THE USE OF SIMULATION AND CAN-Q TO ANALYZE THE CLEANING AND LUBRICATING PROCESSES OF COLD DRAWN TUBING

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PREFACE

A simulation in SLAM and an analytical computer program called CAN-Q were used to study the feasibility of adding cranes to the cleaning and lubing tanks at Southwest Tube Manufacturing.

A comparison is made of the trade-offs and difficulties in using SLAM and CAN-Q in the study. This is accomplished by comparing outputs of both programs, determining confidence intervals and comparing this data with the actual system. A cost analysis is also done on the feasibility of adding the cranes to the tanks.

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## CHAPTER I

## INTRODUCTION

One of the major problems in production planning today is bottlenecks or blockages of material flow through production operations. Southwest Tube in Sand Springs, Oklahoma has such a problem currently in their tank operation.

Southwest Tube produces hydraulic and mechanical tubing to specifications for customers. These tubes are cold-drawn and then heat treated through a furnace to a desired hardness. Before the tubes are cold-drawn, they must be chemically cleaned and lubricated. This operation is done in the tank system. Overhead cranes dip tubes in various tanks and then set them on a dryer after treatment. The tubes are then taken away to the cold-drawing production area. Currently the tanks cannot keep up with the production on the cold-drawing floor. This causes the floor to go idle waiting for more tubes.

One method to increase production is to increase the length of the work shift or add another shift. However, the tanks run 24 hours a day, seven days a week, so this plan has already been implemented. Another approach to the problem is the addition of cranes. This particular approach is the only feasible way that output can be increased
through the tanks.
An analysis must be made of the addition of cranes to the system to find if the new equipment will really increase production, and to decide if the addition of cranes will be economically feasible.

One approach that lends itself well to this type of problem is simulation, however, simulation can be a very expensive and time consuming technique. Another approach that may apply well to this type of problem is an analytical technique called CAN-Q. This method is less costly than simulation. The proposed research deals with the application of simulation and CAN-Q to this type of environment, particularly Southwest Tube's production problem, and the cost effectiveness of adding the cranes.

## CHAPTER II

## LITERATURE REVIEW

## Simulation

Simulation has been defined by Shannon (18) as
the process of designing a computerized model of a system (or process) and conducting experiments with this model for the purpose of understanding the behavior of the system or of evaluating various strategies for the operation of the system (p. 24).

This particular definition of simulation seems to cover the more important aspects for the model building type of problem solving process. Of particular importance is the linking of simulation to the traditional model building approach to problem solving. This model building method, more commonly referred to as the scientific method, contains the following stages:

1. Observation of the system;
2. Formulation of hypotheses or theories that account for the observed behavior;
3. Prediction of the future behavior of the system based on the assumption that the hypotheses are correct; and
4. Comparison of the predicted behavior with the actual behavior.

However, since the scientific method requires previous observations, which is impossible for certain systems
(especially those that do not exist), a slightly different approach to simulation is taken. This approach is called system methodology and consists of four phases: planning, modeling, validation and application.

## Planning

The first phase in systems modeling is planning. It is at this phase that the modeler first encounters the system. The planner first determines a problem definition. Once the problem has been clearly defined, the modeler can collect pertinent data that might help in the problem solving process. The second stage in the planning process is to analyze the system to gain a thorough understanding of the system and the problem. Many simulation models fail because of an incomplete understanding of the system or the problem.

## Modeling

The second phase in systems methodology is modeling. In this phase the analyst constructs a model from the system. The modeling of a system is made easier if: 1) physical laws are available that pertain to the system; 2) a pictorial or graphical representation can be made of the system; and 3) the variability of system inputs, elements, and outputs is manageable [Graybeal and Pooch (5)]. An analyst will try to simplify the system by using boundaries to limit the scope of the simulation within reasonable terms, limit the inputs and outputs to a level that will
both be economical and maintain model integrity. The modeler will also draw a schematic or flow chart of the model so a better understanding of the model can be obtained. If the system is so complex that no representative model can be used, then a method of subsystem modeling is used. In this approach, the system is divided into smaller, less complex subsystems and an overall model is used to link the subsystems together.

Three approaches have been used in identifying subsystems [Graybeal and Pooch (5)]. The first type is the flow approach. This type of approach has been used to analyze systems that have a flow of physical or information items through the system. Subsystems are identified by grouping aspects of the system that produce a particular physical or information change in the flow entity. A second approach used to identify subsystems is the functional approach. This type of approach is used when no observable flowing entities can be found in a system. Instead, a logical sequence of functions being performed is identified and grouped into a particular subsystem containing all system characteristics that perform a certain function. The last method is called the state-change approach. This procedure is used in systems which are characterized by a large number of interdependent relationships and which must be examined at regular intervals to detect state changes. System characteristics that respond to the same stimulus or set of stimuli are then grouped to form a subsystem.

Once the subsystems have been identified they must be modeled. One task in modeling is choosing an appropriate simulation language. This depends on the type of modeling involved, the facilities available, and the analyst's knowledge of certain languages. After the language is chosen, a computer model of the system can be made.

Another task in the modeling phase is the estimation of the system variables and parameters. At this point real world data are summarized into a manageable statistical description of the system's characteristics. This is done by collecting data over some period of time and then computing a frequency distribution for the desired variables.

## Validation

The next phase of system methodology is validation. A model is validated by proving that it is a correct representation of the real system. Certain techniques have proven useful.in the simulation process. One technique is to compare the results of the simulation with results historically produced by the real system operating under the same conditions. A second technique is to use the simulation to predict results. The predictions are then compared with the results produced by the real system at some future period in time.

Naylor and Finger (12) use a three-step approach to validation of a simulation model. The first step is to
develop a model with high face validity. A model that is face valid seems reasonable to people who are knowledgeable about the system under study. This is accomplished through conversations with experts, observations of the system, general knowledge of the system, and intuition on how the system operates. In the second step the assumptions of the model are tested empirically. This includes adequacy of fit tests used to assess distributions used in the model. This step also uses sensitivity analysis to determine the level of detail in a simulation model. The final step determines how representative the simulation output data is. This is accomplished by comparing the output of the real system to the simulation model, using statistical tests such as the ttest.

Just as good experimental design can aid in the data collection of the modeling phase, so can validation aid in correctness of the simulation model. Most standard experimental designs require that observations be taken on the system variables that can be controlled. The simulation model must operate under identical conditions [Graybeal and Pooch (5)]. Only then can valid inferences be drawn about the relationship between the resulting output of the real system and the outputs of the simulation model.

## Application

The final phase of systems analysis is application. After verification, the simulation can finally be employed
at four levels as described by Pritsker (16): l) as explanatory devices to define a system or problem; 2) as analysis vehicles to determine critical elements, components, and issues; 3) as design assessors to synthesize and evaluate proposed solutions; and 4) as predictors to forecast and aid in planning future developments.

Simulation as a tool to solve complex problems has been growing by leaps and bounds with the improvement and reduction in cost in using the digital computer. Problems in fields as diverse as socio-economics, politics, lawenforcement, biology and nuclear engineering have been successfully solved with the use of simulation [Shannon (19)]. If simulation is so good, however, why is any other type of modeling used? The answer is that in problems where simulation is used, and even in cases in which it does apply, there may be easier and less expensive ways of solving the problem. Solberg and Ravindran (21) state that simulation is one of the easiest tools of management science to use, but probably one of the hardest to apply properly and perhaps the most difficult with which to draw accurate conclusions.

## Advantages and Disadvantages

Adkins and Pooch (l) list five advantages of simulation modeling:

1. It permits controlled experimentation. A simulation experiment can be run a number of times with varying
input parameters to test the behavior of the system under a variety of situations and conditions.
2. It permits time compression. Operation of the system over extended periods of time can be simulated in only minutes with ultrafast computers.
3. It permits sensitivity analysis by manipulation of input variables.
4. It does not disturb the real system. This is a great advantage, since most managers would be reluctant to try experimental strategies on an on-line system.
5. It is an effective training tool.

They also list four disadvantages to using the simulation approach to problem solving:

1. A simulation model may become expensive in terms of manpower and computer time.
2. Extensive development time may be encountered.
3. Hidden critical assumptions may cause the model to diverge from reality.
4. Model parameters may be difficult to initialize. These may require extensive time in collection, analysis, and interpretation.

Thus, even though simulation can be a useful tool, it also has its drawbacks. These should be noted in considering the simulation approach to any particular problem.

## Classifications

Simulation models of systems can be classified as either discrete change or continuous change. Pritsker and Pegden (16) describe discrete simulation as when the dependent variables change discretely at specified points in simulated time. These points are referred to as event times. In continuous simulation the dependent variables of the model may change continuously over simulated time. This is accomplished through differential or difference equations. Both discrete models and continuous models can be combined in one model. In this type of "combined simulation" the dependent variables of a model may change discretely, continuously, or continuously with discrete jumps superimposed.

In discrete simulation, the goal is to reproduce the activities that entities in the model engage in, and thereby learn something about the behavior and performance of the system [Pritsker and Pedgen (16)]. According to Kiviat (8), a discrete simulation model can be formulated by what are known as the three alternative world views for discrete simulation modeling. These three views are referred to as the event, activity scanning, and process orientation.

In event orientation, a system is modeled by defining the changes that occur at event times. Events that can change the state of the system are determined and then a logical association is made with each event type.

In activity scanning orientation, activities in which
entities in the system engage are described. Prescribed conditions then cause an activity to start or end. The events which start or end the activity are not scheduled by the modeler, but are initiated from the conditions specified for the activity.

The last world view of discrete simulation is process orientation. In this view, sequences of elements occur in defined patterns.

In a continuous simulation model, the state of the system is represented by dependent variables which change continuously over time [Pugh (17)]. Models of continuous systems are frequently written in terms of the derivatives of what is known as the "state" variables. The state variables are the dependent variables that continuously change over time.

Combined discrete/continuous model variables may change both discretely and continuously. The system can be described in terms of entities, their associated attributes, and state variables.

Pritsker and Pegden (16) state that there are two types of events that can occur in combined simulations. Timeevents are those events which are scheduled to occur at specified points in time. The other type of events that can occur are state-events. These events are not scheduled, but occur when the system reaches a particular state.

According to Mize and Cox (11, p. 123), "the increase in the number, variety and complexity of system simulation
studies has motivated the development of general simulation languages." These languages are designed to take advantage of the common features of simulation studies. They are intended to simplify the programming of the model so the analyst can concentrate on the model building. Emshoff and Sisson (4) state that a user wants a simulation language that: l) facilitates model formulation; 2) is easy to program; 3) provides good error diagnostics; and 4) is applicable to a wide range of problems.

The languages that were considered include:
GASP - a set of subroutines in FORTRAN that provides useful functions in simulation [Pritsker (15)];

GPSS - a complete language oriented toward problems in which items pass through a series of processing and/or storage functions [Dunning (3)];

SIMSCRIPT - a complete language oriented toward event-toevent simulations in which discrete logical processes are common [Markowitz (9)];

CSMP - a complete language oriented toward the solution of problems stated as nonlinear, integral-differential equations with continuous variables [IBM Corp. (7)];

DYNAMO - a complete language oriented toward expressing micro-economic models of firms by means of difference equations;

SLAM - a complete language that makes use of networks and user written FORTRAN subprograms in both continuous and discrete modeling [Pugh (17)].

Emshoff and Sisson (4) classify these languages in Figure 1 in terms of orientation and scope or generality of application. The trade-off between generality (depth of application) and problem orientation is clear.


Source: J. R. Emshoff and R. L. Sisson, Design and Use of Computer Simulation Models (1970), p. 34

Figure 1. Classification of Languages Used For Simulation (Relative Only)

FORTRAN and PL/I are also included as examples of multipurpose languages in which any sort of state-change process can be described. GASP and SIMSCRIPT differ from FORTRAN and PL/I in that GASP and SIMSCRIPT are not complete languages. Both languages (GASP and SIMSCRIPT) are very general, and both can do anything that can be done in FORTRAN or PL/I.

GPSS is oriented more towards a particular kind of problem (queueing problems). Although it is problem oriented, GPSS has many features that permit it to be applied in a wide range of situations. Furthermore, the language can be augmented by subroutines written in Assembly language.

DYNAMO and CSMP are examples of languages oriented toward problems formulated in terms of nonlinear differential or difference equations. DYNAMO was developed for defining models of business and CSMP for engineering design applications. Neither language is very general, but both are quite useful in specifying simulation procedures for particular types of problems.

SLAM is probably the most versatile of all the language described. It can be as problem oriented as DYNAMO and as general as GASP or SIMSCRIPT. SLAM can simulate discrete, continuous, or combined discrete/continuous models. It can also interact with subroutines written in FORTRAN by the user to further extend the scope of the language.

## Data Analysis

According to Mize and Cox (ll, p. 84), "a sample is a subset of population, in simulation, a sample is usually utilized to represent the population as part of the input information into a more extensive model." Random samples of data must be taken to determine the behavior of the system. This data is usually then tested against a particular
distribution for goodness-of-fit. Among different goodness of fit tests available, the Kolmogorov-Smirnov (K-S) test and the Chi-Square test are the most popular.

The K-S test [Massey (10)] consists of comparing the sample cumulative distribution functions with the theoretical cumulative distribution function at each sample observation. The test statistic is the maximum deviation between the two functions at any point in the sample. The statistic is then compared with a critical value, referenced by the size of the sample, and a chosen level of significance. At a given level of significance, the testing hypothesis may be rejected if the sample statistic is greater than the critical value.

In the Chi-Square test [Cochran (2)], the test statistic is the square of the summation of the observed data points in a particular cell minus the expected number of observations in that particular cell quantity squared, divided by the expected value for that particular cell. The test statistic is then compared with a critical value, referenced by the degrees of freedom and a chosen level of significance. As in the $\mathrm{K}-\mathrm{S}$ test, the testing hypothesis may be rejected if the sample statistic is greater than the critical value.

Of the two tests, the $K-S$ test is more powerful, and thus more likely to detect small differences in the actual and hypothesized distributions [Massey (10)]. The differences between the $K-S$ test and the Chi-square test are
beyond the scope of this paper; for further discussion, refer to Massey (10).

The literature review has dealt primarily with the theoretical aspects of what simulation is, the different types of simulation including the world views, the different types of simulation languages, and fitting data to distributions for the simulation. Later, these aspects of simulation will be integrated and applied to a real world model in an industrial environment.

## Alternatives to Simulation

Simulation is a very useful tool in system analysis, however, simulation can be very expensive and time consuming. Also, some companies may not have a computer accessible that is large enough to handle simulation computer models. There are a number of analytical methods today that provide an alternative to simulation. Two such methods, GERT and CAN-Q, will be discussed.

## GERT

GERT (Graphical Evaluation and Review Technique) is a procedure that combines the disciplines of flowgraph theory, moment-generating functions, and PERT to obtain a solution to stochastic problems [Phillips and Garcia-Diaz (14)].

Figure 2 represents a typical GERT network. The nodes of the network can be interpreted as states of the system. The arcs represent transitions from one state to another.

Such transitions can be viewed as activities characterized by a unique probability density function and a probability of realization.


Figure 2. Typical GERT Network

Each node performs two functions, an input function which indicates the condition under which the node can be realized, and an output function which indicates the branching condition following the node realization.

Two types of nodes are associated with GERT (Figure 3). Type a is a deterministic output and type b is a probabilistic output node. The deterministic node is realized when any arc leading into it is realized under the condition that only one arc can be realized at a time. All arcs emanating from the node are then undertaken. The input to the probabilistic node is the same as the deterministic node,
however, only one arc emanating from this node is realized.


Figure 3. GERT Node Types

Time from node to node is described through momentgenerating functions (Table I). These functions can be manipulated in such a way as to determine moments of the distribution of time spent in moving from one node to another. First, a $W$ function must be calculated. The W function of a given arc is defined as the product of the probability of undertaking the arc and the moment-generating function of the duration of the activity represented by the arc [for $W$ calculations of loops, loops of order $n$ and a closed flow graph refer to Phillips and Garcia-Diaz (14)]. An overall value of the moment generating functions can be calculated through

$$
M_{e}=W_{i}(s) / p_{e}
$$

By then determining the jth partial derivative of $M_{e}(s)$ with respect to $s$, and setting $s$ to zero, a mean can be obtained through

$$
\mu_{j e}=\left.\left(d_{j} / d_{s j}\right)\left[M_{e}(s)\right]\right|_{s=0}
$$

In particular, the first moment about the origin, $\mu_{l e}$, produces the mean network realization time while the variance of the network realization time is obtained by computing $\mu_{2 e}$ and subtracting it from the square of $\mu_{l e}$; that is

$$
\sigma^{2}=\mu_{2 e}-\left(\mu_{l e}\right)^{2}
$$

TABLE I
MOMENT GENERATING FUNCTIONS

| Type of Distribution | $M_{E}(s)$ | Mean | Second Moment |
| :---: | :---: | :---: | :---: |
| Binomial (B) | $\left(p e^{s}-1-p\right)^{n}$ | $n p$ | $n p(n p \div 1-p)$ |
| Discrete (D) | $p_{1} e^{s T_{1}}-p_{2} e^{s} T_{2}-\cdots$ | $p_{1} T_{1}-p_{2} T_{2}-\cdots$ | $p_{1} T i-p=T i-\cdots$ |
| Exponential (E) | $p_{1}+p_{2}-\cdots$ $\left(1-\frac{s}{u}\right)^{-1}$ | $\begin{gathered} p_{1}-p_{2}-\cdots \\ \frac{1}{n} \end{gathered}$ | $\begin{gathered} p_{1}-p_{2}-\cdots \\ \frac{2}{a^{2}} \end{gathered}$ |
| Gamma (GA) | $\left(1-\frac{s}{a}\right)^{-b}$ | $\frac{b}{a}$ | $\frac{b(b-i)}{a^{2}}$ |
| Geometric (GE) | $\frac{p e^{s}}{1-e^{s}-p e^{s}}$ | $\frac{1}{p}$ | $\frac{2-p}{p i}$ |
| Negative binomial (NB) | $\left(\frac{0}{1-e^{s}-p e^{s}}\right)^{r}$ | $\frac{r(1-p)}{p}$ | $\frac{r(1-p)(1-r-r p)}{p^{2}}$ |
| Normal (NO) | $e^{s m+(1 ; 2)} s^{2} 0^{2}$ | 'n | $m^{2}-\sigma^{2}$ |
| Poisson (P) |  | $\therefore$ | iíl-i) |
| Uniform (U) | $\frac{e^{s a}-e^{s b}}{(a-b) s}$ | $\frac{a-b}{2}$ | $\frac{a^{2}-a b-j 2}{3}$ |

Source: D. Phillips and A. Garcia-Diaz, Fundamentals of Network Analysis (1981), p. 14.

GERT, as an alternative method to simulation, can be used if no computer is available. GERT, however, is only
useful for small networks. GERT also requires an intricate understanding of the system. Distributions must be determined for service times, and the system must be networked. Thus, a GERT analysis may well require as much involvement as would simulation analysis. Finally, analysis of GERT must be done through manipulating moment-generating functions. These manipulations can be prone to many errors. While GERT is an alternative method to simulation, GERT can be as costly and time consuming as simulation.

## CAN-Q

Another type of analytical method that can be utilized instead of simulation is CAN-Q. This tool was developed in the form of a computer program by James J. Solberg of Purdue University (20). CAN-Q is a mathematical model for analyzing work flow in a production system through queueing theory and Markov Chains. The computer program accomplishes all of the difficult computations involved in translating the natural description of a system, its resources, and the processes involved in converting raw materials to finished product.

To initiate CAN-Q, the user must simply input the number of stations, the mean service time of those stations, the number of services for each station, the number of servers
transports, the mean time of transportation, the number of products and their routing, and the number of entities desired in the system. CAN-Q takes this information and

produces detailed information for each station and product type including where the bottlenecks are located. Sensitivity analysis is also provided by the system.

To run CAN-Q, the user does not need a deep understanding of the system that is being studied, this eliminates the need for model building. The CAN-Q program also is not very long and therefore can run on a microcomputer. The elimination of model building, the reduced data gathering, and less computer time considerably lowers the cost of the system analysis as compared to using simulation. However, CAN-Q is unable to provide a complete, disadv. picture of system behavior over time as simulation would. CAN-Q also provides no information about short-term behavior $\}$, or extremes of system behavior that simulation could provide.

## CHAPTER III

## STATEMENT OF THE PROBLEM

Southwest Tube Manufacturing is a manufacturer of cold drawn tubing used in pressure and mechanical applications. Figure 4 represents the general plant layout and material flow through the plant. Bundles of tubes are transferred from the yard containing inventories of raw tube hollows to a holding area previous to the treating tanks. Tubes are either (1) cleaned and phosphated, (2) tricked, or (3) cleaned and lubed in the treating tanks. Two overhead cranes are used to service these tanks. Each crane services one side of the tanks. The tubes that are cleaned and phosphated and tricked exit the system at this point and are put back into storage.

The cleaned and lubed tubes are then moved to the pointer by overhead crane to allow pointing of the tubes. Pointing allows the grippers on the cold-draw benches to grab the tube through the die.

The tubes are then taken to the three draw benches by crane. The draw benches draw the tube through a die and over a mandrel to a specified outside and inside diameter. Next the tubes are taken by overhead crane to the annealing furnace where at a specified speed and temperature, they are softened to a desired hardness.


Figure 4. General Plant Layout and Material Flow

The tubes are then transferred by overhead crane to the straightener. The tubing is "straightened" by the straightener and is transferred by conveyer to the Eddie Current Tester, which uses a magnetic field to check for flaws in the tubing.

Final cutting is the next operation performed on the tubes. An overhead crane transfers the tubes from the Eddie Current Tester to the auto-saw. Here the tubes are cut to final length and bundled, then transferred by conveyers to the shipping area.

Within this material flow, a major bottleneck occurs at the tank area. Even though two separate cranes service the tanks, bundles of tubes cannot be processed through the tanks fast enough to keep up with the production rate of the rest of the plant. This problem causes the manufacturing floor to go "dry" before the end of a working shift.

The tank area (Figure 5) contains eight treating tanks. These tanks include: caustic, a cold water rinse, sulfuric acid, hot water, phosphate, another cold water rinse, a neutralizer, and a soap-type lube.

For a normal clean and lube operation, movement through the tank area starts at the caustic tank, which contains a detergent to start the cleaning process of the tubes. A "trip" of tubes (a trip can contain one to four bundles) is dipped into the caustic tank, raised and then drained. The tubes are then lowered into the caustic tank (cranes stay connected to the trips while soaking), where they sit for

five minutes before being rinsed and drained. The "trip" is transferred to the cold water rinse, where the tubes are dipped, raised, and drained. A transfer is then made to the sulfuric acid tank. The tubes are set in this tank until all scale is removed. They are then raised, drained, and transferred to the cold water rinse for redipping. The "trip" is taken to the hot water rinse where they are dipped and drained. The next tank is the phosphate tank; the phosphate acts as a secondary lubricant, and leaves a surface that the primary lube can bond to. The tubes are dipped, drained, and set into the phosphate for five minutes. The "trip" is then drained and moved to the second cold water rinse, where the tubes are dipped and drained. The next tank is the neutralizer. This is used to remove any positive charge from the phosphate that would prevent the primary lubricant from bonding to the surface of the tube. The tubes are dipped and drained in the neutralizer, then taken to the final tank where they are lubed. The lubricant is of the "soap" type which clings to the phosphate secondary lubricant. The tubes are dipped into the lube, drained, and then set into the tank for five minutes. The tubes are then drained and taken to the dryers located next to the tanks. The dryers dry the tubing in preparation for drawing.

The other two types of operations, cleaning and phosphate, and tricking, are less frequent than the cleaning and lubing operation. In the cleaning and
phosphate operation, the neutralizer and lube tank are skipped. In the "trick" operation, the phosphate, second cold water rinse, neutralizer, and lube tanks are skipped.

In solving this problem, management first tried what is known as the "pinning off" technique. This entails pinning off a "trip" in a tank. The operator then leaves that "trip" to go get another "trip". The operator would then "pin-off" that trip and get "trip" or move the previously "pinned-off" set of tubes. This type of approach was used to increase utilization time of the crane. This approach was abandoned because the time it took to pin-off was greater than the greatest time allowed in any one tank and actually decreased the efficiency of the tanks and produced a poorer quality lube because of violating time constraints in certain tanks.

Management is currently considering adding two more cranes to the system. They want to know how many more "trips" can be produced by adding these cranes. Management also wants to know the net present value of the project for one, three, and five year periods.

The problem could be approached as a transportation problem using the cranes as transports and the tanks as destinations. However, the system is subject to random variations, and there is already a set pattern moving through the tanks. This causes the transportation method to be useless.

Because of the complexity of the problem, simulation
appears to be the best tool.
The first step in simulating the system was data collection. This step was accomplished by observing and collecting pertinent data from the system. This data includes different types of trips, the breakdowns that occur, time spent in the tanks, and arrival times for bales of tubing. This data was collected from tank reports and actual observation of the system.

After the data was collected, the system was modeled in SLAM. In this stage, boundary lines were determined for the system, inputs and outputs were limited to what was pertinent to the system, and a SLAM network developed for the model. The data collected from the system was then organized into distributions. This was accomplished with a FORTRAN program developed and modified from Phillips (13), utilizing the $\mathrm{K}-\mathrm{S}$ test.

The model was then validated by comparing the outputs to the real system. This was done with the Turing test [Shannon (19)], which involved showing the output from the real system and the output from the simulation to someone who is intimately familiar with the system, and asking him to differentiate between the two sets of outputs. If he succeeds, a question is raised on how the difference was noted. This provides insight on what might be wrong with the model. Finally, a t-test was performed on the model output, comparing the model outputs with the system outputs.

The next step involved adding two more cranes to the
model. An economic analysis was then performed on the output to see if adding the cranes was profitable. This was done by estimating the total profit per "trip." A tonnage was estimated per trip, and a total profit per ton was calculated. A present value was then calculated for periods of one year, three years, and five years.

After the simulation analysis, CAN-Q was applied to the tank problem. A comparison was made of the CAN-Q output to the real system and the simulation output to determine the accuracy of CAN-Q. This was accomplished by determining a confidence interval of the output rate of the system from the simulation output. This interval was compared with the output rate calculated by CAN-Q. From this information it was determined which type of method was more desirable in this type of production situation, CAN-Q, which is less expensive and faster to develop than simulation, or simulation which reflects the system variability and is more accurate than CAN-Q.

## DATA COLLECTION AND ANALYSIS

The first phase in the simulation of the tank system entailed observation of the tanks to determine the boundaries of the system and the data that needed to be collected for the system. The next step consisted of collection, analysis and hypothesis testing of this data so that a manageable statistical description of the system could be made.

## Observation and Data Collecting

Through observation of the system, it was found that data needed to be collected on movement time of the cranes, dipping time in the various tanks, time per trip in the acid tank, time per trip in the dryer, and hooking and unhooking times per trip. Also needed was the type of operation traveling through the tanks, the number of breakdowns, and the time the cranes are down.

Collection of the movement time between tanks was accomplished with a stopwatch. Timing was initiated when horizontal movement started. Timing was stopped when horizontal movement ceased. Table II represents the movement times between all tanks. These times are averages of 20 observatons taken of the tanks.

TABLE II
MOVEMENT TIME BETWEEN TANKS

| Staging Area to Caustic | .12 | minutes |
| :--- | :--- | :--- |
| Caustic to Cold Water Rinse | .0498 minutes |  |
| Cold Water Rinse to Acid | .075 | minutes |
| Acid to Cold Water Rinse | .075 | minutes |
| Cold Water Rinse to Hot Water Rinse | .30 | minutes |
| Hot Water Rinse to Phosphate | .112 | minutes |
| Phosphate to Cold Water Rinse | .114 minutes |  |
| Cold Water Rinse to Neutralizer | .036 | minutes |
| Neutralizer to Soap | .100 | minutes |
| Soap to Dryer | .100 | minutes |
| Dryer to Staging Area | .948 minutes |  |

Dipping times were collected by both the operator and myself. Figure 6 contains the form used in the data collection. Dipping times were taken at random for different size tubing and recorded on the data sheet. Total times in the acid tank and on the dryer were also taken through this method and recorded on the data sheet.

Hooking and unhooking times were collected by observation of the operator. From these times a standard was calculated for the operator. A standard was also developed for a "pinning off" operation. This standard was done for a two crane two operator system which will be described later in this chapter. All standard times are located in Table III. Finally, the type of operation, the number of breakdowns and the length of down time was collected through the Tank Summary Sheet (Figure 7).


Figure 6. Form Used for Dipping Times


Figure 7. Tank Summary Report

TABLE III
STANDARD TIMES FOR HOOKING AND UNHOOKING

|  |  |
| :--- | :--- |
| Staging Area | 6.71 minutes |
| Pinning Off | 2.00 minutes |
| Drying Area | 2.30 minutes |

## Data Analysis and Hypothesis Testing

Analysis and hypothesis testing was done on the dipping times in the tanks, acid soaking time, and drying time of the tubes. All hypothesis testing was accomplished using the $\mathrm{K}-\mathrm{S}$ test. A program initially developed by Phillips (13) was used for all hypothesis testing. The program was modified for user interaction, data insertion, and histogram manipulation for use on the Hewlett-Packard/3000. Appendix A contains the data collected, their respective histograms, and detailed results of the $K-S$ test.

Table IV contains the final accepted distributions and parameters by the $K-S$ tests.

The mean times differ for dipping in the various tanks because of the different properties of the liquids in each tank, such as viscosity and density. Dipping follows distributions because of the effects of the inside diameter and the length of the tubing. A larger inside diameter and a longer tube requires more time to be spent in filling and draining the tubes. The different degrees of scale on the
tubes cause a distribution in the acid tank. When soaking in the acid, more time is needed to remove heavy scale. Drying times differ due to the number of pieces in a trip, the length of the tubes, and the inside diameter of the tubes. A longer period of time is needed for drying larger surface areas. Tonnage per trip was taken from the Tank Summary Report (Figure 7) and the Work Order (Figure 8).

TABLE IV
DISTRIBUTIONS FOR THE TANK SYSTEM

| Type | Distribution | Parameters |
| :---: | :---: | :---: |
| Caustic Dipping | Normal | . 014 mean, . 0035 variance |
| Cold Water Dipping | Normal | . 0119 mean, . 0035 variance |
| Acid Dipping | Normal | . 0139 mean, . 0034 variance |
| Acid Soak | Normal | . 1989 mean, . 0034 variance |
| Hot Water Dipping | Normal | . 012 mean, . 0034 variance |
| Phosphate Dipping | Normal | . 0145 mean, . 0048 variance |
| Neutralizer Dipping | Normal | . 0159 mean, . 00384 variance |
| Soap Dipping | Normal | . 0139 mean, . 00346 variance |
| Drying | Exponential | . 1673 mean |
| Tons/Trip | Gamma | . 42017 alpha, 3.183 beta |
| Breakdown Length | Exponential | 1.023 mean |

Tonnage was calculated by multiplying the weight per foot of the tubes in the trip by the length of the tubes located in the Work Order, and multiplying this number by the number of pieces per trip taken from the Tank Summary Report.

SOUTHWEST TUBE MANUFACIURING COMPANY
INTERNAL WORK ORDER


POINTER

| Bates | Die 1 | Die 2 | 0ie 3 | Salea | Dio. 1 | Die 2 | Die 3 |  | 8ales | Die 1 | Ole 2 | Die 3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-4 | .6077 | 575 |  |  |  |  |  |  |  | 505 | 477 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |


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| Oate 1 $\qquad$ $1-7-\infty$ wnten By Spinda |  |  | kave | w.. - D11-608-2 |  |  | 2900: 3 è |  |  |

Figure 8. Work Order

Finally, calculation of the probability of a breakdown, the probability of a lube operation, phosphate operation, and a trick operation was made through the Tank Summary Report. Tank Summary Reports for the previous three months were used to calculate these probabilities. Breakdowns, lube operations, phosphate operations, and trick operations were tallied and divided by the total number of trips. The probability of a breakdown is 0.17; the probabilities for a lube, phosphate and trick operation are $0.89,0.043$, and 0.067 , respectively.

## CHAPTER V

MODELING OF THE TANK SYSTEM

Three different versions of the tank system were developed for Southwest Tube. These versions include the present system, a two crane one operator system, and a two crane two operator system. Each of these models has the same two major assumptions. The first assumption is that there is an endless supply of tubing for trips. It was determined from the production planning department that the tanks never wait for material. Another major assumption made was that there is always room for more trips in the dryer.

This chapter describes in detail each system and how each system is modeled.

## Present System Model

The present system, as previously described in Chapter III, is modeled completely in network SLAM (Appendix B). Presently, two cranes work the system. Each crane has responsibility for one side of the tank system. Since these cranes operate independently, only one crane will be considered in the network.

The model consists of two major networks. The first network consists of the actual operation of the crane
through the tanks. A create node creates one entity to run through the model. The entity is then determined to be a clean and phosphate trip, a tricked trip, or a clean and lube trip through probabilistic branching. All major attributes are then assigned to the entity. These attributes contain all service times through the tanks and the time an entity starts the tank operation. The entity then goes through the various services of the tanks, branching off to particular nodes depending on what type of operation is assigned to the entity. Resource gates throughout the system stop the flow if any breakdown should occur (breakdowns are modeled in the second network). The entity is then split at the end of the network after the entity is placed in the dryer for service. One entity continues service throughout the dryer and is terminated. The other entity is taken back to the beginning of the network after a crane move time to start through the system again. COLCT nodes are used at the end of the network to allow collection of the time in the system for each entity.

The second network consists of all breakdowns for the crane system. This network starts with a create node to loop one entity through the system.

Through probabilistic branching, it is determined if a breakdown will occur for a particular shift. A breakdown time and a service time are then determined for that particular breakdown. When a breakdown does occur, the resource $C R I$ is closed until the repairs are made. The
resource gate is then opened so the cranes can continue through the system. The entity in the breakdown network then loops to the beginning for the next 12 hour shift.

Two Crane One Operator Model

This system is similar to the original system except for the addition of another crane (Appendix C). In this system one operator operates the two cranes through the tanks. One crane is moved while the other is in a soaking operation. This model includes four networks - one network for each crane, and one network for breakdowns of each crane.

Major problems arise in the modeling of the two crane system due to interference of the two cranes. This problem is solved by determining which crane will be ahead of the other and keeping it that way through a series of resources and gates controlled in the networks representing each crane.

The first network represents the crane that is always in front. The network is the same as the original model except for the resources and gates used to control interference. Gates are used to prevent movement of the other crane when a crane is being manipulated. Another set of gates and resources is used to prevent the overtaking of the first crane and to prevent the use of the same soaking tank. These gates and resources are used in front of the first cold water tank (because of the back-tracking out of
the acid tank), in front of the phosphate tank, and in front of the soap tank. Gates and resources are also placed in the branching of the network for the trick trip and the clean and phosphate trip to prevent the second network from overtaking the first network. The ending of the two crane networks is similar to the original network except for the waiting of the first crane network for the second crane network to finish. This allows the operator to move the cranes together back to the beginning of the tanks.

The two networks that run the crane breakdowns are the same as the present system's crane breakdown network. Gates control resources in the corresponding networks to allow breakdowns of the two crane systems.

Two Crane Two Operator Model

This model utilizes three networks - one for the two cranes, and two for the breakdown of the cranes (Appendix D). Figure 9 represents the assignment of the two cranes to their prospective areas of the tank. It is desirable to have an even balance of time in the tanks for each assigned crane area. Given the present means and time in the soaking tanks, the hot water tank seems to be the best prospective dividing point for the crane assignment areas. The hot water tank will be the "pin-off point" for the cranes. The crane assigned to the first set of tanks in the sequence will "pin-off" a trip in the hot water tank after completion of the tank procedures in its area. This crane will then

hook up with the bale in the hot water tank and complete the tank procedures in its assigned area. This crane will then return to the hot water tank to pick up another trip.

The SLAM model is similar to the Present System Model. The model is the same as the Present System Model until the hot water tank. At this point a resource is added to avoid interference between the two cranes. This resource requires the first crane to wait for the hot water tank to be empty. When the tank is empty a "pin-off" operation can then be performed. The entity is then split to allow the crane to return to the start of the network to pick up a new trip. The other entity continues on through the second crane area. This area begins with a resource to allow the trip to wait for the second crane to finish procedures with the previous entity. The entity then is serviced by the remaining tanks. After service, the entity is split. One entity goes through the dryer where statistics are collected and where the entity is terminated. The other entity releases the resource corresponding to waiting in the hot water tank after move time for the second crane. The entity is then terminated.

The two crane breakdown networks are exactly the same as the breakdown networks in the Two Crane One Operator Model.

## CHAPTER VI

## TANK SIMULATION ANALYSIS

This chapter contains a discussion of each type of model and its outputs. From these outputs confidence intervals are calculated. These intervals will be discussed and analyzed.

Present System Model

The Present System Model was run for a total of 3600 hours (30 12 hour shifts). The model was started in steadystate. Outputs for the 10 runs is located in Appendix E.

## Present System Output

Table $V$ represents the output for all 10 runs of the Present System Model. Trip output per run ranged between 433 and 446 trips, with an average of 439.6 trips. This caused the average output of trips per shift to range between 14.43 trips to 14.87 trips, with an average of 14.65 trips. The tank time (time through the tank system without the dryer) ranged between 0.81 and 0.83 hours, with an average of 0.82 hours. Total time in the system (time in the tank system including dryers) ranged between 0.94 and 0.98 hours, with an average of 0.97 hours. The number of breakdowns in the system contained a low value of 0 and a

TABLE V
OUTPUT FOR PRESENT SYSTEM MODEL

| Run | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | Avg. |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Trip Output | 442 | 437 | 433 | 443 | 433 | 441 | 441 | 436 | 446 | 444 | 439.6 |
| Output/Shift 14.73 | 14.57 | 14.43 | 14.76 | 14.43 | 14.7 | 14.7 | 14.53 | 14.87 | 14.8 | 14.65 |  |
| Tank Time | .81 | .82 | .83 | .81 | .83 | .82 | .82 | .82 | .81 | .81 | .82 |
| Total Time | .96 | .98 | .96 | .94 | .98 | .97 | .98 | .97 | .95 | .96 | .97 |
| Number of <br> Breakdowns | 5 | 4 | 5 | 7 | 7 | 4 | 4 | 8 | 0 | 6 | 5 |
| Ton Output | 589 | 599.7 | 557.6 | 621.7 | 593 | 616.5 | 577.5 | 593.8 | 571.3 | 567 | 588.7 |

high value of eight breakdowns, with an average of five. Ton outputs ranged from 557.6 to 621.7 tons, with an average of 588.7 tons.

## Present System Confidence Intervals

A confidence interval was calculated for all the parameters in Table $V$ to provide a more accurate view on exactly where the range of values lie for each type of parameter. Using a 95 percent confidence interval and the equation

$$
\bar{x}(n) \pm t_{R-1}, .025 \sqrt{\frac{s^{2}(n)}{n}}
$$

computations were made for the set of 10 runs. This equation assumes normality. $X(n)$ is the mean of the distribution, $s^{2}$ is the variance, $t_{R-1}$ is the factor corresponding to a 95\% confidence interval.

Figure 10 shows the confidence interval for the trip output. It can be stated with $95 \%$ confidence that the interval of 429.78 and 449.4 contains the true mean for 30 shifts.

Figure ll represents the confidence interval for tank time. With tank time, there is 95\% confidence that the interval of 0.80 and 0.837 includes the true mean of time spent in the tanks.

The confidence interval for total time in the system including the dryer is represented in Figure 12. There is a
$95 \%$ confidence that the interval bracketed by 0.94 and 1.00 contains the true mean of total time in the system.


Figure 10. Confidence Interval for
Trip Output in the Present System Model


Figure ll. Confidence Interval
for Tank Time in the Present System Model


Figure 12. Confidence Interval
for Total Time
Spent in the Present System Model

The number of breakdowns confidence interval is represented in Figure 13. It can be stated that there is a $95 \%$ confidence that the interval of 0.15 and 9.85 encases the mean number of breakdowns for a 30 shift period.


Figure 13. Confidence Interval for Breakdowns of the Present System Model

Figure 14 represents the confidence interval for ton output. It can be stated that there is a $95 \%$ confidence that the interval of 544.1 and 633.33 bounds the true mean of tons for a 30 shift period.


Figure 14. Confidence Interval for Ton Output of the Present System Model

## Present System Final Analysis

To validate the simulation, a t-test was performed between the trip output and data collected for 10 different sets of 30 shifts each. Table VI represents the final results of this t-test.

Since $t_{o}$ is less than the critical t-test value of ${ }^{t}{ }^{18, .025}$ ' the hypothesis that the mean of the actual output equals the simulation output cannot be rejected. This is a good indication that the model is valid.

TABLE VI
T-TEST OF TRIP OUTPUT VS. ACTUAL OUTPUT

| Simulation Output | Actual Output |
| :---: | :---: |
| 442 | 420 |
| 437 |  |
| 433 |  |
| 443 | 452 |
| 433 | 448 |
| 441 |  |
| 441 |  |
| 436 |  |
| 446 | 440 |
| 444 | 443 |

$$
t_{0}=\frac{440.8-439.6}{92.31 \sqrt{1 / 10+1 / 10}}=.029
$$

$t .025,18=2.101$
$t .025,18>t_{0}$

Cannot Reject $\mathrm{H}_{0}$

Validation was also made through the Director of ColdDraw Operations. Utilizing the Turing Test, a set of output from the actual system of the number of trips per shift and output of trips per shift was given to the Director of ColdDraw Operations. No distinction could be made, thus validating the model further. The director was also given a list of mean times in the tanks and times taken with a stopwatch by the tank operator of time through the system. The director could not tell the difference between these times, either.

The data showing the number of breakdowns also seem to be valid. If there is a $17 \%$ chance of a breakdown during any shift, for a 30 shift period there should be approximately 5.1 breakdowns. The ton output also seems correct with a value of 588.7 tons. The average number of tons per shift is 1.337; multiplying this by the total number of trips, a number of 587.7 tons is obtained. This is well within the $95 \%$ confidence interval calculated for tons.

From the output, it seems that this is an extremely valid and accurate simulation model of the tank system. The next two sections deal with the addition of two cranes to the model and their effect on the output.

## Two Crane One Operator Model

The Two Crane One Operator Model was run for a total of 360 hours, or 30 shifts as was the Present System Model.

Output for the 10 runs is located in Appendix $F$.

## Two Crane One Operator Model Output

Table VII represents a summary of the output for all lo runs. Trip output ranged between 769 and 797 total trips, with an average of 779.3 trips per 30 shift period. This caused the output per shift to range between 25.6 and 26.57 trips per shift, with a mean of 26 trips. The tank time for crane one had a low of 0.88 hours and a high of 0.91 hours, with a mean of 0.897 hours. The total time in the system including the dryer ranged between 1.04 and 1.1 hours, with an average of 1.06 hours. Tank time using crane two had a low of 0.90 hours and a high of 0.93 hours, with a mean of 0.92 hours. Total time in the system through crane two ranged between 1.05 and 1.1 hours, with a mean of 1.09 hours. The number of breakdowns for crane one had a low of 0 breakdowns, a high of 10 breakdowns, and an average of 5.2 breakdowns. The number of breakdowns for crane two ranged between 3 and 9, with a mean of 6.1. Ranges for the total ton output of the system fell between 1020 and 1111 tons, with a mean of 1053.3 tons.

## Two Crane One Operator Confidence Intervals

A confidence interval of $95 \%$ is calculated for all parameters as in the Present System Model to provide a more accurate view of the range of values for the Two Crane One Operator Model.

TABLE VII
OUTPUT FOR TWO CRANE ONE OPERATOR MODEL

| Run | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | Avg. |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Trip Output | 781 | 788 | 773 | 777 | 773 | 773 | 769 | 796 | 776 | 786 | 779.3 |
| Output/Shift | 26 | 26.3 | 25.8 | 25.9 | 25.8 | 25.8 | 25.6 | 26.6 | 25.9 | 26.2 | 26.00 |
| Tank Time <br> System 1 | .90 | .90 | .90 | .89 | .91 | .903 | .91 | .88 | .89 | .89 | .897 |
| Total Time <br> System 1 | 1.1 | 1.04 | 1.06 | 1.07 | 1.06 | 1.06 | 1.07 | 1.05 | 1.05 | 1.06 | 1.06 |
| Tank Time <br> System 2 | .92 | .91 | .92 | .92 | .93 | .93 | .93 | .90 | .92 | .91 | .92 |
| Total Time <br> System 2 | 1.1 | 1.05 | 1.1 | 1.1 | 1.1 | 1.08 | 1.1 | 1.07 | 1.09 | 1.09 | 1.09 |
| Number of <br> Breakdowns <br> System 1 | 3 | 10 | 4 | 4 | 7 | 5 | 9 | 0 | 5 | 5 | 5.2 |
| Number of <br> Breakdowns <br> System 2 | 6 | 7 | 5 | 7 | 7 | 9 | 3 | 5 | 7 | 5 | 6.1 |
| Ton Output | 1046 | 1059 | 1068 | 1040 | 1020 | 1020 | 1083 | 1111 | 1053 | 1033 | 1053.3 |

Figure 15 represents the confidence interval of trip output in the system for this model. There is a $95 \%$ confidence level that the interval of 760.7 and 798 embraces the true mean for the total number of trips for a series of 30 shifts.


Figure 15. Confidence Interval
for Trip Output of
Two Crane One
Operator Model

A 95\% confidence interval for tank time using crane one is represented in Figure 16. It can be stated that there is a $95 \%$ confidence that the interval of 0.877 and 0.917 contains the true mean of tank time for crane one.

Figure 17 represents the $95 \%$ confidence interval for total time using crane one. There is a $95 \%$ confidence that the interval 1.025 and 1.094 includes the true mean for total time in the system.

Figure 18 represents the confidence interval for tank time using crane two. There is a $95 \%$ confidence that the
interval of 0.897 and 0.942 contains the true mean of tank time using crane two.


Figure 16. Confidence Interval for Tank Time of Crane One of Two Crane One Operator Model


Figure 17. Confidence Interval for
Total Tank Time of
Crane One of Two
Crane One Operator Model


Figure 18. Confidence Interval for Tank Time of Crane Two of Two Crane One Operator Model

Total time in the system utilizing crane two is represented by the confidence interval in Figure 19. There is a $95 \%$ confidence that the interval of 1.053 and 1.126 brackets the true mean of total time in the system


Figure 19. Confidence Interval for Total Tank Time of Crane Two of Two Crane One Operator Model

Figure 20 represents the confidence interval for the number of breakdowns for crane one. It can be stated that there is a $95 \%$ confidence that the interval of 0 and 11.4 the true mean for the number of breakdowns for a 30 shift period.

breakdowns 5.2 breakdowns 11,4
MIGAN
Figure 20. Confidence Interval of Breakdowns for Crane One for Two Crane One Operator Model

The confidence interval for the number of breakdowns of crane two is represented in Figure 2l. There is a 95\% confidence that the interval of 2.53 and 9.67 includes the true mean of breakdowns for crane two for a 30 shift period.

Figure 22 represents the $95 \%$ confidence interval for the ton output of this model. It can be stated that for a 30 shift period the interval of 992.1 and 1114.5 contains the true mean for number of tons produced by the system.


Figure 21. Confidence Interval of Breakdowns for Crane Two for Two Crane One Operator Model


Figure 22. Confidence Interval
of Ton Output for
Two Crane One Operator Model

Gate Analysis of the Two Crane One

## Operator Model

TABLE VIII
gate statistics for two crane one operator model

| Run | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | Avg. |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MOV | .426 | .467 | .3799 | .3754 | .4292 | .4159 | .4217 | .4203 | .4076 | .3780 | .4121 |
| SC2 | .633 | .638 | .6242 | .6280 | .6393 | .6401 | .6324 | .6364 | .6367 | .6274 | .6336 |
| SCl | .526 | .521 | .5366 | .5274 | .5285 | .5342 | .5312 | .5233 | .5330 | .5308 | .529 |
| C2 | .897 | .898 | .8951 | .8957 | .9009 | .8875 | .8824 | .8952 | .9002 | .9015 | .895 |
| P2 | .914 | .913 | .9167 | .9185 | .9178 | .9164 | .9135 | .9173 | .9162 | .9161 | .916 |
| SO2 | .878 | .879 | .8833 | .8840 | .8704 | .8716 | .8843 | .8819 | .8782 | .8765 | .879 |
| ACID | .705 | .693 | .7118 | .7114 | .7077 | .7178 | .7138 | .6997 | .7145 | .7086 | .708 |
| PAS1 | .699 | .698 | .7221 | .7238 | .6974 | .7082 | .7176 | .7228 | .7123 | .7126 | .711 |
| PAS2 | .872 | .873 | .8769 | .8786 | .8626 | .8659 | .8741 | .8755 | .8733 | .8692 | .872 |

runs of this system. It is useful to take a look at these statistics to see how the system is operating in the case of crane interference for this model.

The MOV gate allows crane one to wait for crane two before moving back through the system. This gate is open an average of $41 \%$ of the time. This means that $59 \%$ of the time, crane one is waiting for crane two to finish.

SCl and SC2 make sure that only one crane is being worked at a time. These values are $52.9 \%$ and $63.4 \%$ correspondingly of the time these gates are open. It would seem that these values should be approximately $50 \%$ apiece; however, when the two cranes are both in a soak tank, both gates may be open. As soon as a crane is finished soaking, it instantly closes the other crane's gate, thus preventing simultaneous movement.

C2, ACID, P2, and SO2 prevent two cranes using the same soak at the same time. The gate C2 controls the caustic tank and is open $89 \%$ of the time. The gate that controls the acid tank is open (ACID) $70.8 \%$ of the time. P2, which controls the phosphate tank, is open an average of $91.6 \%$ of the time, and $S C l$, which controls the soap tank, is open $87.9 \%$ of the time.

From the amount of time the gates are open, it is obvious that a bottleneck occurs at the acid tank with that particular gate being open only $70.8 \%$ of the time. This is because of the high service time associated with the acid tank.

Two Crane One Operator Final Analysis

Trip output for the Two Crane One Operator System was considerably higher at an average of 779.3 trips for a 30 shift period than the Present System Model at an average of 439.6 trips. This was because of the extra transport in the new model. The output was not doubled because of factors such as crane interference and waiting times.

The tank times in the Two Crane One Operator System were greater than that of the Present Model. However, there are two items in the two crane system which account for the higher output of the two crane system. The tank time of crane one always lags just behind that of crane two. This is because crane two has to wait until crane one is finished so both cranes can move across the system to pick up another trip. The same logic as above follows for the total time in the system.

The average number of breakdowns of 5.2 for crane one and 6.1 for crane two fall in the range of breakdowns for the 95\% confidence interval for the Present System Model of 0.15 and 9.85 breakdowns.

The ton output is correspondingly higher with the new model to the increased number of trips.

## Two Crane Two Operator Model

The Two Crane and Two Operator Model was run for 360 hours or 30 shifts, as the previous two models. Output for the 10 runs are located in Appendix $G$.

## Two Crane Two Operator Output

Table IX represents a summary of the output for the Two Crane Two Operator System. Trip output averaged at 676.9 trips for a 30 shift period, with a high of 689 and a low of 664 trips. The corresponding output per shift ranged between 22.1 and 22.9 trips per shift, with an average of 22.6 trips. Average time in the tanks ranged between 0.87 and 0.91 hours, with an average of 0.89 hours. Corresponding total times had a high of 1.06 hours and a low of 1.03 hours. Number of breakdowns for crane one ranged between 2 and 22, with an average of 7.7. The number of breakdowns for crane two had a low of 2 , a high of 9 and an average of 4.9 breakdowns. Ton output had a low of 884 and a high of 951 tons, with an average of 917.2 tons.

## Two Crane Two Operator Confidence Intervals

To further investigate the range of the values for the Two Crane Two Operator Model, a 95\% confidence interval was calculated as in the previous two models.

Figure 23 represents the confidence interval for trip output of this model. There is a 95\% confidence that for a 30 shift period the interval of 658.1 and 695.7 encompasses the true mean for the number of trips.

The confidence interval that represents tank time in the system is pictured in Figure 24. It can be said that there is a $95 \%$ confidence that the interval of 0.861 and 0.92 bounds the true mean of time in the tanks.

TABLE IX
OUTPUT FOR TWO CRANE TWO OPERATOR MODEL

| Run | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | Avg. |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Trip Output | 667 | 678 | 664 | 686 | 674 | 670 | 689 | 672 | 684 | 685 | 676.9 |
| Output/Shift | 22.2 | 22.6 | 22.1 | 22.9 | 22.5 | 22.3 | 23 | 22.4 | 22.8 | 22.8 | 22.6 |
| Tank Time | .91 | .89 | .89 | .87 | .89 | .90 | .87 | .902 | .88 | .88 | .89 |
| Total Time | 1.06 | 1.03 | 1.03 | 1.03 | 1.04 | 1.04 | 1.02 | 1.05 | 1.03 | 1.03 | 1.036 |
| Number of <br> Breakdowns <br> System 1 | 12 | 5 | 22 | 5 | 8 | 9 | 2 | 9 | 3 | 2 | 7.7 |
| Number of <br> Breakdowns <br> System 2 | 9 | 4 | 4 | 6 | 4 | 2 | 4 | 7 | 4 | 5 | 4.9 |
| Ton Output | 894 | 900 | 919 | 948 | 898 | 884 | 903 | 951 | 924 | 951 | 917.2 |



Figure 24. Confidence Interval of Tank Time for Two Crane Two Operator Model

For the total time in the system (Figure 25), it can be stated that there is a $95 \%$ confidence level that the interval of 1.011 and 1.061 includes the true mean of total time in the system.


Figure 25. Confidence Interval
of Total Time for
Two Crane Two
Operator Model

Figure 26 represents the confidence interval for the number of breakdowns for crane one. This 95\% confidence level states the interval of 0 and 20.6 encases the true mean for breakdowns.


Figure 26. Confidence Interval of Breakdowns for Crane One of Two Crane Two Operator Model

The confidence interval that represents the number of breakdowns for crane two is represented by Figure 27. There is a $95 \%$ confidence level that the interval of 0.67 and 9.1 includes the true mean for breakdowns.


Figure 27. Confidence Interval of Breakdowns for Crane Two of Two Crane One Operator Model

Figure 28 represents the confidence interval for ton output. It can be stated that there is a 95\% confidence that the interval of 862.77 and 971.62 encases the true mean for the number of tons in a 30 shift period.

## Resource Analysis of Two Crane Two

## Operator Model

Table X represents the percentage of time the resources WCl and WC2 were not in use. WCl represents the resource
used in waiting for crane two to pick up a trip. WC2 represents the resource used in waiting for crane two to receive a trip from crane one.


Figure 28. Confidence Interval of Ton Output for Two Crane Two Operator Model

WCl is available $83.5 \%$ of the time, which means crane one hardly ever waits for crane two. WC2 is available 29\% of the time, which means crane two waits for crane one $71 \%$ of the time. This is caused by the imbalance of the tanks at the "pinning off" area. To remedy this type of imbalance the pinning off should be moved over to allow less time for the crane one system and more time for the crane two system. However, this cannot be accomplished. The next tank that can be utilized as a pinning off area is the acid tank. Pinning off cannot be done here because of safety reasons and backtracking problems.

TABLE X
RESOURCE OUTPUT OF TWO CRANE TWO OPERATOR MODEL

| Resource | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | Avg. |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WC1 | .8264 | .8315 | .8447 | .8395 | .8374 | .8346 | .8357 | .8272 | .8347 | .8356 | .835 |
| WC2 | .2887 | .2864 | .3107 | .2848 | .2944 | .2952 | .2837 | .2848 | .2828 | .2856 | .290 |

Two Crane Two Operator Final Analysis
Trip output was higher with 676.9 trips than the Present System Model with an average of 439.6 trips for a 30 shift period. However, because of the imbalance of the system, the trip output was lower than that of the Two Crane One Operator Model with an average of 779.3 trips for a 30 shift period.

The tank time in the system was slightly greater than that of the original system, with an average of 0.89 hours versus 0.82 hours. This is due to the "pinning off" function in the hot water tank. Tank time of the Two Crane One Operator System was approximately equal to that of the Two Crane Two Operator System.

The number of breakdowns for both cranes fall within the range of the other two systems with values of 7.7 and 4.9, respectively.

The ton output was lower than the Two Crane one Operator System, due to the smaller number of trips for 30 shifts at 578.96 tons.

## CAN-Q Input

Can-Q is a computer program that utilizes queueing Theory and Markov Chains to analyze systems. The program uses mean service and travel times as opposed to distributions used in simulation. The following chapter contains CAN-Q input and output for the tank system. All input is simply the mean of times taken for the input used in the simulation. Each tank is divided into a station, a mean processing time and the number of servers is input for each station. Average dipping times plus soaking time (if soaking is required) is used as input for each station. Table $X I$ represents the final input for CAN-Q. A routing for each product type is also required for CAN-Q. In the tank simulation, three different product routings are required. These products are normal lube, phosphate, and trick. Table XII represents the routing for the lube operation, Table XIII represents the routing for the phosphate operation, and Table XIV represents the routing for the trick operation.

Another type of input required for CAN-Q is a transport time between stations. Only one transport time is allowed

TABLE XI
CAN-Q INPUT

| Station | Processing Time | Number of Servers |
| :--- | :--- | :--- |
| 1 Holding | 6.71 minutes |  |
| 2 Caustic | 6.68 minutes | 1 |
| 3 Cold Water I | 0.714 minutes | 1 |
| 4 Acid Water | 12.768 minutes | 1 |
| 5 Hot Water | 0.72 minutes | 1 |
| 6 Phosphate | 6.74 minutes | 1 |
| 7 Cold Water II | 0.714 minutes | 1 |
| $8 \quad$ Neutralizer | 1.908 minutes | 1 |
| 9 | 6.668 minutes | 1 |
| 10 Dry | 2.3 minutes | 1 |
| Crane Move Time | 0.184 minutes | 2 |
| Number of Cranes in |  |  |
| System | 2 |  |

TABLE XII
ROUTING FOR THE LUBE OPERATION

| Operation Number | Station |
| :---: | :--- |
| 1 | Holding |
| 2 | Caustic |
| 3 | Cold Water |
| 4 | Acid |
| 5 | Cold Water |
| 6 | Hot Water |
| 7 | Phosphate |
| 8 | Cold Water |
| 9 | Neutralizer |
| 10 | Soap |
| 11 | Dry |

TABLE XIII
ROUTING FOR PHOSPHATE OPERATION

| Operation Number | Station |
| :---: | :--- |
| 1 | Holding |
| 2 | Caustic |
| 3 | Cold Water |
| 4 | Acid |
| 5 | Cold Water |
| 6 | Hot Water |
| 7 | Phosphate |
| 8 | Cold Water II |
| 9 | Dry |

TABLE XIV
ROUTING FOR TRICK OPERATION

| Operation Number | Station |
| :---: | :--- |
| 1 | Holding |
| 2 | Caustic |
| 3 | Cold Water |
| 4 | Acid |
| 5 | Cold Water |
| 6 | Hot Water |
| 7 | Dry |

in CAN-Q. This time for the tank system is the average time between stations, a value of 0.18 minutes.

The last type of input that must be made for CAN-Q is the number of items in the system. This determines how many items can be in the production at one time. The number of items must be two or greater.

## CAN-Q Output Analysis

Output for CAN-Q (Appendix H) contains a routing for each product type, input data summary, system performance measures, summary for each station, and sensitivity information. However, the only information that is valuable in determining the final analysis of the tank system is located in the summary of each station and the system performance measures, the routings and input data section are mainly used for data input verification. The sensitivity information is useful if product types or service times can be changed.

## System Performance Measures

The System Performance Measures section contains the most valuable information on the system for the tanks.

Table XV contains the final information from the System Performance Measures Section. Production rate is the first value given. For two items (items represent cranes) in the system, the production rate is 2.192 items per hour. Production rates by product type are also given; these are

## TABLE XV <br> SYSTEM PERFORMANCE SUMMARY

```
SYSTEM PERFORMGNCE MEASURES
    PRODUCTION RATE = 2.192 ITEMS PER HOUR
\begin{tabular}{lrr} 
& NUMBER & VALUE \\
LUBE & 1.95 i & 1.951 \\
PHO & .098 & .083 \\
TRI & .153 & .153
\end{tabular}
        total value = 2.192
    AUERGGE TIME IN SYSTEM = 54.74 MINUTES
            PROCESSING 45.14
            TRAVELING 1.92
            WAITING 7.69
    FUACTIONS OF N, NUMEER OF ITEMS IN THE SYSTEM
n production rate average time in the sygtem
\begin{tabular}{|c|c|c|}
\hline 1 & 1.275 & 47.056 \\
\hline 2 & 2.192 & 54.744 \\
\hline 3 & 2.854 & 63.063 \\
\hline 4 & 3.332 & 72.029 \\
\hline 5 & 3.674 & 81.649 \\
\hline 5 & 3.917 & 91.717 \\
\hline 7 & 4.085 & 102.804 \\
\hline - & . & \\
\hline & & \\
\hline I/ lF & 4.412 & INF \\
\hline
\end{tabular}
            THE bOtTlENECK STATION IS 4
```

simply the fraction of the product type in the system multiplied by the overall production rate. An average time in the system is then given. This value is 54.74 minutes. This time is then broken down into actual processing time at 45.14 minutes, traveling time at 1.92 minutes, and waiting time at 7.69 minutes. Finally a production rate and an average time in the system is given for different numbers of items in the system. For one item in the system, the production rate is 1.275 items per hour with an average time in the system of 47.056 minutes.

The only way to compare the one and two crane systems is through the production rate and average time in the system. This is because CAN-Q will not accept a number in the system less than two. However, a good picture of the increase in the system by adding one crane is given through this information. There is an increase in production of almost one item per hour by adding an extra crane. Average time in the system increases by 7.7 minutes because of waiting for processing, but there are two items being processed, increasing the output of the system.

Finally, information is given on where the bottleneck is located in the system. The bottleneck in the tanks is located at the acid tank, station four.

## Station Summary

The Station Summary contains information dealing with each particular station. The most useful summary is
contained within the station containing the bottleneck of the system. Station four is the bottleneck located in the tank system.

Station four is the station that is used for the dipping and soaking of the bales in acid (Table XVI). Server utilization for this particular station is approximately 49.7\%. The average number of items in process and waiting for this station is 1.281 , the average number of items in process is 0.497 , and the average number of items waiting is 0.784 . Average time spent per operation at this station is 35.061 minutes. Processing time takes 13.6 minutes of this time, while waiting takes 21.461 minutes. The fraction of time there are zero items at the station is 0.5031. The fraction of the time there is one item at the station is 0.4969 .

```
TABLE XVI
STATION SUMMARY FOR ACID TANK
```



## CHAPTER VIII

COMPARISON OF CAN-Q AND SIMULATION

This chapter compares the CAN-Q output with the simulation output. This is accomplished through the use of confidence intervals. An economic analysis is also done on the outputs of both the SLAM model and CAN-Q to determine if the addition of the cranes is economically feasible.

Original System Simulation and CAN-Q

In comparing the Present System Simulation with CAN-Q, only two numbers from the output of CAN-Q will be compared to the simulation output: time spent in the system, and output. Comparisons will be made through confidence intervals calculated from the simulation output.

The production rate calculated through CAN-Q is 1.275 items per hour. Multiplying this number by 360 an output of 459 items is obtained. Figure 29 shows where this number lies compared with the simulation's 95\% confidence interval. The number is slightly high, probably because breakdowns cannot be modeled into the system. Taking an average output per day shows how close the production rate for the simulation and CAN-Q really are. CAN-Q's output per day is 15.3 trips, while the average number of trips per day for the simulation model is 14.65 trips.


Figure 29. Confidence Interval of the Present System Output and CAN-Q Output

Average time in the tank is 47.056 minutes, or 0.784 hours. Figure 30 shows where this value lies when compared with the simulation's 95\% confidence interval for tank time in the Present System Model. This number is slightly lower because of the inability of CAN-Q to handle breakdowns.


Figure 30. Confidence Interval of the Present System Tank Time and CAN-Q Tank Time

Two Crane One Operator Simulation and CAN-Q

Output from the Two Crane One Operator System Simulation is extremely close to that of CAN-Q. Figure 31 represents the $95 \%$ confidence interval of the production for 360 hours. The production for CAN-Q of 789.12 trips for 360 hours lies almost midway between the mean of 779.3 trips and the upper limit value of 798 trips with respect to the simulation's output. The CAN-Q output of the production is slightly higher because of the inability to model breakdowns. Another reason the output might be slightly higher is because of the lack of ability for CAN-Q to model crane interference. This is especially true at the drying portion of the tanks. CAN-Q does not allow one crane to wait until the other crane is finished so they both may move back to the beginning of the tanks.


Figure 31. Confidence Interval of Two Crane One Operator Output and CAN-Q Output

The average time of the system, however, is also slightly higher than the average tank time for the Two Crane One Operator Model (Figure 32). This is possibly due to random variation in the simulation model.


Figure 32. Confidence Interval of Two Crane One Operator Tank Time and CAN-Q Tank Time

Two Crane Two Operator Simulation and CAN-Q

The difference between this simulation and CAN-Q is greater than the difference found for the other models. Figure 33 depicts where the value of production output falls for 360 hours calculated through CAN-Q with respect to a confidence interval derived from the Two Crane Two Operator Simulation Model. CAN-Q's value of 789.12 trips lies well above the confidence interval upper value of 695.7 trips.

This is due to the inefficiency of the Two Crane Two Operator Model to utilize the second crane.


Figure 33. Confidence Interval of Two Crane Two Operator System Output and CAN-Q Output

Average time in the system of CAN-Q, however, does fall within this simulation's $95 \%$ confidence interval of tank time (Figure 34). This value of 0.912 hours is slightly greater than the mean value given through the simulation of 0.89 hours. This is also probably due to random variation in the simulation model.

## Economic Analysis of Outputs by <br> Simulation and CAN-Q

A net present worth was calculated for a one, three, and five year period using the averages for tonnage
generated by the simulation models, and average output per trip from data collection.


Figure 34. Confidence Interval of Two Crane Two Operator System Tank Time and CAN-Q Tank Time

In the economic analysis, each net present worth represents the added income above the original model. This means that the total tonnage for each proposed system was adjusted by subtracting the present system's tonnage from them. Management stated that the Minimum Attractive Rate of Return for the company is $12 \%$, and the profit after overhead generated per ton is approximately $\$ 100.00$. Table XVII represents the final tabulations for the Two Crane One Operator Model and the Two Crane Two Operator Model.

The Two Crane One Operator Model had no personnel cost. This is because the same operator operates the added crane.

TABLE XVII
eConomic andlysis of tank system

| System | Personnel | Equipment | Income Generated Above Original Model | NPW Above Original System |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 1 year | 3 year | 5 year |
| Two Cranes One Operator | - | 25,000 | 1,126,700 | 981,030 | 2,681,108 | 4,036,528 |
| Full System | - | 50,000 | 2,253,400 | 1,962,061 | 5,362,216 | 8,073,056 |
| Two Cranes Two Operators | 101,400 | 25,000 | 695,760 | 596,244 | 1,646,076 | 2,483,076 |
| Full System | 202,800 | 50,000 | 1,391,520 | 1,192,488 | 3,292,152 | 4,966,152 |
| CAN-Q |  |  |  |  |  |  |
| Full System | - | 50,000 | 2,142,117 | 1,862,697 | 5,094,940 | 7,671,907 |
| CAN-Q |  |  |  |  |  |  |
|  |  | 25,000 | 969,659 | 840,809 | 2,303,927 | 3,470,427 |
| Full System | 202,800 | 50,000 | 1,939,318 | 1,681,618 | 4,607,854 | 6,940,854 |
| *Tonnage/year * 100.00 - Operator Cost |  |  |  |  |  |  |
| $12 \%$ MARR |  |  |  |  |  |  |

Equipment cost per crane after installation is approximately $\$ 25,000.00$. The total income generated per year is \$1,126,700 for adding a crane to one half of the system and $\$ 2,253,400$ for adding cranes to both halves of the system (the simulation only simulated one side of the tanks). Net present worth for one half of the system was $\$ 981,030$, $\$ 2,681,108$, and $\$ 4,036,528$ for a one, three and five year period, respectively. The net present worth for a one, three and five year period for the full system was \$1,962,061, \$5,362,216, and $\$ 8,073,056$, respectively.

The Two Crane Two Operator Model incurred the cost of personnel. This amounted to $\$ 101,400$ as estimated by management. This includes operators for the day and night shift for both the weekend and the weekday crew. Equipment cost is the same as the previous system at $\$ 25,000$ per crane after installation. Income generated per year from the addition of the cranes was $\$ 797,100$ for half the system, and \$1,594,200 for the full system. Net present worth for half the system was $\$ 596,244, \$ 1,646,076$, and $\$ 2,483,076$ for $a$ one, three and five year period, respectively. The full system generated a net present worth of $\$ 1,192,488$, $\$ 3,292,152$, and $\$ 4,966,152$ for a one, three and five year system, respectively.

CAN-Q, utilizing an average tone output of 1.337 tons per trip and costs incurred for equipment, yields a present value of $\$ 931,349, \$ 2,547,470$, and $\$ 3,835,954$ for one, three and five years for half of the system. The full system

Yields present values of $\$ 1,862,697, \$ 5,094,940$, and \$7,671,097 for one, three and five years, respectively.

The CAN-Q net present value for two operators is $\$ 840,809, \$ 2,303,927, \$ 3,470,427$ for one, three and five years. These values are for one half of the system. The full system present value for two operators is $\$ 1,681,618$, $\$ 4,607,854$, and $\$ 6,940,854$ for one, three and five years, respectively.

Clearly, the Two Crane One Operator system is best in an economical sense for both the simulation and CAN-Q. However, CAN-Q cannot distinguish between the two types of models run by the simulation. All values from both outputs of CAN-Q and simulation are very close, though, and the way in which CAN-Q operates is closer to the Two Crane One Operator Model than the Two Crane Two Operator Model.

## CHAPTER IX

## CONCLUSIONS

In making management decisions, both CAN-Q and simulation can be very valuable. In this particular situation many trade-offs are involved in using the two different techniques.

Simulation requires extensive system analysis and data collection while CAN-Q requires no modeling and very little data collection. This particular simulation project had a data collection period and system analysis of approximately three months. Another two months was required to build and verify these models. CAN-Q would take approximately two weeks of data collection and no distribution testing, plus no modeling.

Simulation requires expertise while CAN-Q does not. This means that management can utilize CAN-Q without an expert in modeling. For simulation, management will either hire someone or have someone else within the company with the expertise run the simulation for them.

Simulation requires a special software package and in most cases, at least a mini-computer to handle this type of software. CAN-Q is approximately 500 lines in length and can fit on a micro-computer.

CAN-Q only gives means, and not ranges. Simulation
does give means and ranges for the poorest and best performance of a particular system. In this particular problem, though, system variability was not very high.

The most important factor in the difference between CAN-Q and simulation is accuracy as compared to the real system. Both CAN-Q and simulation showed the proposed addition of the cranes as extremely, attractive. CAN-Q did not show, as the simulation did, the optimum arrangement of the cranes and how many operators were needed. The simulation showed clearly that the optimum system was a two crane one operator type of setup, while CAN-Q basically showed only that adding an extra crane would be profitable. CAN-Q also could not analyze the breakdowns of the system. In this case, there was not a large difference in the numbers; however, in a system where frequent breakdowns could occur, CAN-Q may become more inaccurate.

CAN-Q may also be a valuable tool in verifying and validating a simulation. In this particular case, values of simulation and CAN-Q were comparable. Even if values in CAN-Q deviate from the values of simulation, and these deviations can be accounted for, CAN-Q can be a quick way to see if a modeler is on the right track with a simulation model.

The bottom line between simulation and CAN-Q is accuracy versus cost. In this case, both types of analysis revealed it was profitable to add another crane. However, simulation told exactly how to situate the crane while CAN-Q
did not. Simulation also enabled the modeling of breakdowns while CAN-Q could not. CAN-Q, though, takes much less time to develop. In this particular case it would take five to seven months to develop the simulation, compared to two weeks for CAN-Q.

Finally, both the simulation and CAN-Q showed it was extremely profitable to add the cranes. Even though CAN-Q was very close to the simulation's findings, the simulation showed it was most profitable to add an extra crane with one operator.

There are trade-offs in using simulation and CAN-Q. Further research should be done on different types of systems to see if CAN-Q or simulation is more appropriate in different situations.

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APPENDIXES

## APPENDIX A

DATA COLLECTED AND CORRESPONDING HISTOGRAMS

## CAUSTIC DIPPING

| ORDERED DATA |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| .003 | .009 | .009 | .009 | .009 |
| .007 | .010 | .010 | .012 | .012 |
| .012 | .012 | .012 | .012 | .012 |
| .012 | .013 | .013 | .012 | .013 |
| .013 | .013 | .013 | .017 | .014 |
| .014 | .014 | .014 | .015 | .015 |
| .016 | .017 | .017 | .017 | .017 |
| .018 | .017 | .017 | .017 | .010 |
|  | .019 | .017 | .023 | .023 |



HYPOTHESIS STATEMENT

NULL HYPOTHESTS = POPLILATION IS NORMAL WITH TRUE MEAN= GL TERWATIVE: IOPOTHESIS: POPUIATION IS HOT NORMÁL WITH TRUE IIEAN=
$x * * * * * * * * * x * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * x$
HUMEER OF OLSERVATIONG: 45


## COLD WATER DIPPING

## ORDERED DATA

| .006 | .006 | .006 | .007 | .008 |
| :--- | :--- | :--- | :--- | :--- |
| .008 | .009 | .009 | .009 | .007 |
| .009 | .009 | .009 | .010 | .010 |
| .010 | .010 | .010 | .011 | .011 |
| .012 | .012 | .012 | .012 | .012 |
| .012 | .012 | .013 | .015 | .014 |
| .014 | .014 | .014 | .014 | .014 |
| .014 | .015 | .015 | .015 | .015 |
| .016 | .017 | .017 | .020 | .021 |



## HOPOTHESIS STATEMEN

NIIL L. HYPOTHESIS:= POPILLATION IS NORMAL WTTH

$x * * x * * * x * * x * * * * * x * * * x * * * * * x * * * * * * * * * * * * * * * * * * * * * *$
NUNEER OF OLISERVATIONS= 45

| Celis | FROif | KOLMOGGOROU - SMIRNOU TEST |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Rance to | OESERUED | OESERUED FREQUENCY | cunhlative oriserved FREquency | THEORETICAL FREQUENCY | cluillative <br> Theoretical <br> FREQUENCY | KOL MOGOROU SMIRNOU statistic |
| 1 | -977.99902 | . $00 \% 50$ | 4.00000 | . 188889 |  |  |  |  |
| 3 | . 00750 | . 00900 | 7.00000 | .20000 | . 288889 | . 04433 | . 04433 | . 04456 |
| 3 | . 00900 | . 01050 | 5.00000 | . 11111 | . 23889 | . 15748 | . 20181 | . 03708 |
| 4 | . 01050 | .01200 | 8.00000 | . 20000 | . 60000 | . 14221 | . 34402 | . 05598 |
| 5 | . 01200 | . 01550 | 2.00000 | - $0.1+44$ | . 6.64444 | - 168880 | . 51281 | . 03719 |
| 6 | . 01350 | . 01500 | 11.00000 | - 24444 | . 64444 | - 16850 | . 6'7931 | . 03487 |
| 7 | . 01500 | . 01650 | 1.00000 | . 02323 | . 83889 | . 13648 | . 81579 | . 07310 |
| 0 | . 01650 | . 01800 | 2.00000 | .04.2.42 | . 91111 | . 09276 | . 90875 | . 00236 |
| 9 | . 01800 | . 0170 | 2. 00000 | . 04.4 .14 | . 95556 | . 05262 | .96136 | . 00501 |
| 10 | . 01950 | .02100 | 2.00000 | . .04444 | .95556 1.00000 | .02475 | . 98611 | . 03055 |
|  |  | .02.0 | 2.00000 | . 0.4444 | 1.00000 | . 00967 | .99578 | . 0012 c |

[^0]ACID DIPPING

## ORDERED DATA

| .008 | .003 | .008 | .007 | .009 |
| :--- | :--- | :--- | :--- | :--- |
| .009 | .011 | .011 | .011 | .011 |
| .012 | .012 | .012 | .012 | .012 |
| .012 | .013 | .015 | .015 | .013 |
| .013 | .014 | .014 | .014 | .014 |
| .014 | .014 | .015 | .015 | .016 |
| .016 | .016 | .016 | .016 | .016 |
| .017 | .017 | .017 | .017 | .017 |
| .017 | .013 | .017 | .022 | .023 |



## $k \pi x x * * * * * * * * * * * * x * * * * * * * * * * * * * * * * * * * * * * * * * * * *$



## ACID SOAK

## ORDERED DATH

| .117 | .117 | .117 | .117 | .150 |
| :--- | :--- | :--- | :--- | :--- |
| .150 | .150 | .167 | .167 | .167 |
| .167 | .167 | .183 | .163 | .183 |
| .183 | .200 | .200 | .200 | .200 |
| .200 | .200 | .200 | .200 | .200 |
| .200 | .200 | .200 | .217 | .217 |
| .217 | .217 | .233 | .233 | .233 |
| .250 | .253 | .250 | .250 | .250 |
| .250 | .250 | .250 | .250 | .233 |


$\qquad$


## HOT WATER DIPPING

## ORDERED DATA

| .006 | .006 | .006 | .006 | .008 |
| :--- | :--- | :--- | :--- | :--- |
| .008 | .009 | .009 | .009 | .007 |
| .009 | .009 | .010 | .010 | .010 |
| .010 | .010 | .011 | .011 | .012 |
| .012 | .012 | .012 | .012 | .012 |
| .012 | .013 | .015 | .014 | .014 |
| .014 | .014 | .014 | .014 | .015 |
| .015 | .015 | .015 | .015 | .016 |
| .016 | .016 | .016 | .019 | .021 |



## HYPOTHESIS STATEMENT

NULLL HYPOTHESIS = POPULATION IS NORMAL
GL TERNATIUE HYPOTHEGIG- TR THE MEAN POPULATION IS NOT NORMELL WITH TRUE MEAN=

```
***************************************************
ININEEER OF OEGERUATIOHS=
```

| CELLS | KOL Mogorou - smirnou test |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | From Railse |  | OESERUED | OESERUEI) FREQIJENCY |  | THEORETICfiL FREQUENCY | cuitllative <br> THEORETICAL <br> frequency | KOLHOCOROU SMIRNOU STGTISTIC |
|  | FROM | TO |  |  | cumllative ORSERUED |  |  |  |
|  |  |  |  |  | FREQUEHCT |  |  |  |
| 1 | -999.99902 | . 00750 |  |  |  |  |  |  |
| 2 | .00'750 | .00960 | 4.00000 | . 10889 | . 08889 |  |  |  |
| 3 | . 00800 | .00900 .01050 | 9.00000 | . 17778 | . 266667 | .04059 | . 04059 | . 049130 |
| 4 | .01050 | . 01200 | 5.00000 | . 11111 | . 3.36678 | -15191 | . 19250 | . 07717 |
| 5 | . 01200 | . 01350 | 9.00000 | . 20000 | . 57778 | . 14069 | . 33319 | . 074178 |
| 6 | .01350 | . 0150 | 2.00000 | . 04444 | . 6.6222 | - 16940 | . 50259 | .07459 .07519 |
| 7 | .01500 | . 01.500 | 11.00000 | . 24444 | . 626662 | . 16893 | . 67151 | . 07519 |
| 3 | . 01650 | . 016180 | 4.00000 | - 0 03309 | . 866678 | . 13952 | . 81103 | .04929 .0556. |
| 9 | . 01600 |  | . 000000 | . 00000 | . 95550 | . $0959+4$ | . 80647 | .0556 .4 .04909 |
| $: 0$ | .01\%50 | $\begin{array}{r} .01950 \\ .02100 \end{array}$ | $1.00000$ | . 02222 | -95:. 56 <br> .97778 | . 05.417 | . 96053 | .04809 $.0045: 3$ |
|  |  | . 03100 |  | .002ee | $\begin{array}{r} .97770 \\ 1.00000 \end{array}$ | . 025537 | .9859'0 | .00493 $.003: 2$ |
|  |  |  |  |  |  | . 011986 | .99576 | .003.2 |
|  |  |  |  |  | THE | Ol.mogorou - | 104 |  |
| EGreeg | IF FREEDOM= |  |  |  |  | Mogarov | SNOU STGTISTIC | .07519 |
|  | . 011977 | コ= |  |  |  |  |  |  |

## PHOSPHATE DIPPING

| ORDERED DATA |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| .007 | .008 | .003 | .008 | .010 |
| .010 | .011 | .011 | .011 | .011 |
| .011 | .011 | .012 | .012 | .012 |
| .012 | .012 | .012 | .015 | .015 |
| .013 | .014 | .014 | .014 | .014 |
| .014 | .014 | .015 | .015 | .017 |
| .017 | .017 | .017 | .017 | .017 |
| .017 | .017 | .017 | .017 | .017 |
| .020 | .021 | .022 | .025 | .033 |


HipOTHESIS statEMEMT
WHIL HYPOTHESIS=F POPULATION IS NORMAL WITH TRUE MEAN= .0145

$x * * * x * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * *$
IIIMEER OF OESERUGTIOHS = $\quad 45$


## NEUTRALIZER DIPPING

ORDERED DATH

| .010 | .010 | .011 | .011 | .011 |
| :--- | :--- | :--- | :--- | :--- |
| .011 | .012 | .012 | .012 | .012 |
| .012 | .014 | .014 | .014 | .014 |
| .014 | .014 | .014 | .014 | .014 |
| .014 | .015 | .015 | .016 | .016 |
| .016 | .017 | .017 | .017 | .017 |
| .017 | .019 | .019 | .019 | .019 |
| .020 | .020 | .020 | .020 | .020 |
| .020 | .020 | .021 | .025 | .026 |

 CLASS
START 010 STOP $\quad .027$ SIZE OF INTERVAL
CALCULATED MEAN= .01589 CALCULATED VARIANCE $=.000017$


## ORDERED DATA

| .007 | .008 | .009 | .009 | .009 |
| :--- | :--- | :--- | :--- | :--- |
| .009 | .011 | .011 | .012 | .012 |
| .012 | .012 | .012 | .012 | .012 |
| .012 | .012 | .015 | .013 | .015 |
| .013 | .013 | .013 | .014 | .014 |
| .014 | .014 | .014 | .014 | .016 |
| .016 | .016 | .016 | .017 | .017 |
| .017 | .017 | .017 | .017 | .017 |
|  | .019 | .019 | .022 | .023 |


***********************************************

| HULL HYPOTHESIG= POPULATION IS NORMAL. WITH TRUE MEAN= . 0139 fiLTERNATIUE HYPOTHESIB: POPULATION IS NOT NORIAL WITH TRLEE HEAN= 0139 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ************************************************* |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| CELIS KOLMGGOROV - SMIRNOU TEST |  |  |  |  |  |  |  |  |
| celles | FROM | TO |  | OLSERUED FREQUENCY | $\begin{aligned} & \text { LATIUE } \\ & \text { RUED } \end{aligned}$ | THEORETICaL FREQUENCY | cuiflimtive THEORETICAL FREQUENCY | holmoggron SMIRNOU statistic. |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| 1 | -949.99902 | . 00350 |  |  |  |  |  |  |
| 2 | . 00860 | . 01020 | 2.00000 | . 0.4444 | . 04444 |  |  |  |
| 3 | . 01020 | . 01130 | 4.00000 | . 008999 | . 13334 | . 02298 |  |  |
| 4 | . 01180 | .01160 .01340 | 2.00000 15.00000 | . 0.1 .4 .44 | . 17778 | .11895 .12912 |  | .00861) |
| 5 | .01340 | . 01500 | 15.00000 6.00000 | - 33333 | . 51111 | . 17028 |  | . 073 Sa |
| 6 | . 01500 | . 01660 | 4.00000 | . 13333 | . 64444 | -1620 |  | . 06973 |
| 7 | . 01660 | . 01320 | 8.0000 | . 09388 | . 73333 | . 15.68 |  | . 02104 |
| 0 | . 01820 | . 01980 | 8.00000 | . 17778 | . 91111 | . 15858 |  | . 0.4703 |
| 9 | . 01980 | . 02140 | 2.00000 | . 0.4444 | . 95556 | . 11097 |  | . 01897 |
| 10 | .02140 | . 02300 | 2.00000 | . 00000 | . 95555 | . 06335 |  | . 00007 |
|  |  | . 02.30 | 2.00000 | . 04444 |  | -10823 |  | . 0 25:16 |
|  |  |  |  |  |  | . 01095 |  | .0043.7 |
| DEGREE$\substack{\text { cilie. }}$ | OF FREEDOM.013911109 |  | 000 |  | THE | Kolmagorou - | Shirious | .09329 |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |

DRYING

```
ORDERED DATA
\begin{tabular}{lllll}
.050 & .083 & .083 & .083 & .083 \\
.083 & .083 & .083 & .083 & .083 \\
.083 & .083 & .033 & .083 & .083 \\
.083 & .083 & .083 & .100 & .117 \\
.117 & .117 & .133 & .133 & .133 \\
.153 & .133 & .133 & .135 & .167 \\
.167 & .167 & .167 & .167 & .167 \\
.250 & .250 & .167 & .167 & .183 \\
& & .250 & .250 & 1.333
\end{tabular}
```



## hipothesis statement

## NULL. HYPOTHESIS\# POPULATION IS EXP WITH TRUE MEAN: <br> GL. TERHATIUE HYPOTHESI:S= POPLLATION IS NOT EXP WITH TRUE MEAN: <br> $x * * x * x * * k * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * *$ <br> HUMEER OF OBSERUATIONS: <br> 45



TONS/TRIP
ORDERED DATA

| .257 | .318 | .329 | .347 | .381 |
| :--- | :--- | :--- | :--- | :--- |
| .410 | .477 | .533 | .535 | .540 |
| .553 | .582 | .583 | .510 | .559 |
| .685 | .706 | .709 | .721 | .759 |
| .764 | .764 | .755 | .304 | .838 |
| .841 | .341 | .841 | .869 | .869 |
| .918 | .943 | .963 | 1.010 | 1.023 |
| 1.051 | 1.059 | 1.063 | 1.080 | 1.080 |
| 1.111 | 1.124 | 1.142 | 1.142 | 1.155 |
| 1.156 | 1.172 | 1.211 | 1.211 | 1.211 |
| 1.216 | 1.332 | 1.332 | 1.332 | 1.332 |
| 1.441 | 1.441 | 1.442 | 1.512 | 1.525 |
| 1.650 | 1.682 | 1.695 | 1.695 | 1.746 |
| 1.756 | 1.780 | 1.814 | 1.895 | 1.913 |
| 1.920 | 2.241 | 2.241 | 2.253 | 2.345 |
| 2.345 | 2.400 | 2.415 | 2.457 | 2.521 |
| 2.909 | 2.932 | 2.982 | 3.009 | 3.012 |
| 3.025 | 3.025 |  |  |  |




## BREAKDOWN LENGTH

| ORDERED DATA |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | .006 | .006 | .006 | .007 |
| .008 | .009 | .009 | .009 | .008 |
| .009 | .009 | .009 | .010 | .010 |
| .010 | .010 | .010 | .011 | .011 |
| .012 | .012 | .012 | .012 | .012 |
| .012 | .012 | .013 | .015 | .014 |
| .014 | .014 | .014 | .014 | .014 |
| .014 | .015 | .015 | .015 | .015 |
| .016 | .017 | .017 | .020 | .021 |


$* * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * x * * * * * * * * * * * *$

HYPOTHESIS STATEMENT
NILL HYPOTHEGISE POPULATION IS NORMAL WITH TRUE MEAN GL TERNATIUE HIPOTHEGY:B POPULATION IS MOT HORMAL WITH TRLIE MEA .0119
$* * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * *$
NUMEER OF OBSERUATIONS: 45

| KOL.MOGOROU - SMIRNOU TEET |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| cells | FROM | Rainge to | corserveo | observed FREQUENCY | CUMULATIVE <br> ohgerved <br> FREELUENCY | THEORETICAL FREQUENCY | Cuhtulative <br> THEORETICAL FREQUENCY | KOL MOGOROU SMIRNOU GTGTISTIC |
| 1 | -999.99902 | . 00750 | 4.00000 | . 008889 | . 08889 |  |  |  |
| 3 | . 00750 | . 00900 | 5.00000 | .20000 | . 286889 | . 15748 | .07433 .20181 | .04756 .08705 |
| 3 | .00900 | . 01050 | 5.00000 | . 11111 | . 40000 |  | . 301810 |  |
| 4 | . 01050 | . 01200 | 9.00000 | .20000 | .60000 | . 16680 | - 51381 | -055,9\% |
| 5 | . 01200 | .01350 | 2.00000 | -0t+it | . $64.7+7$ | -16690 | . 51291 | . 06719 |
| 6 | . 01350 | . 01500 | 11.00000 | . 24444 | . 898089 | . 16650 | .67931 | . $03-267$ |
| 7 | .01500 | . 01650 | 1.00000 | -02.22 | .88389 .91111 | . 13.48 | . 81579 | .07310 |
| 9 | . 01650 | . 01300 | 2.00000 | . $0.4+44$ | . 95111 | . 07276 | .90875 | . 00236 |
| 9 | .01800 | . 01050 | -. 000000 | . 060000 | .9555s | -053ic | . 96136 | . 011551 |
| 10 | . 01950 | .02100 | 2.00000 | . 0.4 .444 | 1.00000 | . 02475 | . 98611 | . 03055 |

[^1]
## APPENDIX B

PRESENT SYSTEM SLAM ATTRIBUTES, LISTING, AND NETWORK

Attribute

## Description

Type of Operation
Caustic Dipping
Cold Water Dipping
Acid Dipping
Acid Soak
Hot Water Dipping
Phosphate Dipping
Neutralizer Dipping
Soap Dipping
Drying
Breakdown Time
Breakdown Length
Time an Entity Starts in the System Tons/Trip

```
GEN,U. R. LEWIS.TANKS,1/04/84,10;
LIMITS.2,14,100;
INIT,0,360;
INTLC, XX(1)=0;
INTLC,XX(2)=0;
TIMST,XX(1),NUMBER IN SYS. 1;
TIMST.XX(2),NUMBER OF BRKDWNS.;
TIMST,XX(3),TON OUTPUT,;
NETWORK;
        GATE/CR1,OPEN,1;
        CREATE;
ST GOON,1.
        ACT . . . 89, LUB;
        ACT, . 043, PHO;
        ACT, . 067,TRI;
LUB ASSIGN,ATRIB(1)=1;
        ACT,.,TAN;
PHO ASSIGN,ATRIB(1)=2;
        ACT,.,TAN;
TRI ASSIGN,ATRIB(1)=3;
        ACT,, TAN;
TAN ASSIGN,ATRIB(2)=2*RNORM(.014,.0035,1);
        ASSIGN,ATRIB(3)=RNORM(.0119,.0035,2);
        ASSIGN,ATRIB(4)=2*RNORM(.0139,.0034,3);
        ASSIGN,ATRIB(5)=RNORM(.1989..0406,4);
        ASSIGN, ATRIB(6)=RNORM(.012,.0034,5):
        ASSIGN,ATRIB(7) =2*RNORM(.0145,.0048,6);
        ASSIGN,ATRIB(8)=RNORM(.0159,.00384,7);
        ASSIGN,ATRIB(9)=2*RNORM(.0139,.00346,8);
        ASSIGN,ATRIB(10)=EXPON(. 1673.9):
        ASSIGN,ATRIB(13) = TNOW ;
        ASSIGN,ATRIB(14)=GAMMA (.42017,3.18293,5);
        ACT :
        GOON;
        ACT,.198+ATRIB(2); CAUSTIC DIP AND SOAK
        AWAIT,CR1;
        ACT,.OOO83+ATRIB(3); COLD WATER RINSE
        AWAIT,CR1;
        ACT,.00125+ATRIB(4)+ATRIB(5);
        AWAIT,CR1;
        ACT,.O0125+ATRIB(3);
        AWAIT,CR1;
        ACT,.005+ATRIB(6);
        AWAIT,CR1,1;
        ACT,,ATRIB(1).EQ.3.T:
        ACT,.0852+ATRIB(7);
        AWAIT,CR1:
        ACT..O019+ATRIB(3);
        AWAIT,CR1,1;
        ACT,,ATRIB(1).EQ.2,P;
        ACT,.0006+ATRIB(8);
        AWAIT,CR1;
        ACT,.085+ATRIB(9),,DRY;
        GOON:
        ACT,.0058 , ,DRY;
    P GOON;
    ACT,.OO21,.DRY; PHOSPHATE
DRY AWAIT,CR1;
        ACT,.04;
        AWAIT,CR1,2:
        ACT,.,EN;
        ACT,.O158;
ACID DIP AND SOAK
COLD WATER RINSE
HOT WATER RINSE
PHOSPHATE
COLD WATER RINSE
NEUTRALIZER
SOAP
TRICK
```




| CR1 | OPEN | 1 |
| :--- | :--- | :--- |










## APPENDIX C

TWO CRANE ONE OPERATOR SLAM ATTRIBUTES, LISTING, AND NETWORK

## ATTRIBUTE DESCRIPTION OF TWO CRANE ONE OPERATOR MODEL

| Attribute | Description |
| :---: | :---: |
| 1 | Type of Operation, Crane 1 |
| 2 | Caustic Dipping, Crane 1 |
| 3 | Cold Water Dipping, Crane 1 |
| 4 | Acid Dipping, Crane 1 |
| 5 | Acid Soak, Crane 1 |
| 6 | Hot Water Dipping, Crane 1 |
| 7 | Phosphate Dipping, Crane 1 |
| 8 | Neutralizer Dipping, Crane l |
| 9 | Soap Dipping, Crane 1 |
| 10 | Drying, Crane 1 |
| 11 | Breakdown Time, Crane 1 |
| 12 | Breakdown Length, Crane 1 |
| 13 | Type of Operation, Crane 2 |
| 14 | Caustic Dipping, Crane 2 |
| 15 | Cold Water Dipping, Crane 2 |
| 16 | Acid Dipping, Crane 2 |
| 17 | Acid Soak, Crane 2 |
| 18 | Hot Water Dipping, Crane 2 |
| 19 | Phosphate Dipping, Crane 2 |
| 20 | Neutralizer Dipping, Crane 2 |
| 21 | Soap Dipping, Crane 2 |
| 22 | Drying, Crane 2 |
| 23 | Breakdown Time, Crane 2 |
| 24 | Breakdown Length, Crane 2 |
| 25 | Time Entity Starts in System, Crane 1 |
| 26 | Time Entity Starts in System, Crane 2 |
| 29 | Tons/Trip, Crane 1 |
| 30 | Tons/Trip, Crane 2 |

2
LIMITS, 11,30,10:
INIT,0,360;
INTLC, $X X(1)=0$;
INTLC, $X X(2)=0$;
INTLC, $X X(3)=0$;
TIMST, XX (1), NUMBER IN Sī. 1;
TIMST, XX(2), NUMBER OF BRKDWNS.;
TIMST, XX(3), NUMBER OF BRKDWNS IN SYS 2:
TIMST, XX(4),TON OUTPUT;
NETWORK:
GATE/CR1. OPEN, 1:
GATE/CR2, OPEN, 2 ;
GATE/MOV, CLOSE, 3 ;
GATE/SC2, CLOSE,4;
GATE/C2, OPEN, 5;
GATE/P2, OPEN, 6 ;
GATE/SO2. OPEN 7 ;
GATE/SC1.OPEN, 8 ;
GATE/ACID. OPEN, 9 :
GATE/PAS 1, OPEN, 10;
GATE/PAS2,OPEN, 11;
CREATE:
GOON, 1 ;
ACT, ,. 89 . LUB :
ACT, . .043, PHO;
ACT,..067,TRI;
LUB ASSIGN, ATRIB(i)=1;
ACT,.,TAN:
PHO ASSIGN, ATRIB(1) $=2$;
ACT,,,TAN:
TRI ASSIGN,ATRIB(1)=3;
ACT, , TAN:
ASSIGN, ATRIB (2) 2 2*RNORM (.014,.0035,1);
ASSIGN, ATRIB (3)=RNORM(.0119,.0035,2)
ASSIGN, ATRIB (4) $=2 *$ RNORM $(.0139, .0034,3)$;
ASSIGN, ATRIB (5) =RNORM (.1989,.O406,4);
ASSIGN, ATRIB(6)=RNORM(.012,.0034,5):
ASSIGN, ATRIB ( 7 ) $=2$ *RNORM $(.0145, .0048,6)$;
ASSIGN, ATRIB ( 8 ) = RNORM (.0159,.00384,7);
ASSIGN, ATRIB(9)=2*RNORM (.0139,.00346,8):
ASSIGN, ATRIB (10)=EXPON(.1673.9);
ASSIGN, ATRIB(25) = TNOW ;
ASSIGN, ATRIB (29) =GAMMA (.42017,3.18293,5):
AWAIT, SC1;
ACT;
CLOSE, SC2;
ACT, . 114+ATRIB(2);
AWAIT, CR1;
OPEN, SC2;
CLOSE,C2:
ACT,O83: CAUSTIC SOAK
AWAIT, CR1;
AWAIT, SC 1 ;
CLOSE,SC2:
OPEN,C2;
ACT, OOO83+ATRIB(3): COLD WATER RINSE
AWAIT, CR1;
ACT. OO125+ATRIB(4): ACID DIP AND SOAK
OPEN, SC2;
CLOSE,ACID;
ACT,ATRIB(5):

```
    AWAIT,SC!:
    CLOSE,SC2;
    AWAIT,CR1;
    ACT,.OO125+ATRIB(3); COLD WATER RINSE
    AWAIT,CR1;
    ACT,.005+ATRIB(6); HOT WATER RINSE
    OPEN,ACID;
    CLOSE,PAS 1;
    AWAIT,CR1,1;
    ACT,,ATRIB(1).EQ.3,T;
    ACT,.0019+ATRIB(7):
    AWAIT,CR1;
    OPEN,SC2:
    CLOSE,P2;
    ACT..O83: PHOSPHATE SOAK
    AWAIT,CR1;
    OPEN,P2;
    AWAIT,SC1;
    CLOSE,SC2:
    ACT..0019+ATRIB(3): COLD WATER RINSE
    CLOSE,PAS2;
    AWAIT,CR1,1;
    ACT,,ATRIB(1).EQ.2,P;
    ACT,.0006+ATRIB(8): NEUTRALIZER
    AWAIT,CR1;
    ACT,.OO17+ATRIB(9): SOAP
    AWAIT,CR1;
    OPEN,SC2;
    CLOSE,SO2:
    ACT,.083;
    AWAIT,CR1;
    ACT...DRY;
    GOON;
    ACT,.0058: TRICK
    AWAIT,CR1;
    OPEN,SC2;
    ACT.,.DRY:
    GOON:
    ACT,.OO21: PHOSPHATE
    AWAIT,CR1;
    OPEN,SC2;
    ACT,.,DRY;
GOON:
    OPEN,PAS 1;
    OPEN,PAS2;
    ACT . O4;
    AWAIT,CR1:
    OPEN,SO2;
    AWAIT,SC1;
    CLOSE,SC2;
    OPEN,SC2;
    COLCT,INT(25),TANK TIME SYS 1,15/.5/.1;
    GOON,2;
    ACT, , ,EN;
    ACT:
    AWAIT,MOV:
    CLOSE,SC2;
    CLOSE,MOV;
    ACT,.0158;
    AWAIT,CR1:
    ACT,.,ST:
EN GOON;
    ACT,ATRIB(10):
    COLCT,INT(25),TOTAL TIME SYS 1,15/.5/.1;
OUT ASSIGN,XX(1)=XX(i)+i;
ASSIGN,XX(4)=XX(4)+ATRIB(29)+ATRIB(30);
```



```
    ACT;
    AWAIT,P2;
    AWAIT,SC2;
    CLOSE,SC1;
    ACT,.OO19+ATRIB(19); PHOSPHATE
    AWAIT,CR2;
    OPEN,SC1: PHOSPHATE SOAK
    AWAIT,CR2;
    AWAIT,SC2;
    CLOSE,SC1;
    ACT..O019+ATRIB(15): COLD WATER RINSE
    AWAIT,CR2,1;
    ACT,.ATRIB(13).EQ.2,PP: NEUTRALIZER
    OPEN,SC1:
    AWAIT.CR2;
    AWAIT,SO2;
    AWAIT,SC2;
    CLOSE.SC1;
    ACT,.OO17+ATRIB(21): SOAP
    AWAIT,CR2;
    OPEN,SC1;
    ACT..O83; SOAP SOAK
    AWAIT,CR2;
    ACT,,.DR2;
T2 GOON;
    OPEN,SC 1:
    AWAIT,PAS 1:
    AWAIT,SC2;
    CLOSE,SC1:
    ACT,.OO58; TRICK
    AWAIT,CR2;
    OPEN,SC1;
    ACT..,DR2;
PP GOON;
    OPEN, SC1:
    AWAIT,PAS2;
    AWAIT,SC2;
    CLOSE,SC1;
    ACT,.OO21: PHOSPHATE
    AWAIT,CR2:
    OPEN,SC1;
    ACT, ,,DR2;
DR2 GOON;
    AWAIT,SC2;
    CLOSE,SC1;
    ACT,.04;
    AWAIT,CR2;
    OPEN,SC1;
    COLCT,INT(26),TANK TIME SYS 2,15/.5/.1;
    GOON, 2;
    ACT,,.E2;
    ACT;
    OPEN,MOV;
    ACT,.,ST2:
    GOON;
    ACT,ATRIB(22);
    COLCT,INT(26),TOTAL TIME SYS 2,15/.5/.1;
    ACT, ,,OUT:
    CREATE: NETWORK TO RUN BREAKDOWNS
    GOON, 1:
    ACT , . 83,GD2;
    ACT...17.DN2; DETERMINE IF BRKDWN OCCURS
GD2 GOON;
    ACT, 12,,SH2;
```

| 261 | DN2 | ASSIGN,ATRIB $(27)=\operatorname{UNFRM}(0,12,10) ;$ |
| :--- | :--- | :--- |
| 262 |  | ASSIGN,ATRIB $(28)=\operatorname{EXPON}(1.023,9) ;$ |
| 263 |  | ASSIGN,XX(3)=XX(3)+1,1; |
| 264 |  | ACT,ATRIB(27); |
| 265 | CLOSE,CR2; |  |
| 266 |  | ACT,ATRIB(28); |
| 267 |  | OPEN,CR2; |
| 268 |  | ACT, 12-ATRIB(27)-ATRIB(28), ,SH2; |
| 269 |  | END; |
| 270 | FIN; |  |



| CR1 | OPEN | 1 | S02 | OPEN | 7 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| CR2 | OPEN | 2 | SC1 | OPEN | 8 |
| MOV | CLOSE | 3 | ACID | OPEN | 9 |
| SC2 | CLIOSE | 4 | PaS1 | OPEN | 10 |
| C2 | OPEN | 5 | PAS2 | OPIN | 11 |
| P2 | OPEN | 6 |  |  |  |

















## APPENDIX D

TWO CRANE TWO OPERATOR SLAM ATTRIBUTES, LISTING, AND NETWORK

# ATTRIBUTE DESCRIPTION OF TWO CRANE TWO OPERATOR MODEL 

Attribute
1
2
3
4
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16

Description
Type of Operation Caustic Dipping
Cold Water Dipping
Acid Dipping
Acid Soak
Hot Water Dipping
Phosphate Dipping
Neutralizer Dipping
Soap Dipping
Drying
Breakdown Time, Crane 1
Breakdown Length, Crane 1
Time an Entity Starts in the System
Breakdown Time, Crane 2
Breakdown Length, Crane 2
Tons/Trip

```
GEN,J. R. LEWIS,TANKS,1/04/84,10;
LIMITS,4,16,10;
INIT,0,360;
INTLC, XX(1)=0;
INTLC, XX(2)=0:
INTLC, XX(3)=0;
TIMST,XX(1),NUMBER IN SYS. 1;
TIMST,XX(2),NUMBER OF BRKDWNS.;
TIMST,XX(3),NUMBER OF BRKDOWNS 2:
TIMST,XX(4),TON OUTPUT;
NETWORK;
    RESOURCE/WC1, 2:
    RESOURCE/WC2,3;
    GATE/CR1,OPEN, 1;
    GATE/CR2, OPEN, 4;
    CREATE;
ST GOON, 1;
    ACT . . 89, LUB;
    ACT, ..043,PHO;
    ACT,..067,TRI;
LUB ASSIGN,ATRIB(1)=1;
    ACT,,,TAN;
PHO ASSIGN,ATRIB(1)=2;
    ACT,,,TAN:
TRI ASSIGN,ATRIB(1)=3;
    ACT ...TAN;
TAN ASSIGN,ATRIB(2)=2*RNORM(.014,.0035,1);
    ASSIGN, ATRIB(3)=RNORM(.0119,.0035,2);
    ASSIGN,ATRIB(4)=2*RNORM(.0139,.0034,3);
    ASSIGN,ATRIB(5)=RNORM(.1989,.0406,4);
    ASSIGN,ATRIB(6)=RNORM(.012,.0034,5);
    ASSIGN,ATRIB(7) =2*RNORM(.0145,.0048,6);
    ASSIGN,ATRIB(8)=RNORM(.0159,.00384,7);
    ASSIGN,ATRIB(9)=2*RNORM(.0139,.00346,8);
    ASSIGN, ATRIB (10)=EXPON(.1673.9);
    ASSIGN,ATRIB(13)=TNOW;
    ASSIGN,ATRIB(16)=GAMMA (.42017,3.18293,5);
    ACT;
    GOON:
    ACT,.198+ATRIB(2); CAUSTIC DIP AND SOAK
    AWAIT.CR1;
    ACT,.00083+ATRIB(3); COLD WATER RINSE
    AWAIT,CR1;
    ACT,.OO125+ATRIB(4)+ATRIB(5); ACID DIP AND SOAK
    AWAIT,CR1;
    ACT,.OO125+ATRIB(3);
    AWAIT,CR1;
    AWAIT,WC1;
    ACT,.033;
    GOON, 2;
    ACT,.00871, ,ST;
    ACT;
    AWAIT,WC2;
    ACT,.033+.005+ATRIB(6):
    FREE, WC1;
    AWAIT,CR2,1;
    ACT, ,ATRIB(3).EQ.3,T;
    ACT,.O852+ATRIB(7): PHOSPHATE
    AWAIT,CR2;
    ACT,.OO19+ATRIB(3): COLD WATER RINSE
    AWAIT,CR2,1;
    ACT,,ATRIB(1).EQ.2,P;
```

```
ACT,.0006+ATRIB(8);
    AWAIT,CR2;
    ACT,.085+ATRIB(9) , DRY:
T GOON;
    ACT ,.0058, ,DRY :
P GOON;
    ACT,.0021,.DRY
DRY AWAIT,CR2;
    ACT,.04;
    AWAIT,CR2,2;
    ACT, ,,EN;
    ACT,.O158;
    AWAIT.CR2;
    COLCT,INT(13),TANK TIME,15/.5/.1:
    ACT,.0158;
    FREE,WC2;
    TERM:
EN GOON:
    ACT,ATRIB(10);
    COLCT,INT(13),TOTAL TIME,15/.5/.1;
    ASSIGN, XX(1)= XX(1)+1;
    ASSIGN,XX(4)=XX(4)+ATRIB(16);
    TERM;
    CREATE: NETWORK TO RUN BREAKDOWNS
SH GOON.1.
        ACT , . 83,GD;
        ACT...17.DN; DETERMINE IF BRKDWN OCCURS
GD GOON
    ACT, 12, ,SH;
DN ASSIGN,ATRIB(11)=UNFRM(0,12,10);
    ASSIGN,ATRIB(12)=EXPON(1.023.9);
    ASSIGN, XX(2)=XX(2)+1,1;
    ACT,ATRIB(11):
    CLOSE,CR1;
    ACT, ,ATRIB(11)+ATRIB(12).GT. 12.E;
    ACT.ATRIB(12):
    OPEN,CR1;
    ACT,12-ATRIB(11)-ATRIB(12),.SH;
E GOON:
    OPEN,CR1;
        ACT,,,SH;
        CREATE:
SH2 GOON,1
        ACT . . . 83,GD2;
        ACT,..17.DN2; DETERMINE IF BRKDWN OCCURS
GD2 GOON
    ACT, 12,,SH2;
DN2 ASSIGN,ATRIB(14)=UNFRM(0,12,10);
    ASSIGN,ATRIB(15)=EXPON(1.023,9);
    ASSIGN, XX(3)=XX(3)+1,1;
    ACT,ATRIB(14);
    CLOSE,CR2;
    ACT.,ATRIB(14)+ATRIB(15).GT.12,EE;
    ACT,ATRIB(15);
    OPEN,CR2;
    ACT, 12-ATRIB(14)-ATRIB(15), ,SH2;
GOON;
    OPEN,CR2;
    ACT,,,SH;
    END:
FIN:
```



| CR1 | OPEN | 1 |
| :--- | :--- | :--- |
| CR2 2 | OPEN | 4 | | WC1(1) | 3 |
| :--- | :--- |
| $W C 2(1)$ | 4 |












## APPENDIX E

## OUTPUT OF PRESENT SYSTEM MODEL












## APPENDIX F <br> OUTPUT OF TWO CRANE ONE OPERATOR MODEL







| **File statistics** |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FILE NUMBER | ASSOCIATED NODE TYPE | AVERAGE <br> LENGTH | STANDARD DEVIATION | MAXIMUM LENGTH | CURRENT LENGTH | average WAITING TIME |
| 1 | AWAIT | 0.0144 | 40.1192 | 1 |  |  |
| 2 | AWAIT | 0.0183 | $3 \quad 0.1341$ | 1 | 0 | 0.0010 0.0014 |
| 3 | AWAIT | 0.0211 | 10.1436 | 1 | 0 |  |
| 4 | AWAIT | 0.1345 | $5 \quad 0.3412$ | 1 | 0 | 0.0198 0.0158 |
| 5 | AWAIT | 0.0000 | 0 0.000 | 1 | 0 | 0.0158 0.0000 |
| 6 | AWAIT | 0.0026 | $6 \quad 0.0505$ | 1 | 0 | 0.0026 |
| 7 | AWAIT | 0.0034 | $4 \quad 0.0586$ | 1 | 0 | 0.0037 |
| 8 | AWAIT | O. 1241 | $1 \quad 0.3297$ | 1 | 0 | 0.0236 |
| 9 10 | AWAIT | 0.0110 0.0066 | ( 0.1041 | 1 | - | 0.0101 |
| 11 | AWAIT | 0.0006 0.0000 | $\begin{array}{ll} \\ 0 & 0.0252 \\ 0.0000\end{array}$ | 1 | 0 | 0.0074 |
| 12 | calendar | 4.0135 | 0.0 .0000 | 0 | 0 | 0.0000 |
| 12 | calendar | 4.0135 |  |  |  | 0.0537 |
| **GATE STATISTICS** |  |  |  |  |  |  |
| GATE NUMBER | GATE LABEL | CURRENT STATUS | PCT. OF <br> TIME OPEN |  |  |  |
| , | CR1 | OPEN | 0.9853 |  |  |  |
| 2 | CR2 | OPEN | 0.9797 |  |  |  |
| 3 | MOV | OPEN | 0.3799 |  |  |  |
| 4 | SC2 | OPEN | 0.6242 |  |  |  |
| 5 | C2 | OPEN | 0.8951 |  |  |  |
| 6 | P2 | Closed | 0.9167 |  |  |  |
| 7 | SO2 | OPEN | 0.8833 |  |  |  |
| 8 | SC1 | OPEN | 0.5366 |  |  |  |
| 9 | ACID | OPEN | 0.7118 |  |  |  |
| 10 | PAS 1 | Closed | 0.7221 |  |  |  |
| 11 | PAS2 | OPEN | 0.8769 |  |  |  |



| **FILE STATISTICS** |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FILE NUMBER | ASSOCIATED NODE TYPE | AVERA <br> LENGT |  | STANDARD DEVIATION | MAXIMUM LENGTH | CURRENT <br> LENGTH | AVERAGE WAITING TIME |
| 1 | AWAIT | 0.0 |  |  |  |  |  |
| 2 | AWAIT | 0.0 |  | 0.1427 | 1 | 0 | 0.0002 |
| 3 | AWAIT | 0.0 |  | O. 1464 | 1 | 0 | 0.0015 |
| 4 | AWA IT | 0.1 |  | 0.3235 | 1 | 0 | 0.0203 |
| 5 | AWAIT | 0.0 |  | 0.0346 | 1 | 0 | 0.0139 |
| 6 | AWA IT | 0.0 |  |  | 1 | 0 | 0.0011 |
| 7 | AWAIT | 0.0 |  | 0.0691 | 1 | 0 | 0.0032 |
| 8 | AWAIT | 0.1 |  | 0.3374 | 1 | 0 | 0.0049 |
| 9 | AWAIT | 0.0 |  | 0. 1100 | 1 | 1 | 0.0247 |
| 10 | AWAIT | 0.0 |  | 0.0000 | 1 | 0 | 0.0113 |
| 11 | AWA IT | 0.00 |  | 0.0000 | 0 | 0 | 0.0000 |
| 12 | CALENDAR | 4.0 |  | 0.0000 0.6930 | 7 | 0 3 | $\begin{aligned} & 0.0000 \\ & 0.0539 \end{aligned}$ |
| **GATE STATISTICS** |  |  |  |  |  |  |  |
| GATE NUMBER | GATE <br> LABEL | CURRENT STATUS | PCT. OF <br> TIME OPEN |  |  |  |  |
| 1 | CR 1 | OPEN | 0.9951 |  |  |  |  |
| 2 | CR2 | OPEN | 0.9779 |  |  |  |  |
| 3 | MOV | CLOSED | 0.3754 |  |  |  |  |
| 4 | SC2 | OPEN | 0.6280 |  |  |  |  |
| 5 | C2 | OPEN | 0.8957 |  |  |  |  |
| 6 | P2 | OPEN | 0.9185 |  |  |  |  |
| 7 | SO2 | OPEN | 0.8840 |  |  |  |  |
| 8 | SC 1 | CLOSED | 0.5274 |  |  |  |  |
| 9 | ACID | OPEN | 0.7114 |  |  |  |  |
| 10 | PAS 1 | CLOSED | 0.7238 |  |  |  |  |
| 11 | PAS2 | OPEN | 0.8786 |  |  |  |  |



| **FILE STATISTICS** |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FILE NUMBER | ASSOCIATED NODE TYPE | AVERAGE <br> LENGTH | STANDARD DEVIATION | MAXIMUM LENGTH | CURRENT LENGTH | AVERAGE WAITING TIME |
| 1 | AWAIT | 0.0162 | 20.1263 |  |  |  |
| 2 | AWAIT | 0.0173 | $3 \quad 0.1302$ | 1 | 0 | 0.0011 |
| 3 | AWAIT | 0.0140 | 0 0.1177 | 1 | 0 | 0.0013 |
| 4 | AWAIT | 0.1190 | 0 0.3238 | 1 | 0 | 0.0131 |
| 5 | AWAIT | 0.0051 | $1 \quad 0.0712$ | 1 | 0 | 0.0140 |
| 6 | AWAIT | 0.0023 | $3 \quad 0.0477$ | 1 | 0 | 0.0047 0.0023 |
| 7 | AWAIT | 0.0108 | $8 \quad 0.1034$ | 1 | 0 | 0.0113 |
| 8 | AWAIT | 0. 1268 | $8 \quad 0.3328$ | , | 0 | 0.0240 |
| 9 10 | AWAIT | 0.0127 | $1 \quad 0.1120$ | 1 | 0 | 0.0118 |
| $\begin{aligned} & 10 \\ & 11 \end{aligned}$ | AWAIT <br> AWAIT | 0.0011 | $1 \quad 0.0336$ | 1 | 0 | 0.0146 |
| $\begin{aligned} & 11 \\ & 12 \end{aligned}$ | AWAIT <br> CALENDAR | 0.0000 4.0177 | $\begin{array}{ll}0.0000 \\ & 0.7123\end{array}$ | 0 | 0 | 0.0000 |
|  | calendar | 4.0177 |  |  |  | 0.0537 |
| **GATE STATISTICS** |  |  |  |  |  |  |
| GATE NUMBER | GATE LABEL | CURRENT <br> STATUS | PCT. OF time open |  |  |  |
| 1 | CR 1 | OPEN | 0.9832 |  |  |  |
| 2 | CR2 | OPEN | 0.9804 |  |  |  |
| 3 | MOV | CLOSED | 0.4159 |  | . |  |
| 4 | SC2 | closed | 0.6401 |  |  |  |
| 5 | C2 | OPEN | 0.8875 |  |  |  |
| 6 | P2 | OPEN | 0.9164 |  |  |  |
| 7 | SO2 | OPEN | 0.8716 |  |  |  |
| 8 | SC 1 | OPEN | 0.5342 |  |  |  |
| 9 | ACID | Closed | 0.7178 |  |  |  |
| 10 | PAS 1 | OPEN | 0.7082 |  |  |  |
| 11 | PAS2 | OPEN | 0.8659 |  |  |  |


**FILE STATISTICS**

| FILE <br> NUMBER | ASSOCIATED NODE TYPE | AVERAGE <br> LENGTH | STANDARD DEVIATION | MAXIMUM LENGTH | CURRENT <br> LENGTH | AVERAGE WAITING TIME |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | AWAIT | 0.0283 | O. 1659 | 1 | 0 | 0.0020 |
| 2 | AWAIT | 0.0118 | 3 O.1079 | 1 | 0 | 0.0009 |
| 3 | AWAIT | 0.0127 | -0.1121 | 1 | 0 | 0.0120 |
| 4 | AWAIT | 0.1221 | 1 0.3274 | 1 | 0 | 0.0144 |
| 5 | AWAIT | 0.0156 | - 0.1241 | 1 | 0 | 0.0146 |
| 6 | AWAIT | 0.0061 | 10.0776 | 1 | 0 | 0.0060 |
| 7 | AWAIT | 0.0041 | 10.0636 | 1 | 0 | 0.0042 |
| 8 | AWA IT | 0.1238 | 0.3293 | 1 | 0 | 0.0236 |
| 9 | AWAIT | 0.0130 | 0 0.1133 | 1 | 0 | 0.0121 |
| 10 | AWAIT | 0.0007 | 0.0258 | 1 | 0 | 0.0109 |
| 11 | AWAIT | 0.0000 | 0.0000 | 0 | 0 | 0.0000 |
| 12 | CALENDAR | 4.0194 | 0.7330 | 7 | 4 | 0.0540 |
| **GATE STATISTICS** |  |  |  |  |  |  |
| GATE NUMBER | GATE <br> LABEL | CURRENT STATUS | PCT. OF <br> TIME OPEN |  |  |  |
| 1 | CR 1 | OPEN | 0.9705 |  |  |  |
| 2 | CR2 | OPEN | 0.9878 |  |  |  |
| 3 | MOV | OPEN | 0.4217 |  |  |  |
| 4 | SC2 | OPEN | 0.6324 |  |  |  |
| 5 | C2 | OPEN | 0.8824 |  |  |  |
| 6 | P2 | OPEN | 0.9135 | , |  |  |
| 7 | SO2 | CLOSED | 0.8843 |  |  |  |
| 8 | SC 1 | CLOSED | 0.5312 |  |  |  |
| 9 | ACID | OPEN | 0.7138 |  |  |  |
| 10 | PAS 1 | CLOSED | 0.7176 |  |  |  |
| 11 | PAS 2 | CLOSED | 0.8741 |  |  |  |




**FILE STATISTICS**

| FILE <br> NUMBER | ASSOCIATED NODE TYPE | AVERA <br> LENGT | STANDARD DEVIATION | MAXIMUM LENGTH | CURRENT <br> LENGTH | AVERAGE WAITING TIME |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | AWAIT | 0.0 |  |  |  |  |
| 2 | AWAIT | 0.0 | 5 0.0606 | 1 |  | 0.0003 |
| 3 | AWAIT | 0.0 | 3 0.1657 | 1 | $0$ | 0.0021 |
| 4 | AWAIT | 0.1 | 40.1657 <br> 0.3254 | 1 | 0 | 0.0264 |
| 5 | AWAIT | 0.0 | 0 0.0000 | 1 | 0 | 0.0141 |
| 6 | AWAIT | 0.00 | $0 \quad 0.0551$ | 1 | 0 | 0.0000 |
| 7 | AWAIT | 0.00 | $1 \quad 0.0776$ | 1 | 0 | 0.0030 |
| 8 | AWAIT | 0.12 | $4 \quad 0.3278$ | 1 | 1 | 0.0064 |
| 9 | AWAIT | 0.0 | 8 (0.1165 | 1 | 1 | 0.0231 |
| 10 | AWA IT | 0.00 | $7 \quad 0.0265$ | 1 | 0 | 0.0127 |
| 11 | AWAIT | 0.00 |  | 0 | 0 | $0.0097$ |
| 12 | CALENDAR | 4.02 | $6 \quad 0.7076$ | $\begin{aligned} & 0 \\ & 7 \end{aligned}$ | $\begin{aligned} & 0 \\ & 3 \end{aligned}$ | $\begin{aligned} & 0.0000 \\ & 0.0535 \end{aligned}$ |
| **GATE STATISTICS** |  |  |  |  |  |  |
| GATE NUMBER | GATE <br> LABEL | CURRENT STATUS | PCT. OF <br> TIME OPEN |  |  |  |
| 1 | CR 1 | OPEN | 0.9921 |  |  |  |
| 2 | CR2 | OPEN | 0.9707 |  |  |  |
| 3 | MOV | OPEN | 0.4076 |  |  |  |
| 4 | SC2 | OPEN | 0.6367 |  |  |  |
| 5 | C2 | OPEN | 0.9002 |  |  |  |
| 6 | P2 | OPEN | 0.9162 |  |  |  |
| 7 | SO2 | OPEN | 0.8782 |  |  |  |
| 8 | SC 1 | CLOSED | 0.5330 |  |  |  |
| 9 | ACID | CLOSED | 0.7145 |  |  |  |
| 10 | PAS 1 | OPEN | 0.7123 |  |  |  |
| 11 | PAS2 | OPEN | 0.8733 |  |  |  |

SIMULATION PRDJECT TANKS
DATE 1/ 4/1984

BY J. R. LEWIS
RUN NUMBER 10 OF
CURRENT TIME $0.3600 E+03$
STATISTICAL ARRAVS CLEARED AT TIME 0.0000E+00
**STATISTICS FOR VARIABLES BASED ON OBSERVATION**

|  | MEAN <br> VALUE |
| :--- | :---: |
|  |  |
| TANK TIME SYS 1 | $0.8905 E+0$ |
| TOTAL TIME SYS 1 | $0.1058 E+0$ |
| TANK TIME SYS 2 | $0.9102 E+00$ |
| TOTAL TIME SYS 2 | $0.1089 E+0$ | TOTAL TIME SYS $20.9102 E+0$ $0.1089 E+01$

$\begin{array}{ll}\text { STANDARD } & \text { COEFF. OF } \\ \text { DEVIATION } & \text { VARIATION }\end{array}$
$0.1146 E+00$
$0.2048 E+00$
$0.1424 E+00$
$0.2048 E+00$
O. $1424 E+00$
$0.2209 E+00$

0. $1287 E+00$
0. $1935 E+00$
$0.1565 E+00$
$0.2027 E+00$

MINIMUM
value
$0.4781 E+00$
$0.5300 E+00$
$0.4736 E+00$
$0.4744 E+00$

MAXIMUM VALUE
O. 1874E+01
$0.2293 E+0$
$0.2043 E+O$
$0.2125 E+01$

NUMBER DF OBSERVATIONS
**STATISTICS FOR TIME-PERSISTENT VARIABLES**

MEAN
VALUE
NUMBER IN SYS. $10.3930 E+03$ NUMBER OF BRKDWN 0.1400E+01 NUMBER OF BRKDWN 0.3200E+01 TON OUTPUT
$0.5205 \mathrm{E}+03$

STANDARD
DEVIATION
0. 2280E +O3
0. $1541 \mathrm{E}+01$ 0.1447E+O1
O. $3026 \mathrm{E}+03$

## MINIMUR

$.0000 E+00$
$0.0000 E+00$
$0.0000 E+00$
$0.0000 E+00$

MAXIMUM
VALUE
$0.7860 E+03$
$0.5000 \mathrm{E}+01$
$0.5000 E+01$
$0.5000 E+01$
-. 1033E+04

TIME
INTERVAL
$0.3600 \mathrm{E}+03$
$0.3600 \mathrm{E}+03$
$0.3600 \mathrm{E}+\mathrm{O}^{0}$
$0.3600 E+03$

CURRENT value
$0.7860 \mathrm{E}+03$
$0.5000 \mathrm{E}+01$
O. $5000 \mathrm{E}+\mathrm{O}$
O. $1033 E+0$

| **FILE Statistics** |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FILE NUMBER | ASSOCIATED NODE TYPE | AVERAGE LENGTH | STANDARD DEVIATION | MAXIMUM LENGTH | CURRENT LENGTH | average WAITING time |
| 1 | awalt | 0.0048 | 80.0692 | 1 | 0 | 0.0003 |
| 2 | AWAIT | 0.0055 | 50.0742 | 1 | 0 | 0.0004 |
| 3 | AWAIT | 0.0157 | $7 \quad 0.1243$ | 1 | 0 | 0.0145 |
| 4 | AWAIT | 0.1271 | $1 \quad 0.3331$ | 1 |  | 0.0147 |
| 5 | AWAIT | 0.0000 | 0.0000 | 1 | 0 | 0.0000 |
| 6 | AWAIT | 0.0029 | - 0.0540 | 1 | 0 | 0.0028 |
| 7 | AWAIT | 0.0065 | - 0.0802 | 1 | 0 | 0.0066 |
| 8 | AWAIT | 0.1226 | - 0.3280 | 1 | 0 | 0.0229 |
| 9 | AWAIT | 0.0108 | - 0.1035 | 1 | 0 | 0.0098 |
| 10 | AWAIT | 0.0006 | - 0.0245 | 1 | 0 | 0.0099 |
| 11 | AWAIT | 0.0001 | $1 \quad 0.0121$ | 1 | 0 | 0.0029 |
| 12 | CALENDAR | 4.0801 | 10.6568 | 7 | 3 | 0.0536 |
| **GATE STATISTICS** |  |  |  |  |  |  |
| gate NUMBER | GATE LABEL | CURRENT STATUS | PCT. OF TIME OPEN |  |  |  |
|  |  |  |  |  |  |  |
| 1 | CR 1 | OPEN | 0.9947 |  |  |  |
| 2 | CR2 | OPEN | 0.9943 |  |  |  |
| 3 | MOV | CLOSED | 0.3780 |  |  |  |
| 4 | SC2 | Closed | 0.6274 |  |  |  |
| 5 | C2 | OPEN | 0.9015 |  |  |  |
| 6 | P2 | OPEN | 0.9161 |  |  |  |
| 7 | SO2 | OPEN | 0.8765 |  |  |  |
| 8 | SC 1 | OPEN | 0.5308 |  |  |  |
| 9 | ACID | OPEN | 0.7086 |  |  |  |
| 10 | PAS 1 | OPEN | 0.7126 |  |  |  |
| 11 | PAS2 | OPEN | 0.8692 |  |  |  |

APPENDIX G

OUTPUT OF TWO CRANE TWO OPERATOR MODEL


| RESOURCE NUMBER | RESOURCE LABEL | CURRENT CAPACITY | **RESOURCE STATISTICS** |  |  | CURRENT <br> UTILIZATION |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | AVERAGE UTILIZATION | STANDARD DEVIATION | MAXIMUM UTILIZATION |  |
| $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & \text { WC1 } \\ & \text { WC2 } \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 0.1736 \\ & 0.7113 \end{aligned}$ | $\begin{aligned} & 0.3787 \\ & 0.4532 \end{aligned}$ | 1 | O |
| RESOURCE NUMBER | RESOURCE LABEL | CURRENT AVAILABLE | AVERAGE AVAILABLE | MINIMUM AVAILABLE | MAXIMUM AVAILABLE |  |
| $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & \text { WC } 1 \\ & \text { WC2 } \end{aligned}$ | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0.8264 \\ & 0.2887 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ |  |
| **GATE STATISTICS** |  |  |  |  |  |  |
| GATE NUMBER | GATE <br> LABEL | CURRENT STATUS | PCT. OF <br> TIME OPEN |  |  |  |
| $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & \text { CR1 } 1 \\ & \text { CR2 } \end{aligned}$ | OPEN | $\begin{aligned} & 0.9775 \\ & 0.9829 \end{aligned}$ |  |  |  |



| RESOURCE NUMBER | **RESOURCE STATISTICS** |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | E RESOURCE | CURRENT <br> CAPACITY | AVERAGE UTILIZATION | STANDARD DEVIATION | MAXIMUM UTILIZATION | CURRENT UTILIZATION |
| $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & \text { WC1 } \\ & \text { WC2 } \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 0.1685 \\ & 0.7136 \end{aligned}$ | $\begin{aligned} & 0.3743 \\ & 0.4521 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 0 \\ & 1 \end{aligned}$ |
| RESOURCE NUMBER | RESOURCE LABEL | CURRENT <br> aVAILABLE | AVERAGE <br> available | MINIMUM AVAILABLE | MAXIMUM AVAILABLE |  |
| $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & W C 1 \\ & W C 2 \end{aligned}$ | 1 0 | 0.8315 0.2864 | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\mathbf{1}$ |  |
| **GATE StATIStics** |  |  |  |  | - | , |
| GATE NUMBER | GATE <br> LABEL | $\begin{array}{ll} \text { CURRENT } & \text { PC } \\ \text { STATUS } & \text { IT } \end{array}$ | PCT. OF <br> TIME OPEN |  |  |  |
| $1 \begin{array}{ll}1 \\ 2\end{array}$ | CR 1 CR2 | $\begin{aligned} & \text { OPEN } \\ & \text { OPEN } \end{aligned}$ | $\begin{aligned} & 0.9890 \\ & 0.9894 \end{aligned}$ |  |  |  |


**RESOURCE STATISTICS**

| RESOURCE NUMBER | RESOURCE LABEL | CURRENT <br> CAPACITY | AVERAGE <br> UTILIZATION | STANDARD DEVIATION | MAXIMUM <br> UTILIZATION | CURRENT <br> UTILIZATION |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & \text { WC } 1 \\ & \text { WC2 } \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 0.1553 \\ & 0.6893 \end{aligned}$ | $\begin{aligned} & 0.3622 \\ & 0.4628 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 0 \\ & 1 \end{aligned}$ |
| RESOURCE NUMBER | RESOURCE LABEL | CURRENT AVAILABLE | AVERAGE AVAILABLE | MINIMUM <br> AVAILABLE | MAXIMUM AVAILABLE |  |
| $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & \text { WC } 1 \\ & \text { WC2 } \end{aligned}$ | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0.8447 \\ & 0.3107 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ |  |


| GATE | GATE | CURRENT <br> NUMBER | LABEL |
| :--- | :--- | :--- | :--- |
|  |  | PTATUS | PCT OF <br> TIME OPEN |
| 1 | CR1 |  |  |
| 2 | CR2 | OPEN | 0.9595 |
|  |  | OPEN | 0.9958 |



| RESOURCE NUMBER | RESOURCE LABEL | CURRENT <br> CAPACITY | **RESOURCE STATISTICS** |  | MAXIMUM UTILIZATION | CURRENT <br> UTILIZATION |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | average <br> UTILIZATION | STANDARD DEVIATION |  |  |
| 2 | WC 1 | 1 |  |  |  |  |
|  | WC2 | 1 | 0.1605 0.7152 | $0.3671$ | 1 | 1 |
| RESOURCE NUMBER | RESOURCE LABEL | CURRENT aVAILABLE | AVERAGE AVAILABLE | MINIMUM AVAILABLE | MAXIMUM AVAILABLE |  |
| 12 | $\begin{aligned} & \text { WC } 1 \\ & \text { WC2 } \end{aligned}$ |  |  |  |  |  |
|  |  | 0 | 0.8395 |  |  |  |
|  |  |  |  | $0$ | 1 |  |
| **GATE STATIStics** |  |  |  |  |  |  |
| GATE NUMBER | GATE LABEL | CURRENT status | PCT. OF <br> TIME OPEN |  |  |  |
| 1 C | $\begin{aligned} & \text { CR1 } \\ & \text { CR2 } \end{aligned}$ | $\begin{aligned} & \text { OPEN } \\ & \text { OPEN } \end{aligned}$ | $\begin{aligned} & 0.9965 \\ & 0.9963 \end{aligned}$ |  |  |  |



| RESOURCE NUMBER | RESOURCE LABEL | CURRENT <br> CAPACITY | **RESOURCE STATISTICS** |  | MAXIMUM UTILIZATION | CURRENT <br> UTILIZATION |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | AVERAGE UTILIZATION | STANDARD DEVIATION |  |  |
| $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | WC 1 | 1 | 0. 1626 |  |  | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ |
|  | WC2 |  | 0.7056 | 0.3690 0.4558 | 1 |  |
| RESOURCE NUMBER | RESOURCE <br> LABEL | CURRENT AVAILABLE | AVERAGE AVAILABLE | MINIMUM AVAILABLE | MAXIMUM AVAILABLE |  |
| 1 | $\begin{aligned} & \text { WC1 } \\ & \text { WC2 } \end{aligned}$ | 0 | $\begin{aligned} & 0.8374 \\ & 0.2944 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ |  |
|  |  |  |  |  |  |  |
| **GATE STATIStics** |  |  |  |  |  |  |
| GATE | GATE | CURRENT | PCT. OF |  |  |  |
| NUMBER | LABEL | StATUS | TIME OPEN |  |  |  |
| 1 C | CR 1 | OPEN |  |  |  |  |
| 2 | CR2 | OPEN | 0.9934 |  |  |  |


|  |  |  | SIMULATION PROJECT TANKS |  |  | BY J. R. LEWIS |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | DATE 1/ 4/1984 |  |  | RUN NUMBER | 6 OF 10 |
|  |  |  | CURRENT TIME O.3600E+O3 <br> STATISTICAL ARRAYS CLEARED AT TIME O.0000e+ +0 |  |  |  |  |
|  |  |  | **STATISTICS FOR VARIABLES BASED ON OBSERVATION** |  |  |  |  |
|  |  | MEAN VALUE | STANDARD DEVIATION | COEFF. OF VARIATION | MINIMUM VALUE | MAXIMUM VALUE | NUMBER OF OBSERVATIONS |
| TANK TIME tOTAL TIME |  | $0.8955 \mathrm{E}+00$ | $0.2201 \mathrm{E}+00$ | $0.2458 \mathrm{E}+00$ | $0.6513 \mathrm{E}+00$ | $0.4002 \mathrm{E}+01$ | 671 |
|  |  | 0.1044E+01 | $0.2793 \mathrm{E}+00$ | $0.2676 E+00$ | $0.6369 \mathrm{E}+00$ | $0.4066 E+01$ | 670 |
| **STATISTICS FOR TIME-PERSISTENT VARIABLES** |  |  |  |  |  |  |  |
|  |  | MEAN VALUE | STANDARD DEVIATION | MINIMUM VALUE | MAXIMUM VALUE | time INTERVAL | CURRENT Value |
| NUMBER IN SYS. 1 NUMBER OF BRKDWN NUMBER OF BRKDOW TON OUTPUT |  | 0.3346E+03 | $\begin{aligned} & 0.1925 \mathrm{E}+03 \\ & 0.3006 \mathrm{E}+01 \\ & 0.8439 \mathrm{E}+00 \\ & 0.2475 \mathrm{E}+03 \end{aligned}$ | 0.0000E+00 <br> $0.0000 \mathrm{E}+00$ <br> $0.0000 \mathrm{E}+00$ <br> $0.0000 \mathrm{E}+00$ | $0.6700 \mathrm{E}+03$ | 0.3600e +03 | 0.6700e+03 |
|  |  | $0.4669 E+01$ |  |  | $0.9000 \mathrm{E}+01$ | $0.3600 \mathrm{E}+03$ | $0.9000 \mathrm{E}+01$ |
|  |  | $0.5667 \mathrm{E}+00$ |  |  | $0.2000 \mathrm{E}+01$ | $0.3600 \mathrm{E}+03$ | 0. 2000e+01 |
|  |  | $0.4391 \mathrm{E}+03$ |  |  | $0.8835 \mathrm{E}+03$ | 0.3600E+03 | $0.8835 \mathrm{E}+03$ |
|  |  | - | **FILE STATISTICS** |  |  |  |  |
| File NUMBER | associated NODE TYPE | average LENGTH | STANDARD DEVIATION | MAXIMUM LENGTH | CURRENT LENGTH | AVERAGE WAITING TIME |  |
| 1 | AWAIT | 0.0215 | 0.1450 | 1 | 0 | 0.0029 |  |
| 2 | AWAIT | 0.0062 | 0.0787 | 1 | 0 | 0.0033 |  |
| 3 | AWAIT | 0.0109 | 0. 1038 | 1 | 0 | 0.0058 |  |
| 4 | AWAIT | 0.0097 | 0.0983 | 1 | 0 | 0.0008 |  |
| 5 | CALENDAR | 4.6390 | 0.7524 | 7 | 6 | 0. 1023 |  |

**RESOURCE STATISTICS**

| RESOURCE NUMBER | RESOURCE LABEL | CURRENT <br> CAPACITY | AVERAGE <br> UTILIZATION | STANDARD DEVIATION | MAXIMUM <br> UTILIZATION | CURRENT <br> UTILIZATION |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | WC 1 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 0.1654 \\ & 0.7048 \end{aligned}$ | $\begin{aligned} & 0.3716 \\ & 0.4562 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $0$ |
| RESOURCE NUMBER | $\begin{aligned} & \text { RESOURCE } \\ & \text { LABEL } \end{aligned}$ | CURRENT <br> AVAILABLE | AVERAGE AVAILABLE | MINIMUM AVAILABLE | MAXIMUM AVAILABLE |  |
| $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & \text { WC } 1 \\ & \text { WC2 } \end{aligned}$ | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0.8346 \\ & 0.2952 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ |  |
| **GATE STATISTICS** |  |  |  |  |  |  |
| GATE NUMBER | GATE <br> LABEL | CURRENT STATUS | PCT. OF <br> TIME OPEN |  |  |  |
| $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & \text { CR } 1 \\ & \text { CR2 } \end{aligned}$ | OPEN OPEN | $\begin{aligned} & 0.9761 \\ & 0.9899 \end{aligned}$ |  |  |  |



| **RESOURCE STATISTICS** |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RESOURCE NUMBER | RESOURCE <br> LABEL | CURRENT <br> CAPACITY | AVERAGE UTILIZATION | STANDARD DEVIATION | MAXIMUM UTILIZATION | CURRENT <br> UTILIZATION |
| 1 | WC1 | 1 | 0. 1643 | 0.3706 | 1 | 0 |
| 2 | WC2 | 1 | 0.7163 | 0.4508 | 1 | 0 |
| RESOURCE NUMBER | RESOURCE label | CURRENT AVAILABLE | AVERAGE <br> AVAILABLE | MINIMUM <br> AVAILABLE | MAXIMUM AVAILABLE |  |
| 2 | WC 1 | 1 | 0.8357 | 0 |  |  |
| 2 | WC2 | 1 | 0.2837 | 0 | 1 |  |
| **GATE STATISTICS** |  |  |  |  |  |  |
| GATE | GATE | CURRENT | PCT. OF |  |  |  |
| NUMBER | label | status | time open |  |  |  |
| 1 | CR1 CR2 | OPEN | 0.9995 |  |  |  |



| **RESOURCE STATISTICS** |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RESOURCE NUMBER | RESOURCE LABEL | CURRENT <br> CAPACITY | average UTILIZATION | STANDARD DEVIATION | MAXIMUM UTILIZATION | CURRENT UTILIZATION |
| 1 | WC 1 WC2 | $1$ | 0.1728 0.7152 | 0.3781 0.4513 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 0 \\ & 1 \end{aligned}$ |
| RESOURCE NUMBER | RESOURCE LABEL | CURRENT <br> AVAILABLE | average <br> available | MINIMUM AVAILABLE | MAXIMUM AVAILABLE |  |
| $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & \text { WC } 1 \\ & \text { WC2 } \end{aligned}$ | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | 0.8272 0.2848 | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ |  |
| **GATE STATISTICS** |  |  |  |  |  |  |
| GATE NUMBER | GATE LABEL | CURRENT Status | PCT. OF <br> TIME OPEN |  |  |  |
| $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | CR1 CR2 | OPEN OPEN | $\begin{aligned} & 0.9796 \\ & 0.9827 \end{aligned}$ |  |  |  |



| **RESOURCE STATISTICS** |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RESOURCE NUMBER | RESOURCE label | CURRENT <br> CAPACITY | AVERAGE UTILIZATION | STANDARD DEVIATION | MAXIMUM UTILIZATION | CURRENT <br> UTILIZATION |
| 1 | WC 1 | 1 | 0. 1653 | 0.3714 | 1 | 0 |
| 2 | WC2 | 1 | 0.7172 | 0.4504 | 1 | 0 |
| RESOURCE NUMBER | RESOURCE LABEL | CURRENT available | AVERAGE <br> AVAILABLE | MINIMUM <br> AVAILABLE | MAXIMUM AVAILABLE |  |
| 1 | WC 1 | 1 | 0.8347 | 0 | 1 |  |
| 2 | WC2 | 1 | 0.2828 | 0 | 1 |  |
| **GATE STATISTICS** |  |  |  |  |  |  |
| GATE | GATE | CURRENT | PCT. OF |  |  |  |
| NUMBER | LABEL | Status | time open |  |  |  |
| 1 | CR 1 | OPEN | 0.9952 |  |  |  |
| 2 | CR2 | OPEN | 0.9926 |  |  |  |


|  |  |  | SIMULATION PROJECT TANKS |  |  | BY J. R. LEWIS |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | - | DATE 1/ 4/1984 |  |  | RUN NUMBER | 10 OF 10 |
|  |  |  | CURRENT TIME O.3600E+03 STATISTICAL ARRAYS CLEARED |  | AT TIME O.OOOOE + O |  |  |
|  |  |  | **STATISTICS FOR VARIABLES BASED ON OBSERVATION** |  |  |  |  |
|  |  | MEAN VALUE | Standard DEVIATION | COEFF. OF VARIATION | minimum Value | MAXIMUM VALUE | NUMBER OF OBSERVATIONS |
| TANK TI TOTAL | ME | $0.8785 \mathrm{E}+00$ | O. 1250e + 00 | O. 1423E +00 | $0.6739 \mathrm{E}+00$ | $0.3411 \mathrm{E}+01$ | 685 |
|  |  | O. 1025E+01 | O. 1945E+00 | 0. 1898E+00 | $0.6992 \mathrm{E}+00$ | $0.3492 \mathrm{E}+01$ | 685 |
|  |  |  | **StATISTICS FOR TIME-PERSISTENT VARIABLES** |  |  |  |  |
|  |  | MEAN value | STANDARD DEVIATION | MINIMUM value | MAXIMUM VALUE | TIME <br> INTERVAI | CURRENT |
| NUMBER IN SYS. 1 NUMIBER OF BRKDWN NUMBER OF BRKDOW ton output |  | O. 3390e +O3 | o. 1983E+O3 <br> $0.8622 \mathrm{E}+\mathrm{O}$ <br> o. $1274 E+01$ <br> $0.2720 \mathrm{E}+\mathrm{O}$ | O. OOOOE + OO <br> $0.0100 \mathrm{E}+00$ <br> O. OCOOE +OO <br> 0.0000E+00 | 0.6850E+O3 <br> $0.2000 \mathrm{E}+01$ <br> $0.5000 \mathrm{E}+01$ <br> $0.9511 \mathrm{E}+03$ | O. $3600 \mathrm{E}+03$ | O.6850E+O3 |
|  |  | O. 1300E + 01 |  |  |  | $0.3600 E+03$ | $0.2000 \mathrm{E}+01$ |
|  |  | $0.2333 E+01$ |  |  |  | 0.3600E+03 | $0.5000 \mathrm{E}+01$ |
|  |  | $0.4842 \mathrm{E}+03$ |  |  |  | 0.3600E+03 | $0.9511 \mathrm{E}+03$ |
| **FILE STATISTICS** |  |  |  |  |  |  |  |
| FILE NUMBER | ASSOCIATED | AVERAGE | STANDARD | MAXIMUM | CURRENT | AVERAGE WAITING TIME |  |
|  |  |  |  |  |  |  |  |
| 1 | AWAIT | 0.0075 | 0.0865 | 1 | 0 | 0.0010 |  |
| 2 | AWAIT | 0.0007 | 0.0264 | 1 | 0 | 0.0004 |  |
|  | AWAIT | 0.0062 | 0.0787 | 1 | 0 | 0.0033 |  |
| 4 | AWAIT | 0.0047 | 0.0683 | 1 | 0 | 0.0004 |  |
| 5 | CALENDAR | 4.0085 | 0.5704 | 6 | 4 | 0.0869 |  |


| **RESOURCE STATISTICS** |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RESOURCE NUMBER | RESOURCE LABEL | CURRENT CAPACITY | AVERAGE UTILIZATION | STANDARD DEVIATION | MAXIMUM UTILIZATION | CURRENT UTILIZATION |
| 1 | WC 1 | 1 | 0.1644 | 0.3707 |  |  |
| 2 | WC2 | 1 | 0.7144 | 0.4517 | 1 | 1 |
| RESOURCE NUMBER | RESOURCE LABEL | CURRENT <br> AVAILABLE | average AVAILABLE | MINIMUM AVAILABLE | MAXIMUM AVAILABLE |  |
| 1 | WC1 | 1 | 0.8356 | 0 | 1 |  |
| 2 | WC2 | 0 | 0.2856 | 0 | 1 |  |
| **GATE STATISTICS** |  |  |  |  |  |  |
| GATE | GATE | CURRENT | PCT. OF |  |  |  |
| NUMBER | Label | Status | time open |  |  |  |
|  | CR 1 | OPEN | 0.9921 |  |  |  |
| 2 | CR2 | OPEN | 0.9942 |  |  |  |

APPENDIX H

CAN-Q OUTPUT

## ROUIING FOK PRGDUCT TYPE: LUHE

| OPERATION Nunterl | GTATION NUMIER | PROCEgSINS TIME: | oferation FREQUENC: |
| :---: | :---: | :---: | :---: |
| 1 | 1 | 6.710 | 1.000 |
| 2 | 2 | 6.680 | 1.000 |
| 3 | 3 | . 710 | 1.000 |
| 4 | 4 | 13.600 | 1.000 |
| 8 | 3 | . 710 | 1.000 |
| 6 | 5 | . 720 | 1.000 |
| 7 | 6 | 6.740 | 1.000 |
| 8 | 7 | 6. 710 | 1.000 |
| 9 | 8 | . 9550 | 1.000 |
| 10 | 9 | 6.670 | 1.000 |
| 11 | 10 | 2.300 | 1.000 |

WORKLOAD SUMMARY FOR THIS PRODUCT TYPE

|  | TION | NUMEER OF UISIIS | UISIT <br> FREQUENCY | $\begin{gathered} \text { TIOTAL } \\ \text { PROCESS TIME } \end{gathered}$ | AUERAGE process time | RELATIUE WGRKLGAD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | HOLD | 1.000 | . 091 | 6.710 | 6.710 | . 610 |
| 2 | Calus | 1.000 | . 071 | 6.680 | 6.680 | . 6107 |
| 3 | CW I | 2.000 | . 102 | 1.420 | . 710 | . 129 |
| 4 | ACID | 1.000 | . $0 \% 1$ | 13.600 | 13.6 .00 | 1.256 |
| 5 | HW | 1.000 | . 091 | . 720 | . 720 | .268 .065 |
| 6 | PHOS | 1.000 | . $0 \% 1$ | 6.740 | 6.740 | .613 |
| 7 | CW II | 1.000 | . 091 | . 710 | . 710 | . 065 |
| 8 | NEUT | 1.000 | . $0 \geqslant 1$ | . 950 | . 750 | . 06.06 |
| 9 | soap | 1.000 | . 091 | 6.670 | 6.670 | . 605 |
| 10 | Lfir | 1.000 | . 15.1 | 2.300 | 2.300 | . 209 |

AUERAGE NUAEER OF OPERATIONS TO COMPLETE ONE 11.000 DESIRED FRACTION OF PRODUCTION : $: .890$

VALUE OF UNE ITEM $=\quad 1.00$

ROLIING FGR PRGDUGT TYPEI PHO

| OPERATION number | STATION NIMMER | PROCESSING TIME | OPERATION FREQUENCY |
| :---: | :---: | :---: | :---: |
| 1 | 1 | 6.710 | 1.000 |
| 2 | 2 | 6.680 | 1.000 |
| 3 | 3 | . 710 | 1.000 |
| 4 | 4 | 13.600 | 1.000 |
| 5 | 3 | . 710 | 1.000 |
| 6 | 5 | . 720 | 1.000 |
| 7 | 6 | 6.740 | 1.000 |
| 6 | 7 | . 710 | 1.000 |
| 9 | 10 | 2.300 | 1.000 |

WORKLOAD SUMMARY FOR THIS PRODUCT TYPE

|  | TION | NUMEER OF | UISIT <br> FREquency | tOTAL <br> Process time | aUERAGE <br> FROCEGS TIUE | RELATIVE WORKLOGID |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | HOLD | 1.000 | . 111 | 6.710 | 6.710 | . 746 |
| 2 | Catus | 1.000 | . 111 | 6.680 | 6.6880 | . 742 |
| 3 | CW 1 | 2.000 | . 222 | 1.420 | . 710 | . 156 |
| 4 | ACID | 1.010 | .111 | 13.600 | 13.600 | 1.511 |
| 5 | HW | 1.000 | . 111 | . 720 | .720 | . 030 |
| 6 | PHOS | 1.000 | . 111 | 6.740 | 6.740 | . 749 |
| 7 | CW II | 1.000 | . 111 | . 710 | . 710 | . 079 |
| 10 | DRY | 1.000 | .111 | 2.300 | 2.300 | . 256 |

DUERGGE NUTIEER OF OPERATIONG TO COMPLETE ONE 9.000 DESIRED FRACIION OF PRODIICTION:= .040

Value of one Item = 1.00


## INPUT DATA summary

|  | TATION | NUMEER OF SERUERS | UISIT <br> FREQUENCY | average <br> PROCESSING TIME | relative: WORKI.DAD | WORKLOAD PER SERUER |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | HOLD | 1 | . 09398 | 6.71000 | . 6.3064 | . 6,306 |
| 2 | calis | 1 | . 09398 | 6.68000 | . 62783 | . 6278 |
| 3 | CW I | 1 | . 18797 | . 71000 | . 13346 | .1335 |
| 4 | ACID | 1 | .093\% | 13.60000 | 1.27820 | 1.2782 |
| 5 | HW | 1 | . 09398 | . 72000 | . 06.767 | . 0677 |
| 6 | PHOS | 1 | . 09741 | 6.74000 | . 58912 | . 5891 |
| 7 | CW II | 1 | . 08741 | .71000 | . 06206 | . 0621 |
| 8 | neut | 1 | . 08365 | . 95000 | . 07946 | . 0795 |
| 9 | SOAP | 1 | . 09365 | 6.67000 | . 55792 | . 5579 |
| 10 | DRY | 1 | . $0 \% 3 \% 8$ | 2.30000 | . 21617 | . 2162 |
| 11 | CRANE | 1 | . 09398 | . 18000 | . 10000 | .1900 |

NUTHER OF ITEIS IN SYSTEM $=2$

MEAN NUMBER OF OPERATIONS TO COIPLETE AN ITEM 10.64000

## system performance measures



SUMIITAR FOR GIATIUN INUMER 1 : HOLD

summart for giation mumler 2 : caus


```
slimmari fok gtatION NUMEER 3 1 CW I
\begin{tabular}{ccc}
\begin{tabular}{c} 
HMMEER OF \\
SERUERS
\end{tabular} & \begin{tabular}{c} 
SERUER \\
UTILIZATION
\end{tabular} & \begin{tabular}{c} 
AUE, NO, OF \\
EUSY SERVERS
\end{tabular} \\
1 & .052 & .052
\end{tabular}
steady state average numger of :
ITEMS WAITING . 107
ITEMS IN PROCESS .052
TEMS WAITING
055
average rime spent at this station
OTAL TIME (MINUTES) Processing
PER OPERATION PER ITEA haIting
```

1.46 .3
.710
.753
2.926
1.420
1.920
1.506

# fraction of time $x$ ITEMS at station $x$ items exceened 

```
\begin{tabular}{lll}
\(x=0\) & .9481 & .0519 \\
\(x=1\) & .0519 & .0000 \\
\(x=2\) & .0016 & \#\#\#
\end{tabular}
```



```
SUMGARTY FOR STATION NUMHER 5 : HIW
```

| NUHEEER OF SERUERS | GERUER UTILIZATION | AVE. ND, OF HUSY SERUERS |
| :---: | :---: | :---: |
| 1 | . 026 | . 026 |

steady stite auerage number of :

| ITENS WAITING | .053 |
| :--- | :--- |
| ITEMS IN PROCESS | .026 |
| I TENS WAITING | .027 |

guerage time spent at this gtation

TOTAL TIME (MINUTES) PROCESSING WAITING
1.462
.720
.742

1. 462
.720
.742

## FRACTION OF TIME $X$ ITEAS AT STATION

$\times$ ITEMS EXCEFDED

## $x=0$ $x=1$ <br> $x=1$ $x=2$

.9737
.026 .3
.02633
.0000
.0000

## SUMIIARY FOR STATION NUMEER $6:$ PHOS



## EUMMARY FUR SIATION NUMEER 7 : CW II



# GURMGRY FOR SIATION AIMILE:R 91 gUAP 

| HIMBER OF <br> GERUERS | GERUER <br> UTILIZATION | AUE, NO, OF <br> GUSY SERUERS |
| :---: | :---: | :---: |
| 1 | .217 | .217 |

StEADY STATE AUERAGE NUMBER OF ,


## SUMMARY FOR STATION NUHIGER 8 : NEUT

| HIMEER OF <br> SERVERS | SERUER <br> UTILIZATION | AUE, NO. OF <br> BUSY SERUERS |
| :---: | :---: | :---: |
| 1 | .031 |  |
|  |  | .031 |

STEADY STATE AUERGGE NUMEER CF :


9691
.0309
0006
.0309
.0000


| HUMEER OF <br> SERUERS | GERUER <br> UTILJZATION | BUE. NO, OF |
| :---: | :---: | :---: |
|  |  |  |
| 1 | .0134 | .084 |

steady gtate fuerabe number of :
$\begin{array}{ll}\text { ITEMS WAITING } & .176 \\ \text { ITERS IN PRGCEGS } & .084 \\ \text { ITEMS WAITING } & .092\end{array}$
average ibme sperit at this siation

TOTAL TIME (MINUTEG)
PROCEESING
WGITING

PER OPERATION

### 4.925

2.300
2.525

PER ITEM
4.825
2.300
2.525
.9160
.0840
.0840
.0041

SUAITARE FOK GIATION NUMBER 11 , CRANE

| NUMEER OF <br> SERUERS | SERUER <br> UTILIZATION | AUE, NOS OF <br> GUERUERS |
| :---: | :---: | :---: |
| 1 | .070 | .070 |

steady state: avergGe numeer dof

ITEMS WAITING
ITEMS IN PROCESS $\quad .146$
I TEMS WAITING $\quad .076$
GULRAGE TIME SPENT AT THIS SIATION

COTAL TIME (MINUTES) PROCESSIHG
WAITING:
.375
.180
180
.195
.195
3.986
1.915
2.071

FRGICTION UF TIAE

9300
$0 \% 00$
$0 \% 00$ 0028
$x$ ITEAS ExCeEDED
. 0700


SEHSITIUITY INFORMATION


| WILL INCREASE THE PRODUCTION RATE |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| $3{ }^{\text {có }}$ | UNITS/HOUR | ( 6.2235 | PERCENT |  |
| . 136 | UHITS/HOUR | ( 0.2189 | PERCENT |  |
| .237 | UNITS/HOUR | <10.8042 | PERCLNT |  |
| . 160 | UNITC,'HOUR | 7.2934 | PERCENT |  |
| . 116 | UNITS/HOUR | 5.2934 | PERCENT |  |
| . 125 | UNITS/HOUR | 5.7241 | PERCEENT |  |
| . 108 | UNITS/HOUR | 4.9142 | PERCENT |  |
| . 104 | UNJTS/HOUR | 4.7285 | PERCENT |  |
| .119 | UNITS/HOUR | 5.4320 | PERCENT |  |
| . 121 | UNITS/HOUR | 5.5387 | PERCENT |  |
| . 373 | UNITS/HDUR | -58. | PERCENT |  |


| A UNE PERCENT DECREASE IN |
| :---: |
| PRUCESSING TIME AT STATION |
| 1 HOLD |
| 2 |
| 3 |

A ONE MINUTE DECREASE IN relative utilization at station
HOLD
CAUS
CWI
ACID
HW
PHOS
CWII
HEUT
GOAP
DRY
CRANE
A DECREASE OF . 01 IN THE
PROPORTION OF PRODUCT TYPE
LUEE
PHO
TRI
will Increase the
FRODUCTION RATE EY
. 065 ITEMS 'HOUR ( 2.9771 PERCENT )
.055 ITEMS/HOUR ( 2.5195 PERCENT)
.045 ITEMS/HOUR ( 2.0671 PERCENT)

WILL INCREASE THE
JALUE OF PRODUCTION PLAN BY
 043 ITEMS/HOUR ( 1.9771 PERCENT )
033 ITEMS/HOUR ( 1.5195 PERCENT )

TRI
. 023 ITEMS/HOUR ( 1.0671 PERCENT )

VITA 2<br>John Russell Lewis Candidate for the Degree of<br>Master of Science

Thesis: THE USE OF SIMULATION AND CAN-Q TO ANALYZE THE CLEANING AND LUBRICATING PROCESSES OF COLD DRAWN TUBING

Major Field: Industrial Engineering
Biographical:
Personal Data: Born in Sioux City, Iowa, August 11, 1959, the son of Thomas M. and Carolyn C. Lewis.

Education: Graduated from West DePere High School, DePere, Wisconsin, in May, 1977; received Bachelor of Science Degree in Industrial Engineering from Oklahoma State University in December, 1983 ; completed requirements for the Master of Science Degree at Oklahoma State University in May 1985.

Professional Experience: Teaching assistant, Department of Industrial Engineering, Oklahoma State University, January 1984 to May, 1984; consulting industrial engineer, Southwest Tube Manufacturing, Sand Springs, Oklahoma, June, 1981 to May, 1984.


[^0]:    DEGREES OF FREEDOM= 10
    111:
    011888988 SIGMA 2=
    .00001196

[^1]:    DEGREES OF FREEDOM=
    . 0110 B8B8日 SIGMA $2=$
    000011965

