.0 | 1 | 2 | 2 | 5 | 20.0 | 1.0 | 10.0 | 0.5 | 500 | 300 | 0.9316 |
| 39 | PA-9 | I | SE | SEC 3 | T5N | RIECM | . | 5.0 | 20 | 1150 | 6.5 | 3.0 | 35.5 | 1 | 2 | 2 | 5 | 20.0 | 0.5 | 1.0 | 1.0 | 250 | 125 | 0.9563 |
| 40 | PA-12 | 1 | SE | SEC 3 | T5N | RIECM | 0.5 | 10.0 | 20 | 10200 | 23.0 | 4.0 | 136.5 | 1 | 2 | 5 | 5 | 45.0 | 1.5 | 25.0 | 1.5 | 14000 | 680 | 0.8428 |
| 41 | PA-13 | M | SE | SEC 3 | T5N | RIECM | - | 5.0 | 20 | 3200 | 12.0 | 7.0 | 50.5 | 1 | 2 | 5 | 5 | 15.0 | 1.5 | 2.5 | 0.5 | 500 | 350 | 0.9580 |
| 42 | PA-17 | $Q$ | SE | SEC 3 | T5N | RIECM | 0.5 | 5.0 | 20 | 2300 | 7.5 | 3.0 | 51.5 | 1 | 2 | 20 | 10 | 30.0 | 1.0 | 5.0 | 16.5 | 250 | 100 | 0.9274 |
| 43 | PA-19 | 5 | SW | SEC2 | T5N | RIECM | . | 10.0 | 25 | 2200 | 16.0 | 8.5 | 99.0 | 1 | 2 | 10 | 5 | 10.0 | 1.0 | 5.0 | 0.5 | 8500 | 425 | 0.8846 |
| 44 | PA-20 | T | SW | SEC 3 | T5N | RIECM | - | 10.0 | 20 | 1600 | 5.0 | 4.5 | 44.5 | 1 | 2 | 10 | 10 | 20.0 | 1.5 | 7.5 | 0.5 | 4250 | 225 | 0.9377 |
| 45 | PA-22 | $v$ | SW | SEC 3 | T5N | RIECM | - | 10.0 | 20 | 1950 | 3.5 | 13.0 | 10.5 | 1 | 2 | 10 | 5 | 10.0 | 0.5 | 5.0 | 0.5 | 1250 | 1120 | 0.8524 |
| 46 | PA-31 | Y | SE | SEC 2 | T5N | R1ECM | - | 5.0 | 20 | 5100 | 16.0 | 5.5 | 92.5 | 1 | 2 | 5 | 10 | 15.0 | 1.0 | 10.0 | 0.5 | 6500 | 400 | 0.9203 |
| 47 | PA-32 | 1 | SE | SEC2 | T5N | RLECM | - | 10.0 | 20 | 1100 | 6.5 | 6.0 | 7.5 | 1 | 2 | 2 | 10 | 2.0 | 0.2 | 2.5 | 0.5 | 750 | 695 | 0.9375 |
| 48 | PA-34 | 3 | SE | SEC2 | T5N | RIECM | - | 0.2 | 20 | 2500 | 6.5 | 5.0 | 2.0 | 1 | 2 | 2 | 5 | 5.0 | 0.5 | 1.0 | 0.5 | 250 | 175 | 0.9542 |
| 49 | PA-3.5 | 4 | SE | SEC2 | T5N | RIECM | - | 10.0 | 20 | 1600 | 9.5 | 12.0 | 32.5 | 1 | 2 | 2 | 5 | 10.0 | 0.5 | 1.0 | 0.5 | 250 | 220 | 0.9420 |
| 50 | PA35A | 5 | SE | SEC2 | T5N | RIECM |  | 15.0 | 20 | 2700 | 13.5 | 6.0 | 27.5 | 1 | 2 | 2 | 5 | 10.0 | 0.5 | 1.0 | 0.5 | 250 | 280 | 0.9465 |
| 51 | NM-1 | A | NE S | SEC18 | T30N | R37E | 2.0 | 25.0 | 25 | 3400 | 23.0 | 9.0 | 39.0 | 1 | 2 | 2 | 35 | 15.0 | 1.5 | 50.0 | 1.0 | 5500 | 1860 | 0.8108 |
| 52 | NM-13 | L | NE S | SEC18 | T30N | R37E | 2.0 | 15.0 | 20 | 3700 | 18.0 | 11.0 | 17.5 | 1 | 2 | 5 | 2 | 15.0 | 0.5 | 15.0 | 0.5 | 8000 | 615 | 0.9038 |
| 53 | NM-17 | P | NE S | SEC18 | T30N | R37E | 0.5 | 15.0 | 20 | 6400 | 13.0 | 12.5 | 76.0 | 1 | 2 | 5 | 5 | 10.0 | 1.0 | 40.0 | 0.5 | 8000 | 1005 | 0.8423 |
| 54 | NM-19 | R | NE S | SEC18 | T30N | R37E | 0.5 | 15.0 | 20 | 8700 | 37.0 | 7.0 | 240.0 | 1 | 2 | 5 | 2 | 15.0 | 1.0 | 27.5 | 1.0 | 6500 | 775 | 0.8536 |
| 55 | RL-1 | A | NH S | SEC12 | T5N R | RIECM |  | 10.0 | 20 | 3350 | 9.5 | 6.0 | 76.5 | 1 | 2 | 2 | 5 | 15.0 | 0.5 | 5.0 | 0.5 | 500 | 20 | 0.9538 |
| 56 | RL-2 | B | NW S | SEC12 | T5N | RIECM | - | 35.0 | 20 | 20400 | 38.0 | 8.5 | 5550.0 | 1 | 5 | 10 | 2 | 25.0 | 4.0 | 285.0 | 3.5 | 37000 | 50500 | 0.2406 |
| 57 | RL-3 | C | NW S | SEC12 | T5N | R1ECM | - | 10.0 | 20 | 13000 | 11.0 | 10.5 | 40.5 | 1 | 2 | 2 | 2 | 30.0 | 0.5 | 10.0 | 0.5 | 1000 | 1000 | 0.9177 |
| 58 | RL-4 | D | NW S | SEC12 | T5N | R1ECM | - | 20.0 | 20 | 1300 | 3.5 | 10.0 | 6.0 | 1 | 2 | 2 | 2 | 10.0 | 0.5 | 5.0 | 0.5 | 750 | 580 | 0.9379 |
| 59 | RL-6 | F | SE S | SEC11 | T5N | RIECM | 0.5 | 25.0 | 20 | 7800 | 24.5 | 5.0 | 725.0 | 5 | 2 | 10 | 5 | 10.0 | 2.0 | 60.0 | 1.5 | 24000 | 2250 | 0.7448 |
| 60 | RL-7A | H | SE S | SEC11 | T5N | R1ECM | 0.5 | 10.0 | 20 | 1700 | 13.5 | 3.0 | 21.5 | 1 | 2 | 2 | 5 | 10.0 | 0.2 | 5.0 | 0.5 | 250 | 115 | 0.9661 |
| 61 | RL-10 | 1 | SE S | SEC14 | T5N | R1.ECM | - | 5.0 | 20 | 750 | 7.0 | 3.0 | 4.0 | 1 | 2 | 2 | 2 | 5.0 | 2.0 | 15.0 | 0.5 | 2500 | 980 | 0.9109 |
| 62 | RL-11 | M | SE S | SEC14 | T5N | R1ECM | - | 5.0 | 20 | 450 | 3.5 | 3.5 | 8.5 | 1 | 2 | 2 | 2 | 2.0 | 1.5 | 10.0 | 0.5 | 750 | 405 | 0.9647 |
| 63 | RL-12 | N | SE S | SEC14 | T5N | R1ECM | 0.5 | 30.0 | 200 | 3300 | 13.5 | 7.0 | 300.0 |  | 5 | 10 | 2 | 30.0 | 3.5 | 80.0 | 2.5 | 27000 | 915 | 0.6915 |
| 64 | RL-13 | 0 | SE S | SEC14 | T5N | R1ECM | - | 30.0 | 20 | 23800 | 15.5 | 5.5 | 450.0 | 1 | 5 | 5 | 2 | 160.0 | 2.0 | 35.0 | 1.0 | 7000 | 6500 | 0.8129 |
| 65 | RL-14 | P | SE S | SEC14 | T5N | RIECM | 0.5 | 15.0 | 20 | 2200 | 8.5 | 4.0 | 250.0 | 1 | 10 | 10 | 2 | 10.0 | 3.5 | 55.0 | 2.0 | 27000 | 6000 | 0.6985 |
| 66 | RL-15 | Q | SW S | SEC13 | T5N | RIECM | . | 10.0 | 25 | 1650 | 5.5 | 3.0 | 17.5 | 1 | 5 | 5 | 2 | 5.0 | 1.0 | 15.0 | 1.0 | 7250 | 300 | 0.9328 |
| 67 | RL-16 | R | SW S | SEC 13 | T5N | R1ECM | - | 10.0 | 25 | 4000 | 6.5 | 7.0 | 3.5 | 1 | 2 | 5 | 2 | 15.0 | 0.5 | 15.0 | 0.5 | 750 | 375 | 0.9192 |
| 68 | RL-17 | S | SH S | SEC13 | T5N | R1ECM | 0.5 | 10.0 | 25 | 7900 | 4.5 | 2.0 | 2.0 | 1 | 2 | 5 | 5 | 30.0 | 1.0 | 20.0 | 0.5 | 1000 | 425 | 0.9528 |
| 69 | RL-19 | U | SW S | SEC13 | T5N | R1ECM | 0.5 | 15.0 | 25 | 4500 | 10.0 | 16.5 | 16.5 | 1 | 2 |  | 2 | 30.0 | 1.0 | 5.0 | 1.0 | 6000 | 1465 | 0.8728 |
| 70 | MJ-1 | A | NW S | SEC10 | T5N | R1ECM | . | 5.0 | 50 | 1375 | 7.5 | 5.5 | 14.0 | 1 | 2 | 10 | 5 | 2.0 | 0.5 | 10.0 | 0.5 | 750 | 205 | 0.9457 |
| 71 | MJ-2 | B | NW | SEC10 | T5N | PIECM | - | 10.0 | 20 | 1450 | 7.5 | 4.0 | 4.5 | 1 | 2 | 10 | 5 | 2.0 | 0.5 | 5.0 | 0.5 | 750 | 235 | 0.9600 |
| 72 | MJ-3 | C | NW S | SEC10 | T5N | R1ECM | - | 15.0 | 50 | 11400 | 23.0 | 5.5 | 95.0 | 1 | 2 | 15 | 5 | 20.0 | 1.5 | 45.0 | 1.5 | 18000 | 1200 | 0.6644 |
| 73 | MJ-5 | E | NW S | SEC10 | T5N | R1ECM | - | 5.0 | 20 | 7000 | 16.5 | 7.0 | 43.0 | 1 | 2 | 5 | 5 | 10.0 | 0.2 | 7.5 | 0.3 | 250 | 350 | 0.9383 |
| 74 | MJ-7 | G | NW | SEC10 | T5N | R1ECM | - | 10.0 | 20 | 950 | 6.0 | 3.5 | 34.5 | 1 | 2 | 5 | 5 | 10.0 | 0.5 | 15.0 | 0.5 | 9000 | 385 | 0.8959 |
| 75 | MJ-8 | H | NW S | SEC 10 | T5N | R1ECM | - | 25.0 | 20 | 800 | 6.0 | 4.5 | 120.0 | 1 | 2 | 2 | 2 | 10.0 | 0.5 | 5.0 | 0.1 | 250 | 135 | 0.9400 |
| 76 | MJ-10 | $J$ | NH S | SEC10 | 15N | R1ECM |  | 15.0 | 20 | 16900 | 43.0 | 12.5 | 287.5 | 1 | 10 | 5 | 10 | 240.0 | 1.5 | 15.0 | 0.5 | 250 | 310 | 0.8499 |
| 77 | MR-1 | A | NW | SEC 3 | T5N | R1ECM | 0.5 | 10.0 | 20 | 2450 | 14.5 | 4.0 | 60.0 | 1 | 2 | 2 | 5 | 5.0 | 1.5 | 15.0 | 0.5 | 5500 | 805 | 0.8382 |
| 78 | MR-2 | B | NH | SEC3 | T5N | RIECM | 0.5 | 20.0 | 20 | 9600 | 35.0 | 7.0 | 840.0 | 1 | 5 | 10 | 2 | 15.0 | 4.0 | 150.0 | 2.0 | 22500 | 12500 | 0.7137 |
| 79 | MR-3 | C | NW | SEC 3 | T5N | RIECM | 0.5 | 10.0 | 20 | 8700 | 18.0 | 13.5 | 87.5 | 1 | 2 | 5 | 2 | 10.0 | 1.0 | 25.0 | 0.5 | 3500 | 1000 | 0.9066 |
| 80 | MR-4 | D | NW | SEC3 | T5N | RIECM | 0.5 | 25.0 | 25 | 12600 | 37.5 | 5.0 | 425.0 | 1 | 2 | 25 | 5 | 35.0 | 4.5 | 70.0 | 2.0 | 23500 | 25000 | 0.7418 |
| 81 | MR-5 | E | NW | SEC 3 | T5N | R1ECM | 0.5 | 5.0 | 20 | 650 | 5.0 | 5.0 | 15.0 | 1 | 2 | 5 | 2 | 5.0 | 1.5 | 5.0 | 0.5 | 250 | 120 | 0.8988 |
| 82 | MR-6 | F | NW | SEC3 | T5N | RIECM | - | 10.0 | 20 | 1500 | 6.0 | 4.0 | 9.0 | 1 | 2 | 5 | 2 | 5.0 | 1.0 | 5.0 | 0.5 | 125 | 100 | 0.9525 |
| 83 | MR-7 | G | NH | SEC3 | T5N | R1ECM | - | 15.0 | 20 | 2850 | 8.5 | 6.5 | 18.5 | 1 | 2 | 5 | 5 | 7.5 | 1.0 | 5.0 | 0.5 | 1000 | 205 | 0.9552 |
| 84 | MR-8 | H | NW | SEC3 | T5N | R1ECM | - | 20.0 | 20 | 8000 | 21.0 | 9.5 | 93.0 | 1 | 2 | 10 | 5 | 20.0 | 1.5 | 30.0 | 1.0 | 13000 | 655 | 0.8679 |
| 85 | MR-9 | I | NW | SEC3 | T5N | R1ECM | 0.5 | 10.0 | 20 | 3450 | 14.5 | 5.0 | 54.0 | 1 | 2 | 10 | 2 | 15.0 | 0.5 | 5.0 | 0.5 | 250 | 160 | 0.9277 |
| 86 | MR-10 | $J$ | Nw | SEC3 | T5N R | R1ECM | 0.5 | 10.0 | 20 | 2800 | 11.0 | 6.0 | 122.5 | 1 | 5 | 10 | 2 | 15.0 | 2.5 | 30.0 | 1.5 | 15500 | 755 | 0.8125 |

GEOCHEMICAL ANALYSIS OF THE MORRISON FORMATION----ELEMENTAL CONCENTRATIONS IN PPM, RESIDUAL IN GM

| OBS | SAMPLE | code |  |  |  | LOC | $u$ | PB | TI | FE | ZN | CU | MN | CR | NI | CO | MO | $v$ | $C D$ | SR | AG | CA | MG | RESID |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 87 | MR-11 | K | NH | SEC3 | T5N | RIECM | 0.5 | 15 | 20 | 1150 | 8.0 | 6.5 | 21.0 | 1 |  | 10 | 2 | 10 | 1.0 | 7.5 | 0.5 | 750 | 340 | 0.9624 |
| 88 | MR-13 | M | NW | SEC3 | T5N | RIECM | 0.5 | 10 | 25 | 3250 | 6.5 | 7.0 | 35.0 | 1 |  | 10 | 5 | 10 | 1.0 | 10.0 | 0.5 | 750 | 775 | 0.9307 |
| 89 | EA-2 | B | SH | SEC18 | T5N | R2ECM | - | 15 | 25 | 13500 | 43.5 | 11.5 | 725.0 | 1 |  | 15 | 5 | 10 | 1.0 | 45.0 | 0.5 | 7000 | 885 | 0.8986 |
| 90 | EA-5 | E | SW | SEC18 | T5N | R2ECM | - | 20 | 20 | 1050 | 27.5 | 9.0 | 22.0 | 5 | 2 | 5 | 2 | 15 | 2.5 | 190.0 | 2.0 | 30000 | 1405 | 0.9111 |
| 91 | EA-6 | F | SW | SEC 18 | 15N | R2ECM | - | 50 | 20 | 23000 | 43.0 | 29.0 | 925.0 | 5 | 20 | 15 | 15 | 135 | 7.0 | 250.0 | 2.0 | 3150 | 6750 | 0.6107 |
| 92 | EA-7 | G | Sh | SEC18 | T5N | R2ECM | - | 25 | 20 | 23800 | 67.0 | 10.5 | 460.0 | 5 | 5 | 5 | 5 | 40 | 6.0 | 320.0 | 2.5 | 34500 | 22500 | 0.5055 |
| 93 | EA-7A | H | SH | SEC 18 | T5N | R2ECM | - | 15 | 20 | 1350 | 10.0 | 16.0 | 21.0 | 1 | 2 | 2 | 5 | 10 | 1.0 | 30.0 | 0.5 | 4250 | 850 | 0.9664 |
| 94 | EA-8 | 1 | SW | SEC18 | T5N | R2ECM | - | 10 | 20 | 4500 | 12.0 | 10.5 | 27.0 | 1 | 2 | 5 | 5 | 5 | 1.0 | 90.0 | 0.5 | 7500 | 2500 | 0.8957 |
| 95 | EA-9 | $k$ | SW | SEC23 | T5N | RIECM | - | 5 | 20 | 1800 | 10.5 | 8.0 | 107.5 | 1. |  | 5 | 2 | 5 | 1.5 | 5.0 | 0.8 | 7500 | 415 | 0.5350 |
| 96 | EA-11 | 4 | SW | SEC 23 | T5N | R1ECM | - | 20 | 20 | 10900 | 33.0 | 5.5 | 1350.0 | 1 |  | 15 | 2 | 15 | 2.5 | 220.0 | 2.0 | 24500 | 18250 | 0.6893 |
| 97 | EA-13 | 0 | SW | SEC23 | T5N | R1ECM | 0.5 | 10. | 20 | 2150 | 8.5 | 4.5 | 42.5 | 1 |  | 5 | 5 | 2 | 0.5 | 5.0 | 0.5 | 125 | 105 | 0.9602 |
| 98 | FL-3 | B |  | SEC 29 | T30N | R29E | 2.0 | 20 | 20 | 3700 | 9.0 | 52.5 | 127.5 | 1 | 10 | 15 | 2 | 10 | 1.0 | 70.0 | 0.8 | 3750 | 1920 | 0.9292 |
| 99 | FL-4 | C |  | SEC 29 | T30N | R29E | 34.0 | 35 | 20 | 4700 | 19.0 | 10.5 | 3635.0 | 10 | 15 | 25 | 5 | 15 | 4.5 | 280.0 | 3.3 | 38500 | 3500 | 0.4754 |
| 100 | FL-5 | D |  | SEC 29 | T30N | R29E | 24.0 | 40 | 20 | 4150 | 16.5 | 10.0 | 5700.0 | 10 | 20 | 20 | 5 | 25 | 4.5 | 315.0 | 3.5 | 48000 | 3250 | 0.3838 |
| 101 | FL-6 | E |  | SEC 29 | T30N | R29E | 3.0 | 15 | 20 | 1650 | 7.5 | 3.0 | 74.0 | 1 | 10 | 5 | 5 | 10 | 0.5 | 45.0 | 0.5 | 7000 | 1280 | 0.9318 |

LITHO=SHALE GP=LOWU

| OBS | SAMPLE | CODE |  |  |  | LOC | U | PB | TI | FE | 2N | cu | MN | CR | NI | CO | MO | $v$ | CD | SR | AG | CA | MG | RESID |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 22 | AB-27 | 1 | NE | SEC3 | 15N | RIECM |  | 10 | 25 | 8000 | 8.0 | 3. | 18.0 | 1 | 2 | 15 | 5 | 10.0 | 1.0 | 30.0 | 0.5 | 5000 | 840 | 0.9222 |
| 103 | AB-29 | $k$ | NE | SEC3 | T5N | RIECM | 3.0 | 5 | 20 | 3800 | 2.5 | 6.0 | 4.5 | 1 | 2 | 5 | 5 | 10.0 | 1.5 | 15.0 | 1.0 | 1625 | 935 | 0.9415 |
| 104 | AB-46 | T | NE | SEC 3 | 15N | R1ECM | 3.0 | 10 | 100 | 22000 | 30. 0 | 10.5 | 16.0 | 1 | 2 | 5 | 5 | 30.0 | 0.5 | 40.0 | 0.5 | 4000 | 1445 | 0.8480 |
| 105 | PA-10 | J | SE | SEC3 | T5N | R1ECM |  | 15 | 50 | 19200 | 12.5 | 11.5 | 60.5 | 1 | 2 | 2 | 5 | 65.0 | 1.0 | 35.0 | 1.0 | 11000 | 885 | 0.8583 |
| 106 | PA-18 | R | SH | SEC2 | T5N | RIECM | 0.5 | 15 | 20 | 12300 | 24.5 | 30.5 | 360.0 | 1 | 2 | 10 | 5 | 25.0 | 3.0 | 50.0 | 1.3 | 20000 | 1635 | 0.7817 |
| 107 | PA-21 | U | SH | SEC3 | T5N | RIECM |  | 10 | 20 | 650 | 3.0 | 3.0 | 342.5 | 1 | 2 | 10 | 5 | 2.0 | 1.5 | 60.0 | 1.0 | 14500 | 480 | 0.8498 |
| 108 | PA31A | z | SE | SEC2 | T5N | RIECM |  | 10 | 20 | 8500 | 14.0 | 15.5 | 19.5 | 1 | 2 | 2 | 10 | 10.0 | 0.5 | 15.0 | 0.5 | 1750 | 745 | 0.8908 |
| 109 | PA-33 | 2 | SE | SEC 2 | T5N | RIECM |  | 10 | 20 | 1850 | 5.5 | 14.0 | 10.0 | 1 | 2 | 2 | 10 | 10.0 | 0.5 | 12.5 | 0.5 | 3250 | 1250 | 0.9102 |
| 110 | NM-6 | F | NE | SEC18 | T30N | R37E | 2.0 | 30 | 20 | 900 | 9.5 | 13.5 | 10.5 | 1 | 2 | 2 | 2 | 15.0 | 1.5 | 15.0 | 0.8 | 750 | 1645 | 0.8761 |
| 111 | NM-11 | J | NE | SEC 18 | T30N | R37E | 3.0 | 15 | 25 | 11200 | 34.5 | 8.5 | 128.5 | 5 | 5 | 10 | 2 | 10.0 | 1.0 | -20.0 | 0.8 | 9500 | 995 | 0.8860 |
| 112 | NM-14 | M | NE | SEC18 | T30N | R37E | . 0 | 15 | 20 | 4450 | 20.0 | 7.5 | 21.0 | 1 | 2 | 5 | 2 | 5.0 | 0.5 | 15.0 | 0.5 | 6000 | 640 | 0.8998 |
| 113 | NM-16 | 0 | NE | SEC18 | T30N | R37E | 2.0 | 20 | 20 | 7300 | 34.5 | 16.5 | 24.0 | 1 | 2 | 2 | 2 | 15.0 | 1.0 | 30.0 | 1.0 | 8500 | 840 | 0.8242 |
| 114 | NM-18 | $Q$ | NE | SEC 1-8 | T30N | R37E | 0.5 | 20 | 20 | 10200 | 33.0 | 8.5 | 68.5 | 1 | 2 | 2 | 2 | 15.0 | 1.0 | 30.0 | 1.0 | 7500 | 895 | 0.8535 |
| 115 | RL-5 | E | SE | SEC 11 | T5N | RIECM |  | 35 | 20 | 3550 | 8.0 | 21.0 | 550.0 | 1 | 2 | 5 | 5 | 20.0 | 2.0 | 85.0 | 2.0 | 17500 | 1925 | 0.7250 |
| 116 | RL-7 | G | SE | SEC 11 | T5N | RIECM | 0.5 | 20 | 20 | 13500 | 21.5 | 28.5 | 350.0 | 5 | 2 | 5 | 2 | 30.0 | 2.0 | 80.0 | 1.5 | 25000 | 2500 | 0.7495 |
| 117 | RL-78 | I | SE | SEC11 | T5N | RIECM | 8.0 | 30 | 20 | 1100 | 10.5 | 12.5 | 8.0 | 1 | 2 | 2 | 2 | 10.0 | 0.2 | 10.0 | C. 5 | 750 | 315 | 0.9432 |
| 118 | RL-8 | $J$ | NE | SEC 15 | T5N | R1ECM | 2.0 | 15 | 25 | 11500 | 13.0 | 15.5 | 325.0 | 5 | 2 | 2 | 2 | 15.0 | 1.0 | 95.0 | 1.0 | 20500 | 3125 | 0.7901 |
| 119 | RL-9 | K | NE | SEC15 | T5N | RIECM | 3.0 | 25 | 20 | 9500 | 21.0 | 19.0 | 208.0 | 1 | 2 | 5 | 5 | 0.5 | 1.5 | 35.0 | 0.5 | 3200 | 2500 | 0.9421 |
| 120 | RL-18 | $T$ | SW | SEC13 | T5N | RIECM | 0.5 | 5 | 25 | 8800 | 7.0 | 9.5 | 66.5 | 1 | 2 | 10 | 2 | 15.0 | 1.0 | 55.0 | 1.0 | 6000 | 1255 | 0.8858 |
| 121 | MJ-4 | D | NW | SEC 10 | T5N | RIECM |  | 15 | 20 | 3800 | 9.5 | 25.0 | 11.0 | 1 | 2 | 5 | 5 | 5.0 | 0.5 | 15.0 | 0.5 | 1250 | 1640 | 0.9028 |
| 122 | MJ-6 | F | NH | SEC10 | T5N | RIECM |  | 15 | 20 | 8500 | 7.0 | 24.5 | 7.5 | 1 | 2 | 5 | 2 | 15.0 | 0.2 | 20.0 | 0.5 | 2000 | 1200 | 0.7968 |
| 123 | MJ-9 | 1 | NW | SEC 10 | T5N | RIECM |  | 30 | 20 | 7000 | 17.0 | 10.5 | 7.0 | 1 | 5 | 5 | 2 | 10.0 | 0.5 | 15.0 | 0.3 | 1500 | 860 | 0.9090 |
| 124 | MJ-11 | K | NH | SEC 10 | T5N | RIECM |  | 15 | 20 | 7700 | 14. 5 | 32.0 | 25.5 | 1 | 10 | 2 | 5 | 45.0 | 1.5 | 30.0 | 0.5 | 2000 | 800 | 0.9163 |
| 125 | EA-1 | A | SH | SEC18 | T5N | R2ECM |  | 20 | 20 | 14100 | 18.0 | 23.5 | 50.5 | 5 | 10 | 10 | 5 | 25.0 | 1.0 | 85.0 | 0.5 | 10500 | 2750 | 0.8327 |
| 126 | EA-3 | C | SW | SEC 18 | T5N | R2ECM |  | 15 | 20 | 9800 | 11.0 | 13.0 | 14.0 | 1 | 2 | 2 | 5 | 20.0 | 0.5 | 40.0 | 0.5 | 2000 | 1455 | 0.9433 |
| 127 | EA-4 | 0 | SW | SEC18 | T5N | R2ECM |  | 10 | 20 | 2300 | 9.5 | 21.5 | 20.0 | 1 | 2 | 5 | 2 | 15.0 | 1.0 | 30.0 | 0.5 | 1500 | 2500 | 0.9329 |
| 128 | EA-8A | J | SW | SEC 23 | T5N | RIECM |  | 10 | 20 | 9000 | 4.5 | 5.0 | 5.5 | 1 | 2 | 2 | 5 | 10.0 | 1.5 | 20.0 | 0.5 | 3750 | 1030 | 0.9590 |
| 129 | EA-10 | L | SW | SEC23 | T5N | RIECM |  | 15 | 20 | 10400 | 12.5 | 9.0 | 53.0 | 1 | 2 | 5 | 2 | 20.0 | 1.5 | 45.0 | 1.0 | 14500 | 1775 | 0.8900 |
| 130 | EA-12 | N | SH | SEC23 | T5N | RIECM |  | 55 | 20 | 2650 | 20.5 | 20.5 | 330.0 | 1 | 2 | 10 | 5 | 15.0 | 2.0 | 55.0 | 1.5 | 5500 | 1650 | 0.8792 |
| 131 | EA-14 | P | SH | SEC23 | T5N | RIECM | 3.0 | 35 | 20 | 1300 | 6.0 | 12.0 | 16.5 | 1 | 2 | 15 | 2 | 10.0 | 1.0 | 15.0 | 0.8 | 1500 | 440 | 0.9219 |
| 32 | FL-2 | A |  | SEC2 | T30N | R29E |  | 20 | 20 | 5700 | 3.5 | 19 | 68. | 1 | 10 | 15 | 5 | 15. | 1.5 | 360. | 1.5 | 1000 | 43 | 0.8158 |

GEOCHEMICAL ANALYSIS OF THE MORRISON FORMATION----ELEMENTAL CONCENTRATIONS IN PPM, RESIDUAL IN GM

| OBS | SAMPLE | CODE |  |  | LCC |  | 0 | PB | TI | FE | ZN | Cu | MN | CR | NI | CO | MO | $v$ | CD | SR | AG | CA | MG | RESID |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 133 | $A B-1$ | A | NE | SEC 3 | T5N | R1ECM | 2200 | 55 | 100 | 3175 | 8.0 | 17.5 | 4.5 | 1 | 2 | 2 | 70 | 12.5 | 2.5 | 50 | 0.5 | 6500 | 1590 | 0.8663 |
| 134 | $A B-2$ | B | NE | SEC3 | T5N | RIECM | 720 | 45 | 50 | 23500 | 14.5 | 35.0 | 13.0 | 1 | 30 | 20 | 815 | 20.0 | 2.0 | 50 | 0.5 | 7000 | 1475 | 0.8765 |
| 135 | $A B-3$ | C | NE | SEC 3 | T5N | R1ECM | 2600 | 65 | 200 | 3250 | 7.5 | 18.0 | 5.0 | 1 | 2 | 5 | 80 | 15.0 | 1.5 | 55 | 0.5 | 7250 | 1620 | 0.8927 |
| 136 | $A B-5$ | E | NE | SEC3 | T5N | RIECM | 1450 | 110 | 50 | 3275 | 18.0 | 13.0 | 16.0 | 1 |  | - 15 | 10 | 85.0 | 2.5 | 45 | 1.0 | 5000 | 1830 | 0.8391 |
| 137 | AB-39 | M | NE | SEC 3 | T5N | R1ECM | 270 | 20 | 20 | 6300 | 7.0 | 12.0 | 76.5 | 1 | 2 | 10 | 55 | 10.0 | 1.5 | 30 | 1.0 | 3750 | 685 | 0.8626 |
| 138 | $A B-40$ | N | NE | SEC3 | T5N | R1ECM | 700 | 80 | 20 | 3750 | 18.0 | 20.0 | 35.5 | 1 | 2 | 20 | 5 | 125.0 | 1.5 | 30 | 1.5 | 5250 | 960 | 0.8783 |
| 139 | $A B-41$ | 0. | NE | SEC 3 | T5N | RIECM | 375 | 25 | 50 | 4200 | 4.5 | 9.0 | 12.0 | 1 | 2 | 15 | 75 | 10.0 | 1.0 | 30 | 0.5 | 2000 | 1010 | 0.8380 |
| 140 | AB-42 | P | NE | SEC 3 | T5N | RIECM | 1000 | 35 | 50 | 3000 | 8.0 | 6.0 | 8.5 | 1 | 2 | 5 | 5 | 25.0 | 1.0 | 30 | 0.5 | 3750 | 780 | 0.9105 |

APPENDIX B

DESCRIPTIVE STATISTICS OF THE GEOCHEMICAL ANALYSIS

DESCRIPTIVE STATISTICS OF THE GEOCHEMICAL ANALYSIS————NORMALIZED DATA BY LOG TRANSFORMATION LITHO=CHERT GP=LOW U

| VARIABLE | $N$ | ME AN | STANOARD DEVIATION | SKEWNESS | KURTOS IS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| U | 9 | 1. 03657115 | 0.69853620 | -0.61492247 | 0.30927713 |
| FE | 10 | 3. 53682282 | 0.46040659 | -0.17635343 | -1.39579266 |
| ZN | 10 | 1.11685575 | 0.21061640 | 0.16528905 | -1.39544671 |
| CU | 10 | 0.88728284 | 0.14260236 | $-1.64273961$ | 3.64828318 |
| PB | 10 | 1.11465000 | 0.21800896 | -0.34359894 | -0.03169486 |
| MN | 10 | 1.85129941 | 0.67218517 | 0.65731972 | 0.60458611 |
| CD | 10 | 0.04475360 | 0.31483180 | 0.78487816 | 0.77867313 |
| CO | 10 | 0.98277413 | 0.44367072 | -0.39019158 | -0.49697836 |
| CR | 10 | -0.00015625 | 0.00025409 | -0.83495011 | -0.64222676 |
| NI | 10 | 0.51056475 | 0.33749285 | 1.03509712 | -1.22448968 |
| TI | 10 | 1.39984375 | 0.16239707 | 1.54256641 | 0.84676212 |
| V | 10 | 1.34827145 | 0.37777644 | -0.32934068 | -0.45695947 |
| MO | 10 | 0.97485600 | 0.33201701 | $1.67710279$ | 3. 57355255 |
| AG | 10 | -0.22636744 | 0.38395313 | 0.03435152 | $2.84025456$ |
| CA | 10 | 3.11617899 | 0.64765885 | 1.98312321 | 4.95760374 |
| SR | 10 | 1. 08666593 | 0.46050146 | 1.94832315 | 4.67315788 |
| MG | 10 | 2.71998619 | 0.27187457 | $-1.08780488$ | 1.29696647 |
| LITHG=LIMESTONE |  |  |  |  |  |
| U | 8 | 0.51254632 | 0.54395918 | -0.80635580 | -0.56546514 |
| $F E$ | 11 | $3.87202276$ | 0.39474277 | $-1.43361993$ | 1.82766915 |
| ZN | 11 | 1.43517219 | 0.32237191 | -0.92094317 | -0.45078847 |
| CU | 11 | 0.97288671 | 0.12482400 | -0.78958277 | 1.45533398 |
| PB | 11 | 1.34870632 | 0.15311187 | 0.41879961 | -1.22208034 |
| MN | 11 | 2.83133234 | $0.49071686$ | -0.41904946 | -1.27174483 |
| $C D$ | 11 | $0.45829344$ | $0.24431055$ | $-0.48699778$ | -0.44735726 |
| $\mathrm{CO}$ | 11 | $0.95900070$ | $0.27277179$ | 0.34806011 | -1.58656260 |
| CR | 11 | 0.34535320 | $0.40520540$ | 0.38841315 | -1.91536633 |
| NI | 11 | $0.55292604$ | $0.32118711$ | $0.90506761$ | -0.44315720 |
| TI | 11 | 1.33747956 | 0.12077431 | 3.31660862 | 10.99992199 |
| $V$ | 11 | 1. 15056525 | 0.21755272 | -0.63830136 | 0.46457573 |
| MO | 11 | 0.81429525 | $0.47434620$ | 0.31260857 | $-0.93036405$ |
| AG | 11 | 0.33703366 | 0.23008412 | -0.12353925 | -0.88571273 |
| CA | 11 | 4.35979260 | 0.28347713 | -0.19899577 | 0.66600668 |
| SR | 11 | $2.16592159$ | $0.33547690$ | $-1.19824046$ | 1.60716785 |
| MG | 11 | 3.45513684 | 0.40723944 | 0.37094165 | -1.39495496 |

DESCRIPTIVE STATISTICS OF THE GEOCHEMICAL ANALYSIS———nORMALIZED DATA BY LOG TRANSFORMATION LITHO=LIMESTONE GP=HIGH U

| VARIABLE | N | MEAN |
| :--- | :---: | :---: |
|  |  |  |
|  |  |  |
| U | 1 | 2.41497335 |
| FE | 1 | 3.88636046 |
| ZN | 1 | 1.55617223 |
| CU | 1 | 1.06056757 |
| PB | 1 | 1.17596099 |
| MN | 1 | 2.78874485 |
| CD | 1 | 0.54393778 |
| CO | 1 | 0.69883974 |
| CR | 1 | 0.69883974 |
| NI | 1 | 0.30089973 |
| TI | 1 | 1.69883974 |
| V | 1 | 0.99986973 |
| MO | 1 | 1.30089973 |
| AG | 1 | 4.39780974 |
| CA | 1 | 2.50501971 |
| SR | 1 | 3.47699099 |

## STANDARD

SKEWNESS
KURTOS IS


|  |  |  |
| :--- | ---: | ---: |
| U | 30 | 0.03361647 |
| FE | 79 | 3.51314603 |
| ZN | 79 | 1.06642393 |
| CU | 79 | 0.80630454 |
| PB | 79 | 1.07078609 |
| MN | 79 | 1.73618655 |
| CD | 79 | 0.03666572 |
| CD | 79 | 0.80578312 |
| CR | 79 | 0.06038723 |
| NI | 79 | 0.46772772 |
| TI | 79 | 1.34701077 |
| V | 79 | 1.12548049 |
| MO | 79 | 0.63640925 |
| AG | 79 | -0.17317287 |
| CA | 79 | 3.36079725 |
| SR | 79 | 1.17479589 |
| MG | 79 | 2.80745039 |

0.58069546
0.41953895
0.32149205
0.25774828
0.32517191
0.76414304
0.33577238
0.38628197
0.21679347
0.35367952
0.14190151
0.44989464
0.28585614
0.37148236
0.74499144
0.61928264
0.61467578

1. 54913691 0.33718128 0.30442988 0.45366538 -1.89893172 0.52589531 0.08834157 0.95277511 3. 46372015 2. 57832412 4.77776314 0.94246905
0.72009736 0.52913985 0.04943390 0.04943390
0.36290150 0.86527545 1.07982174
-0.76645015
-0.22576178
1.33254120
10.14718564
0.17361080
0.13042033
2.28954247
10.82152404
7.41938334
27.28695241
2.47516442
0.85552257
2.33504771
-1.29677433
-0.27248702
1.23555852

DESCRIPTIVE STATISTICS OF THE GEOCHEMICAL ANALYSIS--ー-NORMALIZED DATA BY LOG TRANSFORMATION LITHO =SHALE GP=LOWU

| VARIABLE | $N$ | MEAN | STANDARD DEVIATION | SKENNESS | KURTOSIS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| U | 15 | 0.21091717 | 0.39991976 | -0.28847639 | -1.17733339 |
| FE | 31 | 3.75625532 | 0.39637587 | -0.90478177 | 0.01057306 |
| 2N | 31 | 1.08834994 | 0.29806395 | -0.44648472 | -0.21735543 |
| CU | 31 | 1. 11478339 | 0.26099301 | -0.68854120 | 0.18656279 |
| PB | 31 | 1.20392925 | 0.23355887 | -0.03153789 | 0.37492869 |
| MN | 31 | 1.58512035 | 0.62826820 | 0.43932249 | -1.06410374 |
| CD | 31 | -0.02310345 | 0.27942035 | -0.77952713 | 0.46540597 |
| CO | 31 | 0.66220243 | 0.31230543 | 0.14144709 | -1.29445204 |
| CR | 31 | 0.09018973 | 0.23816758 | 2.32733483 | 3.64805068 |
| NI | 31 | 0.39434586 | 0.22458547 | 2.20944203 | 3.44997961 |
| TI | 31 | 1.34891876 | 0.14299205 | 3.85917583 | 15.65574160 |
| $V$ | 31 | 1. 10006779 | 0.38574252 | -1.66398876 | 5.37629403 |
| MO | 31 | 0.53867651 | 0.23109621 | 0.20326798 | -1.25065456 |
| AG | 31 | -0.13176709 | 0.20237954 | 0.31904812 | -0.82386109 |
| CA | 31 | 3.65620429 | 0.44499247 | -0.05216440 | -1.14295325 |
| SR | 31 | 1.51024245 | 0.33772219 | 0.94198111 | 1.48066169 |
| MG | 31 | 3.05894600 | 0.25213368 | -0.27238724 | -0.39924034 |
| LITHO=SHALE |  |  |  |  |  |
| U | 8 | 2.95332370 | 0.34789398 | -0.14711255 | -1.02952602 |
| FE | 8 | 3.67161381 | 0.30096039 | 2.25629646 | 5.25980243 |
| ZN | 8 | 0.98134084 | 0.21784139 | 0.12550267 | -1.17920913 |
| CU | 8 | 1.15852360 | 0.23306633 | -0.03801917 | 0.37151373 |
| PB | 8 | 1.67415890 | 0.25178178 | -0.13094584 | -0.90745136 |
| MN | 8 | 1.13899971 | 0.41496322 | 0.72821105 | 0.08300709 |
| CD | 8 | 0.20305571 | 0.15592414 | -0.05571585 | -1.20056183 |
| CO | 8 | 0.95655930 | 0.35811973 | -0.88292091 | -0.18579684 |
| CR | 8 | -0.00009226 | 0.00011473 | -0.43953934 | 1.33811078 |
| NI - | 8 | 0.44794914 | 0.41581326 | 2.82842669 | 7.99999817 |
| TI | 8 | 1.71227899 | 0.33133429 | 0.46407884 | 0.33998139 |
| $V$ | 8 | 1.37469526 | 0.41961443 | 1.06254348 | -0.32652674 |
| MO | 8 | 1.58399644 | 0.75102591 | 0.37309991 | -0.08470319 |
| AG | 8 | -0.16622460 | 0.19391290 | 0.96643859 | -0.80123960 |
| CA | 8 | 3.67322914 | 0.18715951 | -1.13591045 | 1.21518920 |
| SR | 8 | 1.58740776 | 0.12028562 | 0.13702462 | -2.49581024 |
| MG | 8 | 3.06947436 | 0.16127807 | -0.27990680 | -1.74470034 |

APPENDIX C

CORRELATION MATRICES

correlation matrices--- mormalized data by log transformation
Correlation ccefficients / prob > IRI under ho: rho =o / number of observations

| RESID | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 11 \end{array}$ | $\begin{aligned} & 0.34600 \\ & 0.4012 \end{aligned}$ | $\begin{gathered} 0.71484 \\ 0.0134 \\ 11 \end{gathered}$ | $\begin{array}{r} 0.71323 \\ 0.0137 \end{array}$ | $\begin{array}{r} 0.22056 \\ -0.5146 \\ 0.11 \end{array}$ | $\begin{array}{r} -0.70133 \\ 0.0162 \\ 11 \end{array}$ | $\begin{array}{r} 85604 \\ 0.0008 \\ 11 \end{array}$ | $\begin{array}{r} 85838 \\ 0.0007 \\ 11 \end{array}$ | $\begin{array}{r} 45389 \\ 0.1608 \\ 11 \end{array}$ | $\begin{gathered} 43840 \\ 0.1774 \\ 11 \end{gathered}$ | $\begin{array}{r} -0.42833 \\ 0.1887 \\ 11 \end{array}$ | $\begin{array}{r} 3-0.40340 \\ 7 \\ \hline \end{array} \begin{array}{r} 0.2186 \\ 11 \end{array}$ | $\begin{gathered} 0.42962 \\ 0.1873 \\ 11 \end{gathered}$ | $\begin{array}{r} -0.10884 \\ -1.7501 \\ 11 \end{array}$ | $\begin{array}{r} 0.90366 \\ 0.0001 \\ 11 \end{array}$ | $\begin{gathered} 0.40038 \\ 0.2224 \\ 11 \end{gathered}$ | $\begin{array}{r} 0.65117 \\ 0.0300 \\ 11 \end{array}$ | $\begin{array}{r} 0.28683 \\ 0.3925 \\ 11 \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $u$ | $\underset{8}{012}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \end{array}$ | $\begin{array}{r} 0.0761 \\ \hline \end{array}$ | $0.1870$ | $\begin{array}{r} -0.15799 \\ 0.7087 \\ 0 \end{array}$ | $\begin{array}{r} -0.29805 \\ 0.474 \\ \hline-8 \end{array}$ | $\begin{array}{r} 0.380005 \\ 0.3531 \\ \quad . \end{array}$ | $\begin{array}{r} 26570 \\ 0.548 \\ -\quad 8 \end{array}$ | $\begin{array}{r} -0.31 \\ 0.4 \end{array}$ | $\begin{array}{r} 0.15 c 87 \\ 0.7214 \\ 8 \end{array}$ | $\begin{array}{r} 7-0.48856 \\ 4.2193 \end{array}$ | $\begin{array}{r} -0.12876 \\ 0.7612 \end{array}$ | $\begin{aligned} & 12367 \\ & 0.7705 \end{aligned}$ | $\begin{array}{r} 14497 \\ 0.7320 \end{array}$ | $\begin{array}{r} 0.40169 \\ 0.3239 \end{array}$ | $\begin{aligned} & 54 \\ & 70 \end{aligned}$ | $\begin{aligned} & 02 \\ & 88 \end{aligned}$ | $\begin{aligned} & 57 \\ & 00 \end{aligned}$ |
| FE | $\begin{gathered} 0.71484 \\ 0.0134 \end{gathered}$ | $-0.65795$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 11 \end{array}$ | $\begin{array}{r} 0.95259 \\ 0.0001 \\ 11 \end{array}$ | $\begin{array}{r} 0.03362 \\ 0.9218 \\ 111 \end{array}$ | $\begin{array}{r} -0.13448 \\ 0.6934 \\ 11 \end{array}$ | $\begin{array}{r} -0.40784 \\ 0.2131 \\ 11 \end{array}$ | $\begin{array}{r} -0.50913 \\ 0.1097 \\ 11 \end{array}$ |  | $\begin{array}{r} -0.02029 \\ 0.952 \\ 11 \end{array}$ | $\begin{array}{r} 0.02136 \\ 0.9503 \\ 11 \end{array}$ | $\begin{gathered} 6.41044 \\ \begin{array}{c} -0.41 \\ 0.209 \\ 1 \end{array} \\ \hline 11 \end{gathered}$ | $\begin{array}{r} 0.16410 \\ 0.629 \\ 11 \end{array}$ | $\begin{array}{r} -0.22300 \\ 0.5098 \\ 11 \end{array}$ | $\begin{array}{r} -0.52834 \\ 0.0948 \\ 11 \end{array}$ | $\begin{array}{r} -0.10340 \\ 0.7623 \\ 11 \end{array}$ | $\begin{array}{r} 0.51396 \\ 0.1058 \\ 11 \end{array}$ |  |
| 2N | $\begin{array}{r} 0.71323 \\ 0.0137 \\ 11 \end{array}$ | $\begin{array}{r} -0.51953 \\ 0.1870 \end{array}$ | $\begin{array}{r} 0.95259 \\ 0.0001 \\ 11 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 11 \end{array}$ | $\begin{array}{r} 0.05635 \\ 0.8693 \\ 11 \end{array}$ | $\begin{array}{r} 0.6157 \\ 11 \end{array}$ | $\begin{array}{r} 0.0962 \\ 11 \end{array}$ | $\begin{array}{r} 0.0657 \\ 11 \end{array}$ | $\begin{array}{r} 0.8028 \\ 11 \end{array}$ | $\begin{array}{r} 0.09933 \\ 0.7714 \\ 11 \end{array}$ | $\begin{array}{r} 0.6621 \\ 11 \end{array}$ | $\begin{array}{r} 0.1247 \\ 11 \end{array}$ | $\begin{array}{r} 0.10049 \\ 0.7688 \\ 11 \end{array}$ | $\begin{array}{r} -0.16155 \\ 0.6351 \\ 11 \end{array}$ | $\begin{array}{r} 0.56468 \\ 0.0703 \\ 11 \end{array}$ | 11 | $\begin{gathered} 546 \\ 11 \end{gathered}$ | $\begin{array}{r} 08865 \\ 2121 \\ \hline 11 \end{array}$ |
| cu | $\begin{array}{r} -0.22056 \\ 0.5146 \\ 11 \end{array}$ | $-0.1579$ | $\begin{array}{r} 0.03362 \\ 0.9218 \\ 11 \end{array}$ | $\begin{array}{r} 0.05635 \\ 0.8693 \\ \quad 11 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 11 \end{array}$ | $\begin{gathered} 0.42702 \\ 0.1902 \\ 11 \end{gathered}$ | $\begin{array}{r} 0.16221 \\ 0.6337 \\ 11 \end{array}$ |  | $\begin{array}{r} 0.04997 \\ 0.8840 \\ 11 \end{array}$ |  | $\begin{array}{r} 0.34873 \\ 0.2932 \\ 11 \end{array}$ |  | $\begin{gathered} 0.10157 \\ 0.7663 \\ 11 \end{gathered}$ | $\begin{array}{r} 0.2721212 \\ 0.4182 \\ 11 \end{array}$ | $\begin{array}{r} 0.29345 \\ 0.3811 \\ 11 \end{array}$ |  | $\begin{array}{r} 0.17867 \\ 0.5991 \\ 11 \end{array}$ | $\begin{array}{r} 2568 \\ 5046 \\ 1 \end{array}$ |
| PB | $\begin{array}{r} -0.70133 \\ 0.0162 \\ 11 \end{array}$ | $\begin{gathered} 0.29865 \\ 0.4734 \end{gathered}$ | $\begin{array}{r} 0.13448 \\ 0.6934 \\ 11 \end{array}$ | $\begin{array}{r} -0.17073 \\ 0.6157 \\ 11 \end{array}$ | $\begin{array}{r} 0.1902 \\ 11 \end{array}$ | $\begin{array}{r} 0000 \\ 11 \end{array}$ | $\begin{array}{r} 0.67349 \\ 0.0231 \\ 11 \end{array}$ | $\begin{array}{r} 0.0627 \\ 11 \end{array}$ | $\begin{array}{r} 0.59112 \\ 0.0555 \\ 11 \end{array}$ | $\begin{array}{r} 0.66591 \\ 0.0253 \\ 11 \end{array}$ | $\begin{array}{r} 0.71511 \\ 0.0134 \\ 11 \end{array}$ | $\begin{array}{r} 0.28375 \\ 0.3978 \\ 11 \end{array}$ | $\begin{gathered} 0.42729 \\ 0.1899 \\ 11 \end{gathered}$ | $\begin{array}{r} -0.28489 \\ 0.3958 \\ 11 \end{array}$ | $\begin{array}{r} 0.68773 \\ 0.0193 \\ 111 \end{array}$ | $\begin{array}{r} 0.28463 \\ 0.3963 \\ 11 \end{array}$ | $\begin{aligned} & 0.22160 \\ & 0.5126 \\ & 12 \end{aligned}$ | $\begin{array}{r} 13156 \\ .6998 \\ 11 \end{array}$ |
| NN | 11 | $\begin{array}{r} 0.3800 \\ 0.35 \end{array}$ | $\begin{array}{r} .40784 \\ 0.2131 \\ 11 \end{array}$ | $\begin{array}{r} 2647 \\ 0962 \\ 0962 \\ \hline 12 \end{array}$ | $11$ | $\begin{array}{r} 231 \\ 11 \end{array}$ |  |  |  |  | $\begin{array}{r} 0.26502 \\ 0.4309 \\ 11 \end{array}$ |  |  |  |  |  | $\begin{array}{r} 0.77045 \\ 0.0055 \\ 11 \end{array}$ |  |
| co | $\begin{array}{r} -0.85838 \\ -0.0007 \\ 11 \end{array}$ | $\begin{array}{r} -0.26570 \\ 0.5248 \end{array}$ | $\begin{array}{r} 0.50913 \\ 0.1097 \\ 11 \end{array}$ | $\begin{array}{r} 0.57244 \\ 0.0657 \\ 11 \end{array}$ | $\begin{array}{r} 0.30518 \\ 0.3615 \\ 11 \end{array}$ | $\begin{array}{r} 0.57772 \\ 0.0627 \\ 11 \end{array}$ | $\begin{array}{r} 0.91516 \\ 0.0001 \\ 11 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 11 \end{array}$ | $\begin{array}{r} 0.29464 \\ 0.3791 \\ 11 \end{array}$ | $\begin{array}{r} 0.48793 \\ 0.1279 \\ 11 \end{array}$ | $\begin{array}{r} 0.23776 \\ 0.4814 \\ 11 \end{array}$ | $0.321711$ | $\begin{array}{r} 0.48896 \\ 0.1287 \\ 11 \end{array}$ | $\begin{array}{r} 0.41309 \\ 0.2067 \\ 11 \end{array}$ | $\begin{array}{r} 0.95670 \\ 0.0001 \\ 11 \end{array}$ | $\begin{array}{r} 0.47850 \\ 0.1365 \\ 11 \end{array}$ | $\begin{array}{r} 0.88557 \\ 0.0002 \\ 11 \end{array}$ | $\begin{array}{r} 16887 \\ -6196 \\ \hline 11 \end{array}$ |
| co | $\begin{gathered} 5389 \\ 1808 \\ 11 \end{gathered}$ | $\begin{array}{r} -0.31598 \\ 0.4458 \\ 8 \end{array}$ | $\begin{gathered} 906 \\ \hline 861 \\ 11 \end{gathered}$ | $\begin{array}{r} 8028 \\ 11 \end{array}$ |  | $\begin{array}{r} 0555 \\ 11 \end{array}$ | $\begin{array}{r} 2506 \\ 11 \end{array}$ | $\begin{array}{r} 3791 \\ 11 \end{array}$ | ${ }^{.0000}$ | $\begin{array}{r} 58505 \\ -0587 \\ -11 \end{array}$ | $\begin{array}{r} 0055 \\ 11 \end{array}$ | $\begin{array}{r} 3489 \\ 11 \end{array}$ | $\begin{gathered} 58734 \\ 0874 \\ 0.057 \end{gathered}$ | $\begin{array}{r} 31262 \\ \hline 3493 \\ 11 \end{array}$ | $\begin{array}{r} 0.37891 \\ 0.2505 \\ 111 \end{array}$ | $\begin{array}{r} 0.65627 \\ 0.0283 \\ 11 \end{array}$ | $\begin{array}{r} .04337 \\ 0.8993 \\ 11 \end{array}$ | $\begin{array}{r} 13787 \\ 0.6860 \\ \hline \end{array}$ |
| cR | $\begin{array}{r} 0.43840 \\ 0.1744 \\ 11 \end{array}$ | $\begin{aligned} & 0.1508 \\ & 0.721 \end{aligned}$ | $\begin{array}{r} 0.02029 \\ 0.9528 \\ 11 \end{array}$ | $\begin{array}{r} 0.09933 \\ -.9714 \\ 11 \end{array}$ | $\begin{gathered} 0.43344 \\ 0.1944 \\ 11 \end{gathered}$ | $\begin{array}{r} 0.66591 \\ 0.0253 \\ 11 \end{array}$ | $\begin{array}{r} 0.60867 \\ 0.0469 \\ 11 \end{array}$ | $\begin{array}{r} 0.48793 \\ 0.1279 \\ 11 \end{array}$ | $\begin{array}{r} 0.58505 \\ 0.0587 \\ 11 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 11 \end{array}$ | $\begin{array}{r} 0.52615 \\ 0.0964 \\ 11 \end{array}$ | $\begin{array}{r} 50.28115 \\ 4 \\ 4.4023 \\ 11 \end{array}$ | $\begin{array}{r} 0.26763 \\ 0.4263 \\ 11 \end{array}$ | $\begin{array}{r} 0.29817 \\ -0.3731 \\ 11 \end{array}$ | $\begin{array}{r} 45208 \\ 0.1627 \\ 11 \end{array}$ | $\begin{array}{r} 0.63855 \\ 0.0345 \\ 11 \end{array}$ | $\begin{gathered} 0.30779 \\ 0.3572 \\ 11 \end{gathered}$ | $\begin{array}{r} .20424 \\ 0.5469 \\ 11 \end{array}$ |
| NI | $\begin{array}{r} -0.42833 \\ 0.1887 \\ 11 \end{array}$ | $0.219$ | $\begin{array}{r} 0.9503 \\ 11 \end{array}$ | $\begin{array}{r} 0.6621 \\ 11 \end{array}$ | $\begin{array}{r} 0.2932 \\ 11 \end{array}$ | $\begin{array}{r} 0.0134 \\ 11 \end{array}$ | $\begin{array}{r} 4309 \\ 11 \end{array}$ | $\begin{array}{r} 0.4814 \\ 11 \end{array}$ | $\begin{array}{r} 0.0055 \\ 11 \end{array}$ | $\begin{gathered} 0.52615 \\ 0.0964 \\ 11 \end{gathered}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 11 \end{array}$ | $0.4449$ | $\begin{gathered} 0.19756 \\ 0.5604 \\ 11 \end{gathered}$ | $\begin{array}{r} 0.20039 \\ 0.5547 \\ 11 \end{array}$ | $\begin{array}{r} 0.38373 \\ 0.2440 \\ 112 \end{array}$ | $\begin{array}{r} 0.56023 \\ 0.0731 \\ 11 \end{array}$ | $\begin{array}{r} 0.6635 \\ 11 \end{array}$ | $\begin{array}{r} .27733 \\ 0.4090 \\ 11 \end{array}$ |
| II | $\begin{gathered} 0340 \\ 2886 \\ 2186 \\ 11 \end{gathered}$ | 28 | $\begin{array}{r} 0.41044 \\ 0.2099 \\ 11 \end{array}$ | $\begin{array}{r} -0.49150 \\ 0.1247 \\ 11 \end{array}$ | $\begin{array}{r} 561 \\ 11 \end{array}$ | $\begin{array}{r} 0.28375 \\ 0.3978 \\ 11 \end{array}$ | $\begin{array}{r} 0.31542 \\ 0.3447 \\ 11 \end{array}$ | $\begin{array}{r} 0.32997 \\ 0.3217 \\ 111 \end{array}$ | $\begin{array}{r} .31286 \\ 0.3489 \\ 11 \end{array}$ | $\begin{array}{r} 0.28115 \\ 0.4023 \\ 11 \end{array}$ | $\begin{array}{r} -0.25734 \\ -0.4449 \\ 11 \end{array}$ | $0.0000$ | $\begin{array}{r} 0.23309 \\ 0.4903 \\ 11 \end{array}$ | $\begin{array}{r} 13138 \\ 0.7002 \\ 11 \end{array}$ | $\begin{array}{r} 0.38550 \\ 0.2416 \\ 11 \end{array}$ | $\begin{array}{r} 0.63703 \\ 0.0350 \\ 11 \end{array}$ | $\begin{array}{r} 0.31705 \\ 0.3421 \\ 0.11 \end{array}$ | $\begin{array}{r} 0.24653 \\ 0.4649 \\ 11 \end{array}$ |
| $v$ | $\begin{array}{r} 0.42962 \\ 0.1873 \\ 11 \end{array}$ | $\begin{array}{r} -0.12367 \\ 0.7705 \\ 8 \end{array}$ | $\begin{array}{r} -0.16410 \\ -0.6297 \\ 11 \end{array}$ | $\begin{array}{r} -0.10049 \\ 0.7689 \\ 11 \end{array}$ | $\begin{array}{r} 11 \\ 11 \end{array}$ | $\begin{gathered} 0.42729 \\ 0.1899 \\ 11 \end{gathered}$ | $\begin{array}{r} 0.41511 \\ 0.2042 \\ 11 \end{array}$ | $\begin{array}{r} 0.48696 \\ 0.1287 \\ 11 \end{array}$ | $\begin{gathered} 0.58734 \\ 0.0574 \\ 11 \end{gathered}$ | $\begin{array}{r} 0.26763 \\ 0.4263 \\ 11 \end{array}$ | $\begin{array}{r} 0.19756 \\ 0.5604 \\ 11 \end{array}$ | $\begin{array}{r} 0.23309 \\ 0.4903 \\ 111 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 11 \end{array}$ | $\begin{array}{r} 10462 \\ 0.7595 \\ 11 \end{array}$ | $\begin{array}{r} 0.55372 \\ 0.0772 \\ 11 \end{array}$ | $\begin{array}{r} 0.25774 \\ 0.4442 \\ 11 \end{array}$ | $\begin{array}{r} 0.37641 \\ 0.2539 \\ 11 \end{array}$ | $\begin{array}{r} .07425 \\ 0.8282 \\ 11 \end{array}$ |
| мо | $\begin{array}{r} 0.10884 \\ 0.7501 \\ 11 \end{array}$ | $\begin{array}{r} 0.14497 \\ 0.7320 \end{array}$ | $\begin{array}{r} 0.22300 \\ 0.5098 \\ 11 \end{array}$ | $\begin{array}{r} 0.16155 \\ 0.6351 \\ 11 \end{array}$ | $\begin{array}{r} 0.27212 \\ 0.4182 \\ 11 \end{array}$ | $\begin{array}{r} 0.28489 \\ 0.3958 \\ 11 \end{array}$ | $\begin{gathered} 0.06854 \\ 0.8413 \\ 11 \end{gathered}$ | $\begin{array}{r} 0.41309 \\ 0.2067 \\ 11 \end{array}$ | $\begin{array}{r} 0.31262 \\ 0.3493 \\ 11 \end{array}$ | $\begin{array}{r} -0.29817 \\ 0.3731 \\ 11 \end{array}$ | $\begin{array}{r} 70.20039 \\ 1 \\ 1 \\ 1.5547 \\ 11 \end{array}$ | $\begin{array}{r} 0.13138 \\ 0.7002 \\ 11 \end{array}$ | $\begin{array}{r} 0.10462 \\ 0.7595 \\ 11 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 11 \end{array}$ | $\begin{array}{r} 0.33261 \\ 0.3176 \\ 11 \end{array}$ | $\begin{array}{r} 0.12781 \\ 0.7080 \\ 1 \end{array}$ | $\begin{array}{r} 0.54209 \\ 0.0849 \\ 11 \end{array}$ | $\begin{array}{r} 0.40448 \\ 0.2172 \\ 11 \end{array}$ |
| ${ }^{\text {ab }}$ | $\begin{array}{r} 0.90366 \\ 0.0001 \\ 11 \end{array}$ | $\begin{array}{r} 0.4016 \\ 0.323 \end{array}$ | $\begin{array}{r} 0.52834 \\ 0.0948 \\ 11 \end{array}$ | $\begin{array}{r} 0.56468 \\ 0.0703 \\ 11 \end{array}$ | $\begin{array}{r} 0.29345 \\ 0.3811 \\ 0.11 \end{array}$ | $\begin{array}{r} 0.68773 \\ 0.0193 \\ 11 \end{array}$ | $\begin{array}{r} 0.87818 \\ 0.004 \\ 11 \end{array}$ | $\begin{array}{r} 0.95670 \\ 0.0001 \\ 11 \end{array}$ | $\begin{array}{r} 0.2505 \\ 0.25 \end{array}$ | $\begin{array}{r} 0.45208 \\ 0.1627 \\ 11 \end{array}$ | $\begin{array}{r} 0.38373 \\ 0.2440 \\ 11 \end{array}$ | $\begin{gathered} 0.38550 \\ 0.2416 \\ 11 \end{gathered}$ | $\begin{array}{r} 0.55372 \\ 0.0772 \\ 111 \end{array}$ | $\begin{array}{r} 0.33261 \\ 0.3176 \\ 11 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 11 \end{array}$ | $\begin{array}{r} 0.45654 \\ 0.1581 \\ 11 \end{array}$ | $\begin{array}{r} .73042 \\ 0.0098 \\ 11 \end{array}$ | $\begin{array}{r} 0.32118 \\ 0.3355 \\ 11 \end{array}$ |
| ca | $\begin{array}{r} -0.40038 \\ 0.2224 \\ 11 \end{array}$ | $\begin{array}{r} -0.4254 \\ -0.2970 \\ 0.20 \\ 8 \end{array}$ | $\begin{array}{r} -0.10340 \\ 0.7623 \\ 11 \end{array}$ | $\begin{array}{r} -0.03941 \\ 0.9084 \\ 11 \end{array}$ | $\begin{array}{r} 0.19957 \\ 0.5563 \\ 11 \end{array}$ | $\begin{array}{r} 0.28463 \\ 0.3963 \\ 11 \end{array}$ | $\begin{array}{r} 0.43982 \\ 0.1758 \\ 11 \end{array}$ | $\begin{array}{r} 0.47850 \\ 0.1365 \\ 11 \end{array}$ | $\begin{array}{r} 0.65627 \\ 0.0283 \\ 11 \end{array}$ | $\begin{array}{r} 0.63855 \\ 0.0345 \\ 11 \end{array}$ | $\begin{array}{r} 0.56023 \\ 0.0731 \\ 11 \end{array}$ | $\begin{array}{r} -0.63703 \\ 0.0350 \\ 11 \end{array}$ | $\begin{gathered} 0.25774 \\ 0.4442 \\ 11 \end{gathered}$ | $\begin{array}{r} 0.12781 \\ 0.7080 \\ 11 \end{array}$ | $\begin{array}{r} 0.45654 \\ 0.1581 \\ 11 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 11 \end{array}$ | $\begin{array}{r} 0.32188 \\ 0.3344 \\ 11 \end{array}$ | $\begin{array}{r} 0.00524 \\ 0.9878 \\ 11 \end{array}$ |
| SR | $\begin{array}{r} -0.65117 \\ 0.0300 \\ 11 \end{array}$ | $\begin{array}{r} 0.03802 \\ 0.9288 \\ 8 \end{array}$ | $\begin{array}{r} 0.51396 \\ 0.1058 \\ 11 \end{array}$ | $\begin{array}{r} -0.59272 \\ 0.0546 \\ 11 \end{array}$ | $\begin{array}{r} 0.17867 \\ 0.5991 \\ 11 \end{array}$ | $\begin{gathered} 0.22160 \\ 0.5126 \\ 11 \end{gathered}$ | $\begin{gathered} 0.77045 \\ 0.0055 \\ 11 \end{gathered}$ | $\begin{array}{r} 0.88957 \\ 0.0002 \\ 0.021 \end{array}$ | $\begin{array}{r} 0.8993 \end{array}$ | $\begin{array}{r} 0.30779 \\ 0.3572 \\ 11 \end{array}$ | $\begin{array}{r} -0.14827 \\ 0.6635 \\ 11 \end{array}$ | $\begin{array}{r} 0.31705 \\ 0.3421 \\ 0.11 \end{array}$ | $\begin{array}{r} 0.37641 \\ 0.2539 \\ 11 \end{array}$ | $\begin{array}{r} 0.54209 \\ 0.0849 \\ 11 \end{array}$ | $\begin{array}{r} 0.73642 \\ 0.0098 \\ 11 \end{array}$ | $\begin{array}{r} 0.32188 \\ 0.3344 \\ 11 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 11 \end{array}$ | $\begin{array}{r} 0.00957 \\ 0.9777 \\ 11 \end{array}$ |
| ${ }^{\text {mG }}$ | $\begin{array}{r} 0.28683 \\ 0.3925 \\ 111 \end{array}$ | $\begin{array}{r} -0.09657 \\ -0.8200 \\ -8 \end{array}$ | $\begin{array}{r} 0.50046 \\ 0.1119 \\ 11 \end{array}$ | $\begin{array}{r} 0.40865 \\ 0.2121 \\ 11 \end{array}$ | $\begin{array}{r} 0.22568 \\ 0.5046 \\ 11 \end{array}$ | $\begin{array}{r} -0.13156 \\ 0.6998 \\ 11 \end{array}$ | $\begin{array}{r} 0.08966 \\ 0.7932 \\ 11 \end{array}$ | $\begin{array}{r} -0.16887 \\ 0.6196 \\ 11 \end{array}$ | $\begin{array}{r} 0.13787 \\ 0.6860 \\ 11 \end{array}$ | $\begin{array}{r} 0.20424 \\ 0.5469 \\ 11 \end{array}$ | $\begin{array}{r} 0.27733 \\ 0.4090 \\ 11 \end{array}$ | $\begin{array}{r} -0.24653 \\ 0.4649 \\ 11 \end{array}$ | $\begin{array}{r} 0.07425 \\ 0.8282 \\ 0.11 \end{array}$ | $\begin{array}{r} -0.40448 \\ -0.4172 \\ 0.11 \end{array}$ | $\begin{array}{r} -0.3218 \\ -3355 \\ 0.311 \end{array}$ | $\begin{array}{r} 0.00524 \\ 0.9878 \\ 11 \end{array}$ | $\begin{array}{r} 0.00957 \\ 0.9777 \\ 11 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 11 \end{array}$ |



| essio | 00000 . 0000 | $\begin{gathered} 40443 \\ .0266 \end{gathered}$ | $\begin{aligned} & 48921 \\ & 0.0001 \end{aligned}$ | $\begin{array}{r} -0.51491 \\ 0.0001 \end{array}$ | $\begin{array}{r} 0.25725 \\ 0.0221 \\ 79 \end{array}$ | $\begin{array}{r} -0.46765 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} -0.73604 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} -0.69441 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} .33135 \\ 0.0029 \\ 79 \end{array}$ | $\begin{array}{r} 55522 \\ 0.0001 \\ 79 \\ 79 \end{array}$ | $\begin{array}{r} 39065 \\ 0.0004 \\ 79 \end{array}$ | $\begin{array}{r} .14121 \\ 0.2145 \\ 79 \end{array}$ | $\begin{array}{r} 0.28534 \\ 0.0108 \\ 0.019 \end{array}$ | $\begin{array}{r} 0.09341 \\ 0.4129 \\ 79 \end{array}$ | $\begin{array}{r} 0.63223 \\ 0.0001 \\ 79 \end{array}$ | $\begin{gathered} 1000 \\ 1001 \\ 79 \end{gathered}$ | $\begin{aligned} & 12 \\ & 01 \\ & 79 \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | $\begin{array}{r} -0.40443 \\ 0.0266 \\ 30 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 30 \\ 30 \end{array}$ | $\begin{array}{r} 0.18594 \\ 0.3252 \\ 30 \end{array}$ | $\begin{array}{r} 0.00124 \\ 0.9946 \\ 30 \end{array}$ | $\begin{array}{r} 0.27739 \\ 0.1378 \\ 30 \end{array}$ | $\begin{array}{r} 0.31913 \\ 0.0856 \\ 30 \end{array}$ | $\begin{array}{r} 0.31599 \\ 0.0869 \\ 30 \end{array}$ |  |  |  |  |  |  |  |  |  |  |  |
| FE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 0.44465 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.54941 \\ 0.0011 \\ 79 \end{array}$ |  |
| 2N | $\begin{array}{r} -0.51491 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.00124 \\ 0.9948 \\ 30 \end{array}$ | $\begin{array}{r} 0.77630 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 79 \end{array}$ |  | $\begin{array}{r} 0.49714 \\ 0.0001 \\ 79 \end{array}$ | $\begin{gathered} 0.73444 \\ 0.0001 \\ 79 \end{gathered}$ |  |  | $\begin{array}{r} 0.0032 \\ 79 \end{array}$ |  |  |  |  |  |  |  |  |
| cu | $\begin{array}{r} -0.25725 \\ 0.0221 \\ 79 \end{array}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 0.31115 \\ 0.0053 \\ 79 \end{array}$ | $\begin{array}{r} 0.34376 \\ 0.0019 \\ 79 \end{array}$ |
| PB | $\begin{array}{r} -0.46765 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.31913 \\ 0.0856 \\ 30 \end{array}$ | $\begin{array}{r} 0.44957 \\ 0.0001 \\ 0.079 \end{array}$ | $\begin{gathered} 0.49714 \\ 0.0001 \\ 79 \end{gathered}$ | $\begin{array}{r} 0.27599 \\ 0.0138 \\ 0 . \end{array}$ |  | $\begin{array}{r} 0.60383 \\ 0.0001 \\ 79 \end{array}$ |  | 79 | $\begin{aligned} & 35 \\ & 307 \\ & 79 \end{aligned}$ |  |  |  |  | $\begin{array}{r} 30875 \\ \hline .00756 \\ \hline 79 \end{array}$ |  |  |  |
| w | $\begin{array}{r} -0.73604 \\ -0.0001 \\ 79 \end{array}$ | 30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| co | $\begin{array}{r} 0.69441 \\ -0.0001 \\ 79 \end{array}$ |  | $\begin{array}{r} 0.43905 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.48943 \\ 0.0001 \\ 79 \end{array}$ | $\begin{gathered} 0.16053 \\ 0.1576 \\ 79 \end{gathered}$ | $\begin{gathered} 0.46625 \\ 0.0001 \\ 79 \end{gathered}$ | $\begin{array}{r} 0.61626 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 79 \end{array}$ | $\begin{array}{r} 791 \\ \hline 90 \end{array}$ |  | $791$ |  |  | $\begin{aligned} & 41 \\ & 54 \\ & 79 \end{aligned}$ |  | $\begin{array}{r} 0.65221 \\ 0.0001 \\ \hline 0.0 \end{array}$ | $\begin{gathered} 896 \\ 001 \\ 096 \end{gathered}$ |  |
| co | $0.0029$ |  |  |  | $\begin{array}{r} 0.10720 \\ 0.3470 \\ 79 \end{array}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| cR | 0.0001 79 | $\begin{array}{r} 0.55837 \\ 0.0014 \\ 30 \end{array}$ | $\begin{array}{r} 0.19549 \\ 0.0842 \\ 79 \end{array}$ | $\begin{array}{r} 0.32761 \\ 0.0032 \\ 79 \end{array}$ | $\begin{array}{r} 0.24123 \\ 0.0322 \\ 79 \end{array}$ | $\begin{array}{r} 0.37435 \\ 0.0007 \\ 79 \end{array}$ | $\begin{array}{r} 0.45216 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.48233 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.20320 \\ 0.0725 \\ 79 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 79 \end{array}$ | $\begin{array}{r} 0.34056 \\ 0.0021 \\ 79 \end{array}$ | $\begin{array}{r} -0.09127 \\ 0.4237 \\ 79 \end{array}$ | $\begin{array}{r} 0.17228 \\ 0.1290 \\ 79 \end{array}$ | $\begin{array}{r} 0.07575 \\ 0.5070 \\ 79 \end{array}$ | $\begin{array}{r} 0.42999 \\ 0.0001 \\ 79 \end{array}$ |  | $\begin{array}{r} 0.53043 \\ 0.0001 \\ 79 \end{array}$ |  |
| ni | $\begin{array}{r} -0.39065 \\ 0.0004 \\ 79 \end{array}$ | $\begin{gathered} 0.45789 \\ 0.0109 \\ 0.30 \end{gathered}$ | $\begin{gathered} 002 \\ 79 \end{gathered}$ | $0.00 C 1$ | $\begin{array}{r} 0.16792 \\ 0.1391 \\ 79 \end{array}$ |  | 0.0001 79 |  |  |  |  |  |  |  |  |  |  |  |
| II | $\begin{array}{r} -0.14121 \\ 0.2145 \\ 79 \end{array}$ | 30 |  |  |  |  |  |  | $\begin{gathered} 0.24127 \\ 0.0322 \\ 79 \end{gathered}$ | $\begin{array}{r} 0.09127 \\ 0.4237 \\ 79 \end{array}$ | $\begin{array}{r} 0.01479 \\ 0.8970 \\ 79 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 79 \end{array}$ | $\begin{gathered} 0.07884 \\ 0.4898 \\ 79 \end{gathered}$ | $\begin{array}{r} -0.02367 \\ -0.8360 \\ 79 \end{array}$ | $\begin{array}{r} 0.17641 \\ 0.1199 \\ 0.199 \end{array}$ | $\begin{array}{r} 0.19120 \\ 0.0914 \\ 79 \end{array}$ | $\begin{array}{r} 0.17685 \\ 0.1196 \\ 79 \end{array}$ | $\begin{array}{r} .04199 \\ 0.7133 \\ \hline 99 \end{array}$ |
| $v$ | $\begin{array}{r} -0.28534 \\ 0.0108 \\ 79 \end{array}$ | $\begin{array}{r} 0.15949 \\ 0.3999 \\ 30 \end{array}$ | $\begin{array}{r} 0.66743 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.55184 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.25120 \\ 0.0255 \\ 79 \end{array}$ | $\begin{array}{r} 79001 \\ \hline \end{array}$ | $\begin{array}{r}79 \\ \hline 0.051\end{array}$ | $\begin{array}{r} 0.0005 \\ 79 \end{array}$ |  | $\begin{array}{r} 0.17228 \\ 0.1290 \\ 79 \end{array}$ |  | $\begin{array}{r} 0.07884 \\ 0.4898 \\ 79 \end{array}$ | 79 |  | $\begin{array}{r} 27321 \\ 0.0148 \\ 79 \end{array}$ | $\begin{array}{r} 22224 \\ 0.0490 \\ 79 \end{array}$ | $\begin{array}{r} 32677 \\ 0.0033 \\ \hline 079 \end{array}$ | $\begin{array}{r} 888787 \\ 0101 \\ \hline 9 \end{array}$ |
| мо | $\begin{array}{r} 0.09341 \\ 0.4129 \\ 79 \end{array}$ | $\begin{array}{r} 0.42010 \\ 0.0208 \\ 30 \end{array}$ | $\begin{aligned} & 0.11788 \\ & 0.2256 \\ & 79 \end{aligned}$ | $\begin{array}{r} 1178 \\ \hline 79 \end{array}$ | $161$ | $\begin{array}{r} 0.05874 \\ 0.6071 \\ 79 \end{array}$ | $\begin{gathered} 0.04984 \\ 0.6627 \\ 79 \end{gathered}$ | $\begin{array}{r} -0.04941 \\ -0.6654 \\ 79 \end{array}$ | $\begin{gathered} 0.26689 \\ 0.0174 \\ 79 \end{gathered}$ | $\begin{array}{r} 0.07575 \\ 0.5070 \\ 79 \end{array}$ | $\begin{gathered} 0.22428 \\ 0.0469 \\ 79 \end{gathered}$ | $\begin{array}{r} -0.02367 \\ 0.8360 \\ 79 \end{array}$ | $\begin{array}{r} 0.31495 \\ 0.0047 \\ 79 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 79 \end{array}$ | $\begin{array}{r} 0.11120 \\ 0.3292 \\ \\ 79 \end{array}$ | $\begin{gathered} 569 \\ 707 \\ 79 \end{gathered}$ | $\begin{aligned} & 64 \\ & 79 \end{aligned}$ | $\begin{gathered} 13 \\ 13 \\ 79 \end{gathered}$ |
| ${ }^{\text {a }}$ | $\begin{array}{r} -0.63223 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} -0.02992 \\ 0.8753 \\ 30 \\ 30 \end{array}$ | $\begin{array}{r} 0.399 c 2 \\ 0.0003 \\ 79 \end{array}$ | $\begin{gathered} 0.42108 \\ 0.0001 \\ 79 \end{gathered}$ | $\begin{array}{r} 0.16858 \\ 0.1375 \\ 79 \end{array}$ | $\begin{array}{r} 0.3087 \\ 0.0056 \\ 79 \end{array}$ | $0.0001$ | $\begin{array}{r} 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.0029 \\ \\ \hline 9 \end{array}$ | $0.0001$ | $\begin{array}{r} 0.27400 \\ 0.0145 \\ 79 \end{array}$ | $\begin{array}{r} 0.17641 \\ 0.199 \\ 0.79 \end{array}$ |  | $\begin{array}{r} 0.11120 \\ 0.3292 \\ \hline 99 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.000 \\ 0.00 \end{array}$ | $\begin{array}{r} 0.57094 \\ 0.0001 \\ 0.09 \end{array}$ | $\begin{array}{r} 0.57753 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 5509 \\ 0001 \\ 79 \end{array}$ |
| ca | $\begin{array}{r} 0.66000 \\ -0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.6337 \\ 30 \end{array}$ | $\begin{array}{r} 0.4465 \\ 0.0001 \\ 79 \end{array}$ | $\begin{gathered} 0.48084 \\ 0.0001 \\ 79 \end{gathered}$ | $\begin{gathered} 0.25484 \\ 0.0234 \\ 79 \end{gathered}$ | $\begin{array}{r} 4.4659 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.56107 \\ 0.0001 \\ \hline 99 \end{array}$ | $\begin{array}{r} 0.65221 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.34253 \\ 0.0020 \\ 79 \end{array}$ | $\begin{gathered} 0.39084 \\ 0.0004 \\ \hline 9 \end{gathered}$ | $\begin{array}{r} 0.29443 \\ 0.0044 \\ 79 \end{array}$ | $\begin{array}{r} 0.19120 \\ 0.0914 \\ 79 \end{array}$ | $\begin{array}{r} 0.22224 \\ 0.0490 \\ 79 \end{array}$ | $\begin{array}{r} 0.15569 \\ 0.1707 \\ \hline 9 \end{array}$ | $\begin{array}{r} 0.57094 \\ 0.0001 \\ 0.09 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 79 \end{array}$ | $\begin{gathered} 0.80068 \\ 0.0001 \\ 79 \end{gathered}$ | $\begin{array}{r} 15147 \\ 0.0001 \\ 79 \end{array}$ |
| SR | $\begin{array}{r} 0.69012 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.34476 \\ 0.0621 \\ 30 \end{array}$ | $\begin{array}{r} 0.54941 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.56819 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.31115 \\ 0.0053 \\ 79 \end{array}$ | $\begin{array}{r} 0.62620 \\ \left.\begin{array}{c} 0.0001 \\ 79 \end{array}\right) \end{array}$ | $\begin{array}{r} 0.63764 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.68896 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.42061 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.53043 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.46264 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.17685 \\ 0.1190 \\ 79 \end{array}$ | $\begin{array}{r} 0.0033 \\ 79 \end{array}$ | $\begin{array}{r} 0.068877 \\ 0.5464 \\ 79 \end{array}$ | $\begin{array}{r} 0.57753 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.80068 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 79 \end{array}$ | $\begin{array}{r} 0.79502 \\ 0.0001 \\ 79 \end{array}$ |
| MG | $\begin{array}{r} -0.71164 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.08988 \\ 0.6367 \\ 30 \end{array}$ | $\begin{array}{r} 0.56533 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.53060 \\ 0.0001 \\ 79 \end{array}$ | $\begin{gathered} 0.34376 \\ 0.0019 \\ 79 \end{gathered}$ | $\begin{array}{r} 0.51188 \\ 0.0001 \\ =\begin{array}{c} 79 \end{array} \end{array}$ | $\begin{array}{r} 0.57892 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.63666 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 0.27885 \\ 0.0128 \\ 0.79 \end{array}$ | $\begin{gathered} 0.36780 \\ 0.0009 \\ 79 \end{gathered}$ | $\begin{array}{r} 0.34602 \\ 0.0018 \\ 79 \end{array}$ | $\begin{array}{r} 0.04199 \\ 0.7133 \\ 79 \end{array}$ | $\begin{array}{r} 0.28787 \\ 0.0101 \\ 079 \end{array}$ | $\begin{array}{r} -0.15913 \\ 0.1613 \\ 79 \end{array}$ | $\begin{array}{r} 0.55509 \\ 0.0001 \\ \hline 79 \end{array}$ | $\begin{array}{r} 0.75147 \\ 0.0019 \\ 79 \end{array}$ | $\begin{array}{r} 0.79502 \\ 0.0001 \\ 79 \end{array}$ | $\begin{array}{r} 00000 \\ 0.0000 \\ 79 \end{array}$ |



| RES ID | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 31 \end{array}$ | $\begin{array}{r} 0.67249 \\ 0.0060 \\ 15 \end{array}$ | $\begin{array}{r} .25146 \\ 0.1724 \\ 31 \end{array}$ | $\begin{array}{r} 0.31000 \\ 0.0897 \\ 31 \end{array}$ | $\begin{array}{r} 0.40153 \\ 0.0252 \\ 31 \end{array}$ | $\begin{array}{r} 0.22590 \\ 0.2217 \\ 31 \end{array}$ | $\begin{array}{r} 0.62739 \\ 0.0002 \\ 31 \end{array}$ | $\begin{array}{r} 0.27760 \\ 0.1305 \\ 31 \end{array}$ | $\begin{array}{r} .14378 \\ -0.4403 \\ 0.41 \end{array}$ | $\begin{array}{r} 0.33146 \\ 0.0342 \\ 31 \end{array}$ | $\begin{array}{r} .04848 \\ 0.7957 \\ 31 \end{array}$ | $\begin{array}{r} 0.09561 \\ 0.6089 \\ 31 \end{array}$ | $\begin{array}{r} .36191 \\ 0.0454 \\ 31 \end{array}$ | $\begin{array}{r} 05155 \\ 5735 \\ 31 \end{array}$ | $\begin{array}{r} 1004 \\ 0001 \\ 001 \\ 31 \end{array}$ | $\begin{array}{r} 056 \\ 002 \\ 002 \\ 31 \end{array}$ | $\begin{array}{r} 873 \\ 003 \\ 003 \\ 31 \end{array}$ | 73 91 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $u$ | $\begin{gathered} 0.67249 \\ 0.0060 \end{gathered}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ \hline \end{array}$ | $\begin{array}{r} 44948 \\ 0.0928 \\ 0.09 \end{array}$ | $\begin{array}{r} -0.24574 \\ 0.3773 \\ 15 \end{array}$ | $\begin{array}{r} -0.40948 \\ 0.1296 \\ 15 \end{array}$ | $\begin{array}{r} 0.19915 \\ 0.4767 \\ 15 \end{array}$ | $\begin{array}{r} 0.56609 \\ 0.0278 \\ 15 \end{array}$ | $\begin{array}{r} 0.64925 \\ 0.0088 \\ 15 \end{array}$ | $\begin{array}{r} -0.28479 \\ 0.3036 \\ 15 \end{array}$ | $\begin{array}{r} -0.06746 \\ 0.812 \\ 15 \end{array}$ | $\begin{array}{r} -0.22391 \\ 0.422 \\ 15 \end{array}$ | $\begin{array}{r} 0.16955 \\ 0.5458 \\ 15 \end{array}$ | $\begin{array}{r} 0.40705 \\ 0.1321 \\ 15 \end{array}$ | $\begin{array}{r} -0.08294 \\ 0.7689 \\ 15 \end{array}$ | $\begin{array}{r} 0.79516 \\ 0.004 \\ 15 \end{array}$ | $\begin{array}{r} 0.64119 \\ 0.0100 \\ 015 \end{array}$ | $\begin{array}{r} -0.6 e 910 \\ -0.0045 \\ 15 \end{array}$ | $\begin{array}{r} 0.27124 \\ 0.3281 \\ 15 \end{array}$ |
| FE | $\begin{array}{r} -0.25146 \\ -0.1724 \\ 31 \end{array}$ | $\begin{array}{r} -0.44948 \\ 0.0928 \\ 15 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 31 \end{array}$ | $\begin{array}{r} 0.52721 \\ 0.0023 \\ 31 \end{array}$ | $\begin{array}{r} 0.17950 \\ 0.3339 \\ 31 \end{array}$ | $\begin{array}{r} 0.22261 \\ 0.2287 \\ 31 \end{array}$ | $\begin{array}{r} 0.15608 \\ 0.4018 \\ 31 \end{array}$ | $\begin{array}{r} 0.06000 \\ 0.7485 \\ 31 \end{array}$ | $\begin{array}{r} 0.7451 \\ 0.71 \end{array}$ | $\begin{array}{r} 0.33679 \\ 0.0639 \\ 31 \end{array}$ | ${ }_{31}^{0.2958}$ | $\begin{array}{r} 0.0194 \\ 31 \end{array}$ |  | $\begin{array}{r} 0.05532 \\ 0.7675 \\ 31 \end{array}$ | $\begin{array}{r} 0.02659 \\ 0.8871 \\ 31 \end{array}$ | $\begin{array}{r} 156 \\ 153 \\ 31 \end{array}$ | $\begin{array}{r} 0.31171 \\ 0.0878 \\ 31 \end{array}$ |  |
| 2 N | $\begin{array}{r} 0.31000 \\ -.0897 \\ 31 \end{array}$ | $\begin{array}{r} 0.3773 \\ 15 \end{array}$ |  |  |  |  |  |  |  |  |  |  | $\begin{gathered} 0.20074 \\ 0.2789 \\ 31 \end{gathered}$ |  |  |  |  |  |
| cu | $\begin{array}{r} -0.40153 \\ 0.0252 \\ 31 \end{array}$ | $\begin{array}{r} \begin{array}{r} 40948 \\ 0.1296 \\ 15 \end{array} \end{array}$ | $\begin{array}{r} 0.17950 \\ 0.3339 \\ 31 \end{array}$ | $\begin{array}{r} 0.41248 \\ 0.0211 \\ 31 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 31 \end{array}$ | $\begin{gathered} 0.40354 \\ 0.0244 \\ 31 \end{gathered}$ | $\begin{array}{r} 0.21370 \\ 0.2484 \\ 31 \end{array}$ | $\begin{array}{r} 0.04054 \\ 0.8286 \\ 31 \end{array}$ | $\begin{array}{r} 0.10606 \\ 0.5701 \\ 31 \end{array}$ | $\begin{array}{r} 0.18235 \\ 0.3262 \\ 31 \end{array}$ | $\begin{array}{r} 0.1588 \\ 31 \end{array}$ | $\begin{array}{r} .14828 \\ 0.4260 \\ 31 \end{array}$ | $\begin{array}{r} 0.31098 \\ 0.0886 \\ 31 \end{array}$ | $\begin{array}{r} 0.02442 \\ 0.8962 \\ 31 \end{array}$ | $\begin{array}{r} 0.12018 \\ 0.5196 \\ 31 \end{array}$ | $\begin{array}{r} 0.01268 \\ 0.9460 \\ 31 \end{array}$ | $\begin{array}{r} 0.22571 \\ 0.2221 \\ 31 \end{array}$ | $\begin{array}{r} 0.43610 \\ 0.0142 \\ 31 \end{array}$ |
| PB | $\begin{array}{r} -0.22590 \\ 0.2217 \\ 31 \end{array}$ | $\begin{array}{r} 0.19915 \\ 0.47675 \\ 15 \end{array}$ | $\begin{array}{r} -0.22261 \\ 0.2287 \\ 31 \end{array}$ | $\begin{array}{r} 40509 \\ -0238 \\ \hline \quad 31 \end{array}$ |  | $\begin{array}{r} 00000 \\ .0000 \\ \mathbf{3 1} \end{array}$ | $\begin{array}{r} 0.27154 \\ 0.1395 \\ 31 \end{array}$ |  | $\begin{array}{r} 0.02949 \\ 0.8749 \\ 31 \end{array}$ | $\begin{array}{r} 0.05786 \\ 0.7572 \\ 31 \end{array}$ | $\begin{array}{r} 0.13611 \\ 0.4653 \\ 31 \end{array}$ | $\begin{array}{r} 0.22736 \\ 0.2187 \\ 31 \end{array}$ | $\begin{array}{r} 0.00438 \\ 0.9813 \\ 31 \end{array}$ | $\begin{array}{r} 0.22391 \\ 0.2259 \\ 31 \end{array}$ | $\begin{array}{r} 118943 \\ 0.3074 \\ 31 \end{array}$ | $\begin{array}{r} 742 \\ 259 \\ 31 \end{array}$ | $\begin{array}{r} 0.08638 \\ 0.6440 \\ 31 \end{array}$ |  |
| MN | $\begin{array}{r} -0.62739 \\ 0.0002 \\ 31 \end{array}$ | $\begin{array}{r} 0.56609 \\ 0.0278 \\ \begin{array}{r} 15 \end{array} \end{array}$ | $\begin{array}{r} 0.15608 \\ 0.4018 \\ 31 \end{array}$ | $\begin{array}{r} 0.33207 \\ 0.0680 \\ 31 \end{array}$ | $\begin{array}{r} 0.21370 \\ 0.2484 \\ 31 \end{array}$ | $\begin{array}{r} 0.27154 \\ 0.1395 \\ 31 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 31 \end{array}$ | $\begin{array}{r} 0.61749 \\ 0.0002 \\ 31 \end{array}$ | $\begin{array}{r} 0.31817 \\ 0.0811 \\ .31 \end{array}$ | $\begin{array}{r} 0.39345 \\ 0.0285 \\ 31 \end{array}$ | $\begin{array}{r} 0.01106 \\ 0.9529 \\ 31 \end{array}$ | $\begin{array}{r} 0.02107 \\ 0.9104 \\ 31 \end{array}$ | $\begin{array}{r} -0.02984 \\ 0.8734 \\ 31 \end{array}$ | $\begin{array}{r} 0.01027 \\ 0.9563 \\ 31 \end{array}$ | $\begin{array}{r} 0.70056 \\ 0.0001 \\ 31 \end{array}$ | $\begin{array}{r} 0.78979 \\ \begin{array}{r} 0.0001 \\ 31 \end{array} \end{array}$ | $\begin{array}{r} 0.68455 \\ 0.0001 \\ 31 \end{array}$ | $\begin{array}{r} 0.34735 \\ 0.0555 \\ 31 \end{array}$ |
| cD | $\begin{array}{r} -0.27760 \\ -1305 \\ 31 \end{array}$ | 0.0088 15 | $\begin{aligned} & 0.7485 \\ & 31 \end{aligned}$ | $\begin{array}{r} 1704 \\ 31 \end{array}$ | $\begin{aligned} & 0.8286 \\ & 31 \end{aligned}$ | $\begin{array}{r} 6541 \\ 31 \end{array}$ | 0.0002 31 | $\begin{array}{r} 00000 \\ .0000 \\ \mathbf{3 1} \end{array}$ | $\begin{array}{r} 1074 \\ \hline \end{array}$ | $\begin{array}{r} 13761 \\ .4604 \\ \hline 31 \end{array}$ | 0.5822 31 | $\begin{array}{r} 0.14700 \\ 0.4300 \\ 31 \end{array}$ | $\begin{array}{r} 0.07768 \\ 0.6779 \\ 31 \end{array}$ | $\begin{array}{r} 0.12390 \\ 0.5066 \\ 31 \end{array}$ | $\begin{array}{r} 0.66811 \\ 0.0001 \\ 31 \end{array}$ | $\begin{array}{r} 0.53972 \\ 0.0017 \\ 31 \end{array}$ | $\begin{array}{r} 0.52258 \\ 0.0025 \\ 31 \end{array}$ | $\begin{array}{r} 0.30645 \\ 0.096 \\ 31 \end{array}$ |
| co | $\begin{array}{r} -0.14378 \\ 0.403 \\ 31 \end{array}$ | $\begin{array}{r} 0.28479 \\ 0.3036 \\ 15 \end{array}$ | $\begin{array}{r} 0.06083 \\ 0.7451 \\ 31 \end{array}$ | $\begin{array}{r} 0.01079 \\ 0.9541 \\ 31 \end{array}$ | $\begin{array}{r} -0.10606 \\ 0.5701 \\ 31 \end{array}$ | $\begin{array}{r} 0.02949 \\ 0.8749 \\ 31 \end{array}$ | $\begin{array}{r} 0.31817 \\ 0.0811 \\ 31 \end{array}$ | $\begin{array}{r} 0.29482 \\ 0.1074 \\ 31 \end{array}$ | $\begin{array}{r} 1.000 c 0 \\ 0.0000 \\ 31 \end{array}$ | $\begin{array}{r} 0.10979 \\ \begin{array}{r} 0.5566 \\ 31 \end{array} \end{array}$ | $\begin{array}{r} 0.23380 \\ 0.2056 \\ 31 \end{array}$ | $\begin{array}{r} 0.02841 \\ 6.8794 \\ 31 \end{array}$ | $\begin{array}{r} -0.17981 \\ 0.3331 \\ 31 \end{array}$ | $\begin{array}{r} -0.02773 \\ 0.8823 \\ 31 \end{array}$ | $\begin{array}{r} 0.24710 \\ 0.1802 \\ 31 \end{array}$ | $\begin{array}{r} 0.26839 \\ 0.1443 \\ 31 \end{array}$ | $\begin{array}{r} 0.37358 \\ 0.0382 \\ 31 \end{array}$ | $\begin{array}{r} 309 \\ 360 \\ 31 \\ 31 \end{array}$ |
| CR | $\begin{array}{r} -0.39146 \\ 0.0342 \\ 31 \end{array}$ | $\begin{array}{r} 0.8112 \\ 15 \end{array}$ | $\begin{array}{r} 0.0639 \\ 31 \end{array}$ | $\begin{array}{r} 1125 \\ 31 \end{array}$ | $\begin{array}{r} 0.18235 \\ 0.3262 \\ 31 \end{array}$ | $\begin{array}{r} 7572 \\ 31 \end{array}$ | $\begin{array}{r} 0285 \\ 31 \end{array}$ | $\begin{array}{r} 0.4604 \\ 31 \end{array}$ | $\begin{array}{r} 0.5566 \\ 31 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 31 \end{array}$ | $\begin{array}{r} 31532 \\ 0.0840 \\ 0.01 \end{array}$ | $\begin{array}{r} 0.00138 \\ 0.9941 \\ 0.91 \end{array}$ | $\begin{array}{r} 0.16526 \\ 0.3743 \\ 31 \end{array}$ | $\begin{array}{r} 23392 \\ 0.2053 \\ 0 . \\ 31 \end{array}$ | $\begin{array}{r} 0.14744 \\ 0.4286 \\ 31 \end{array}$ | $\begin{array}{r} 0.45807 \\ 0.0096 \\ 31 \end{array}$ | $\begin{array}{r} 0.31009 \\ 0.0896 \\ 31 \end{array}$ | $\begin{array}{r} 42424 \\ 0.014 \\ 31 \end{array}$ |
| n | $3$ | $\begin{aligned} & 224 \\ & 15 \end{aligned}$ | $\begin{gathered} 0.19397 \\ 0.2958 \\ 31 \end{gathered}$ | $\begin{array}{r} 0.29939 \\ 0.1018 \\ 31 \end{array}$ | $\begin{array}{r} 0.25938 \\ 0.1588 \\ 31 \end{array}$ | $\begin{array}{r} 13611 \\ -4653 \\ \hline 31 \end{array}$ | $\begin{array}{r} 91106 \\ .9529 \\ .31 \end{array}$ | $\begin{array}{r} 0.10276 \\ 0.5822 \\ 31 \end{array}$ | $\begin{array}{r} .23380 \\ 0.2056 \\ 31 \end{array}$ | $\begin{array}{r} 31532 \\ 3.0840 \\ \quad 31 \end{array}$ | $\begin{array}{r} 1.00000 \\ \begin{array}{r} 0.0000 \\ 31 \end{array} \end{array}$ | $\begin{array}{r} -0.10339 \\ 0.5799 \\ 31 \end{array}$ | $\begin{gathered} 0.21909 \\ 0.2364 \\ 31 \end{gathered}$ | $\begin{array}{r} 0.09477 \\ 0.6121 \\ 31 \end{array}$ | $\begin{array}{r} 0.11939 \\ 0.5223 \\ 31 \end{array}$ | $\begin{array}{r} 0.06154 \\ 0.7423 \\ 31 \end{array}$ | $\begin{array}{r} .34520 \\ 0.0572 \\ 31 \end{array}$ | $\begin{array}{r} 408 \\ \hline 060 \\ 31 \end{array}$ |
| II | $\begin{array}{r} -0.09561 \\ 0.6089 \\ 31 \end{array}$ | $\begin{array}{r} 0.16955 \\ 0.5458 \\ 15 \end{array}$ | $\begin{array}{r} 0.41763 \\ 0.0194 \\ 31 \end{array}$ | $\begin{array}{r} 0.21885 \\ 0.23 \in 9 \\ 31 \end{array}$ | $\begin{array}{r} 0.14828 \\ 0.4260 \\ 31 \end{array}$ | $\begin{array}{r} 0.22736 \\ 0.2187 \\ 31 \end{array}$ | $\begin{array}{r} 0.9104 \\ 01 \end{array}$ | $\begin{array}{r} 14700 \\ 0.4300 \\ 31 \end{array}$ | $\begin{array}{r} -0.02841 \\ -0.8794 \\ 31 \end{array}$ | $\begin{array}{r} 0.00138 \\ 0.9941 \\ 31 \end{array}$ | $0.5799$ | $\begin{array}{r} 1.00000 \\ -0.0000 \\ 0.0 \end{array}$ | $\begin{array}{r} 0.32831 \\ 0.0714 \\ 31 \end{array}$ | $\begin{array}{r} 0.12357 \\ 0.5078 \\ 31 \end{array}$ | $\begin{array}{r} 0.06140 \\ 0.7428 \\ 31 \end{array}$ | $\begin{array}{r} 0.11849 \\ 0.5255 \\ 31 \end{array}$ | $\begin{array}{r} 0.08428 \\ 0.6521 \\ 31 \end{array}$ | $\begin{array}{r} 0.04877 \\ 0.7944 \\ 31 \end{array}$ |
| $v$ | $\begin{array}{r} -0.36191 \\ 0.0454 \\ 31 \end{array}$ | $\begin{array}{r} -0.40705 \\ 0.1321 \\ 15 \end{array}$ | $\begin{array}{r} 0.37432 \\ 0.0380 \\ 31 \end{array}$ | $\begin{array}{r} 0.20074 \\ 0.2789 \\ 31 \end{array}$ | $\begin{array}{r} 0.31098 \\ 0.0886 \\ 31 \end{array}$ | $\begin{array}{r} 0.00438 \\ 0.9813 \\ 0.91 \end{array}$ | $\begin{array}{r} 0.02984 \\ 0.8734 \\ 31 \end{array}$ | $\begin{array}{r} 0.07768 \\ 0.6779 \\ 31 \end{array}$ | $\begin{array}{r} -0.17981 \\ 0.3331 \\ 31 \end{array}$ | $\begin{array}{r} 0.16526 \\ 0.3743 \\ 31 \end{array}$ | $\begin{array}{r} 0.21909 \\ 0.2364 \\ 31 \end{array}$ | $\begin{array}{r} 0.32831 \\ 0.0714 \\ 0.31 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 31 \end{array}$ | $\begin{array}{r} 0.06813 \\ 0.7157 \\ 31 \end{array}$ | $\begin{array}{r} 0.25219 \\ 0.1711 \\ 31 \end{array}$ | $\begin{array}{r} 0.19866 \\ 0.2840 \\ 31 \end{array}$ | $\begin{array}{r} .22548 \\ 0.2226 \\ 31 \end{array}$ | $\begin{array}{r} 0.11133 \\ 0.5510 \\ 31 \end{array}$ |
| Mо | $\begin{array}{r} 0.10515 \\ 0.5735 \\ 31 \end{array}$ | $\begin{array}{r} 0.08294 \\ 0.7689 \\ 15 \end{array}$ | $\begin{array}{r} 0.05532 \\ 0.7675 \\ 31 \end{array}$ | $\begin{array}{r} -0.21058 \\ 0.2546 \\ 31 \end{array}$ | $\begin{array}{r} 0.02442 \\ 0.8962 \\ 31 \end{array}$ | $\begin{array}{r} -0.22391 \\ 0.2259 \\ 31 \end{array}$ | $\begin{array}{r} 0.01027 \\ 0.9563 \\ 31 \end{array}$ | $\begin{array}{r} 0.12390 \\ 0.5066 \\ 31 \end{array}$ | $\begin{array}{r} 0.02773 \\ 0.8823 \\ 31 \end{array}$ | $\begin{array}{r} 0.23392 \\ 0.2053 \\ 31 \end{array}$ | $\begin{array}{r} 0.09477 \\ 0.6121 \\ \quad .31 \end{array}$ | $\begin{array}{r} 0.12357 \\ 0.5078 \\ 31 \end{array}$ | $\begin{array}{r} 0.06813 \\ 0.7157 \\ 31 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 31 \end{array}$ | $\begin{array}{r} 0.073322 \\ 0.6951 \\ \quad 31 \end{array}$ | $\begin{array}{r} -0.00297 \\ 0.9873 \\ 31 \end{array}$ | $\begin{array}{r} 0.09640 \\ 0.6059 \\ 31 \end{array}$ | $\begin{array}{r} 0.00503 \\ 0.9786 \\ \quad 31 \end{array}$ |
| ${ }^{\text {a }}$ | $\begin{array}{r} -0.64004 \\ 0.0001 \\ 31 \end{array}$ | $\begin{array}{r} 0.79516 \\ 0.0004 \\ 15 \end{array}$ | $\begin{array}{r} 0.02659 \\ 0.8771 \\ 31 \end{array}$ | $\begin{array}{r} 0.6397 \\ 31 \end{array}$ | $\begin{array}{r} 0.12018 \\ 0.5196 \\ 31 \end{array}$ | $\begin{gathered} 0.18943 \\ 0.3074 \\ 31 \end{gathered}$ | $\begin{array}{r} 0.70056 \\ 0.0001 \\ 31 \end{array}$ | $\begin{array}{r} 0.66811 \\ 0.0001 \\ 31 \end{array}$ | $\begin{array}{r} 0.24710 \\ 0.1802 \\ 31 \end{array}$ | $\begin{array}{r} 0.14744 \\ 0.4286 \\ 31 \end{array}$ | $\begin{array}{r} 0.11939 \\ 0.523 \\ 31 \end{array}$ | $\begin{array}{r} 0.06140 \\ 0.7428 \\ 31 \end{array}$ | $\begin{array}{r} 0.25219 \\ 0.1711 \\ 31 \end{array}$ | $\begin{array}{r} 0.07332 \\ 0.6951 \\ 31 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 31 \end{array}$ | $\begin{array}{r} 0.65219 \\ \mathbf{c} .0001 \\ 31 \end{array}$ | $\begin{array}{r} 0.60755 \\ 0.0003 \\ 31 \end{array}$ | $\begin{array}{r} 0.09962 \\ 0.5939 \\ 31 \end{array}$ |
| cA | $\begin{array}{r} -0.69056 \\ 0.0001 \\ 31 \end{array}$ | $\begin{array}{r} -0.64119 \\ 0.0100 \\ 15 \end{array}$ | $\begin{array}{r} 0.43156 \\ 0.0153 \\ 31 \end{array}$ | $\begin{array}{r} C_{.} 31008 \\ 0.0896 \\ 31 \end{array}$ | $\begin{array}{r} -0.01268 \\ 0.9460 \\ 31 \end{array}$ | $\begin{array}{r} -0.01742 \\ 0.9259 \\ 31 \end{array}$ | $\begin{array}{r} 0.78979 \\ 0.0001 \\ 31 \end{array}$ | $\begin{array}{r} 0.53972 \\ 0.0017 \\ 31 \end{array}$ | $\begin{array}{r} 0.26839 \\ 0.1443 \\ 31 \end{array}$ | $\begin{array}{r} 0.45807 \\ 0.0096 \\ 31 \end{array}$ | $\begin{array}{r} 0.06154 \\ 0.7423 \\ 31 \end{array}$ | $\begin{array}{r} 0.11849 \\ 0.5255 \\ -31 \end{array}$ | $\begin{array}{r} 0.19866 \\ 0.2840 \\ 31 \end{array}$ | $\begin{array}{r} -0.00297 \\ -0.9873 \\ 31 \end{array}$ | $\begin{array}{r} 0.65219 \\ 0.0001 \\ 31 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 31 \end{array}$ | $\begin{array}{r} 0.71226 \\ 0.0001 \\ 31 \end{array}$ | $\begin{array}{r} 0.27358 \\ 0.1364 \\ 31 \end{array}$ |
| SR | $\begin{array}{r} -0.60873 \\ 0.0003 \\ 31 \end{array}$ | $\begin{array}{r} 0.68910 \\ 0.0045 \\ 15 \end{array}$ | $\begin{array}{r} 0.31171 \\ 0.0878 \\ 31 \end{array}$ | $\begin{array}{r} 0.26502 \\ 0.1496 \\ 31 \end{array}$ | $\begin{array}{r} 0.22571 \\ 0.2221 \\ 31 \end{array}$ | $\begin{array}{r} 0.08638 \\ 0.6440 \\ 31 \end{array}$ | $\begin{array}{r} 0.68455 \\ 0.0001 \\ 31 \end{array}$ | $\begin{array}{r} 0.52298 \\ 0.0025 \\ 31 \end{array}$ | $\begin{array}{r} 0.37398 \\ 0.0382 \\ 31 \end{array}$ | $\begin{array}{r} 0.31009 \\ 0.0896 \\ \quad 31 \end{array}$ | $\begin{array}{r} 0.34520 \\ 0.0572 \\ 31 \end{array}$ | $\begin{array}{r} 0.08428 \\ 0.6521 \\ 31 \end{array}$ | $\begin{gathered} 0.22548 \\ 0.2226 \\ 32 \end{gathered}$ | $\begin{array}{r} 0.09640 \\ 0.6059 \\ 31 \end{array}$ | $\begin{array}{r} 0.60755 \\ 0.0003 \\ 31 \end{array}$ | $\begin{array}{r} 0.71226 \\ 0.0001 \\ 31 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 31 \end{array}$ | $\begin{array}{r} 0.28399 \\ 0.1215 \\ 31 \end{array}$ |
| MG | $\begin{array}{r} -0.30173 \\ 0.0990 \\ 31 \end{array}$ | $\begin{array}{r} -0.27124 \\ 0.381 \\ 0.35 \end{array}$ | $\begin{array}{r} 0.37708 \\ 0.0365 \\ 31 \end{array}$ | $\begin{array}{r} 0.16342 \\ 0.3797 \\ 31 \end{array}$ | $\begin{array}{r} 0.43610 \\ 0.0142 \\ 31 \end{array}$ | $\begin{array}{r} 0.00722 \\ 0.9693 \\ 31 \end{array}$ | $\begin{array}{r} 0.34735 \\ 0.0555 \\ 31 \end{array}$ | $\begin{array}{r} 0.30645 \\ 0.0936 \\ 31 \end{array}$ | $\begin{array}{r} -0.06309 \\ 0.7760 \\ 31 \end{array}$ | $\begin{gathered} 0.62424 \\ 0.0174 \\ 31 \end{gathered}$ | $\begin{array}{r} -.12408 \\ 0.5060 \\ 31 \end{array}$ | $\begin{array}{r} 0.04877 \\ 0.7944 \\ =31 \end{array}$ | $\begin{array}{r} 0.11133 \\ 0.5510 \\ 31 \end{array}$ | $\begin{array}{r} 0.00503 \\ 0.9786 \\ -31 \end{array}$ | $\begin{array}{r} 0.09962 \\ 0.5939 \\ 31 \end{array}$ | $\begin{array}{r} 0.27358 \\ 0.1364 \\ 31 \end{array}$ | $\begin{array}{r} 0.28399 \\ 0.1215 \\ 31 \end{array}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \\ 31 \end{array}$ |



| ID | 0 | FE | 2N | cu | PB | MN | CD | co | CR | NI | II |  | мо | AG | cA | SR | MG |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} 1.00000 \\ 0.0000 \end{array}$ | $\begin{gathered} 0.31401 \\ 0.4488 \end{gathered}$ | $0 .$ | $0.940$ | -93 | $\begin{array}{r} -0.00778 \\ 0.9854 \end{array}$ | $0.52$ | $\begin{array}{r} -0.31235 \\ 0.4513 \end{array}$ | $\begin{array}{rr} 5 & -0.36772 \\ 3 & 0.3702 \end{array}$ | $\begin{array}{r} 0.373 \\ 0.36 \end{array}$ | $\begin{array}{r} 0.09778 \\ 0.8178 \end{array}$ | $\begin{array}{r} 0.21105 \\ 0.6159 \end{array}$ | $\begin{array}{r} 0.00831 \\ 0.9844 \end{array}$ | $\begin{array}{r} -0.15868 \\ 0.7074 \end{array}$ | $\begin{array}{r} -0.24048 \\ 0.5662 \end{array}$ | $\begin{array}{r} 0.40213 \\ 0.3233 \end{array}$ | $\begin{aligned} & 3452 \\ & 9353 \\ & 935 \end{aligned}$ | $\begin{array}{r} 0.23956 \\ 0.5677 \end{array}$ |
| $401$ | $\begin{array}{r} 1.00 \\ 0.0 \end{array}$ | $\begin{array}{r} 0.390 \\ 0.33 \end{array}$ | $\begin{gathered} 0.23097 \\ 0.5821 \end{gathered}$ | $\begin{gathered} 0.20621 \\ 0.6242 \end{gathered}$ | $\begin{gathered} 0.71265 \\ 0.0473 \end{gathered}$ | $\begin{array}{r} -0.788 \\ 0.02 \end{array}$ | $\begin{gathered} 0.4717 \\ 0.238 \end{gathered}$ | $\begin{array}{r} -0.59231 \\ 0.1218 \end{array}$ | $\begin{gathered} 0.20889 \\ 0.6196 \end{gathered}$ | $\begin{array}{r} -0.11143 \\ 0.7928 \end{array}$ | $\begin{array}{r} 0.80049 \\ 0.0170 \end{array}$ |  | $17$ | $\begin{array}{r} 30933 \\ 0.4559 \end{array}$ | $\begin{array}{r} 0.68648 \\ 0.0601 \end{array}$ | $\begin{array}{r} 0.76212 \\ 0.0279 \end{array}$ | $\begin{array}{r} 0.74996 \\ 0.0321 \end{array}$ |
| $\begin{array}{r} -0.03 \\ 0.9 \end{array}$ | $\begin{array}{r} -0.39063 \\ 0.3387 \end{array}$ | c. | $0 .$ | $0 .$ | $0.53$ | $\begin{array}{r} 0.25577 \\ 0.5409 \end{array}$ | $0.6$ |  |  | $\begin{gathered} 0.93893 \\ 0.0005 \end{gathered}$ | $\begin{array}{r} -0.22817 \\ 0.5868 \end{array}$ | $\begin{array}{r} -0.18574 \\ 0.6597 \end{array}$ | $\begin{array}{r} 0.75133 \\ 0.0316 \end{array}$ | 9 | $\begin{aligned} & 58 \\ & 84 \end{aligned}$ | $\begin{aligned} & 18866 \\ & \hline .6546 \end{aligned}$ | $.74$ |
| $\begin{array}{r} 0.03 \\ 0.9 \end{array}$ | $\begin{gathered} 0.2 \\ 0 . \end{gathered}$ | ${ }_{0.61}^{0.21}$ |  |  | $0.7$ |  | $0.5$ |  | $\begin{array}{r} -0.21340 \\ 0.6119 \end{array}$ |  |  | $\begin{array}{r} 0.86181 \\ 0.0059 \end{array}$ | $\begin{array}{r} -0.23169 \\ 0.5809 \end{array}$ | $6$ | $\begin{aligned} & 0.57265 \\ & 0.1379 \end{aligned}$ | $\begin{aligned} & 93 \\ & 88 \end{aligned}$ |  |
| $\begin{array}{r} -0.032 \\ 0.93 \end{array}$ | $\begin{gathered} 0.2 \\ 0 . \end{gathered}$ | $0.6$ |  |  | $\begin{gathered} 0.3 \\ 0 . \end{gathered}$ | $0 .$ | $\begin{gathered} 0.628 \\ 0.09 \end{gathered}$ | $0.56$ | $0.57$ |  |  | $\begin{gathered} 0.15265 \\ 0.7182 \end{gathered}$ | $\begin{array}{r} 0.59532 \\ 0.1195 \end{array}$ | $\begin{array}{r} 0.09669 \\ 0.8198 \end{array}$ | $\begin{array}{r} 0.73171 \\ 0.0391 \end{array}$ | $\begin{array}{r} 0.62101 \\ 0.1003 \end{array}$ | $\begin{gathered} 0.53712 \\ 0.1698 \end{gathered}$ |
| $\begin{array}{r} -0.00 \\ 0.9 \end{array}$ |  | $-0.2$ |  | $0.3 .$ | ${ }_{0}^{1}$ | $\begin{array}{r} -0.28556 \\ 0.4930 \end{array}$ | $0.6$ | $0 .$ |  |  | $0.5$ | $\begin{gathered} 0.76375 \\ 0.0274 \end{gathered}$ | $\begin{array}{r} -0.30737 \\ 0.4590 \end{array}$ | $54$ | $\begin{array}{r} 62010 \\ \mathbf{6} 1010 \end{array}$ | $25$ | $\begin{gathered} 0.72215 \\ 0.0431 \end{gathered}$ |
| $0.2$ | -0. | $\begin{gathered} 0.2 \\ 0 . \end{gathered}$ |  |  | $0.2$ | $0$ | $0.1$ | $0.6$ |  | $-0.02459$ | $\begin{array}{r} -0.90522 \\ 0.0020 \end{array}$ | $0.2$ | $\begin{aligned} & 61 \\ & 94 \end{aligned}$ | $\begin{aligned} & 0.7 \\ & 0.7 \end{aligned}$ | -0.30246 0.4665 |  |  |
| $\begin{array}{r} -0.3123 \\ 0.451 \end{array}$ | $0.4$ | $\begin{aligned} & 0.1 \\ & 0.1 \end{aligned}$ | $0 .$ | $0.6$ | $0 .$ | $\begin{array}{r} -0.10857 \\ 0.7980 \end{array}$ |  |  |  |  | $\begin{gathered} 0.176 \\ 0.6 \end{gathered}$ | $0.5521$ | $0.56$ | $\begin{gathered} 0.17733 \\ 0.6744 \end{gathered}$ | $\begin{gathered} 0.69114 \\ 0.0577 \end{gathered}$ | $\begin{aligned} & .70155 \\ & 0.0525 \end{aligned}$ | $\begin{gathered} 0.72238 \\ 0.0430 \end{gathered}$ |
| $\begin{array}{r} 0.3677 \\ 0.370 \end{array}$ | $\begin{gathered} -0.59231 \\ 0.1218 \end{gathered}$ | $\begin{gathered} 0.49 \\ 0.2 \end{gathered}$ | $\begin{gathered} 0.43439 \\ 0.2822 \end{gathered}$ | $\begin{array}{r} 0.2419 \\ 0.563 \end{array}$ | $\begin{gathered} 0.04695 \\ 0.9121 \end{gathered}$ | $\begin{gathered} 0.626 \\ 0.09 \end{gathered}$ | $\begin{aligned} & 0.120 \\ & 0.77 \end{aligned}$ | $\begin{gathered} 1.0 \\ 0.0 \end{gathered}$ | $\begin{array}{r} -0.47039 \\ 0.2395 \end{array}$ |  | $\begin{array}{r} -0.61025 \\ 0.1081 \end{array}$ | $\begin{aligned} & .45033 \\ & .02628 \\ & 0.2628 \end{aligned}$ | $\begin{array}{r} 0.036 \\ 0.93 \end{array}$ | $1.20$ | $\begin{array}{r} -0.25430 \\ 0.5433 \end{array}$ |  |  |
| $\begin{gathered} 0.373 \\ 0.36 \end{gathered}$ |  | $\begin{array}{r} -0.06219 \\ 0.8837 \end{array}$ | $\begin{array}{r} -0.21340 \\ 0.6119 \end{array}$ | $\begin{gathered} 0.23 \\ 0.5 \end{gathered}$ | $\begin{array}{r} 0.07828 \\ 0.8538 \end{array}$ | $\begin{array}{r} 0.38 \\ 0.3 \end{array}$ | $0.0$ | 0.2 | $0.0$ | $\begin{array}{r} 0.01 \\ 0.9 \end{array}$ | $\begin{array}{r} 0.199 \\ 0.63 \end{array}$ | $\begin{array}{r} -0.21752 \\ 0.6048 \end{array}$ | $\begin{array}{r} 0.13557 \\ 0.7489 \end{array}$ | $\begin{array}{r} -0.28321 \\ 0.4967 \end{array}$ | $\begin{array}{r} 0.20933 \\ 0.6288 \end{array}$ | $\begin{array}{r} 0.05 \\ 0.8 \end{array}$ | .04745 |
| $\begin{array}{r} 0.097 \\ 0.81 \end{array}$ | $\begin{gathered} -0.1 \\ 0.1 \end{gathered}$ | $\begin{gathered} 0.93 \\ 0.0 \end{gathered}$ | $\begin{array}{r} 0.33370 \\ 0.4192 \end{array}$ |  | $0 .$ | $0 .$ |  | $0$ |  | $\begin{array}{r} 1.00000 \\ 0.0000 \end{array}$ |  |  | $\begin{gathered} 0.71402 \\ 0.0466 \end{gathered}$ | $\begin{array}{r} 0.28115 \\ 0.5000 \end{array}$ | $\begin{array}{r} 0.37092 \\ 0.3657 \end{array}$ | $\begin{gathered} 4 E \\ 67 \end{gathered}$ | $\begin{aligned} & 60 \\ & 27 \end{aligned}$ |
| $0.615$ |  |  |  | $\begin{array}{r} 0.10848 \\ 0.7982 \end{array}$ | $\begin{gathered} 0.27549 \\ 0.5090 \end{gathered}$ | $\begin{aligned} & 0.905 \\ & 0.00 \end{aligned}$ | $0.67$ | $0.61$ |  | $0.01$ | $\begin{array}{r} 1.00000 \\ 0.0000 \end{array}$ | $0.3$ | 0.321 0.43 | 0.72065 0.0437 | 0.40447 0.3203 | 0.76526 0.0269 | 0.67315 0.0673 |
| $\begin{array}{r} 0.008 \\ 0.98 \end{array}$ |  | $0.6$ | $0 .$ | 0.152 0.71 | $\begin{gathered} 0.76375 \\ 0.0274 \end{gathered}$ | $0.56$ | $\begin{array}{r} 0.2489 \\ 0.552 \end{array}$ | $\begin{array}{ll} 6.450 \\ 1 & 0.26 \\ 0 \end{array}$ | $\begin{array}{r} -0.21752 \\ 0.6048 \end{array}$ |  | $\begin{array}{r} -0.35091 \\ 0.3941 \end{array}$ | $00$ | $\begin{gathered} 0.62 \\ 0.0 \end{gathered}$ | $\begin{aligned} & 0.69974 \\ & 0.0533 \end{aligned}$ | $\begin{gathered} 0.24344 \\ 0.5613 \end{gathered}$ | $0.8274$ | $\begin{gathered} 0.16909 \\ 0.6889 \end{gathered}$ |
| $\begin{array}{r} -0.1 \\ 0 . \end{array}$ | ${ }^{-0.0} 0$ | $0.1$ |  | $\begin{array}{r} 0.59532 \\ 0.1195 \end{array}$ | $\begin{aligned} & 0.3 \\ & 0 . \end{aligned}$ | $\begin{array}{r} -0.191 \\ 0.64 \end{array}$ | $\begin{array}{r} 0.2425 \\ 0.562 \end{array}$ | $\begin{array}{cc} 5 & 0.03684 \\ 7 & 0.9310 \end{array}$ | 0.135 0.74 | $\begin{aligned} & 0.714 \\ & 0.04 \end{aligned}$ | $\begin{gathered} 0.321 \\ 0.43 \end{gathered}$ | $\begin{array}{r} 0.62 \\ 0.0 \\ 0.0 \end{array}$ | $0.0$ | $\begin{array}{r} 0.54055 \\ 0.1666 \end{array}$ | 0.23555 | 0.52742 0.1792 | 0.32666 0.4297 |
| $\begin{array}{r} -0.24048 \\ 0.5662 \end{array}$ | $\begin{array}{r} 0.3093 \\ 0.455 \end{array}$ | $\begin{array}{r} -0.1354 \\ 0.749 \end{array}$ | $\begin{gathered} 0.58156 \\ 0.1305 \end{gathered}$ | $\begin{array}{r} 0.09669 \\ 0.8198 \end{array}$ | $\begin{gathered} 0.31394 \\ 0.4489 \end{gathered}$ | $\begin{array}{r} 0.78063 \\ 0.0222 \end{array}$ | $\begin{gathered} 0.1773 \\ 0.674 \end{gathered}$ |  | $0.4$ | $\begin{array}{r} .28115 \\ 0.5000 \end{array}$ | $\begin{array}{r} 0.72065 \\ 0.0437 \end{array}$ | $\begin{gathered} 0.69974 \\ 0.0533 \end{gathered}$ | $\begin{gathered} 0.54055 \\ 0.1666 \end{gathered}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \end{array}$ | $\begin{array}{r} 0.00065 \\ 0.9988 \end{array}$ | 0.40514 0.3194 | . 246885 |
| $\begin{array}{r} 0.40213 \\ 0.3233 \end{array}$ | $\begin{gathered} 0.68648 \\ 0.0601 \end{gathered}$ | $\begin{array}{r} 0.20958 \\ 0.6184 \end{array}$ | $\begin{gathered} 0.57265 \\ 0.1379 \end{gathered}$ | $\begin{array}{r} 0.73171 \\ 0.0391 \end{array}$ | $\begin{array}{r} 0.62010 \\ 0.1010 \end{array}$ | $\begin{array}{r} -0.30246 \\ 0.4665 \end{array}$ | $\begin{gathered} 0.691 \\ 0.05 \end{gathered}$ | $\begin{array}{r} -0.25430 \\ 0.5433 \end{array}$ | $\begin{gathered} 0.20933 \\ 0.6188 \end{gathered}$ | $\begin{gathered} 0.37092 \\ 0.3657 \end{gathered}$ | $\begin{aligned} & 0.40447 \\ & 0.3203 \end{aligned}$ | $\begin{gathered} 0.243 \\ 0.56 \end{gathered}$ | $\begin{array}{r} 0.23555 \\ 0.5744 \end{array}$ | $\begin{gathered} c .00065 \\ 0.9988 \end{gathered}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \end{array}$ | $\begin{array}{r} 0.77963 \\ 0.0225 \end{array}$ | $\begin{gathered} 0.60407 \\ 0.1127 \end{gathered}$ |
| $\begin{gathered} 0.03452 \\ 0.9353 \end{gathered}$ | $\begin{gathered} 0.76212 \\ 0.0279 \end{gathered}$ | $\begin{gathered} 0.18866 \\ 0.6546 \end{gathered}$ | $\begin{gathered} 0.23293 \\ 0.5788 \end{gathered}$ | $\begin{array}{r} 0.62101 \\ 0.1003 \end{array}$ | $\begin{gathered} 0.52425 \\ 0.1823 \end{gathered}$ | $\begin{array}{r} -0.62364 \\ 0.0985 \end{array}$ | $\begin{array}{r} 0.7015 \\ 0.052 \end{array}$ | $\begin{array}{rr} 5 & -0.32623 \\ 5 & 0.4303 \end{array}$ | $\begin{gathered} 0.05374 \\ 0.8994 \end{gathered}$ | $\begin{array}{r} 0.37448 \\ 0.3607 \end{array}$ | $\begin{array}{r} 0.765 \\ 0.02 \end{array}$ | $\begin{array}{r} -0.09260 \\ 0.8274 \end{array}$ | $\begin{gathered} 0.52742 \\ 0.1792 \end{gathered}$ | $\begin{array}{r} -0.40514 \\ 0.3194 \end{array}$ | $\begin{gathered} 0.77963 \\ 0.0225 \end{gathered}$ | $\begin{array}{r} 1.00000 \\ 0.0000 \end{array}$ | $\begin{array}{r} 0.89888 \\ 0.0024 \end{array}$ |
| $\begin{array}{r} 0.23956 \\ 0.5677 \end{array}$ | 0.7499 0.032 | 0.03174 0.9405 | 0.36073 0.3800 | 0.53712 0.1698 | 0.72215 0.0431 | -0.60760 0.1101 | 0.72238 0.0430 | $\begin{array}{r} -0.135 \\ -0.74 \end{array}$ | 0.04745 0.9112 | $\begin{array}{r} 0.24860 \\ 0.5527 \end{array}$ | $\begin{gathered} 0.67315 \\ 0.0673 \end{gathered}$ | $\begin{array}{r} 0.16909 \\ 0.6889 \end{array}$ | $\begin{array}{r} 0.32666 \\ 0.4297 \end{array}$ | $\begin{array}{r} -0.24685 \\ 0.5556 \end{array}$ | $\begin{array}{r} 0.60407 \\ 0.1127 \end{array}$ | $\begin{gathered} 0.89888 \\ 0.0024 \end{gathered}$ | $\begin{array}{r} 1.00000 \\ 0.00000 \end{array}$ |

APPENDIX D

FACTOR ANALYSIS

FACTOR ANALYSIS CF LOW URANIUM CHERT-----NORMALIZED DATA BY LOG TRANSFORMATICN ROTATION METHOD: VARIMAX

|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| EIGENVALUES | 7.041928 | 2.516572 | 1.230482 | 0.986920 | 0.580261 | 0.439499 | 0.143062 |  |
| PORTION | 0.542 | 0.194 | 0.095 | 0.076 | 0.045 | 0.034 | 0.011 |  |
| CUM PCRTION | 0.542 | 0.735 | 0.830 | 0.906 | 0.950 | 0.984 | 0.995 |  |
|  |  |  | 9 | 10 | 11 | 12 | 13 |  |
|  |  | 9 | 10 | 12 |  |  |  |  |
| EIGENVALUES | 0.061278 | 0.000000 | 0.000000 | 0.000000 | -0.000000 | -0.000000 |  |  |
| PORTION | 0.005 | 0.000 | 0.000 | 0.000 | -0.000 | -0.000 |  |  |
| CUM PCRTION | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |  |  |

ROTATED FACTOR PATTERN

|  |  | FACTOR1 | FACTOR2 |
| :--- | ---: | ---: | ---: | FACTOR3

FACTOR ANALYSIS CF LOH URANIUM LIMESTONE———-NORMALIZED DATA BY LOG TRANSFORMATION INITIAL FACTOR METHOD: PRINCIPAL AXIS


FACTOR PATTERN

|  | FACTOR1 | FACTOR2 | FACTOR3 |
| :--- | ---: | ---: | ---: |
|  |  |  |  |
| RES ID | -0.92522 | -0.12514 | -0.01850 |
| U | -0.46886 | 0.29713 | 0.63251 |
| FE | 0.57084 | -0.68935 | -0.38852 |
| ZN | 0.29015 | -0.74921 | -0.43933 |
| PB | 0.74922 | -0.35411 | 0.02567 |
| CD | 0.82250 | 0.54821 | -0.12883 |
| MN | 0.92899 | 0.26672 | 0.09605 |
| SR | 0.53654 | 0.76483 | 0.03188 |
| CO | 0.75917 | -0.54617 | 0.27960 |
| MO | -0.02249 | 0.65213 | -0.63859 |
| V | 0.78140 | 0.01115 | 0.35643 |
| CA | 0.90715 | 0.35955 | -0.14301 |
| MG | 0.43652 | -0.26322 | 0.53535 |

> FACTCR ANALYSIS OF LOW URANIUM SANDSTONE————NORMALIZED DATA BY LOG TRANSFORMATION INITIAL FACTOR METHOD: PRINCIPAL AXIS

|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EIGENVALUES | 4.585399 | 1.130211 | 1.097418 | 0.929388 | 0.470358 | 0.364690 | 0.233674 | 0.121931 | 0.066930 |
| PORTION | 0.509 | 0.126 | 0.122 | 0.103 | 0.052 | 0.041 | 0.026 | 0.014 | 0.007 |
| CUM PORTICN | 0.509 | 0.635 | 0.757 | 0.860 | 0.913 | 0.953 | 0.979 | 0.993 | 1.000 |
|  |  |  | 3 F | TORS WILL | BE RETAI |  |  |  |  |

FACTOR PATTERN
FACTOR1 FACTOR2 FACTOR3

| RESID | -0.83372 | 0.31228 | 0.00373 |
| :--- | ---: | ---: | ---: |
| FE | 0.70107 | 0.57277 | -0.08902 |
| CU | 0.39280 | -0.25417 | -0.04357 |
| ZN | 0.71461 | 0.38674 | -0.41209 |
| MN | 0.85375 | -0.31673 | -0.09879 |
| SR | 0.90118 | -0.16832 | -0.07045 |
| CO | 0.54545 | -0.25846 | 0.70164 |
| V | 0.45180 | 0.54315 | 0.61919 |
| MG | 0.83139 | $-6.04 E-05$ | -0.16540 |

FACTOR ANALYSIS OF LOW URANIUM SHALE————NORMALIZED DATA BY LOG IRANSFORMATION

## ROTATIUN METHOD: VARIMAX



```
    FACTOR ANALYSIS OF HIGH URANIUM SHALE-----NORMALIZED DATA BY LOG TRANSFDRMATION
```

INITIAL FACTOR METHOD: PRINCIPAL AXIS


## vita

Marvin Milton Abbott Candidate for the Degree of Master of<br>Master of Science

Thesis: A BASIC EVALUATION OF THE URANIUM POTENTIAL OF THE MORRISON FORMATION OF NORTHWESTERN CIMARRON COUNTY, OKLAHOMA, AND AdJOINING AREAS OF NEW MEXICO AND COLORADO

Major Field: Geology
Biographical:
Personal Data: Born in Ada, Oklahoma, May 23, 1948, the son of Mr. and Mrs. Charlie II. Abbott. Married Phyllis Jean Dautenhahn, May 24, 1975.

Education: Graduated from Shawnee High School, Shawnee Oklahoma, in May 1966; received Bachelor of Science degree in Geology from Oklahoma State University, in May, 1975; completed requirements for Master of Science degree at Oklahoma State University in May, 1979, with a major in Geology.

Professional Experience: Junior member of the American Association of Petroleum Geologists: member of the Geological Society of America; Junior Geologist, Ketal Oil Producing Company, Summer 1975-1976; Roughneck, Bodard and Hale Drilling Company, Summer 1976; Geologist, Cities Service Oil Company, Summer 1977; Teaching assistant, Oklahoma State University, 1977.


[^0]:    ${ }^{1}$ It is not known if the Jackpile sandstone is a formal member of the Morrison Formation at this time but is so used in this investigation based on the work of Flesch (1975), Schlee and Moench (1961), and Kittel (1963).

