

APPLICATION OF NUMERICAL MODEL FOR
GROUND-WATER MANAGEMENT OF
PIEDMONT AQUIFER IN
CENTRAL DINAJPUR,
BANGLADESH

By

SYED ABUL HOSSAIN

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Bachelor of Science
University of Dacca
Dacca, Bangladesh
1959

Master of Science
University of Dacca
Dacca, Bangladesh
1961

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Thesis Approved:



Thesis Adviser







Dean of the Graduate College

PREFACE

In the present study, an attempt has been made to evaluate the geologic and hydrogeologic properties of the Piedmont aquifer in the Dinajpur district and to use those evaluated values in a ground-water management model. The primary objective is to determine the maximum annual yield and corresponding annual pumping allocation for the basin based on allowable limiting drawdown up to 22 feet from the surface. The computer model is used to determine the maximum annual yield based on predicted changes in the potentiometric surface (water table) caused by irrigation pumpage prior to 1977 and subsequent allocated irrigation pumpage until 1997.

The author is indebted to Dr. Douglas C. Kent, his thesis adviser, for his valuable advice and guidance during this study. It was only due to his sincere and untiring efforts that the author was able to undertake a research project in his own country and was able to present the paper in the present form and standard. Sincere appreciation is extended to him for always being patient beyond limits, constantly fair beyond measure, and extremely helpful in directing organization of data and this research.

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CHAPTER I

ABSTRACT

The Piedmont alluvial deposit in the central part of Dinajpur district extends over an area of approximately 588 square miles. The aquifer, which consists of unconsolidated sand, gravel and clay, is the principal source of ground-water supply of 266 wells for irrigation and about 10,500 dug and handpump wells for domestic purposes. The water table contour map and lithology indicate that the aquifer is homogeneous, isotropic, and unconfined. The estimated values used for hydraulic conductivity and specific yield in all areas were 1.02×10^{-3} ft/sec and 0.25, respectively. The net surface recharge was determined to be 24 inches per year.

Concern has been expressed that extensive irrigation pumpage might lower the water table below 22 feet and stop or severely limit the use of 10,500 dug and hand pump wells for domestic purposes. In order to solve this problem, geological and hydrogeological investigations were conducted. A digital model (Trescott - Pinder model) was then used to provide a quantitative description of the aquifer and to predict maximum annual allocation for the aquifer based on allowable drawdown at a specified future time.

The computer simulation, with the help of Trescott-Pinder model, was first run for one year period in order to calibrate the model. It is assumed that the aquifer is in recharge - discharge equilibrium. After calibration was completed, a 20-year simulation was run to determine a mass balance relationship and maximum annual allocation for the aquifer based on irrigation requirements and allowable drawdown. An annual allocation of 2.23 acre-feet/acre was established for an allowable drawdown of 22 feet in the Piedmont aquifer.

CHAPTER II

INTRODUCTION

General

Bangladesh is located between $20^{\circ}45'$ and $26^{\circ}41'$ North latitude and $88^{\circ}03'$ and $92^{\circ}40'$ East longitude, with an area of 55,000 square miles. It is a major part of the Ganges-Bhramaputra Meghna delta which is roughly twice the size of the Mississippi delta (Figure 1). With the population averaging 1300 persons per square mile and the projection for the next 25 years exceeding 3000 per square mile, the internal food demand is likely to double. But the agricultural production is not sufficient to feed the rapidly increasing population. Thus the only way in which Bangladesh can meet her future food requirements is by expanding agriculture into the dry season by using irrigation. An extensive program is now underway to provide irrigation water from wells.

Location

The study area lies approximately between latitudes $26^{\circ}23'$ and $25^{\circ}57'N$ and longitudes $88^{\circ}18'$ and $88^{\circ}48'E$ (Figure 2). The area comprises 588 square miles and is

LOCATION MAP OF BANGLADESH

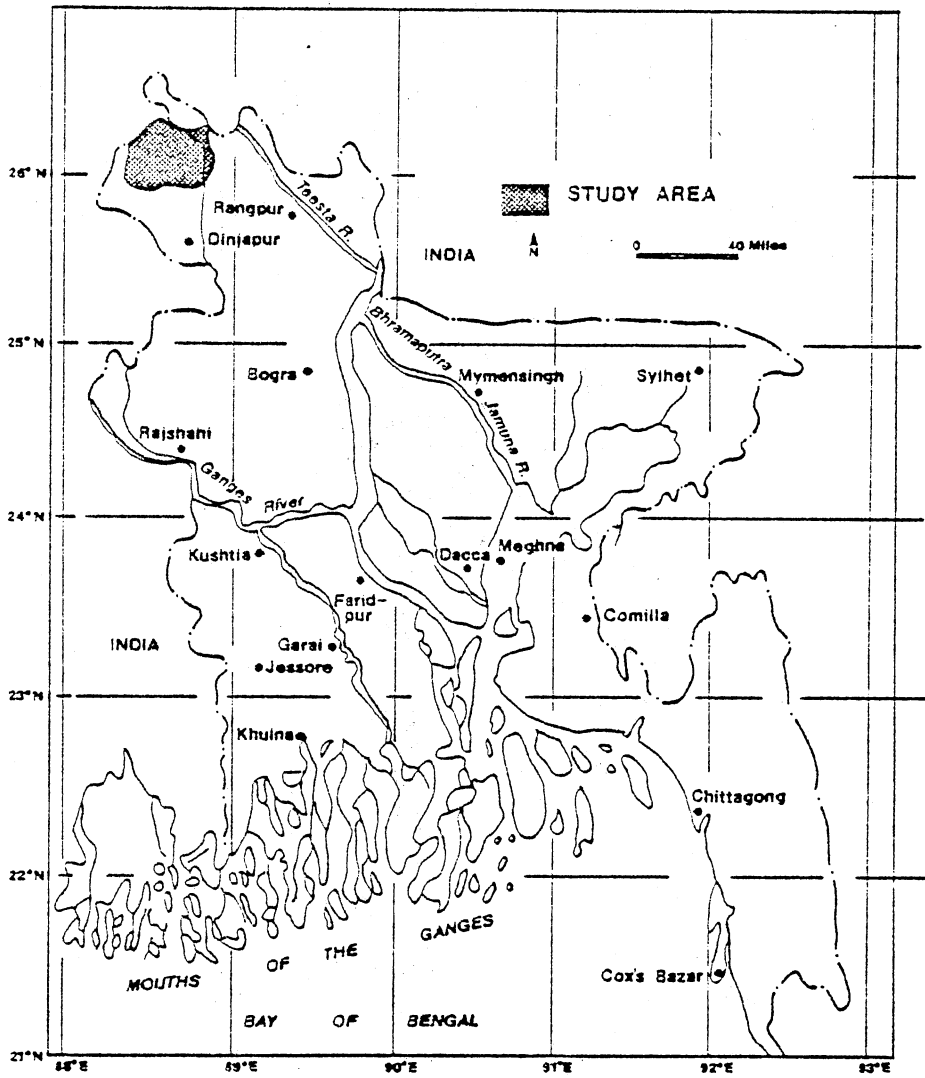


Figure 1. Location Map of Bangladesh

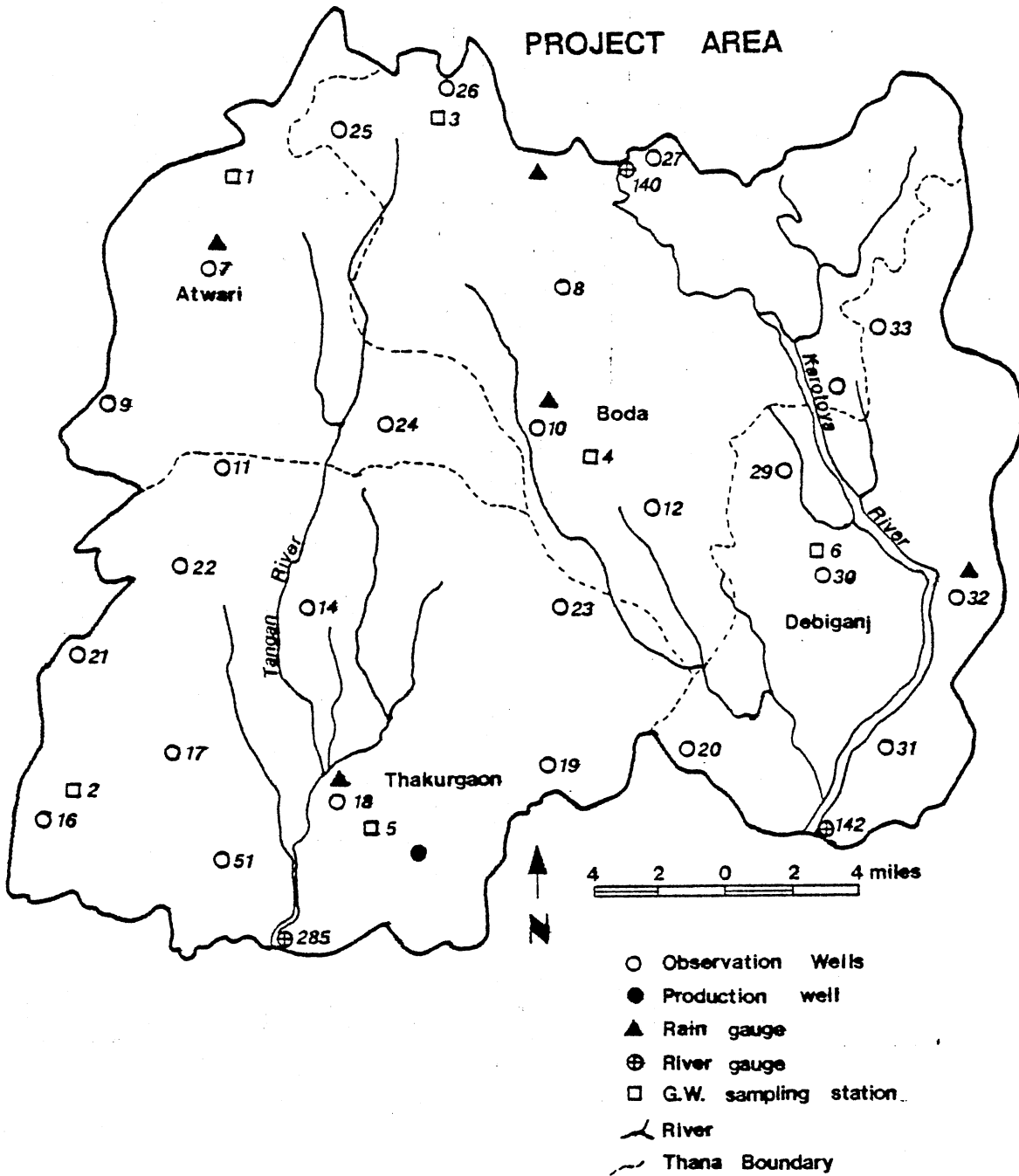


Figure 2. Location of Study Area

located in a central part of Dinajpur district of Bangladesh. The principal topographic features of the area are flat high plains lying in the Piedmont plain. Altitudes range from 253 feet near the northeast edge to approximately 160 feet near the southernmost end of the area. It slopes almost uniformly from the north in a general south and southeast direction. The land gradient ranges from three feet per mile in the north to two feet per mile or less in the south and southeast parts of the area.

The area is drained by two major rivers Karotoya and Tangan. Karotoya has its source in India and enters Dinajpur district at Bardesware. Tangan river originates in or near the border of the country and flows southward past Thakurgaon.

According to the Soil Survey of Bangladesh (1973), the project area is characterized by a good sandy soil which responds well to irrigation and fertilizers. The very favorable geology, abundant recharge possibilities, the high water-table, and present performance of the well field indicate that the ground-water basin will be enough to supply required irrigation water.

Problem Assessment

Concern has been expressed by the Agricultural Authority that the existing dug wells and hand pump wells used for domestic purposes may be dewatered as a result

of excessive drawdown due to irrigation pumping in the area. It appears that about 10,500 domestic water supply dug and hand pump wells which are now being used by 0.4 million people in this area will be severely affected. It is therefore proposed that the problem could be averted if the irrigation includes a plan allowing withdrawal of water for irrigation at a maximum annual yield for 20 years from the basin. This would maintain the allowable declination of water table down to 22 feet depth from surface throughout the irrigation period. Tentatively, the average yield of each irrigation well has been established by the Agricultural Authority to be two cfs spread over 70 acres of land at the rate of twelve hours per day for 150 days (November to March).

Objectives

The objectives of this study are to utilize the available hydrogeologic data of the area and to determine the maximum annual yield and pumping rate allocation in order to protect shallow domestic wells by limiting drawdown throughout the irrigated area. The study includes:

1. Determination of the occurrence and availability of ground-water in the area;
2. Calculation of a preliminary hydrologic budget for the area with emphasis on the ground-water component

of the budget;

3. Adaptation, calibration, and application of a mathematical model that will adequately simulate the operation of the hydrogeologic systems;

4. Determination of safe drawdown limit to protect shallow wells;

5. Computer simulation runs to establish maximum annual yield and pumping rate allocation in order to limit regional drawdown caused by irrigation to a safe limit.

Previous Works

Some previous studies have been made in this area. These have covered all aspects of the development potential in agriculture, irrigation, and mineral abstractions. The United Nation Food and Agriculture Organization (1966) studied the area on the assumption that good aquifers are present as revealed by exploring borings and electric resistivity surveys and recommended a detailed field investigation prior to undertaking any project for a large scale ground-water development. Karim (1968) and Mowla (1968) worked on this project and they determined the aquifer properties from limited available aquifer test data and from geologic analysis. The results were mostly based on qualitative data.

Some geological investigations have been made concerning the mineral development and it is only lately

that attention has been directed towards the sediment loss, hydrogeology, and amount of the ground-water storage. Some general regional geological descriptions have been made but the data are very sparse and the detail required for the mathematical modeling of the aquifer was not available. The Soil Survey of Bangladesh (1973) and Publications by Brammer (1969) and Huizing (1971) provide very comprehensive information on soil genesis and soil properties related to the potential for agriculture development. These studies have been used to make general statements about the geology of the country on the basis of regional soil characteristics.

Most of the previous surveys report that there is an adequate aquifer available for exploitation within the study area and that irrigation wells drilled to 300 feet would yield at least two cfs. Some reservations about recharge potential and water quality have been expressed by McDonald. The same consultant has asserted that shallower tubewells drilled to approximately 180 feet deep could function as efficiently as 300 feet deep wells using a standard design, provided they were individually designed for the aquifer available.

CHAPTER III

METHOD OF APPROACH

Method of Study

In order to determine the maximum annual yield and a corresponding pumping rate allocation for the aquifer during a 20-year period from 1977 to 1997, the author accomplished the following tasks. A flow chart showing those tasks is shown in Figure 3 and details of the approach used are discussed in the following chapter under the respective headings.

Task I. Collection of Raw Data

It includes (a) geologic investigation, (b) collection of well records, (c) precipitation records, (d) prior requirements of water for irrigation, and (e) hydrogeologic investigations.

Geological information was collected from Geological Survey of Bangladesh; publications include those by Coleman (1969), Morgan (1959), and Brammer (1969). Lithological characteristics were determined from Driller's Log. Bore logs were collected from Bangladesh Agricultural Development Corporation and Water Development

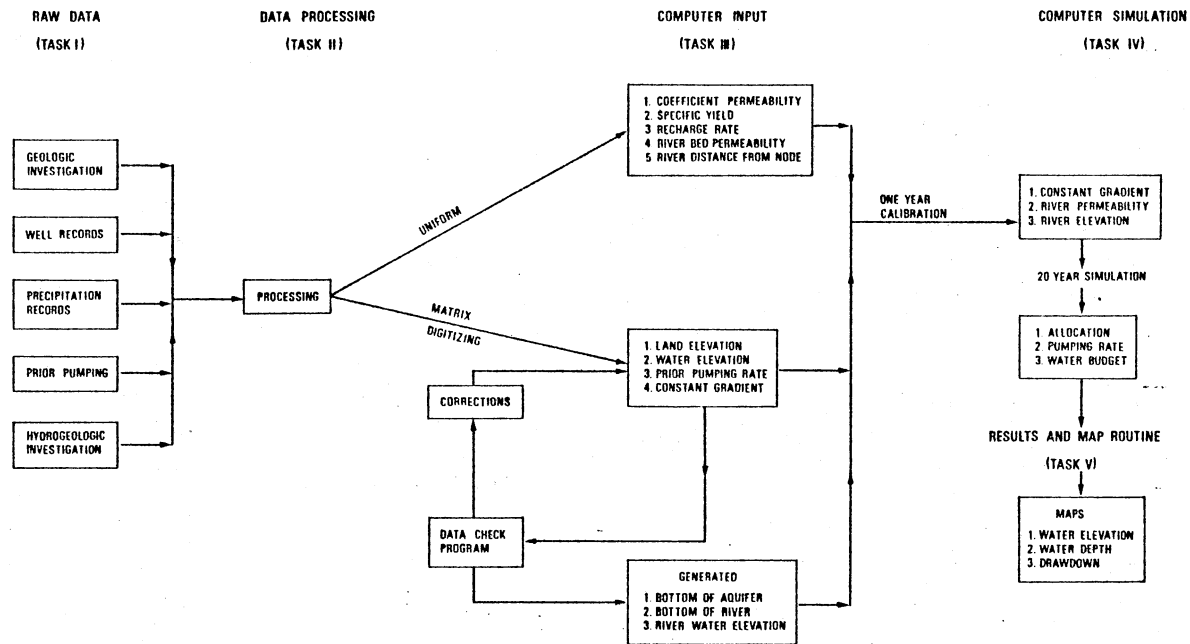


Figure 3. Flow Chart of Computer Modeling

Board. Aquifer materials are generally uniform, homogeneous, and unconsolidated Piedmont type deposits.

All of the records for the 266 existing irrigation wells were collected from Bangladesh Agricultural Development Corporation and the Water Development Board and were plotted on the maps. Precipitation records for the last ten years of five different stations in the study area were collected from the Meteorological Department. The average weighted annual rainfall in the study area is 86.11 inches.

Hydrogeological data such as long term aquifer testing data, well observation data, drawdown discharge of existing wells, and river discharge data were collected from the Water Development Board. The weekly water level survey which is published periodically by the Water Board consists of 26 observation wells in the study area.

Task II. Data Analysis and Processing

The collected raw data described in Task I were analyzed and processed for computer input. Contour maps were prepared and values were determined after processing the raw data. The details of these are discussed in the following chapters.

Task III. Data Digitizing and Use

The input data were divided into uniform matrix and nonuniform matrix parameters. Uniform matrix values were entered directly into the model.

The contoured data were gridded, digitized, and read into the IBM terminal for computer input. The 1:1.10 mile grid map shown in Figure 4 was drawn at the same scale as the base map and was overlaid onto each contour map. Values were assigned to each node of the grid. The grid spacing was used to establish a matrix.

The uniform matrix parameters included:

1. Recharge rates from precipitation and irrigation
2. Coefficient of permeability
3. Specific yield
4. Distance of river influence on node elevation
5. Coefficient of permeability of riverbed

Recharge was considered in two forms: precipitation and return flow from irrigation. Return flow from irrigation was estimated 20 percent of the total water pumped. The initial recharge rate was calculated to be 28% of precipitation. The permeability coefficient of the aquifer consisted of a homogeneous value and was calculated to be 600 gpd/ft². Similarly, the S_y of the upper part of the aquifer is estimated to be 20 percent. The riverbed consisted of silts and clays, and they

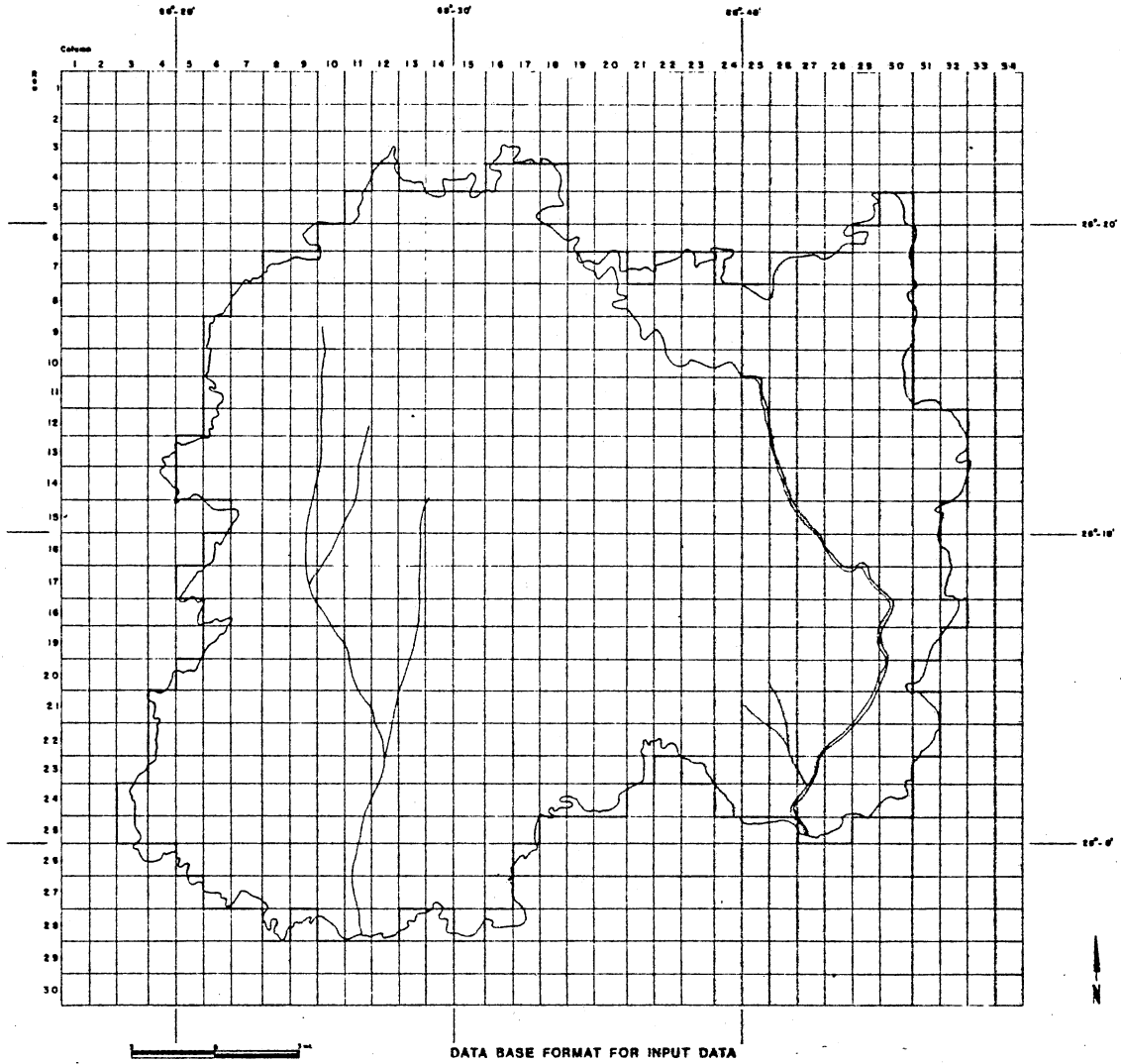


Figure 4. Data Base Format Map

served as a local aquitard to the underlying aquifer material.

The non-uniform matrix parameters included:

1. Water table elevations
2. Land elevations
3. Bottom elevations of the aquifer
4. Prior irrigation pumpage
5. Boundary subsurface flow gradient.

The water levels of existing 26 observation wells were obtained from Water Development Board and interpolated head values were used for the computer matrix. The land elevations were assigned to a grid by using the Survey of Bangladesh topographic map. The bottom of aquifer was considered as a function of the depth of well penetration and land elevations.

Prior irrigation pumping was determined by the Agriculture Department for use in the land irrigation at a rate for which a beneficial use can be shown. Prior pumping requirement rates (acre-ft/year) were acquired from the Agriculture Department converted to acre-ft per acre per year and assigned to nodes with respect to their one mile location (Figure 5). The pumping rate used from each irrigation well was two to three cfs or about four acre-feet per acre during 150 days irrigation period (November to March) at the rate of twelve hours continuous pumping per day. The well yields were determined by

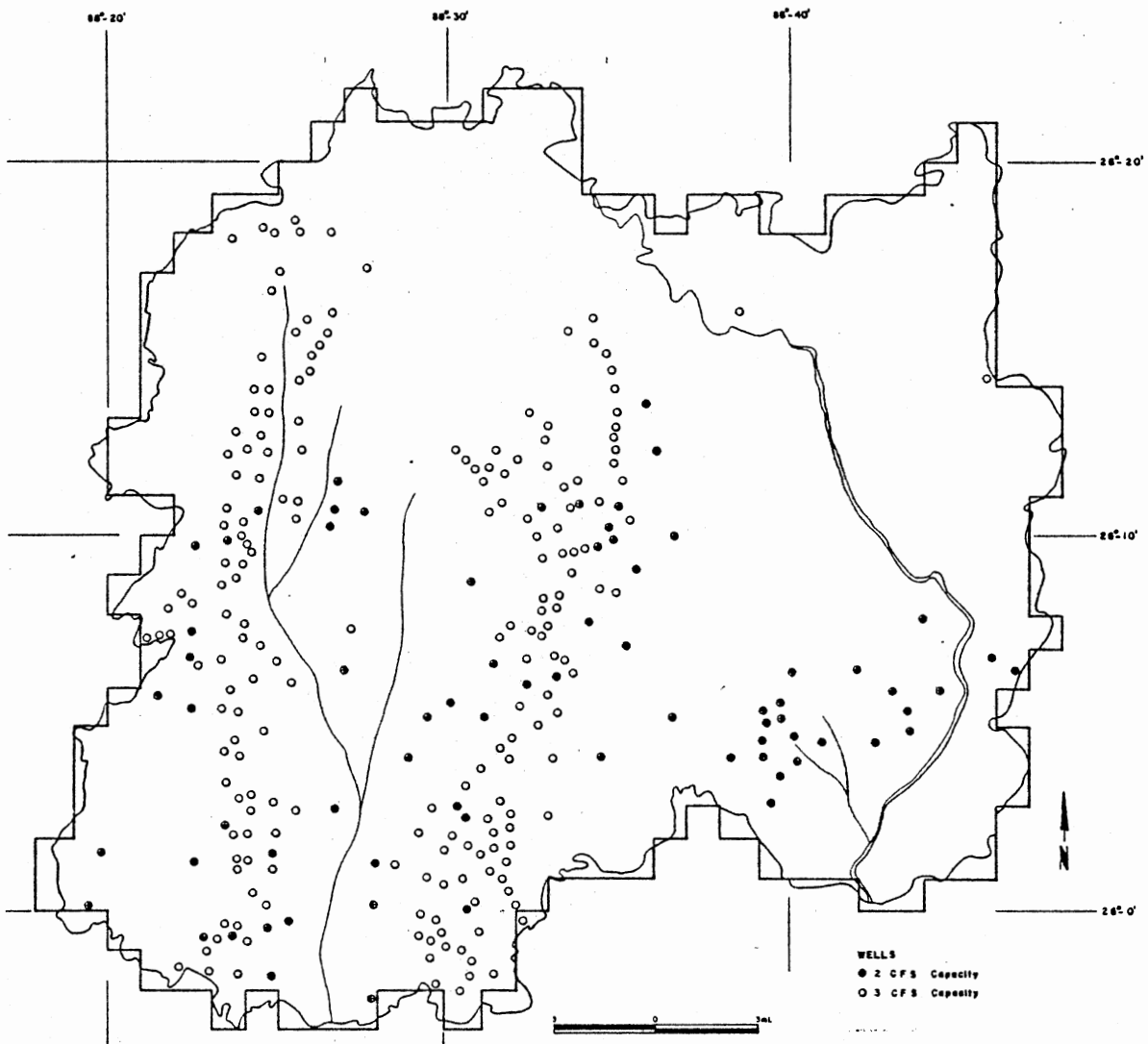


Figure 5. Well Location Map (1977)

dividing total withdrawal of water per year by the total number of wells pumped per year. The approximate range of discharge in thousand acre-feet per square mile at the end of 1977 are shown in Figure 6.

The 1977 water-table map of the study area was used to calculate the hydraulic gradients of recharge and discharge nodes located at the boundaries of the modeled aquifer. The fluxes at these boundaries were calculated using Darcy's law:

$$Q = KAI \quad (1)$$

where

Q = the amount of inflow or outflow (L^3/T)

K = hydraulic conductivity of aquifer material
(L/T)

A = cross sectional area of the nodes through
which flow takes place (L^2)

I = hydraulic head gradient or slope of water
table (L/L)

The equation can be written as

$$Q = K(W.D)(\Delta H \div L) \quad (2)$$

where

D = saturated thickness of the adjacent node.

W = the cross sectional width of the node.

The distance between centers of nodes (L) are cancelled out when a square size node is used. The model calculates flux as the data entered was ΔH .

Task IV. Calibration

One year computer simulations were performed using the observed 1977 water head elevations. One year simulation runs were used to calibrate the model. Calibration was achieved by adjusting the river elevation and constant gradient.

Task V. Allocation

A 20-year computer simulation (1977 to 1997) was conducted using the results of calibration. Repeated runs were performed using prior irrigation pumping rate and various allocation pumping rates in order to prevent no more than 50 percent of the nodes from going below 22 feet. For comparison, an additional run was made using only the prior irrigation pumping rate.

Task VI. Model Output

Data output from these versions were plotted using the computer printer. The computer simulation results were summarized in the ground-water budget for the study area.

CHAPTER IV

GEOLOGY

Regional Geology

Bangladesh is generally covered by Quaternary sediments deposited by the Ganges-Brahmaputra Meghna river system. Most of the country is a vast alluvial plain of Recent age. Except for Tertiary hill ranges of Chittagong and Sylhet, and the uplifted Pleistocene Barind and Madhupur tracts and the Lalmai hills of Comilla.

Rocks ranging in age from Paleocene to Pleistocene are exposed in the eastern and northeastern parts of the country. The Tura sandstones of the Paleocene and early Eocene ages are the oldest rocks exposed (near Takerhat in Sylhet District) and represent the platform facies, whereas the folded rocks of the Chittagong area are exposed miogeosynclinal sediments of the Miocene Surma Group.

The western and northwestern parts of the country are characterized by a stable shelf area in which rocks vary from Paleocene to Pleistocene in age and have been deposited on the eroded Archean Basement complex. The Basement complex consists mainly of crystalline metamorphic and igneous rocks which have been found in the bore holes

at depths between 2030 and 7090 feet in the Bogra-Rajshahi district. Drilling at Madhyapara in the Dinajpur District has revealed the presence of quartz-diorite and granodiorite at very shallow depths between 422 and 506 feet below the surface. The age of this unit is uncertain.

Figure 7 represents the estimated thickness of the sedimentary deposits within Bangladesh. There is a major discontinuity which trend from the Shillong plateau to the southwest towards Bogra. This zone is referred to as the "Hinge Line" which separates the shelf sediments of the northwest from the basin/geosynclinal sediments of the south and the east. The Sylhet basin is extremely deep and there is a strong gravimetric evidence of continuing subsidence. It can be noted in Figure 7 that minimum thicknesses, about 400 feet, occur in the Project area (Dinajpur District) but a very rapid increase to over 9000 feet in thickness occurs in the southern part (Pabna District). However, of these thicknesses only a small percentage of these thick sediments are economically exploitable aquifers which normally occur in the upper 300 feet.

The generalized stratigraphy of Bangladesh is summarized in Table I which includes a description of the water bearing properties.

Typical deep geological profiles for southern Dinajpur District are illustrated in Figure 8. In this

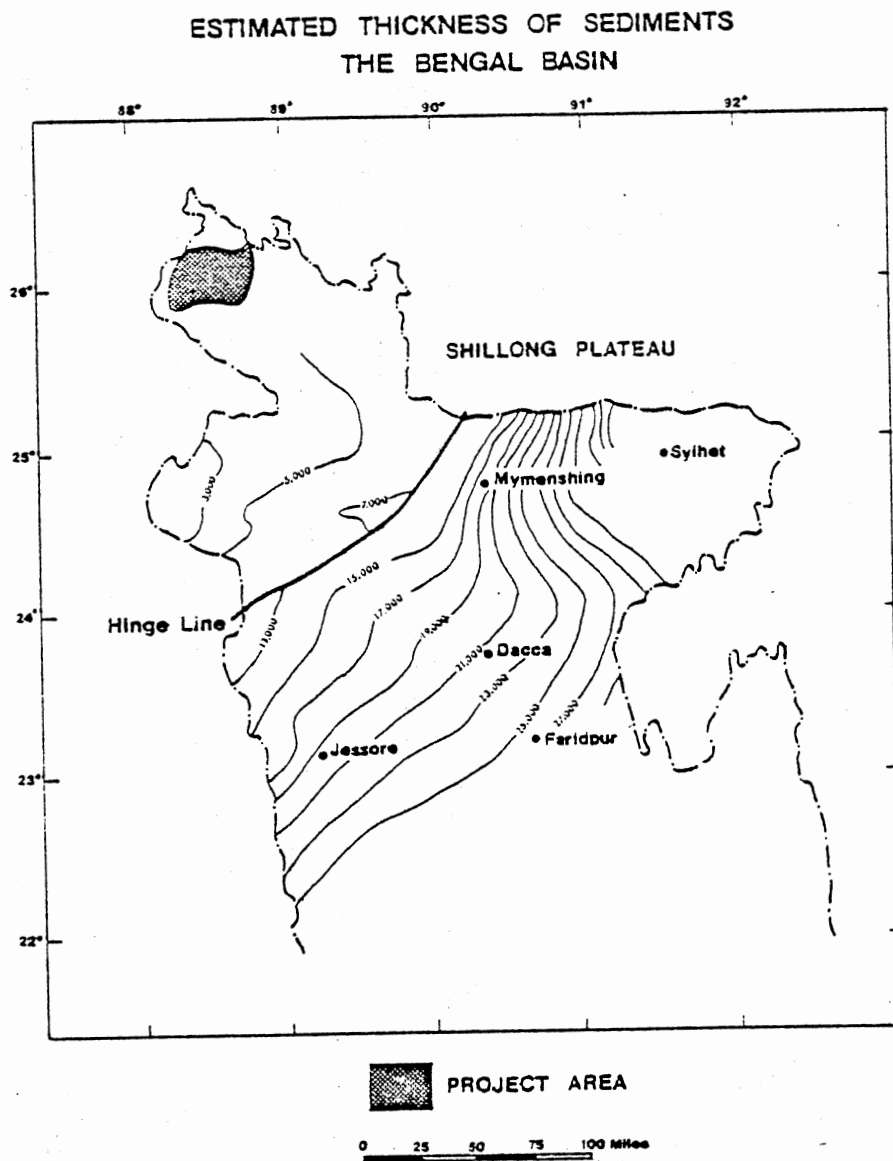


Figure 7. Map Showing Sediment Thickness in Bangladesh (After Brammer)

TABLE I

GENERALIZED STRATIGRAPHY AND AQUIFER UNITS IN BANGLADESH

		: Geosynclinal Sedi-: Shelf Sediments :				
		: ment South & East : Northwest :		Physical Characteristics		
		: Bangladesh : Bangladesh :				
Age	: Group	: Formation:	Group	: Formation:	Major Lithologic types	: Water Bearing Properties
Pre Holocene:		:Alluvium :		:Alluvium :	Sand, Silt & clay	: Excellent aquifer
Holocene :		:		: (300) :		
unconformity						
Late Pliocene	:	:Modhupur :		: Dihing :	Clay, Pebbly Sandstone	: Aquiclude in Northwest
Pleistocene :		: (151+) :		:		
unconformity						
Late Miocene	: Dupitila :	Upper Dupitila :	Dupitila :		Claystone, siltstone & gravel	: Aquiclude, Aquitard
	: (6,000) :	: Dupitila :	: (1000) :			
	:	: (over 5000) :	:	:		
Middle-Pliocene	:	: Lower Dupitila :		:	Sandstone	: Aquifer
	:	: (2000) :	:	:		
unconformity						
Middle Miocene	: Tipam :	Giruhan clay :	Surma (1355) :	Jamal-gans (1355) :	Claystone, siltstone & sandstone	: Aquiclude
	: (7132) :	: (3188) :				
	:	: Tipam :	:	:	Sandstone	: Aquifer
	:	: Sandstone:	:	:		

TABLE I (Continued)

Early Miocene	: Surma (19000)	: Bakabil (6000)	: : : : : : :	: Siltstone, shale, and sandstone	: Aquiclude	
		: Bhuban (13000)	: : : : : : :	: Siltstone, sandy shale & sandstone	: Aquiclude/ Aquitard	
unconformity						
Oligocene	: Barail	: Jenam (2120+)	: Barail (535)	: Bogra (535)	: Siltstone, Carbonaceous shale and sandstone	: Aquiclude
					: shale	
Late Eocene	: : : : : : :	: : : : : : :	: : : : : : :	: Kopill Alternations (492+)	: Shale, carbonaceous fossiliferous with sandstone & limestone	: Aquiclude
Middle Eocene	: : : : : : :	: : : : : : :	: Jaintia (1091)	: Sylhet (800)	: Fossiliferous limestone w/ subordinate sandstone	: Aquifer (mineralized)
Early Eocene	: : : : : : :	: : : : : : :	: : : : : : :	: Tura sandstone (790+)	: Sandstone, coal & shale	: Aquifer (mineralized)

TABLE I (Continued)

unconformity						
Late-middle	:	:	:	Sibhani	Shale, calca-	No aquifer
Cretaceous	:	:	:	Trapwash	aceous, sand-	
	:	:	:		stone, Ferru-	
	:	:	:		genous shale,	
	:	:	:		clay, sand-	
	:	:	:		stone	
unconformity						
Late	:	:	:	Rajmahal	Basalt flows	No aquifer
Jurassic	:	:	:			
Early	:	:	:	Trap		
cretaceous	:	:	:	(1790+)		
Unconformity						
Late	:	:	:	Raniganij	Paharpur	Sandstone with
Permian	:	:	:	(1443+)		thick coal
	:	:	:			seam
unconformity						
Early	:	:	:	Barakar	Kuchma	Coarse grained
Permian	:	:	:		(1601+)	sandstone w/
	:	:	:			170 thick
	:	:	:			coal reach
unconformity						
Archean	:	:	:	Basement	Gneiss and	No aquifer
	:	:	:	complex	Basalt	
	:	:	:	(393+)		

Note: Maximum thickness of rock shown in parenthesis (feet)

section the width of the column is made proportional to grainsize.

The two boreholes sections as shown in Figure 8 are representative of deposits in most of the Dinajpur area although the age interpretation is exceedingly difficult because these formations are not fossiliferous. It is of interest to note the occurrence of kaolinite in both sections. This may indicate massive down faulting in the order of 600 feet between these boreholes following a time when this zone was weathered from the exposed basement diorites which were uniformly deposited over the area. The lowest sedimentary units classified are the Permian Gondwana deposits which were deposited in a lacustrine environment. The coarse conglomerates are possibly indicative of the marginal glaciofluvial deposition. Subsequent upfaulting to the southeast may have caused the removal of this Unit from the section GDH26 (Figure 8).

Above the kaolinized zone are sequences of shallow siltstone and muddy sandstones, provisionally classified as the Tura formation of Eocene Age by Geological Survey of Bangladesh. The upper part of this formation becomes increasingly coarse grained between 80 and 150 feet below the Pleistocene clay deposits. There is fairly strong evidence that the upper deposits may be unconformable with Tura and considerably younger Dupi Tila of Mio-Pliocene Age or even Pleistocene interglacial deposits.

DEEP EXPLORATORY BORES IN S. DINAJPUR DISTRICT

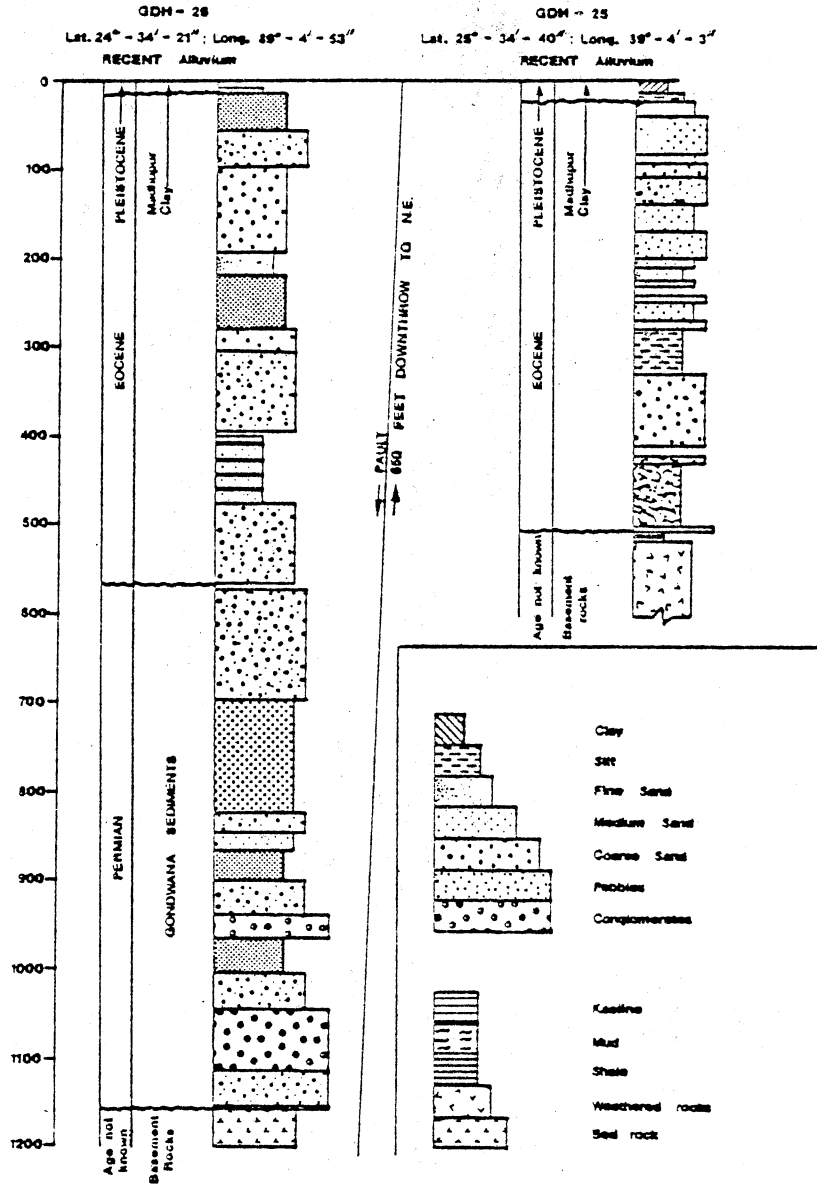


Figure 8. Geologic Profiles from Deep Bore Holes (After Sir MacDonal)

The Pliocene-Pleistocene Barind and Modhupur clay rests unconformably on the underlying sedimentary rocks. The impervious clay beds are 20 to 100 feet in thickness and are predominantly gray in color but are reddish in outcrop areas. These clay beds form the base of the unconfined aquifer. Covering these earlier deposits (Pleistocene clay) are Sub-Recent to Recent alluvium composed of grey and yellow sands, gravels, clay, and silty soils. These mark the areas of Recent and present fluvial activity. These more recent deposits constitute the aquifer which is modeled in this study.

The tectonic history of the region is complex and difficult to interpret because of the thicknesses of masking alluvium. Bangladesh geology is strongly affected by the fact of being squeezed between the Himalayan thrust and older Arakan anticline flanking the Burmese geosyncline. This bidirectional compression has generated much secondary folding and faulting over and above that normally found following the east-west Himalayan trend. The net result has been that many shear faults associated with the compression and vertical faults associated with the folding have remained active throughout the period of deposition. It is even claimed by some that fault throws can be detected at depth in the alluvial cross section.

Nevertheless, there can be little doubt that tectonics are responsible for the lateral separation of

the Barind and Piedmont units and that faulting is probably responsible for many other observed lateral changes in aquifer characteristics as shown in Figure 9 which show the tectonic features and structures of Bangladesh.

Local Geology

The plain area of Bangladesh has been divided geomorphologically into seven units by Coleman (1969) and Brammer (1969) as shown in Figure 10. Generally the features used in the geomorphological classification are land gradients, erosional maturity, degree of weathering, flooding, drainage, and type of soil developed.

The two units, the Piedmont and Karotoya flood plains, are found in the Project area. The Piedmont represents the coarser grained, sandy deposits along the foot hills of the Himalayas. These areas have fairly well developed and drained soil profiles. In the northeastern part of the Project area, the Karotoya river debouches from the mountains and has modified the older Piedmont area, forming a well marked tract of recent flood plain alluvial deposits which trend north-south across the area. Both are of recent age but are flanked on the south by Pleistocene Barind alluvium. Nowhere is there evidence of the younger sediments being deposited on top of the older sediments. Within the depth limits of water well drilling, the change is always lateral, so that tectonic

MAJOR TECTONIC FEATURES AND STRUCTURE OF BANGLADESH

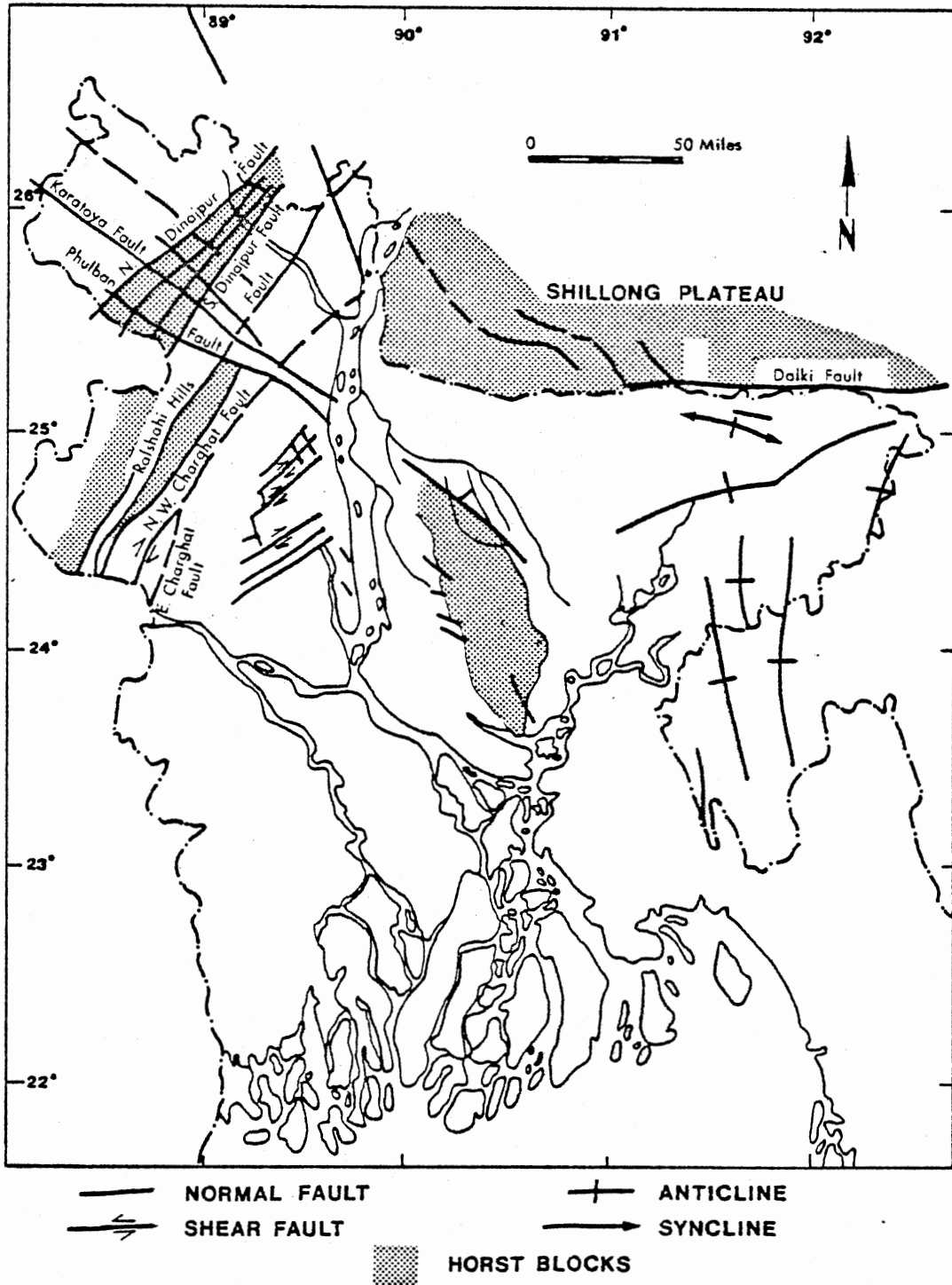
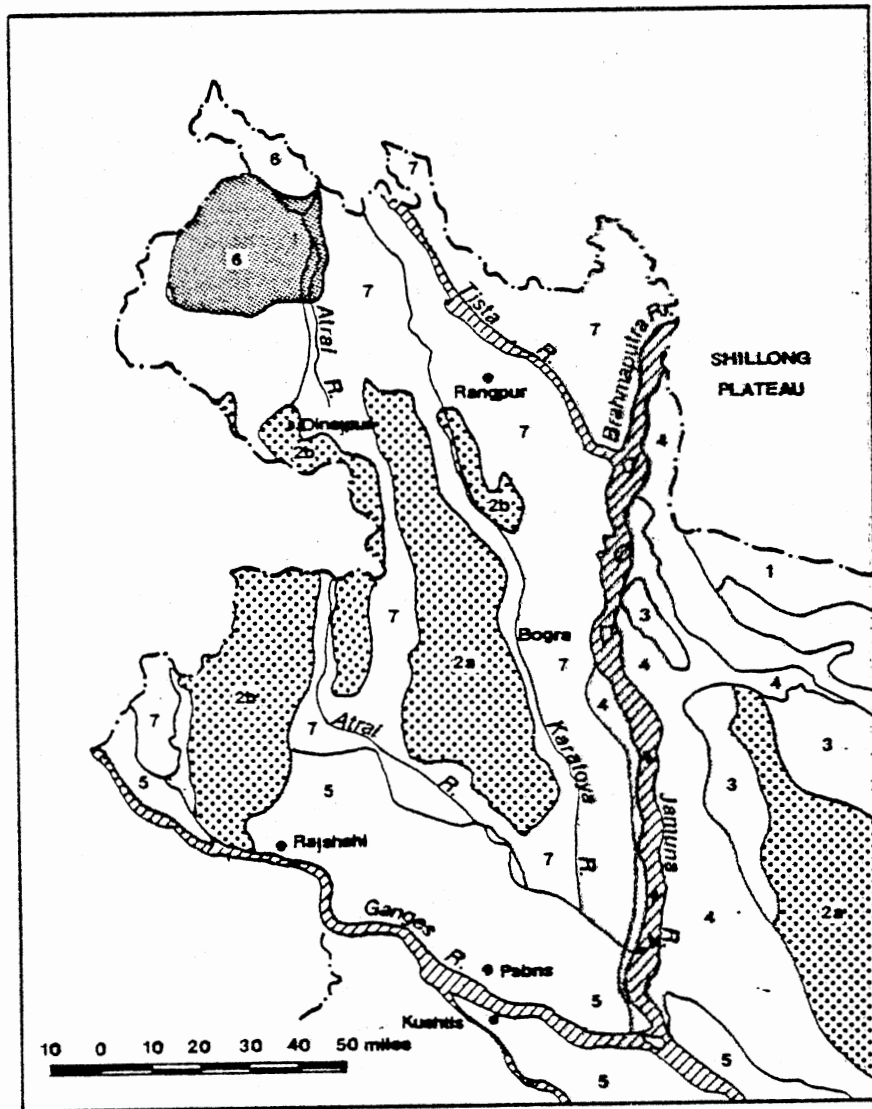


Figure 9. Tectonic Features and Structure Map
(After Sir MacDonalld)

GEOMORPHIC MAP



1	Northern and Eastern piedmont plains
2a	Maulpur tract
2b	Berind tract
3	Old Brahmaputra floodplain
4	Young Brahmaputra (including Jamuna) floodplain
5	Ganges floodplain
6	Old Himalayan piedmont plain
7	Tista, Atrai, and Karatoys floodplains

Figure 10. Geomorphologic Map of North of Bangladesh (After Sir MacDonal)

movements must have been effective in determining the boundaries.

It is agreed by many that the Karotoya represents a unit which is composed of a Piedmont material reworked by a river system; therefore the deposits can be named as Piedmont deposits. A north-south lithologic cross section as shown in Figure 11 represents a unit in the Project area which consists of mainly uniformly deposited medium to coarse sands with fine sands with less than ten percent clays and occasional gravels. The gravels increase in frequency and in grain size from south to north. Silt sizes seem to be completely absent which indicate intermittent outwash deposition rather than large, permanent river systems. The absence of silt is diagnostic of the unit.

N-S GEOLOGIC CROSS SECTION

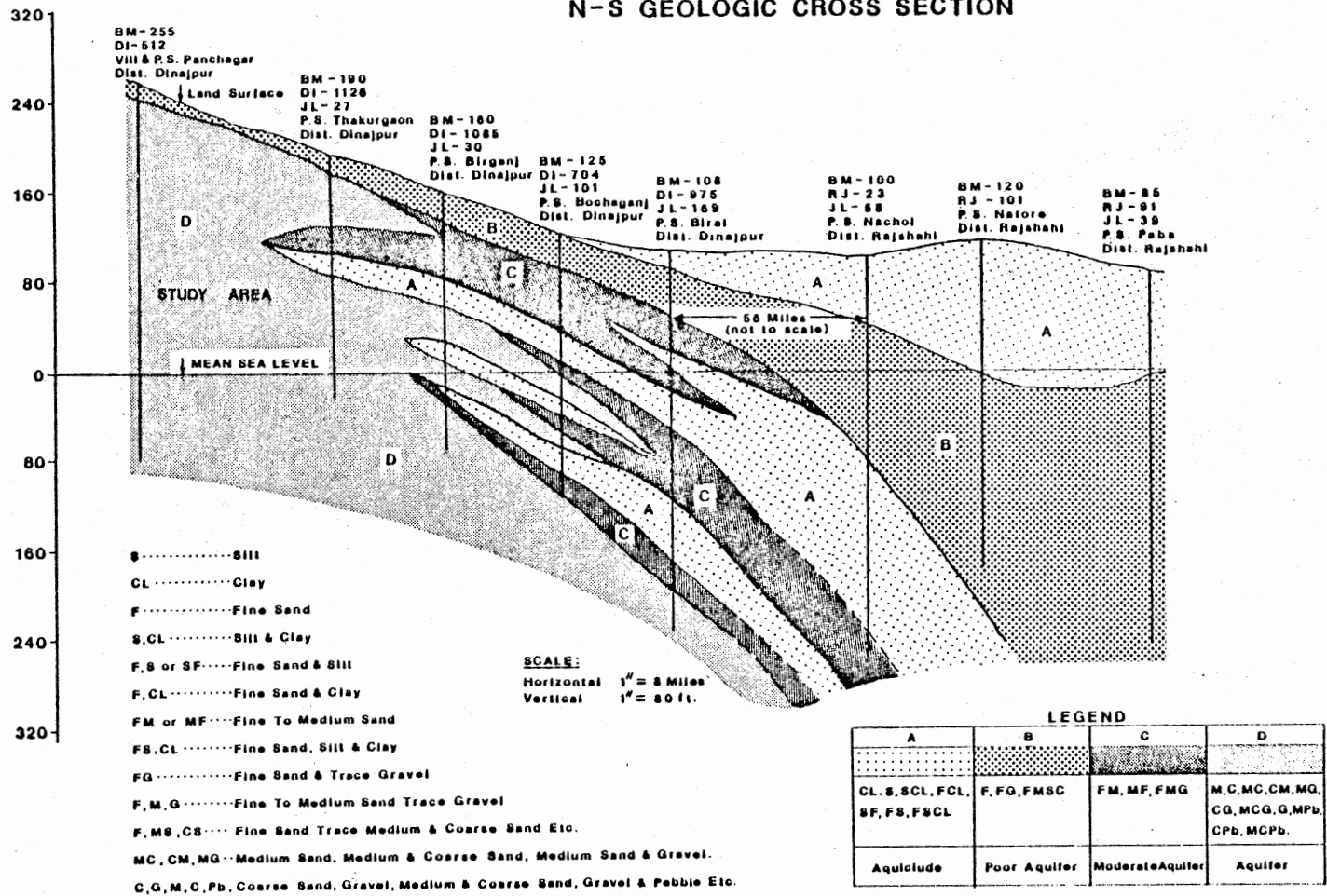


Figure 11. North-South Geologic Cross Section of Dinajpur and Rajshahi

CHAPTER V

HYDROGEOLOGY

General

Ground-water is the major, if not the sole, source of water for irrigation and domestic uses in the study area. The Piedmont aquifer is an unconfined aquifer. The base of this alluvial aquifer is impermeable in nature with finer materials preventing a downward loss of water. Therefore, rechargeable ground-water is restricted to the overlying alluvium. The aquifer appears to be a homogeneous north-south trending sand bounded by multilayered finer textured sediments (Figure 11).

Water-Table

The observed minimum and maximum depths to the water-table in the study area for the year 1977 are shown on maps in Figures 12 and 13. The minimum depth is associated with the July-August period which is during the monsoon; the maximum depths occur during April and May which is dry season. Data represented on the maps are collected from 26 number observation wells in the study area. The difference between the highest and the lowest

**GROUND WATER CONTOUR MAP
OF MINIMUM ELEVATION
(APRIL - MAY, 1977)
(DRY PERIOD)**

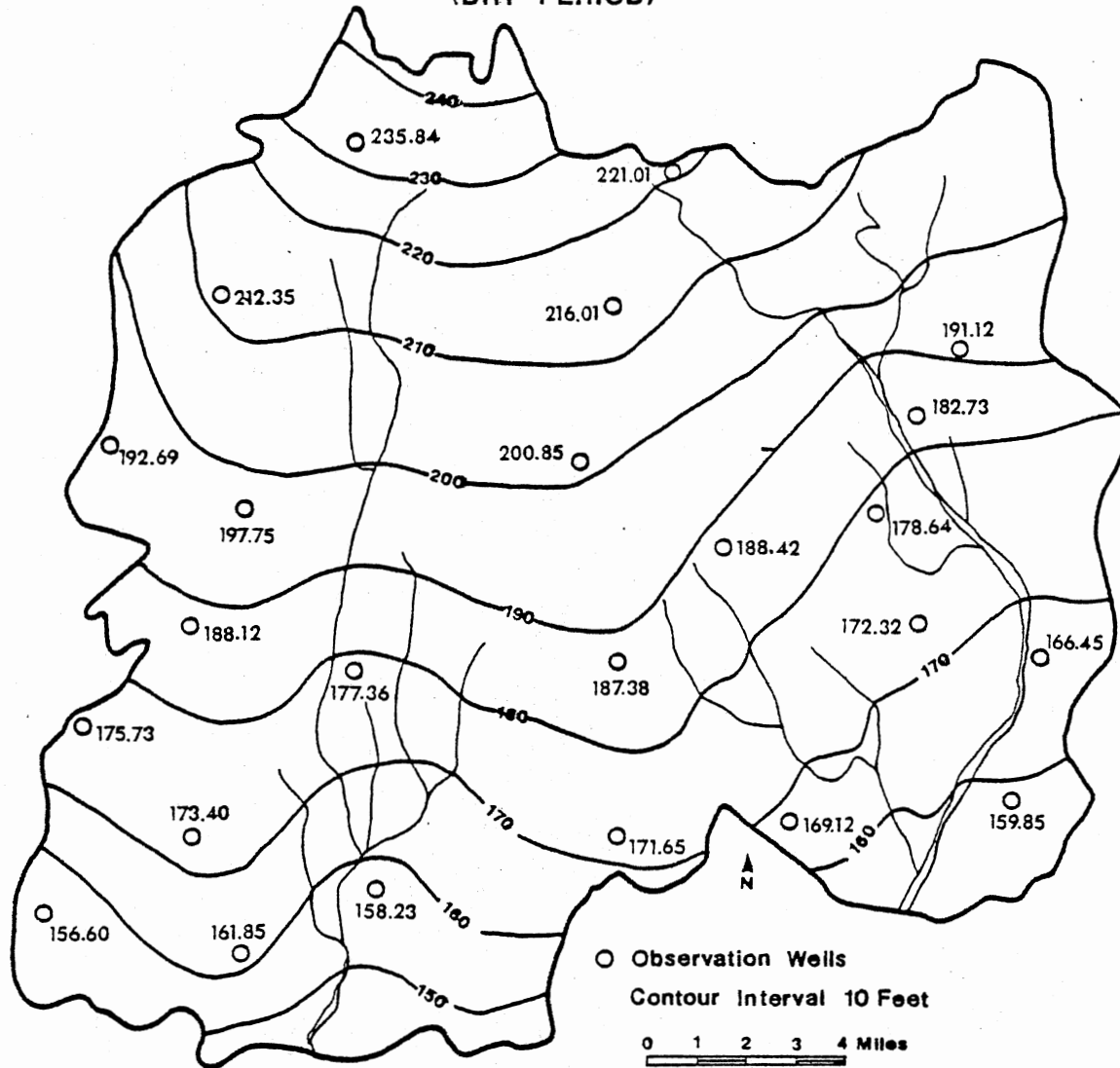


Figure 12. Minimum Water-table Elevation Contour Map (1977)

GROUND WATER CONTOUR MAP OF
 MAXIMUM ELEVATION
 (AUG-SEPT, 1977)
 (WET PERIOD)

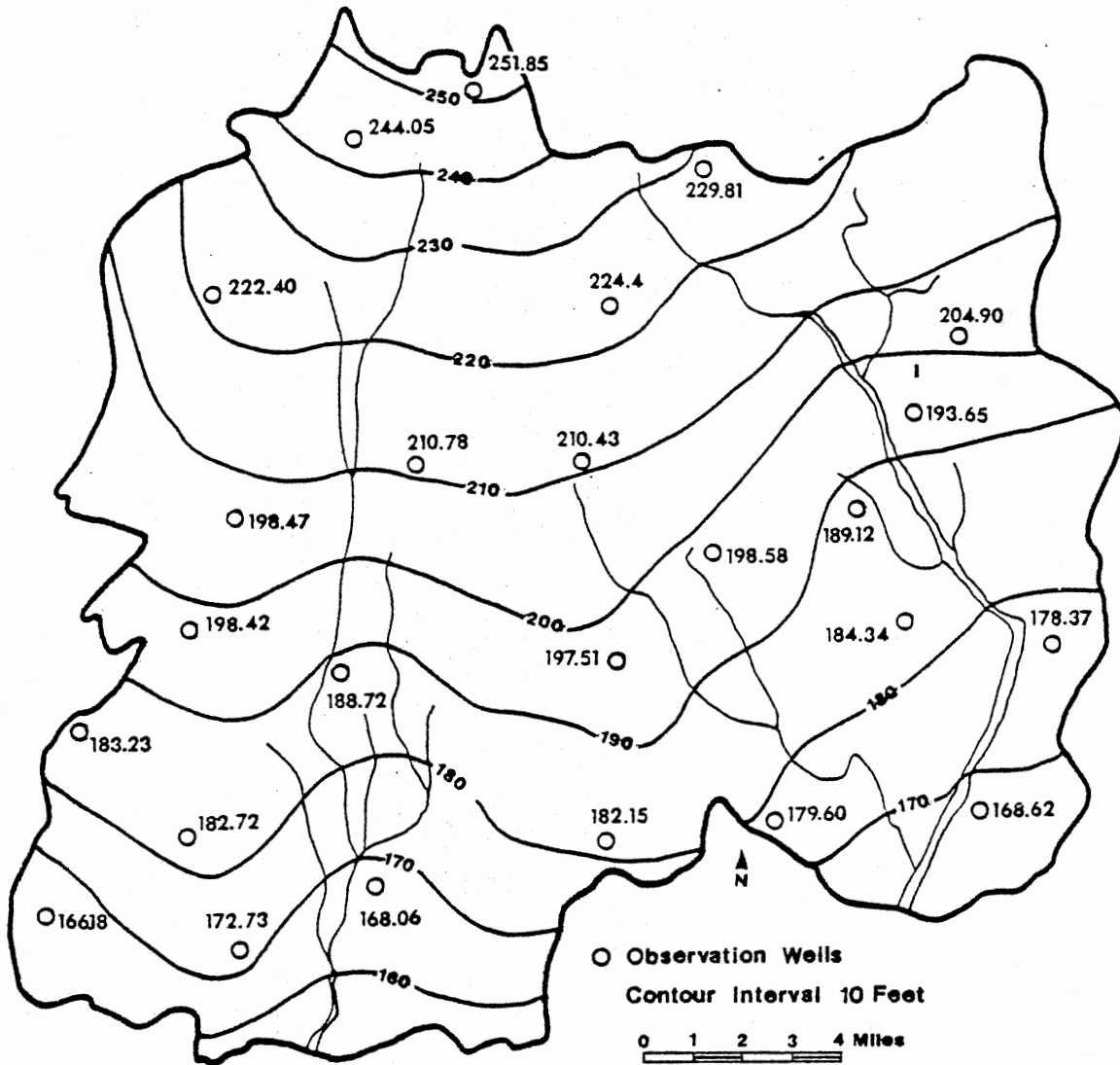


Figure 13. Maximum Water-table Elevation Contour Map (1977)

water levels ranges from eight to twelve feet in most wells. The water-table generally follows the topography of the area (Figure 14) and slopes generally to the south. The water-table contours also bend upstream, indicating that groundwater is discharging into the stream. A relatively uniform hydraulic conductivity (coefficient of permeability) gives rise to equidistant spacing of water-table contours. The average hydraulic gradient in the study area is approximately three feet per mile.

Climate

The study area experiences a tropical climate characterized by a very humid, wet, south-west monsoon from May to October. This accounts for some 85 percent of the annual rainfall. During the period between November and April, a cool, dry northeast monsoon blows from Central Asia bringing, initially, the lowest temperatures and humidities and later on, convectional storms. During the cool period, temperatures may vary from a minimum of 39°F to a maximum of 94°F and in the wet period temperatures vary from 54°F to 107°F.

The average of monthly precipitation and evapotranspiration between 1968 and 1977 for the same station in the study area are listed in Table II. The average annual precipitation of different stations in the study area is shown in Table III. The average annual precipi-

SURFACE ELEVATION CONTOUR MAP

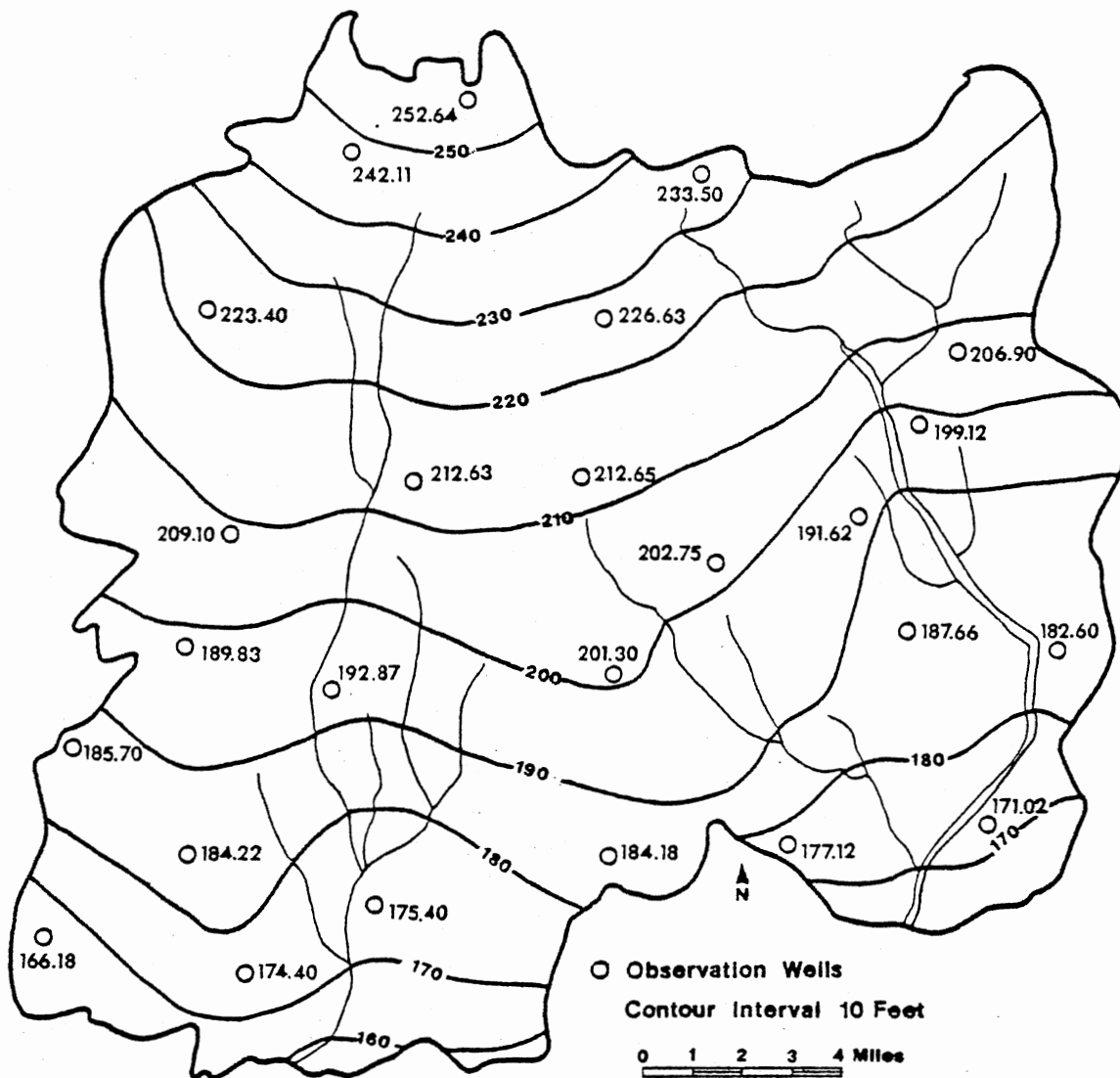


Figure 14. Surface Elevation Contour Map

TABLE II
AVERAGE MONTHLY PRECIPITATION AND
EVAPOTRANSPIRATION (INCHES)
(1968 - 1977)

Month	Average Precipitation (Inches)	Average Evapotranspiration (Inches)
January	0.40	2.08
February	0.44	2.79
March	0.62	4.48
April	2.85	5.90
May	10.33	6.10
June	15.96	5.31
July	20.82	5.11
August	15.52	5.0
September	14.48	4.80
October	4.50	4.21
November	0.145	2.80
December	0.045	2.08
Total	86.11	50.67

TABLE III
WEIGHTED AVERAGE PRECIPITATION

Station	: Average ; Precipita- : tion : (in/yr)	; ; : Area : (Sq. mi.):	; Percentage : of area	; Weighted : Average : (in/yr)
Chotadap	: 89.12	: 76	: 13	: 11.58
Pachagarh	: 78.57	: 53	: 9	: 7.07
Buda	: 90.95	: 130	: 22	: 20.00
Debigan	: 88.14	: 100	: 17	: 14.98
Thakurgaon:	83.25	: 229	: 39	: 32.46
Total		588	100%	86.11

tation is 86.11 inches.

Ground-water Recharge

The term natural recharge refers to water that percolates down through the unsaturated zone to the water-table and actually enters the dynamic ground-water flow system (Freeze, 1967). This definition excludes that portion of the soil moisture surplus that enters the ground and increases the soil moisture but does not enter the flow pattern itself. The rate of ground-water recharge depends on several factors including precipitation, permeability, depth to water-table, soil type, moisture conditions, topography, vegetation type and density and temperature.

Because of several variables and difficulties involved in attempting to measure ground-water recharge rates, experiments along these lines have been relatively few and exceedingly complex. Nonetheless, recharge rates can be of considerable importance in the design of well fields because the recharge that can be captured by the cone of depression surrounding a pumping well is equal or nearly equal to the long term yield that the well can provide without drawing from storage (W. A. Pettyjohn and Henning, 1979).

Recharge to the ground-water reservoir in the study area occurs mainly by percolation of rain water. The

conditions are favourable for recharge during June to October. There is much precipitation in excess of evaporation and transpiration in the study area during this time. Duration of rainfall also varies from a few hours to a few days and is widely distributed. During these periods, the soil seldom becomes dry and little water is required to replenish soil moisture. Therefore the rainfall of the monsoon season is very favourable for recharge. The top soil is comprised of silt and fine sand which permits a good infiltration rate to occur. Practically the entire area is farmed which increases the soil permeability by loosening up the top soil. Puddling of the soil by rain drops is reduced by the vegetal cover which further lowers runoff, and enhances percolation. The universal practice of subdividing rice fields by the construction of low dikes increases infiltration since the dikes store two to four inches of water.

Figures 15 and 16 are well hydrographs which show that the water level in the observation wells rises during the rainy season and recedes during the dry season, reaching a maximum depth by the end of the dry period. During the months of May to July, the water level rise in the observation well is rapid. After that, the water levels in the wells slowly rise until the months of August and September when the water levels reach the minimum depth. The average fluctuation of ground-water level is ten feet.

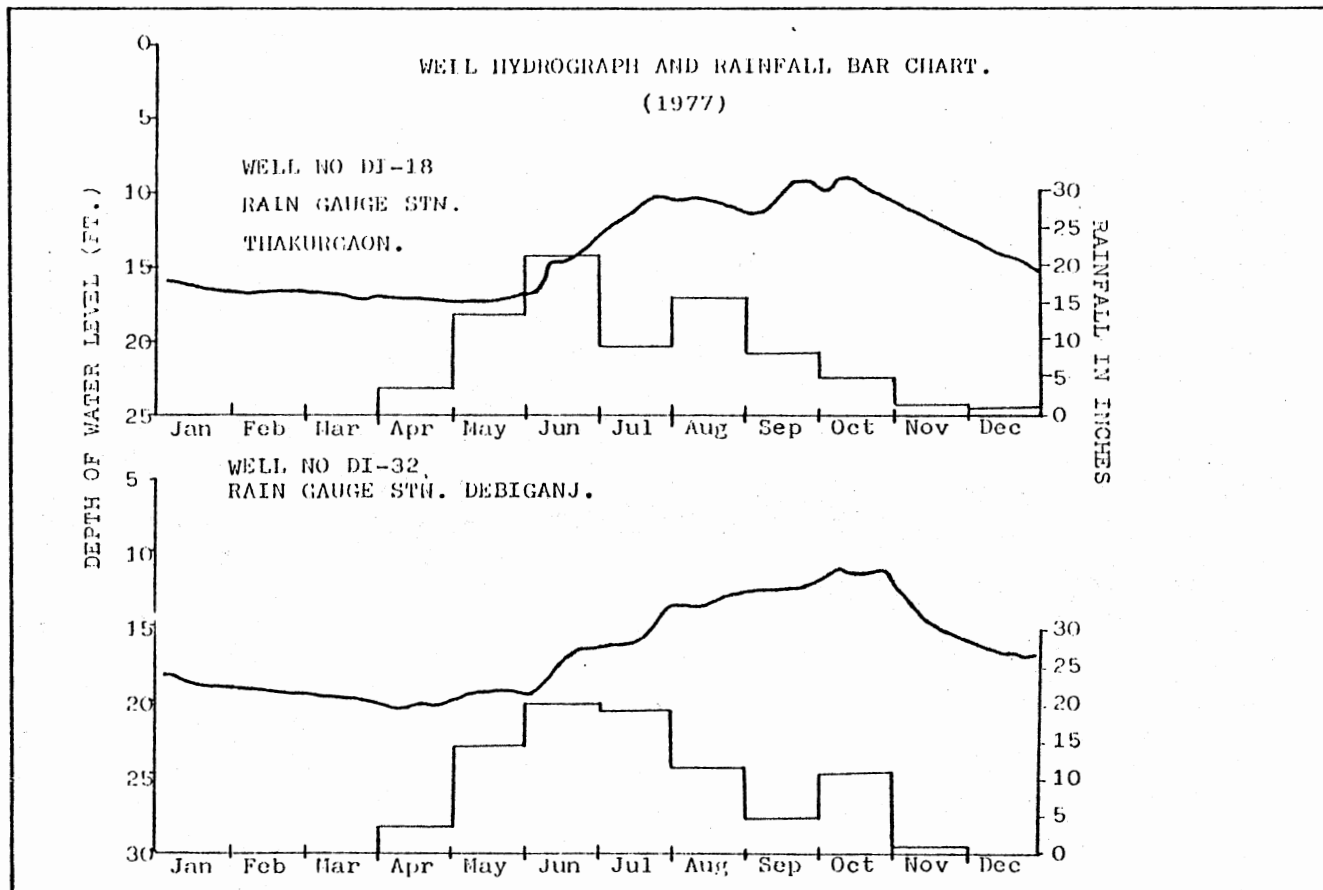


Figure 15. 1977 Well Hydrograph and Rainfall Bar Chart (W-18,32)

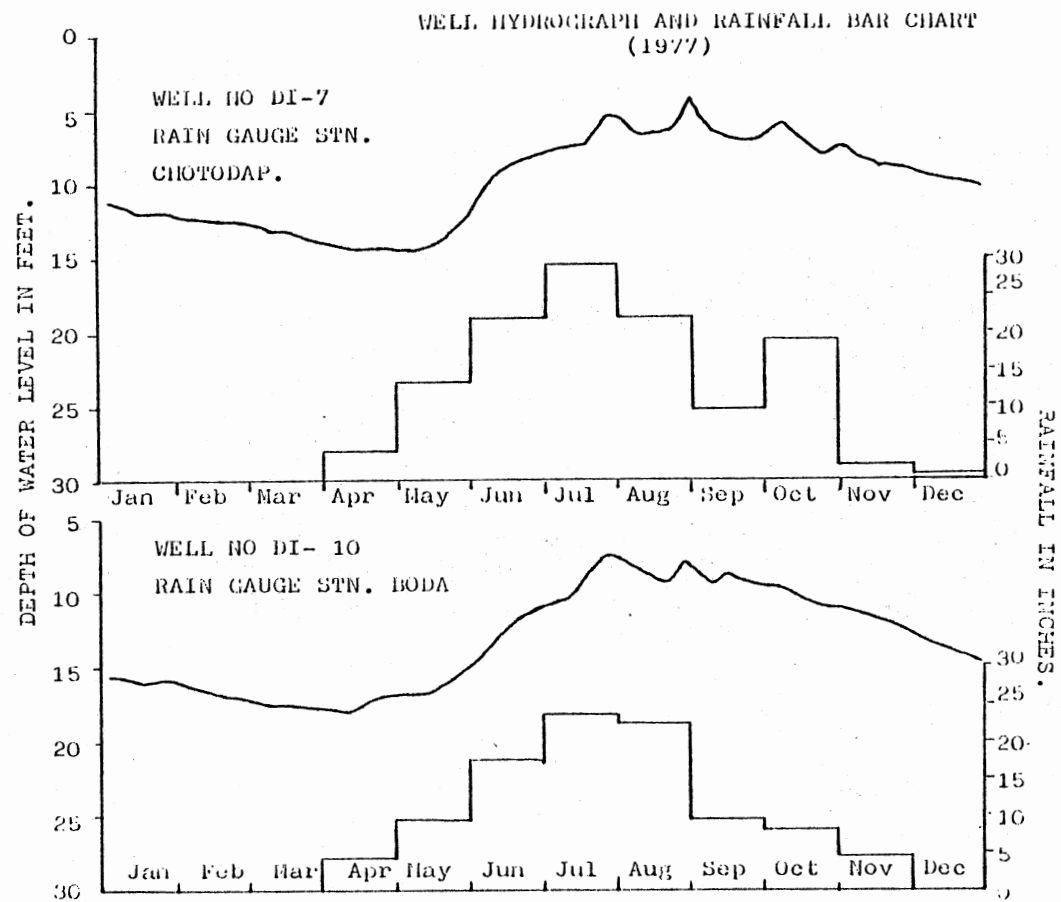


Figure 16. 1977 Well Hydrograph and Rainfall Bar Chart
(W-7,10)

During the wet season ground-water is still continuously discharging in a small amount to the river (see Figure 13).

The minimum depth to the water-table as shown in Figure 13 is only two to three feet below the land surface over most of the area during the months of July and August. During this period, recharge by percolation of rainwater could not occur because the water table lies very close to land surface and is subject to evapotranspiration and runoff.

There are several methods by which estimates of regional ground-water recharge can be made. Three widely used methods will be summarized for the purpose of evaluating the accuracy of the results as well as some constraints inherent in each.

1. Actual Field Measurement

The volume of material which has been recharged or dewatered is calculated using the following equations:

$$\text{GW storage} = A \cdot \Delta h \cdot S_y \quad (3)$$

where

A = surface recharge area

Δh = water-table fluctuation

S_y = specific yield

The recharge area is 376,640 acres. The average water-table fluctuation is ten feet and is derived from maximum and minimum depths to the water-table using the 1977

contour map. The specific yield for the upper twenty-five feet of the aquifer was estimated to be twenty percent based on lithologic characteristics. Therefore the annual ground-water storage will be

$$376,640 \text{ acre} \times 10 \text{ ft} \times .20 = 753,280 \text{ acre-ft}$$

$$\approx 753,000 \text{ acre-ft.}$$

When the storage is spreaded over the study area (376,640 acres) the ground-water storage will be two feet of water ($753,280 \div 376,640 = 2$). Estimates of natural recharge based on actual field measurement such as these will provide more realistic results than any of the other methods.

2. From Hydrologic Budget

The hydrologic budget is an accounting of all water that enters or leaves the area. The formulation of a hydrologic budget is essential for optimum development of water resource of an area. An expression for the hydrologic budget is given below (modified from Todd, 1959 and Kent, 1973).

$$\left[\begin{array}{l} \text{precipitation + surface} \\ \text{inflow + subsurface inflow} \\ \text{+ imported water + decrease} \\ \text{in ground-water storage +} \\ \text{decrease in surface storage} \end{array} \right] = \left[\begin{array}{l} \text{evapotranspiration + sur-} \\ \text{face outflow + subsurface} \\ \text{outflow + increase in} \\ \text{ground-water storage +} \\ \text{increase in surface stor-} \\ \text{age + exported water} \end{array} \right]$$

(4)

The difference between sub-surface inflow and sub-surface outflow in the study area is assumed to be negligible. There is no imported and exported water and the change of the surface storage from May to August is also assumed negligible. Therefore, the equation for the hydrologic budget for the periods can be written as follows:

$$\left[\begin{array}{l} \text{precipitation} \\ + \text{ surface inflow} \end{array} \right] = \left[\begin{array}{l} \text{evapotranspiration} + \\ \text{surface outflow} + \\ \text{change of ground-} \\ \text{water storage} \end{array} \right] \quad (5)$$

The records of river flow from discharge station (Figure 2) ground-water levels, rainfall, and evaporation have been analyzed to study the hydrologic budget of the area. The total May to August inflow and outflow of the two rivers Karotoya and Tangan, is given in Table IV for the year 1977.

TABLE IV

TOTAL SURFACE INFLOW AND OUTFLOW
OF RIVERS IN THE STUDY AREA

Streams	: Discharge :	May to August	
		Inflow,	Outflow,
	: Station :	: Acre - feet :	: Acre - feet
	: No. :		
Karotoya	: 140 :	894,000	:
	: 142 :		: 1,736,000
Tangan	: 285 :		: 265,000
Total		894,000	2,001,000

The average precipitation for the period May through August for the year 1977 has been computed from the daily records of the rainfall of five stations in the area (Figure 2). The pan evaporation data for the study area in the months of July and August are adjusted to be equivalent to evapotranspiration for these periods. The evapotranspiration for the months of May and June has been estimated using the Thornthwaite method (Thornthwaite, 1948). The total surface inflow and outflow, rainfall, evapotranspiration, and the change of ground-water level for the periods May through August are shown in Table V.

TABLE V

SUMMARY CHART OF THE SURFACE INFLOW AND OUTFLOW,
PRECIPITATION, EVAPOTRANSPIRATION, AND THE
CHANGE OF GROUNDWATER LEVEL FOR THE MONTHS
MAY TO AUGUST, 1977

Total surface inflow as of Table IV		:	Total surface outflow as of Table IV		:	Preci- : pitation:	Evapo- : transpi- : ration
Acre-ft	: Inches	:	Acre-ft	: Inches	:	Inches	: Inches
894,000	28.48	:	2,000,000	63.75	:	69.75	14.42

Note: Study area for the hydrologic budget = 376,640 acres

The change of ground-water storage is computed by substituting the values in Table VI to Equation (6) as

follows:

$$\begin{aligned}
 \text{GW storage} &= \text{precipitation} + \text{surface inflow} \\
 &\quad - \text{evapotranspiration} - \text{surface} \\
 &\quad \text{outflow} \qquad \qquad \qquad (7) \\
 &= 69.76 + 28.48 - 14.42 - 63.75 \\
 &= 20.07 \text{ inches} \approx 20 \text{ inches}
 \end{aligned}$$

using the computed change in ground-water storage, the ground-water recharge can be calculated from the following equation by Schicht and Walton (1962):

$$P_g = R_g + ET_g + U + \Delta S_g \qquad (8)$$

where

P_g = Ground-water recharge

R_g = Groundwater component (baseflow) to river
flow

ET_g = Groundwater evapotranspiration

U = Subsurface underflow

ΔS_g = Change in ground-water storage

The groundwater component (baseflow) to the river flows was adjusted using the separation method for river flow hydrographs. Estimated baseflow is 3.95 inches over the 3.77×10^5 acres study area comprising the river reach.

The component of evaporation (ET_g) from the ground-water table is included in the estimate of evapotranspiration. The change of subsurface inflow and outflow (U) is assumed to be negligible. Therefore by substituting the values of the change of ground-water storage and the

groundwater component (baseflow) to the river reach

ground-water component to streams to Equation (8), ground-water recharge of the area is calculated for the period May through August, 1977. Equation (8) can be rewritten as follows:

$$\begin{aligned} P_g &= R_g + \Delta S_g & (9) \\ &= 3.95 + 20.07 = 24 \text{ inches} \end{aligned}$$

3. Baseflow Recession

Baseflow represents withdrawal of ground-water from aquifer storage after ground-water recharge has ceased. If the logarithm of river discharge is plotted against time, a linear relationship between the two variables may be obtained for the recession period after peak discharge has occurred. A "best fit" line can be used for the ground-water recession portion of the river hydrograph. Hydrographs for two successive years, 1976-78 are shown in Figures 17, 18, 19, and 20 for the Tangan and Karotoya Rivers. The recession curve which represents baseflow, has been separated from the other runoff components by a linear "best fit" line. The total potential ground-water discharge into the river Q_{tp} , is the amount indicated by the recession line (Mayboom, 1961). The value of Q_{tp} is found from the following relation:

$$Q_{tp} = \frac{Q_0 t_1}{2.3} \quad (10)$$

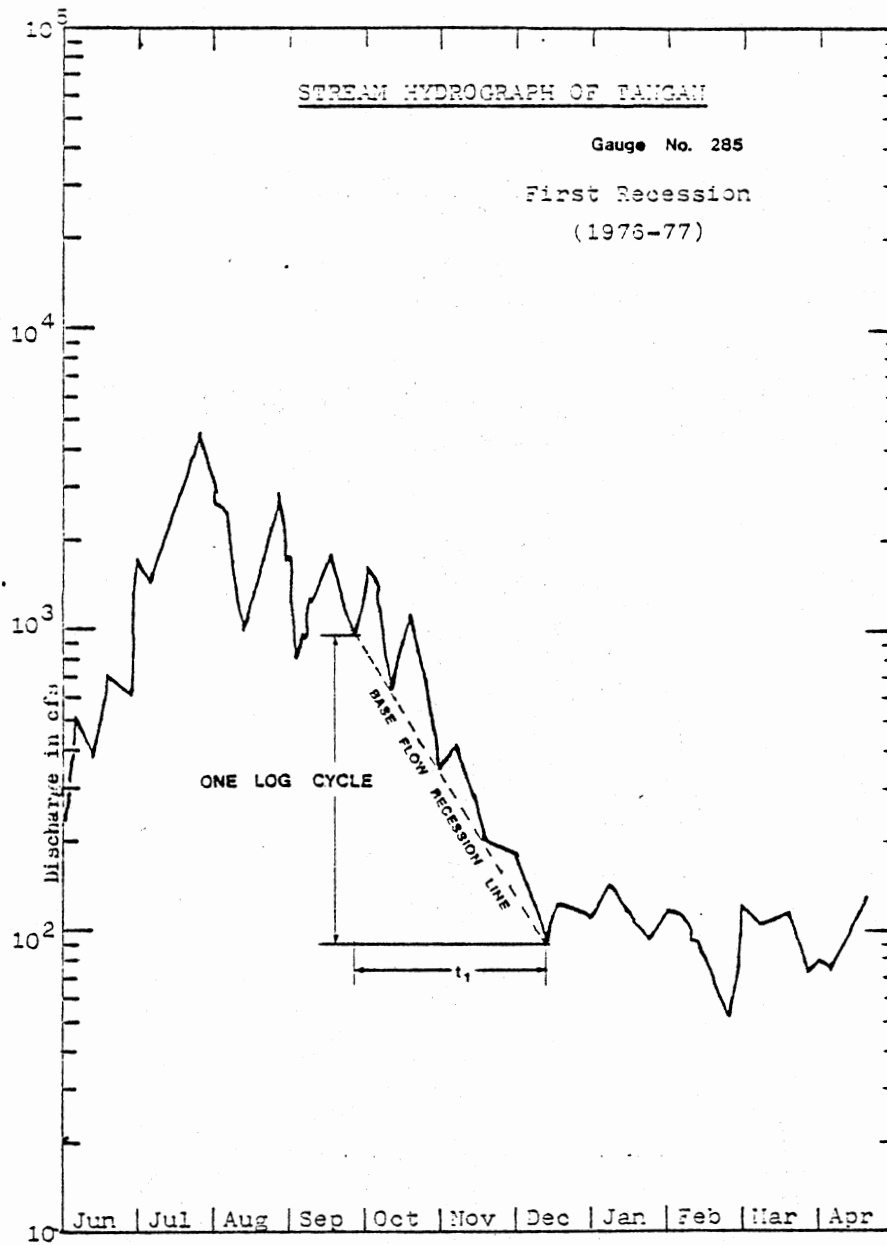


Figure 17. Stream Hydrograph of Tangan
(1976-77)

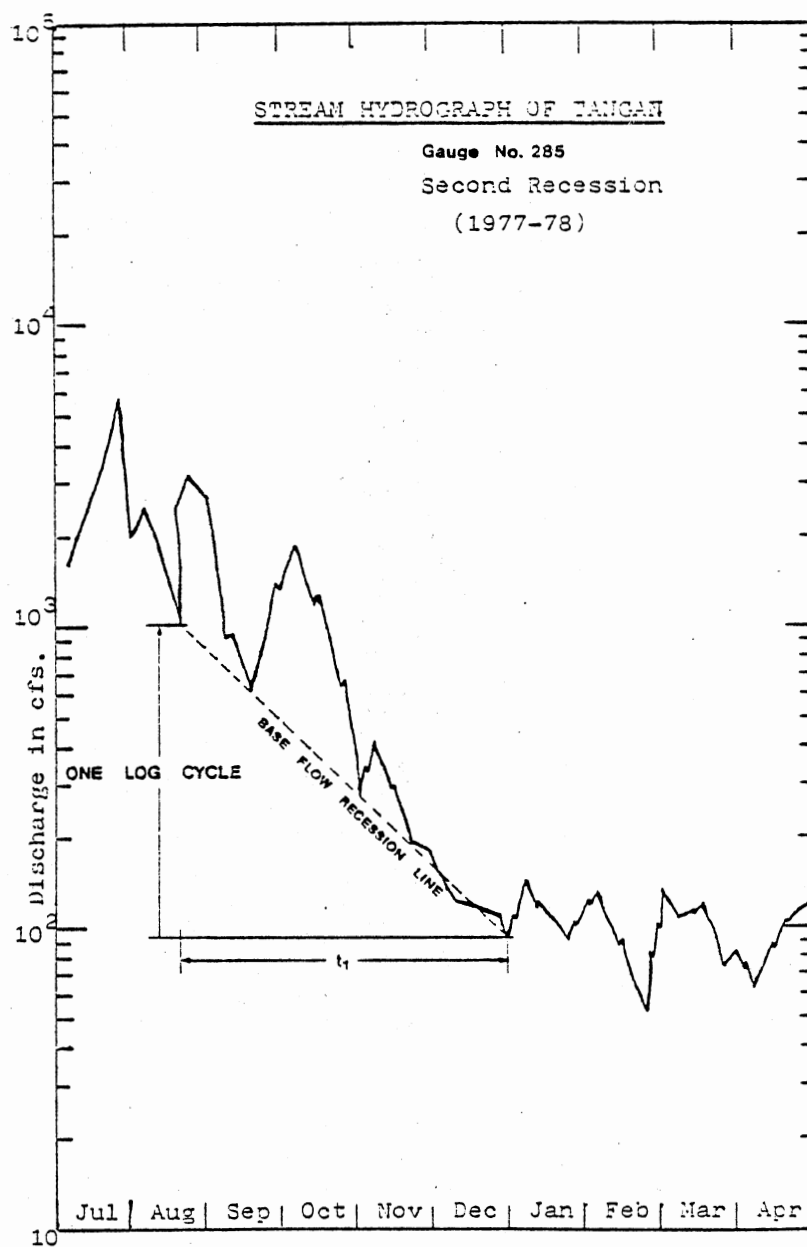


Figure 18. Stream Hydrograph of Tangan
(1977-78)

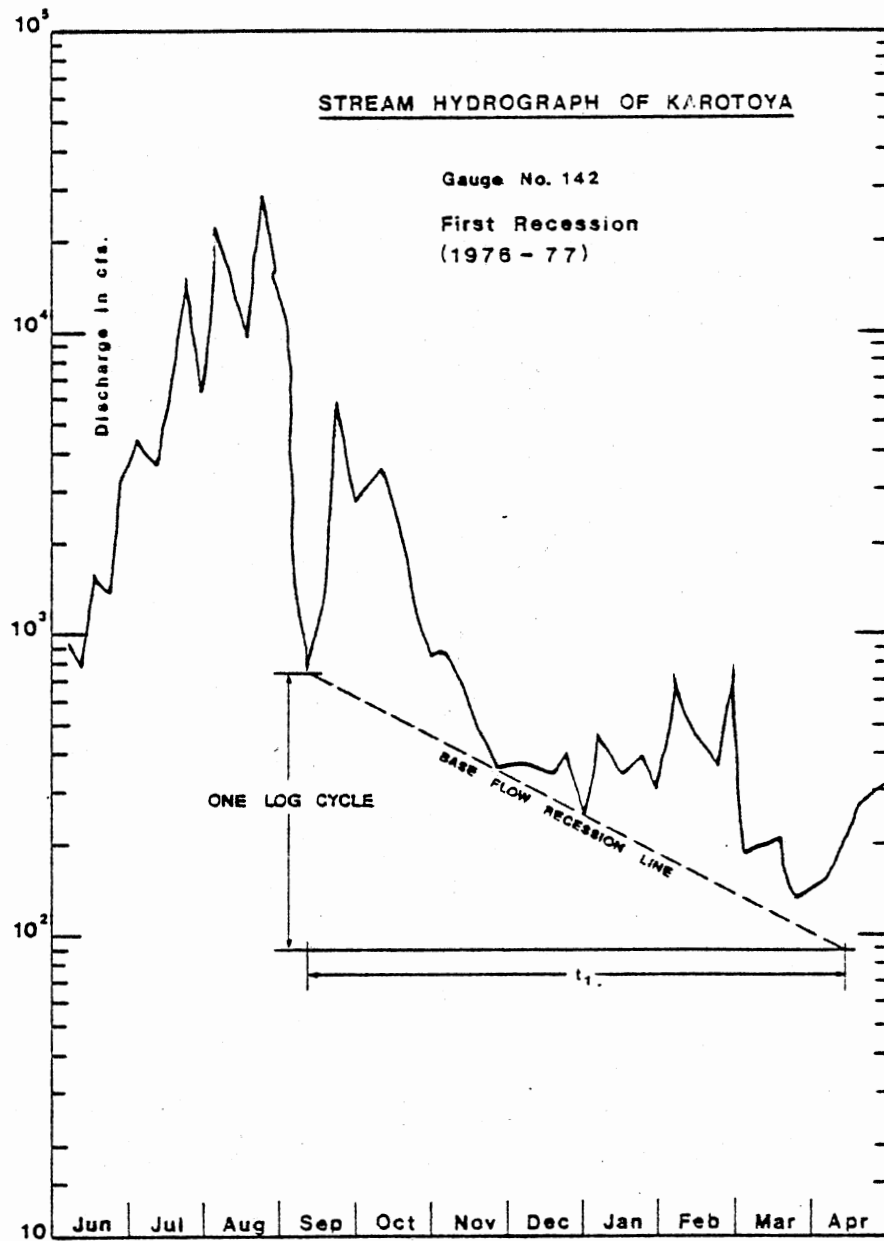


Figure 19. Stream Hydrograph of Karotoya
(1976-77)

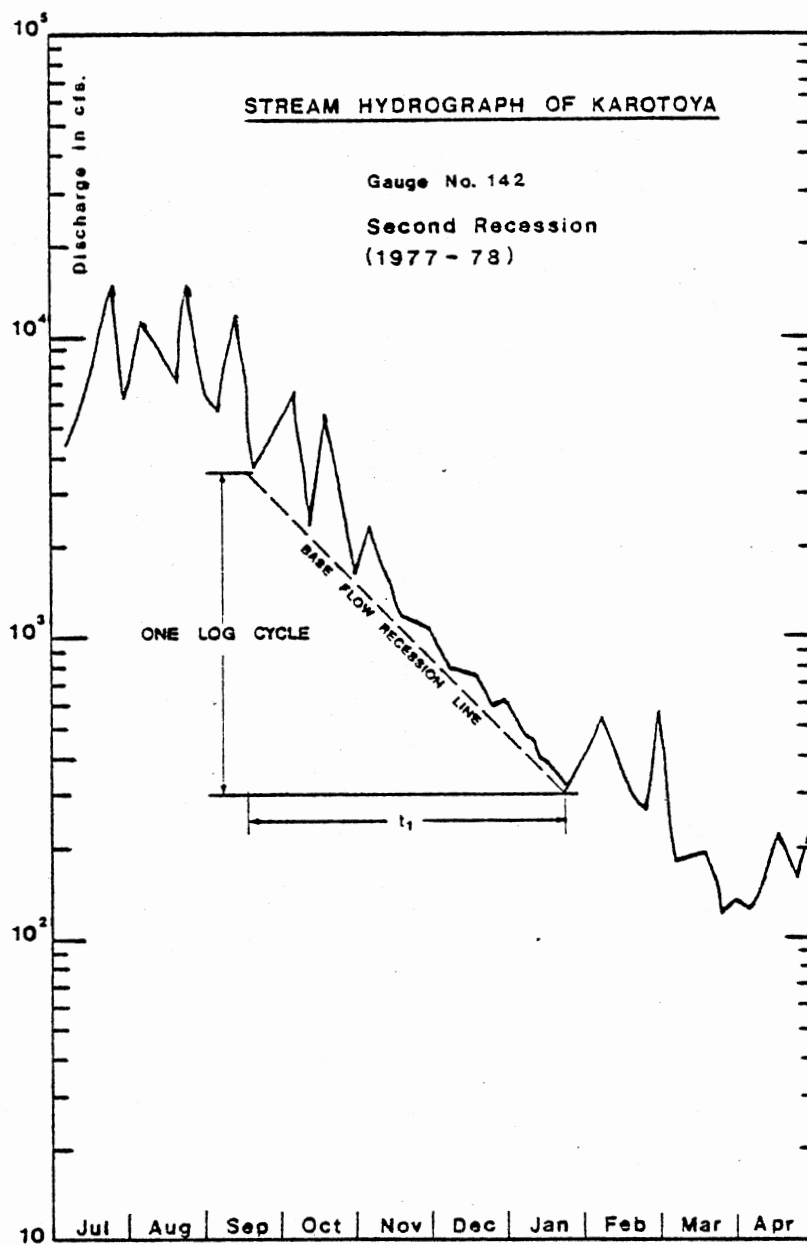


Figure 20. Stream Hydrograph of Karotoya
(1977-78)

where

Q_0 is the baseflow at the start of the recession

t_1 is the time it takes for the baseflow to go

from Q_0 to $0.1Q_0$.

The remaining potential ground-water discharge Q_t can be found from

$$Q_t = \frac{Q_{tp}}{10^{(t/t_1)}} \quad (11)$$

The amount of potential baseflow, Q_t , remains for a period t , after the start of a baseflow recession. The difference between the total potential ground-water discharge at the beginning of a baseflow recession period and the remaining potential ground-water discharge at the end of preceding baseflow recession period is a measure of ground-water recharge.

Ground-water discharge during the first recession period of the Tangan River hydrograph (Figure 17) is computed to be $900 \text{ ft}^3/\text{sec}$, Q_0 , and it takes approximately three months for the discharge to reach $0.1Q_0$ (one log cycle). The total potential discharge is calculated from Equation (10).

$$\begin{aligned} Q_{tp} &= \frac{Q_0 t_1}{2.3} \\ &= (900 \text{ ft}^3/\text{sec} \times 3 \text{ months} \times 30 \text{ days/month} \\ &\quad \times 86,400 \text{ sec/day})/2.3 \end{aligned}$$

or $Q_{tp} = 3.04 \times 10^9 \text{ ft}^3$

The value of Q_t at the end of recession which lasts for 7.5 months, is

$$Q_t = \frac{Q_{tp}}{10^{(t/t_1)}} = \frac{3.04 \times 10^9}{10^{(7.5/3)}} = 9.61 \times 10^6 \text{ ft}^3$$

The value of Q_0 or next year's recession (2nd recession) period as shown in Figure 18 is $1100 \text{ ft}^3/\text{sec}$, and t_1 is again 4.5 months. Therefore,

$$\begin{aligned} Q_{tp} &= \frac{1100 \text{ ft}^3/\text{sec} \times 4.5 \times 30 \times 86,400}{2.3} \\ &= 5.58 \times 10^9 \text{ ft}^3 \end{aligned}$$

The amount of recharge is equal to the total potential baseflow remaining at the end of the first baseflow recession subtracted from Q_{tp} for the beginning of the next recession:

$$\begin{aligned} \text{Recharge} &= 5.58 \times 10^9 - 3.04 \times 10^6 \\ &= 5.57 \times 10^9 \text{ ft}^3 \end{aligned}$$

Similarly, the recharge, calculated from the baseflow recessions of the Karotoya River hydrograph in Figures 19 and 20, is $2.05 \times 10^{10} \text{ ft}^3$. Therefore, the total recharge on the basin is

$$5.57 \times 10^9 + 2.05 \times 10^{10} = 2.60 \times 10^{10} \text{ ft}^3$$

This quantity represents approximately 19 inches of recharge in the 1977 year over the 588 square miles aquifer area. The result is comparable to results calculated by the former two methods. By comparing the results

of the three methods as shown in Table VI, 24 inches of recharge can be considered as a representative annual ground-water recharge of the study area. Therefore, the recharge from deep percolation of precipitation is estimated to be 27.87 percent of total weighted annual rainfall of 86.11 inches ($24 \times 100/86.11 = 27.87\%$).

It is already stated as well as noted on the well hydrographs that the recharge may not occur during the months of August through September because the water table lies very close to the land surface. The recharge of the ground-water reservoir could be increased if the ground-water table was lowered by an additional ten to fifteen feet due to the withdrawal of ground-water in the dry season. Accordingly, the ground-water table would rise again to the same elevation in the months of September and October during normal years of rainfall.

Coefficient of Permeability

The hydraulic properties of the aquifer are needed as input to the model. This can be obtained accurately by using aquifer tests. Accuracy of results depends largely on how accurate and purposeful the pumping test data are and how closely the real aquifer resembles the ideal mathematical model on which all the equations of flow to wells depend. Many equations of flow to a pumping well are available in the literature and all of these equations

TABLE VI
COMPARABLE RESULTS OF ANNUAL RECHARGE
FROM DIFFERENT METHODS

Methods	Results (in/yr)
1. Field measurements	24
2. Hydrologic budget	24
3. Baseflow recession from river discharge hydrograph	19

Note: 24 inches/year recharge was considered in
the model.

are based on ideal mathematical models. But in nature, it is rarely found that an aquifer satisfies all the conditions of an ideal mathematical model, and moreover, sometimes data are inadequate and are not being collected in a planned way to fit them in a certain mathematical model. The selection of any given flow system model to represent the field conditions is, therefore, a matter of judgment left to the analyst, who must be aware of the geohydrologic boundaries of the aquifer in order to obtain accurate results as far as practicable.

In the study area, 266 wells have been drilled for irrigation, but practically no systematic and purposeful aquifer test was done in order to determine aquifer characteristics more precisely. Moreover, the thickness of the aquifer is not yet ascertained which complicates the situation still further. An attempt was made to analyze the data in several ways using several mathematical solutions which approximate field conditions.

1. Theim Method of Determining "T"

The transmissivity can be determined from the discharge and drawdown of the pumped well by the Theim equation assuming steady state was reached. Seventy representative wells of the 266 irrigation wells were selected in the entire study area to determine transmissivity. Johnson and others (1966) present the Theim equation as

follows:

$$T = \frac{527.7 Q}{S_w} \text{Log} \frac{r_e}{r_w} \quad (12)$$

where

Q = discharge in gallons per minute

T = transmissivity in gallons per day per ft

r_e = radius of influence which is assumed 1000 ft

r_w = well effective radius (0.83 ft)

$$S_w = S_{wp} - CQ^2$$

where S_w is the drawdown without loss

S_{wp} = observed drawdown (ft) in pumping well

C = constant for entrance loss which is estimated for average value of 0.5

Q = discharge in cfs

The values of S_w for ten selected wells are listed as examples in Column 6 of Table VII. Finally, Equation (12) has been reduced to

$$T = 1625 \times \frac{Q}{S_w} \quad (13)$$

where

Q/S_w is the specific capacity of the well

From this relationship, "T" and "K" have been computed for all 70 wells, 10 of which are shown in Table VII. The permeability "K" has been computed by dividing the "T" values calculated for all 70 wells with the saturated thickness of the well. The average "K" values range between

TABLE VII

HYDRAULIC PROPERTIES OF THE AQUIFER
 COMPUTED FROM THE DEVELOPMENT
 TEST DATA OF THE WELLS

Well No.	Aquifer thickness, (ft)	Static water level in well before pumping, (ft)	Drawdown, (ft)	Computed drawdown, (ft)	Depth to pumping level, (ft)	Drawdown per cfs, (ft)	Specific capacity, US gal/ft ² /minute	Transmissivity, US gal/ft/day	Coeff. of permeability, $\frac{gpd}{ft^2}$	Remarks
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)
HAK-E-28	250	8.33	16.46	14.66	27.82	5.49	91.81	149,000	596	Discharge
HAK-E-284	210	10.33	17.09	15.29	29.42	5.70	88.10	143,000	681	of
H - 74	180	7.60	19.79	17.99	27.08	6.60	74.87	122,000	678	each well
H - 76	275	5.67	25.74	13.94	32.67	8.58	96.62	157,000	571	is 3 cfs
H - 67	200	7.60	18.54	16.74	25.54	6.18	80.46	131,000	655	
H - 81	280	6.00	14.63	12.83	20.92	4.88	104.98	179,000	639	
H - 33	200	6.00	17.47	15.67	23.83	5.82	85.96	140,000	700	
H - 34	295	6.25	19.64	12.84	26.50	6.54	104.90	170,000	576	
H - 138	180	7.58	21.83	19.03	29.50	7.28	70.78	123,000	683	
H - 200	250	5.25	15.58	13.78	18.92	5.19	90.75	147,000	588	

500 and 680 gal/day/ft².

It is already stated that due to limited available data within the study area, the coefficient of permeability and transmissivity for this entire area could not be furnished directly. Therefore, another method was used to generate the coefficient of permeability and to distribute these values over the entire study area. Information related to thickness and lithology of the Piedmont deposit were obtained from drillers log in the study area. A number of Driller's Logs have been analyzed and frequency of occurrence of various types of materials is shown in Table VIII. The estimate based on the average percentage of occurrence for each class of material within a stated depth interval. The lithology was divided into 4 ranges: range one was associated with silt and clay; range two was very fine to fine sand; range three was medium to coarse sand; and range four was associated with coarse sand and gravel. A weighted average permeability was introduced by multiplying a weighting factor for the four grain size ranges by the percentage of the total saturated thickness which each range represents and finally is summed. The permeability values used for each range was obtained from the coefficient of permeability-grain size envelope developed by Kent et al. (1973) as shown in Figure 21. The ranges were chosen to represent various median grain sizes which correspond to the average

TABLE VIII
 FREQUENCIES OF OCCURRENCES OF AQUIFER MATERIAL

Depth Interval (ft)	Material Percentage				
	Clay Percent	Silt Percent	Fine Sand Percent	Medium to Coarse Percent	Gravel Percent
10- 20	40	0	30	25	2
20- 40	16	0	28	55	1
40- 70	16	0	17	61	6
70-100	10	0	15	68	7
100-130	7	0	12	74	7
130-160	8	0	10	78	4
160-180	13	0	19	68	0
180-250	16	0	15	69	0

Note: Percentages are averages based on data from 70 well logs.

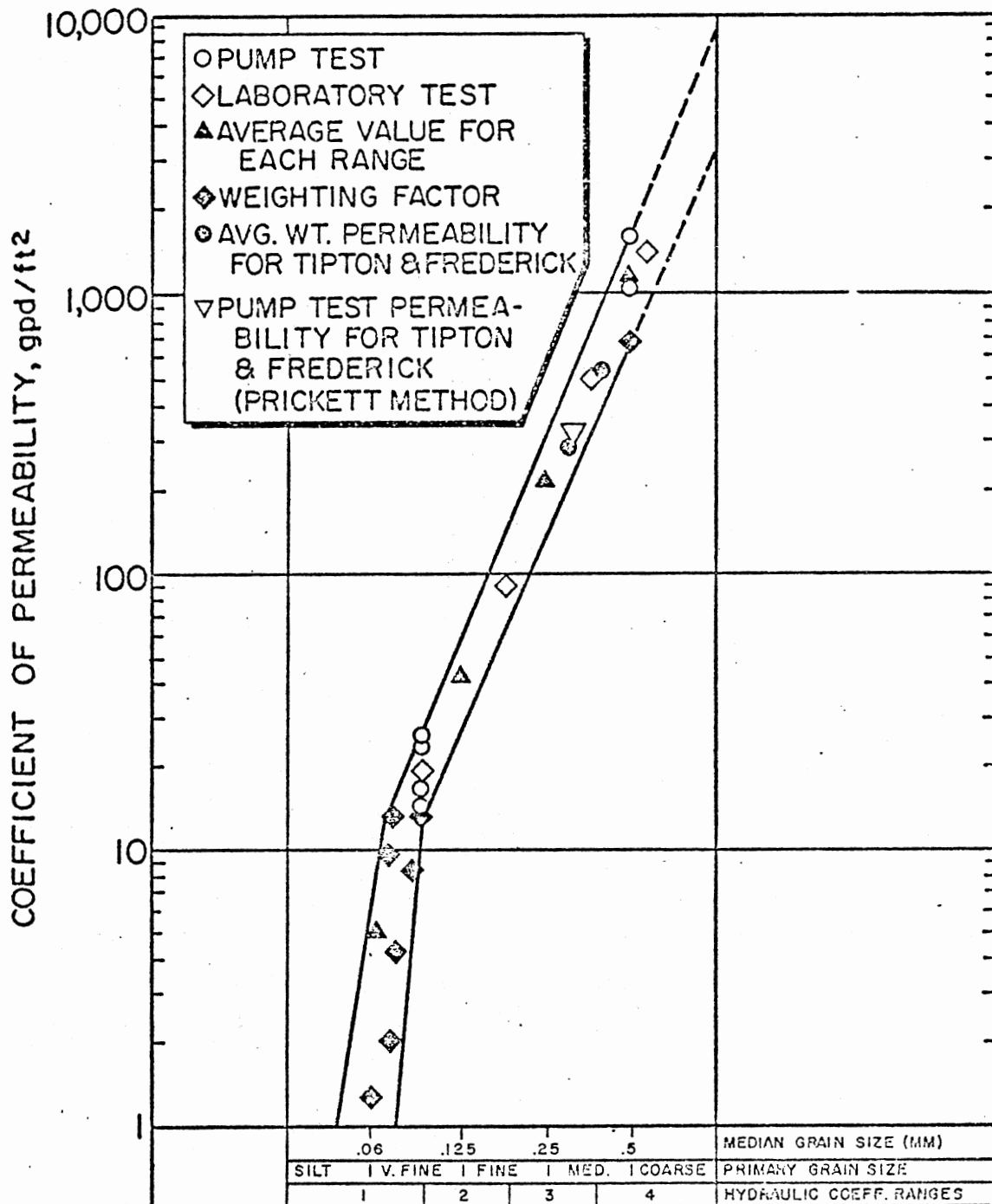


Figure 21. Coefficient of Permeability Vs. Grain Size Envelope (After Kent)

coefficient of permeability for each range as shown in Figure 21. Weighted average permeabilities were computed by this method for all available wells within the area and are shown in Table IX.

To supplement the permeability data and to verify computed values, the results of a long term aquifer test in the area were analyzed using various methods including the Jacob, Boulton, Hantush, and Pricket methods. The Pricket type curve is shown in Figure 22. The methods and the results are given in Tables X, XI, XII and corresponding Figures 23, 24, 25, and 26. These techniques were designed for aquifer tests conducted under varying groundwater conditions including consideration of delayed drainage due to gravity. Permeability coefficients from 520 to 576 gallons per day per foot squared are obtained from the above results. These results compare favorably with the weighted average of 588 gallons per day per foot squared (see Table IX) using the permeability envelope in Figure 21 and samples obtained from the same well. The favorable correlation was considered to be justification for using the permeability grain size envelope to determine an average permeability for each driller's log.

Specific Yield

It is anticipated that on the basis of the geology in the study area, the effective specific yield will

TABLE IX
WEIGHTED AVERAGE PERMEABILITY FOR
KOCHABARI WELL AND OTHER
WELLS IN STUDY AREA

Kochabari Well				
Range	: Layer Per- meability, (gpd/ft ²)	: Saturated Interval thickness, (ft)	: Percentage of total thickness	: Weighting of permea- bility co- efficient, (gpd/ft ²)
1	: 15	: 13	: 5	: 0.75
2	: 80	: 73	: 26	: 20.80
3	: 300	: 109	: 39	: 117
4	: 1500	: 85	: 30	: 450
				588.55

(K) Average weighted permeability

All other available Driller's log in the study area				
Range	: Layer Per- meability, (gpd/ft ²)	: Saturated Interval thickness, (ft)	: Percentage of total thickness	: Weighting of permea- bility co- efficient, (gpd/ft ²)
1	: 15	: 509	: 11	: 1.65
2	: 80	: 330	: 7	: 5.6
3	: 300	: 2468	: 54	: 162.0
4	: 1500	: 1283	: 28	: 420.0
				589.25

(K) Average weighted permeability

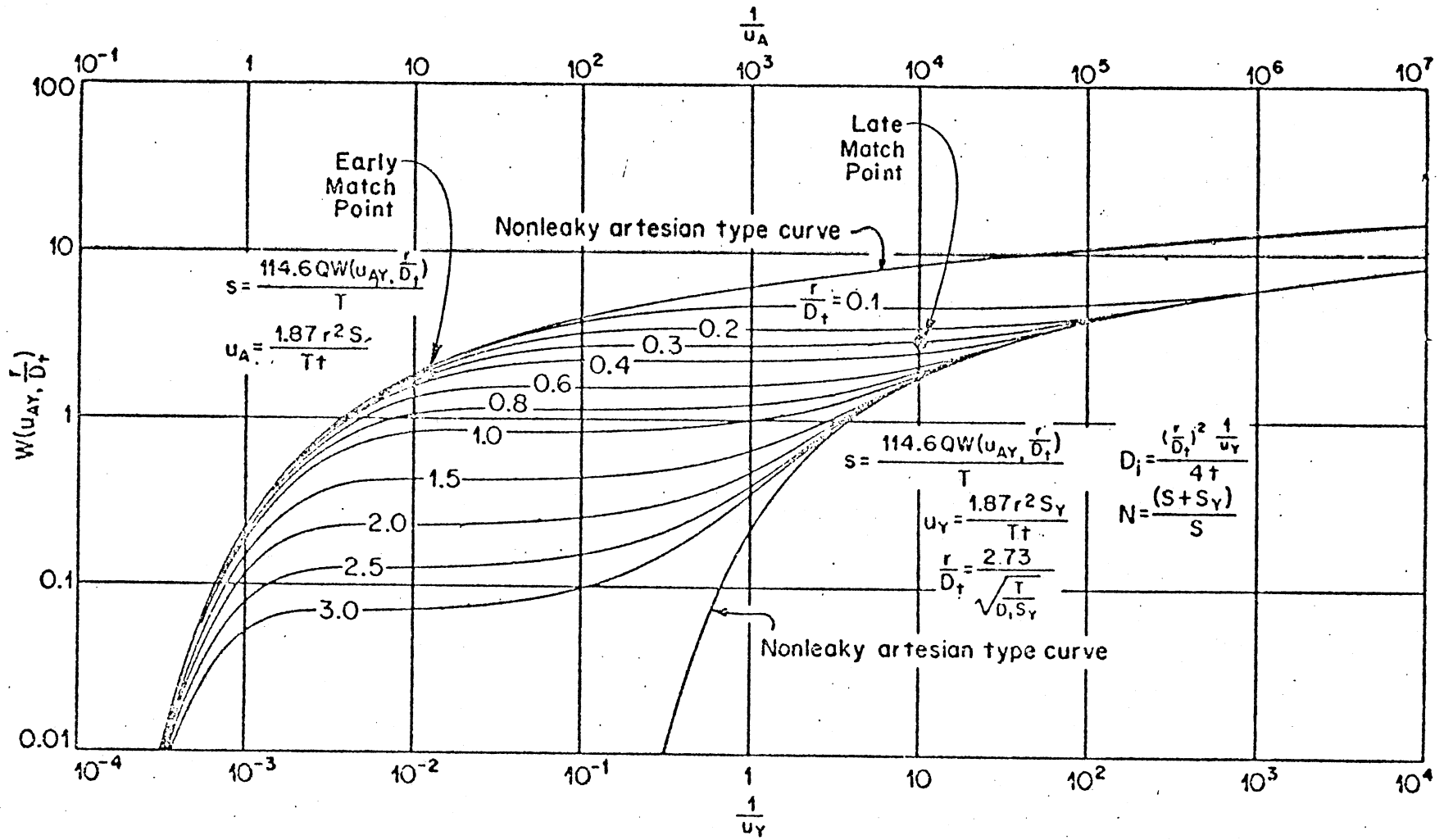


Figure 22. Prickett's Time-Drawdown Type Curve

TABLE X

PUMP TEST RESULT USING PRICKETT FOR
KOCHABARI OBSERVATION WELL #1

Saturated thickness = 250 ft	Q = 1600 gpm
	r = 50 ft

Early match point

$$W(U_A \cdot \frac{r}{D_t}) = 3.5$$

$$S = 4.5 \text{ ft}$$

$$t = 2.7 \text{ minutes}$$

$$T = \frac{114.6 Q}{S} (W_{U_A} \cdot \frac{r}{D_t})$$

$$K = \frac{T}{\text{Saturated thickness}}$$

$$T = \frac{(114.6)(1600)}{4.5} (3.5)$$

$$K = \frac{142,613}{250}$$

$$T = 142,613 \text{ gpd/ft}$$

$$K = 571 \text{ gpd/ft}^2$$

Late match point

$$W(U_y \cdot \frac{r}{D_t}) = 5.5$$

$$S = 7 \text{ ft}$$

$$t = 11 \text{ minutes}$$

$$T = \frac{114.6 Q}{S} (W_{U_y} \cdot \frac{r}{D_t})$$

$$K = \frac{T}{\text{Saturated thickness}}$$

$$T = \frac{(114.6)(1600)}{7} (5.5)$$

$$K = \frac{144069}{250}$$

$$T = 144069 \text{ gpd/ft}$$

$$K = 576 \text{ gpd/ft}^2$$

PRICKETT METHOD PLOTTING

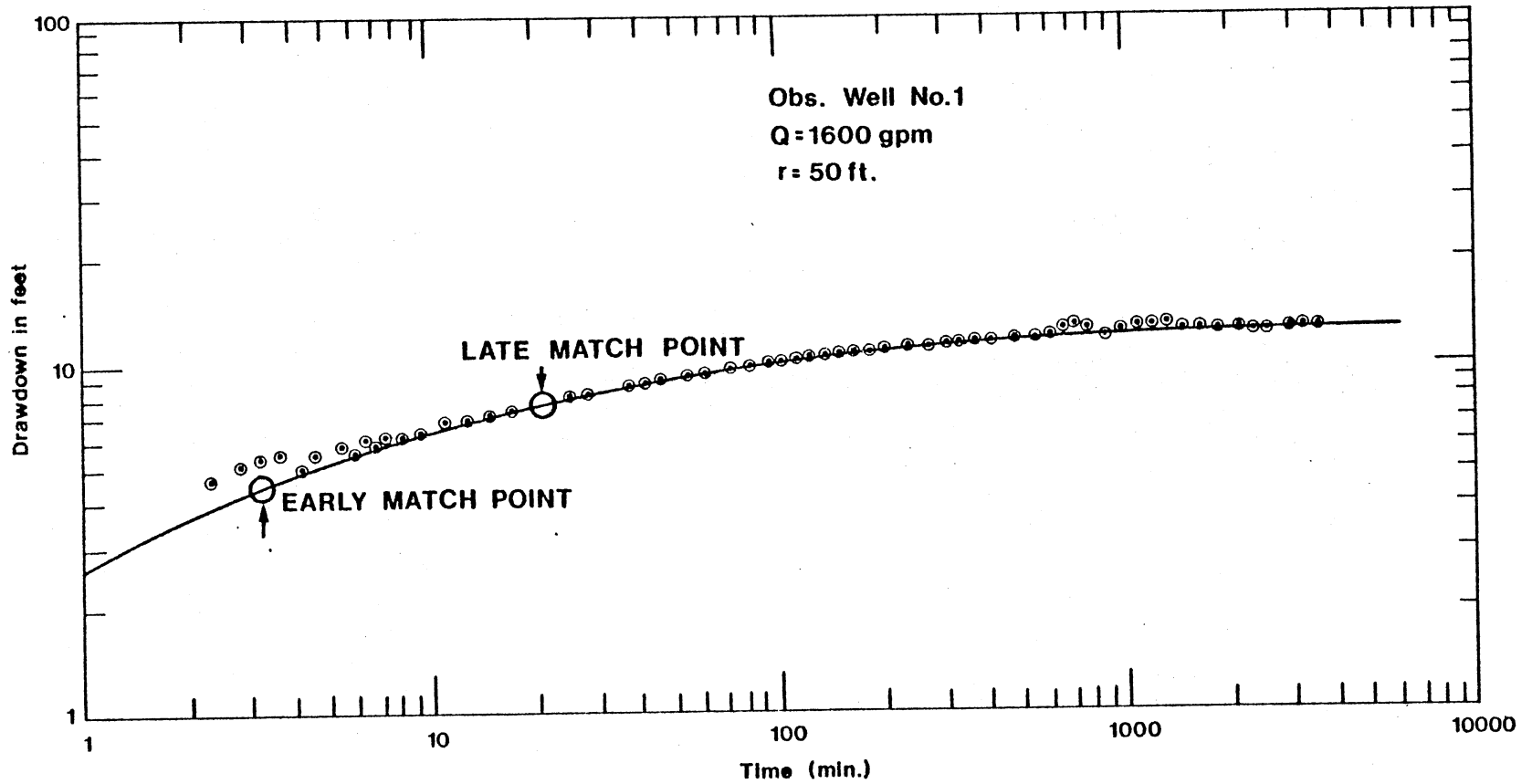


Figure 23. Prickett's Pump Test Time - Drawdown Graphs

TABLE XI

CALCULATION OF TRANSMISSIVITY "T" FOR
OBSERVATION WELL #1 USING HANTUSH
MODIFIED METHOD AND JACOB METHOD

$$Q = 1600 \text{ gpm}$$

$$r = 50 \text{ ft}$$

$$\text{Saturated thickness} = 250 \text{ ft}$$

Hantush Method

$$T = \frac{Q}{4\pi S} H(U,B)$$

$$H(U,B) = 7.8$$

$$T = \frac{1600 \times 7.8 \times 1440}{4 \times 3.142 \times 11 \times 7.78}$$

$$S = 11 \text{ ft}$$

$$T = 17,379 \text{ ft}^2/\text{day}$$

$$t = 150 \text{ minutes}$$

$$T = 129,993 \text{ gpd/day}$$

$$K = \frac{T}{\text{Sat. thickness}}$$

$$K = 520 \text{ gpd/ft}^2$$

Jacob Method

$$Q = 1600 \text{ gpm}$$

$$S = 3 \text{ ft}$$

$$T = \frac{264 Q}{S}$$

$$K = \frac{140800}{250}$$

$$T = \frac{264 \times 1600}{3}$$

$$K = 563 \text{ gpd/ft}^2$$

$$T = 140,800 \text{ gpd/ft}$$

HANTUSH MODIFIED
METHOD PLOT

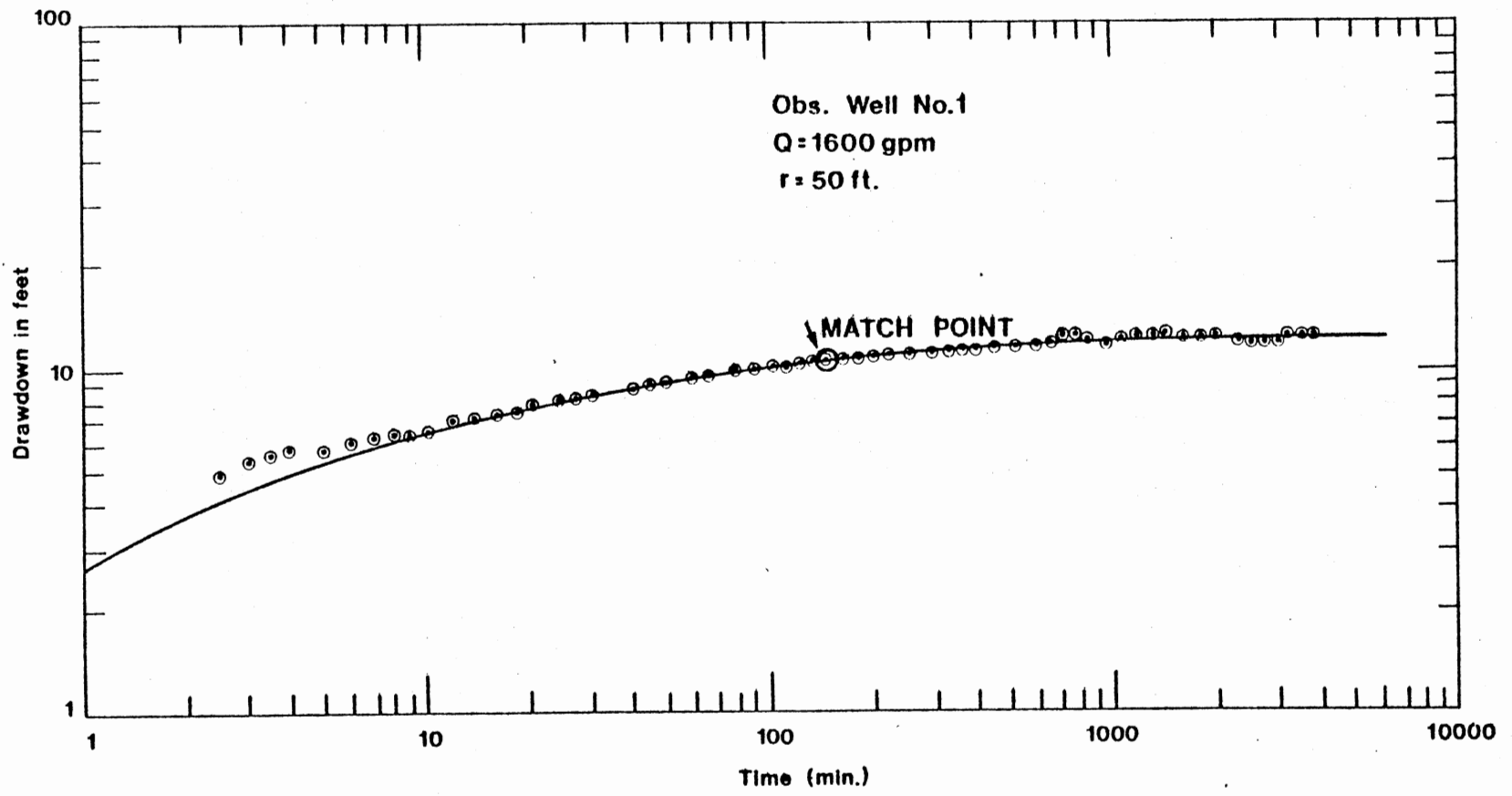


Figure 24. Hantush's Pump Test, Time-Drawdown Graph

JACOB PLOT

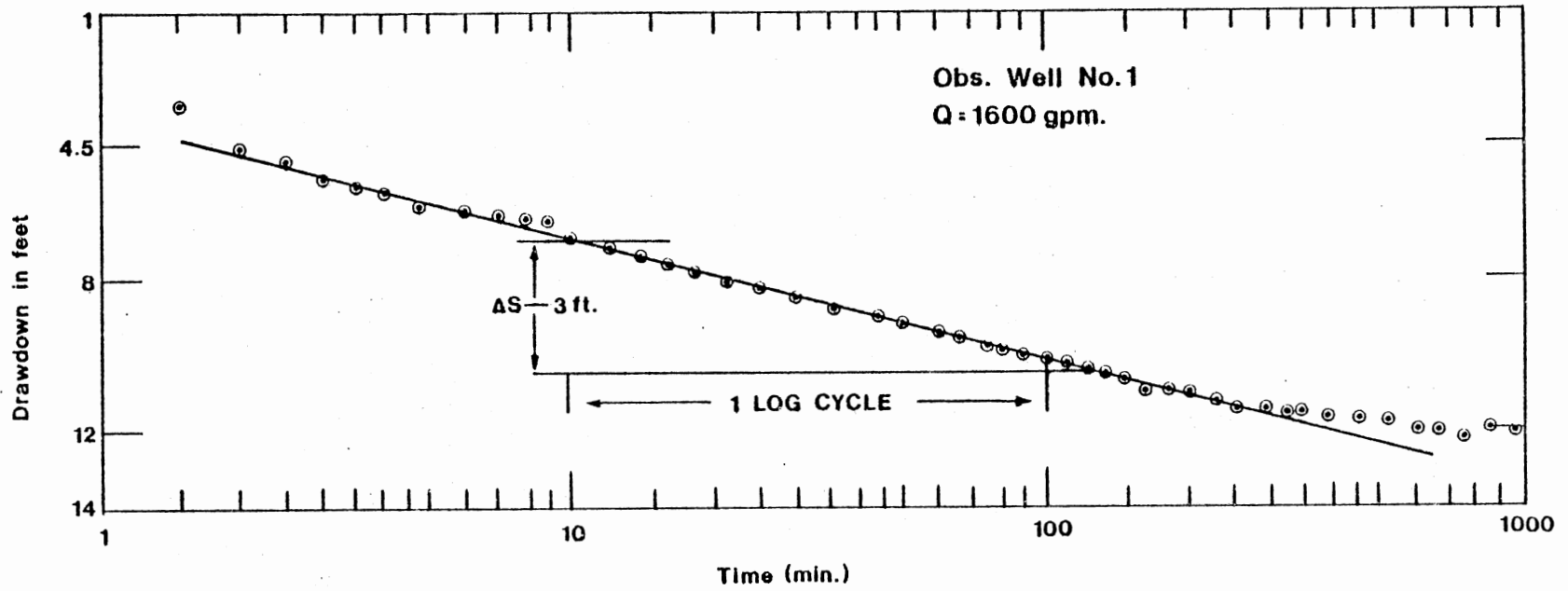


Figure 25. Jacob's Pump Test, Time-Drawdown Graph

TABLE XII

CALCULATION OF TRANSMISSIVITY "T"
FOR OBSERVATION WELL NO. 1 USING
BOULTON - THEIS METHOD

Saturated thickness = 250 ft

Q = 3.56 cfs

r = 50 ft

Early match point

$$W(U_A, \frac{r}{B}) = 6.7$$

$$S = 8.8 \text{ ft}$$

$$\frac{t}{r^2} = 0.011$$

$$T = \frac{Q}{4\lambda S} W(U_A, \frac{r}{B})$$

$$K = \frac{T}{\text{Saturated thickness}}$$

$$T = \frac{(3.56)}{4 \times 3.142 \times 8.8} (6.7)$$

$$K = \frac{139595}{250}$$

$$T = 0.216 \text{ ft}^2/\text{sec}$$

$$K = 558 \text{ gpd/ft}^2$$

$$T = 139,595 \text{ gpd/ft}$$

Late match point

$$W(U_y, \frac{r}{B}) = 8.6$$

$$S = 11.5 \text{ ft}$$

$$\frac{t}{r^2} = 0.11$$

$$T = \frac{Q}{4\lambda S} W(U_y, \frac{r}{B})$$

$$K = \frac{T}{\text{Saturated thickness}}$$

$$T = \frac{3.56 \times 8.6}{4 \times 3.142 \times 11.5}$$

$$K = \frac{137656}{250}$$

$$T = 137,656 \text{ gpd/ft}$$

$$K = 551 \text{ gpd/ft}^2$$

BOULTON THEIS PLOT

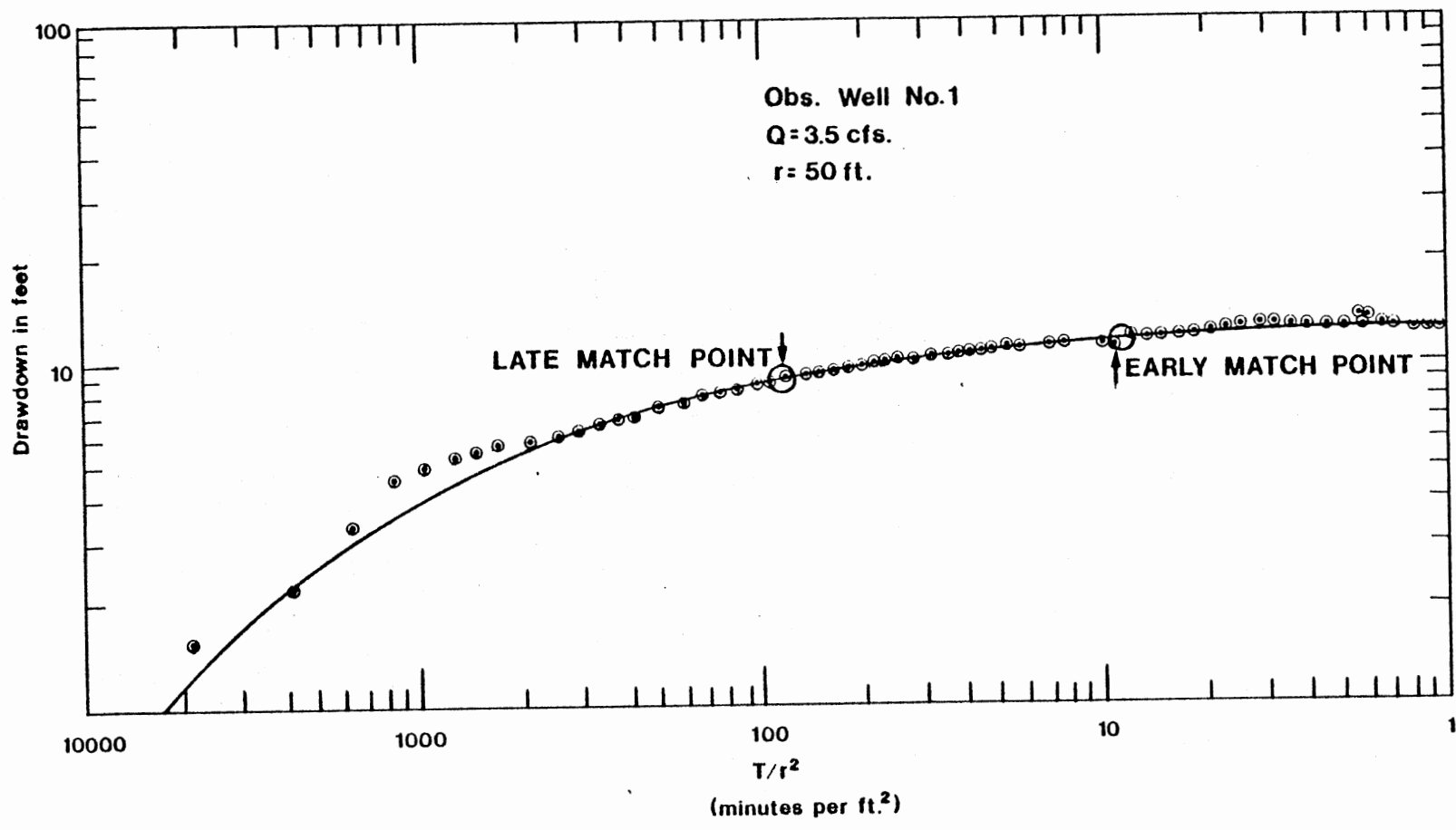


Figure 26. Boulton's Pump Test, Time-Drawdown Graph

positively correlate with lithologic type. Figure 27 illustrates representative lithologic types for unconsolidated sediments together with estimates of their associated specific yields, porosity and specific retention.

Direct methods of computing specific yield are either by hydrological balances over time or by longterm aquifer pumping tests with observation wells which frequently provide conflicting answers differing by several orders of magnitude. It has been noted by numerous observers that during longterm aquifer tests of the water-table aquifer, the rate of decline was not in accordance with the classical Theis non-equilibrium predictions. Boulton (1954) developed a semi-empirical mathematical model that regarded the water released from storage as the sum of two components: S , the volume of water instantaneously released by elastic compression of the aquifer, and S_y , the exponentially time varying drainable ground-water in storage that becomes quasi-constant after a finite time. It was noted by observers that this interpretation fitted the observed data fairly closely. Prickett (1965) attempted, with some success, to correlate Boulton's delay index with lithology. Walton (1970) and Dagan (1967) also observed that the calculated specific yield suggests that, apart from obvious lithological correlation, it varies both with time and the rate of water table decline (being a function of partially saturated flow).

RELATIONSHIP OF POROSITY AND SPECIFIC YIELD TO ROCK TYPE

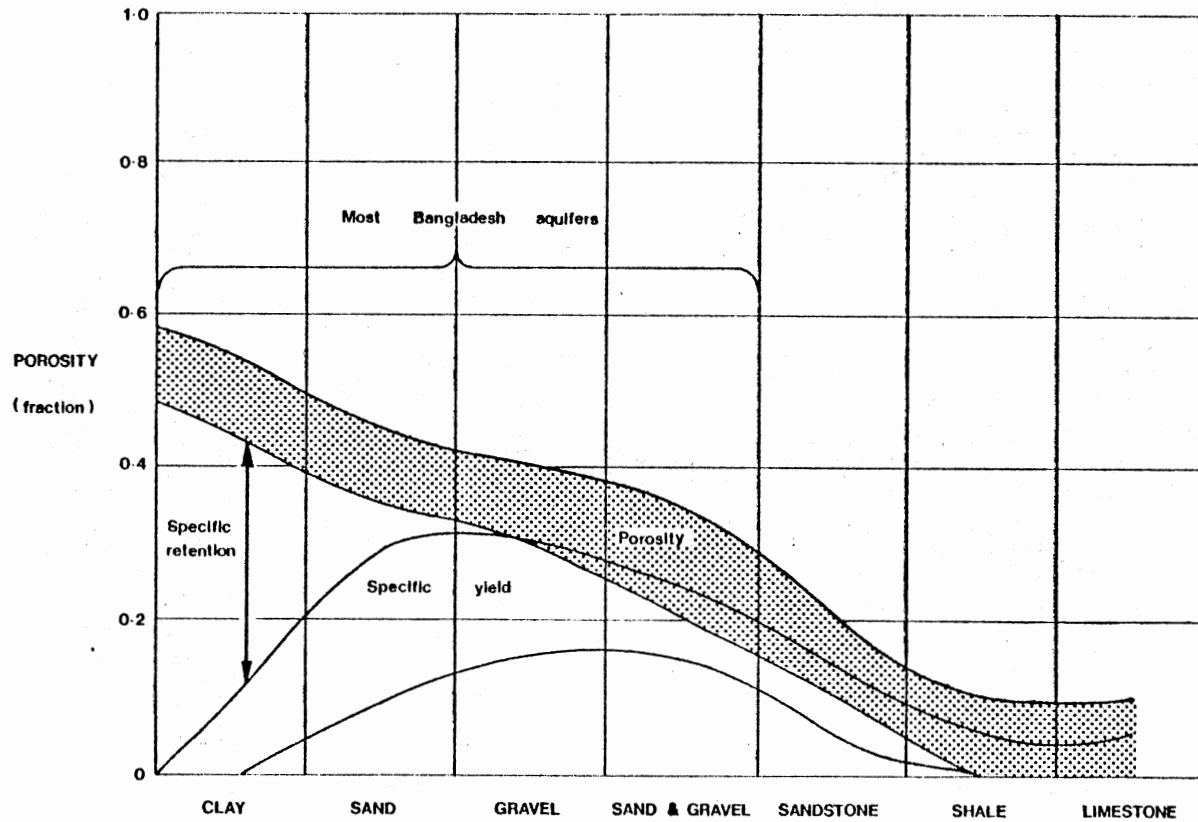


Figure 27. Relation of Specific Yields and Aquifer Materials

Hence specific yield evaluation from rising and falling water data of the project area must be conducted with some caution if realistic results are to be obtained. It is expected that analysis based on lithology will give good estimate of the specific yield over the depth dewatered. It has been noticed that the majority of unconfined aquifers are characterized by coarser sediments near the base. Thus, it is normal to have clays and silts at or near the surface with the aquifer material becoming coarser with depth. It is reasonable to expect that the specific yield will vary with sediment type, i.e., as the sediment becomes coarser with depth, the specific yield also increases with depth.

The graph shown in Figure 28 (after Johnson, 1967) was used to provide a relationship between median grain size and specific yield. The dominant grain sizes in Figure 21 were considered to be equivalent to the median grain sizes of the permeability envelope. The values of specific yield along with the corresponding permeability coefficient of the four ranges were plotted on semi-logarithmic paper to produce the relationship shown in Figure 29. Using this curve, the average specific yield in the study area was estimated to be 25 percent.

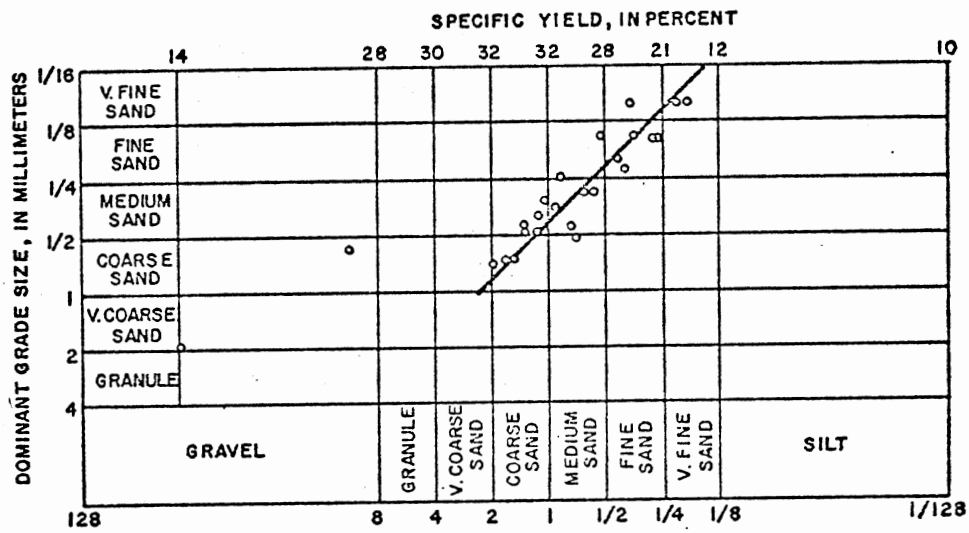


Figure 28. Specific Yield Vs. Grain Size

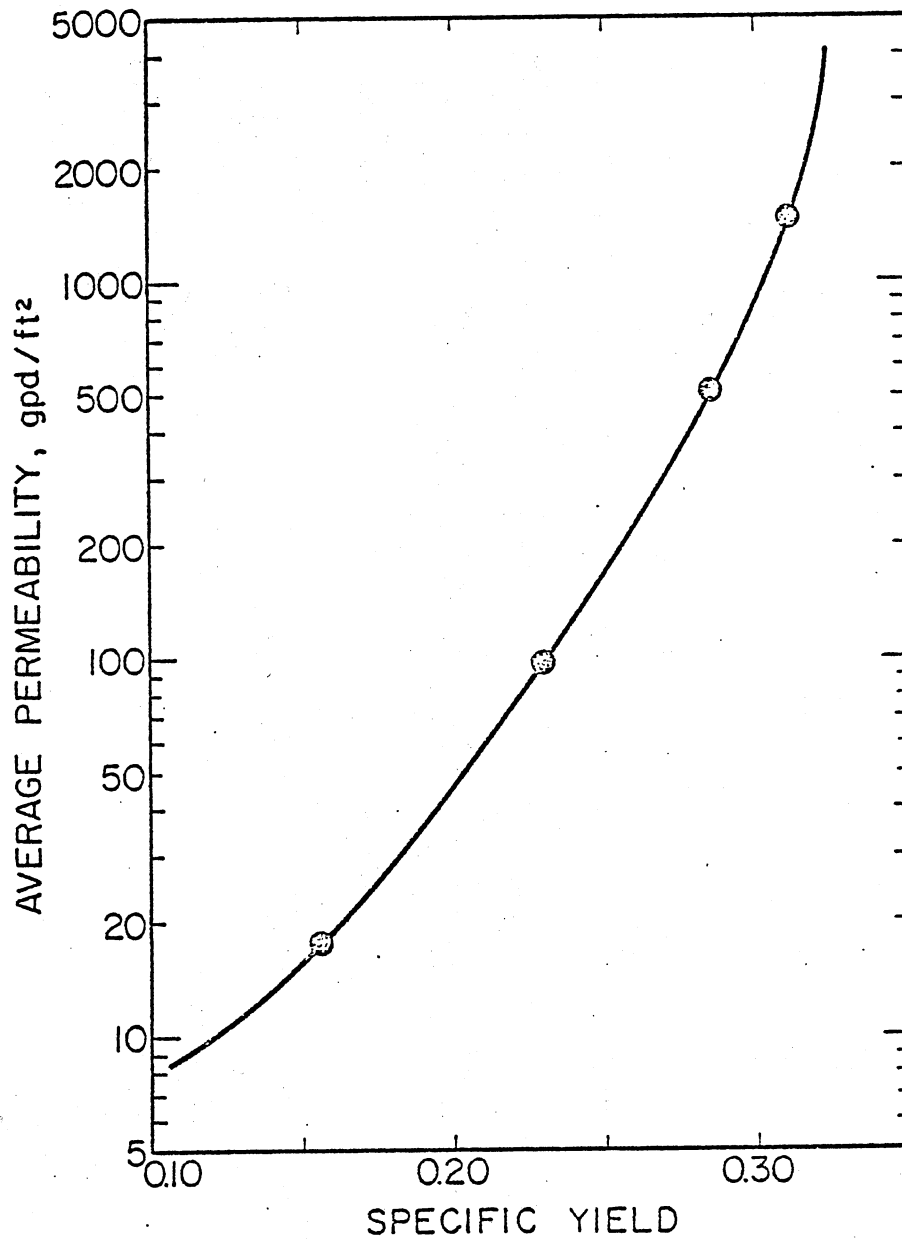


Figure 29. Specific Yield Vs. Coefficient of Permeability

Ground-water Quality

Ground-water quality must be considered in relation to rate of pumping and type of well completion in order to identify the modifying the insitu ground-water quality:

1. Possible public health hazards
2. Possible toxicity of irrigation water to plants
3. Alteration of soil zone physical properties due to ground-water use
4. Impairment of well performance due to corrosion and incrustation.

Chemical data for six wells are presented in Table XIII. Location of these wells are shown in Figure 2. The waters are of the bicarbonate type with cations of varying dominance are slightly alkaline, having a pH range of between 7 and 8. The total dissolved solids (TDS) concentration was generally low, having a value less than 250 mg/l. Most waters were undersaturated with respect to carbonate minerals, indicating propensity to dissolve soluble aquifer materials.

Sulfate was almost totally absent from the ground-water. This might be due to either the absence of sulfate source or to chemical reduction of available sulfate within the aquifer.

TABLE XIII
GROUNDWATER QUALITY ANALYSIS
(1976-77)

Well No.	Ca ⁺⁺ : mg/l	Mg ⁺⁺ : mg/l	Na ⁺ : mg/l	HCO ₃ ⁻ : mg/l	SO ₄ ⁻⁻ : mg/l	Cl ⁻ : mg/l	NO ₃ ⁻ : mg/l	Fe : mg/l	SiO ₂ : mg/l	TDS : mg/l	PH	SAR
1	25.0	22.9	4.2	116.0	0	8.0	T	0.25	36.0	201.6	7.9	6.85
2	26.0	9.0	34.9	130.0	T	11.0	n.d.	0.55	34.0	265.6	8.0	6.42
3	24.0	8.5	24.0	92.0	0	20.5	T	1.25	26.0	200.0	7.6	4.24
4	12.0	7.3	31.3	68.0	T	12.0	n.d.	0.27	33.5	151.6	7.7	2.83
5	17.0	7.3	30.4	88.0	T	5.5	T	0.15	35.5	204.2	7.65	2.57
6	18.0	7.3	31.0	88.0	0	7.0	T	0.55	36.5	160.0	8.0	8.51

T = trace

n.d. = not detected

The extensive use of irrigation could cause leaching of nitrate from fertilizers into the aquifer. This nitrate could pose a health hazard, especially since the people are drawing their drinking water from the top of the aquifer where the nitrates would enter.

CHAPTER VI

COMPUTER MODELING

Concept of Model

The rate of water level decline is the most important information for ground-water management in this study area. In particular, it is paramount to know how rapidly the water is being depleted, where and when the water level decline will seriously affect existing domestic shallow water supplies and what impacts alternative management practices will have on the system. Digital simulation offers a reliable means for evaluating the effects of various development alternatives on an aquifer system such as the Dinajpur Piedmont aquifer.

Obviously, it is impossible either to carry out experiments and tests in the aquifer itself in order to determine its response to various management alternatives proposed in the future or to make comparisons among responses to different possible alternatives in order to determine the most desirable one, according to some specified criteria. Whenever the treatment of real systems or phenomena is impossible or the cost of such treatment is prohibitive, models of the considered system or phenomena

are introduced. Instead of treating the real system, we manipulate its model and use the results of these manipulations in order to make decisions regarding the operations of the real system.

A simulation model is a simplification of a complex physical reality and the processes in it. There is no need to elaborate on the fact that most real systems, and certainly aquifer systems, are indeed complicated beyond our capability to describe them exactly as they are. Simplifications are necessary. They take the form of a set of assumptions which should be kept in mind whenever the model is being employed in the course of investigations. On the basis of these simplifying assumptions, a model of an investigated ground-water system is constructed.

Ground-water flow obeys a well defined set of physical laws which can be expressed mathematically. The equations are balance equations based on the principle of conservation of mass and Darcy's law. The mathematical equation describing the two dimensional ground-water flow through an areally extensive aquifer is given by the following partial differential equation (Bittinger and others, 1967):

$$\frac{\partial}{\partial x} K_b \frac{\partial H}{\partial x} + \frac{\partial}{\partial y} K_b \frac{\partial H}{\partial y} = S \frac{\partial H}{\partial t} + \frac{Q}{\Delta x \Delta y} \quad (14)$$

where

K = hydraulic conductivity (L/T)

(L) denotes units of length, (T) denotes units of time.

b = saturated thickness (L)

H = hydraulic head (L)

S = specific yield (dimensionless)

Q = net withdrawal flow (L^3/T)

$\Delta x \Delta y$ = incremental distances

t = time (T)

This equation is based on the continuity equation and Darcy's law and is consistent with the Dupuit assumptions. The Dupuit assumptions are (1) the velocity of ground-water flow is proportional to the slope of the hydraulic gradient and (2) the ground-water flow is horizontal and uniform every where in the vertical section (Todd, 1959). The above equation also assumes that both hydraulic conductivity and specific yield are isotropic and that the density of the fluid is constant in time and space.

The above equation has no general solution; therefore a finite difference approximation is used to allow a numerical solution with a digital computer. Applications of the finite difference approach requires subdivision of the study area into a system of finite grids or subregions. The differentials of the above equations can be approximated by first order finite difference expressions.

Characteristic values of all variables used in finite difference expressions are specified for each sub-region. These discrete values represent the value for the entire node.

One extremely versatile finite difference model has been developed by Trescott and Pinder (1973) and several problem options and input-output features have also been added. A modification of the 1974 version of this model has been used in this study. The computer methodology explains the steps used, as shown in Figure 3.

Data Input

Data input includes all data used in the model consisting of scalars, uniform matrices and non-uniform matrices. In addition, some matrices used by the program were generated from other matrix input. The scalar and uniform data were entered directly into the model. The matrix data were digitized and assigned to each node using an interactive data entry program running under IBM 370 TSO. Values were required for the following program variables:

A. Scalars

1. Number of rows used in the grid(DIML)
2. Number of columns used in the grid (DIMW)
3. Grid spacing in x-direction (DELX)

4. Grid spacing in y-direction (DELY)
5. Length of time steps (DELTA)
6. Length of pumping period (TMAX)
7. Number of pumping periods in total simulation time (NPER)

B. Uniform Matrices

1. Coefficient of permeability (PERM)
2. Specific yield (SY)
3. Recharge rate (QRE)
4. Coefficient of permeability for riverbed (RATE)
5. Distance of river influence node elevation (M)

C. Non-uniform Matrices

1. Land elevation from topographic map (LAND)
2. 1977 - water table elevation (STRT)
3. Prior irrigation pumping rate (WELL)
4. Constant gradient (GRAD)

D. Computer Generated Matrices

1. Elevation of bottom of aquifer (BOTTOM)
2. Elevation of bottom of river (TOP)
3. River water elevation (RIVER)

The model area has approximately 588 square miles. A rectangular grid spacing (5280 feet x 5808 feet) was chosen and the resulting grid system consisting of 34 columns and 30 rows is shown in Figure 4. The model system contains 535 nodes. A one-year run of two periods was used for calibration. The allocation simulation period was divided into 40 pumping periods and a time step of 10 days was used. A time step is the period of time in which water table elevations are computed to accommodate recharge and/or discharge in the system. The length of the pumping period was 150 days for the dry period when the river was gaining water from the basin, and 210 days for the wet period when the basin was recharging from precipitation.

A homogeneous value of 600 gpd/ft² for permeability coefficient and 0.20 for specific yield were used as uniform matrices. Recharge rate from precipitation was calculated to be 24 inches per year. Water gained into the basin during the wet period was drained to the river during dry period. Therefore, the river was considered to be spread over three percent of the area. The coefficient of permeability for river bed was, therefore, adjusted in the model to be 180 gpd/ft² (600 x 3%). The distance of influence of the river to adjacent nodes was 100 feet.

The land and water table elevations were derived from topographic and water table maps, respectively, and

and the identified values were assigned to each node. Prior irrigation pumping rates were calculated from pumping rates in existing wells.

The elevation of the base of aquifer was set 300 feet below the surface. The river water elevation was set to the initial water elevation plus a constant calibration. The bottom of the river was set sixteen feet below the initial water elevations.

The model was used to simulate one-year and twenty-year periods. One-year simulation runs were used to calibrate the model. The twenty-year simulation runs were initiated on April, 1977 and terminated on March, 1997. The longer simulation period was used to assign predicted annual pumping allocation rates based on predicted drawdown.

Assumptions for Calibration

In order to protect the shallow dug and hand pump wells as well as to meet the existing irrigation requirements, the digital model used in this study is based on the following assumptions:

1. The maximum allowable drawdown is set at 22 feet of water depth from the surface
2. Time periods are assumed to be five months for the dry period and seven months for the wet period. These represent limiting recharge

during the wet period and river flows during the dry period.

Most of the hand pump wells are $1\frac{1}{2}$ inches diameter cased well with average 100 feet deep. Each well yields approximately 3240 gallons per day at the rate of 0.1 cfs discharge with 12 hours continuous pumping per day. The drawdown is calculated using the following equation (Walton, 1970):

$$\frac{Q}{S} = \frac{T}{264 \text{ Log} \frac{Tt}{2693 r_w^2 S_y} - 65.5} \quad (15)$$

where

$\frac{Q}{S}$ = specific capacity in gpm/ft

Q = discharge in gpm

S = drawdown in feet

T = coefficient of transmissivity in gpd/ft

S_y = specific yield, fraction

r_w = nominal radius of well, feet

t = time after pumping started, minutes

The calculated drawdown is less than 0.15 feet. It is very insignificant and is ignored in selecting pumping level. The practical suction lift for those shallow hand pump wells according to international standard (Campbell and Lehr, 1973) is 22 feet. The maximum drawdown for irrigation wells is therefore restricted to 22 feet only. The resulting water depth during 20 years simulation run

were subdivided into ranges as shown in the 20-year sequence computed map in Figures 34, 35, 36, 37, and 38. The depth of 22 feet is considered critical depth because pumping below this depth will cause the existing shallow hand pump wells to be inoperative.

The conceptual models of the study area is shown in Figures 30, 31, and 32. These models were based on available data and is used with the computer model for better calibration. The water table rises during wet period and recedes during the dry period. Based on water table data, rainfall and river discharge data, April to October (7 months) was chosen as the wet period, when the river is gaining water from excess surface runoff and the ground-water table rises due to heavy infiltration from precipitation. Thus, the dry period is from November to March (5 months), when the ground-water table recedes and the river is gaining water from the basin. The annual result is a recharge-discharge equilibrium.

Calibration

Calibration was achieved by running the model on the basis of the conceptual model and comparing the 1977 observed head elevations with the computed values. The main objective of this calibration was to establish the recharge-discharge equilibrium. Equilibrium is established when the mass balance shows the inflow and the

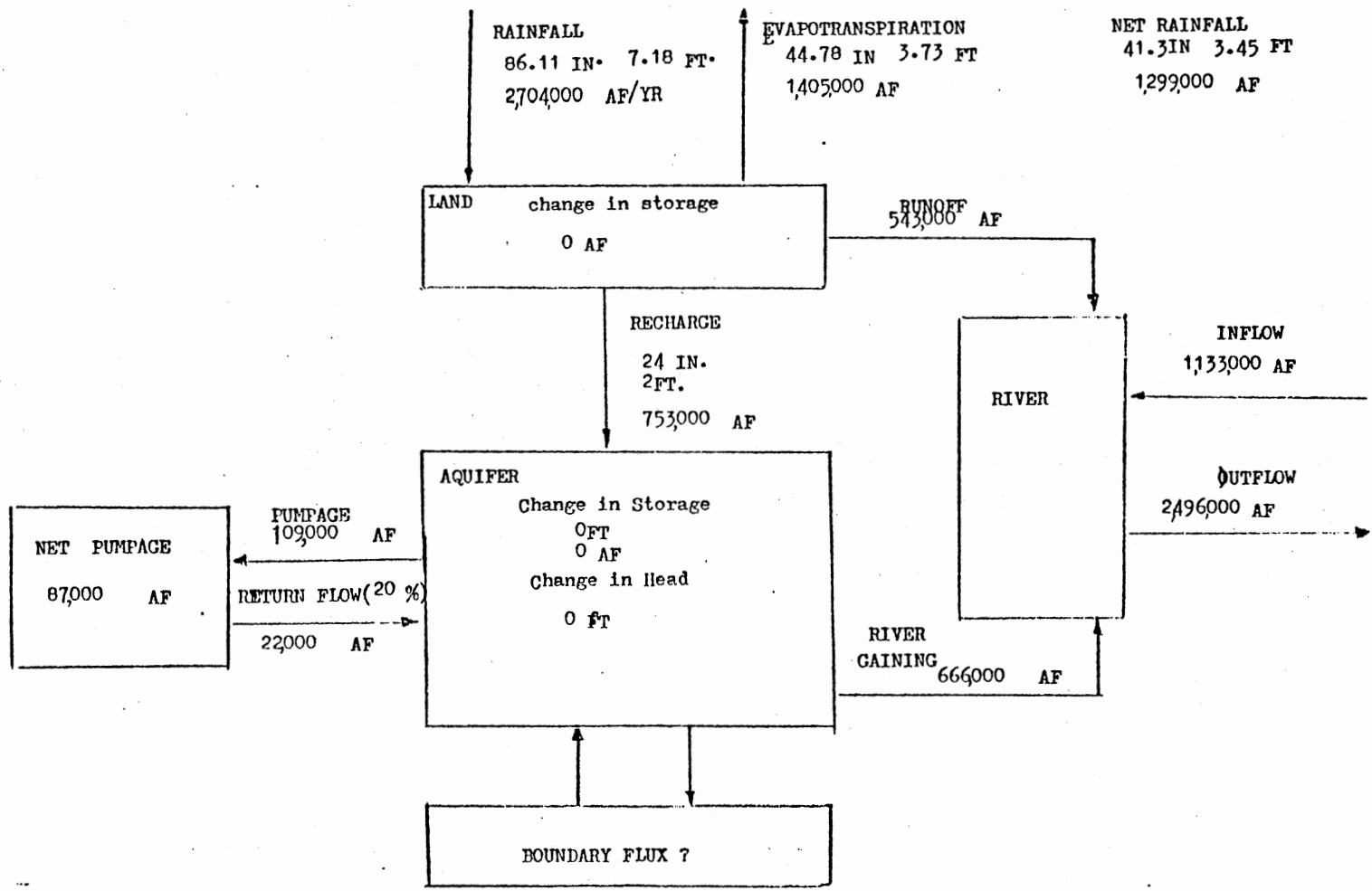


Figure 30. Conceptual Model for One Year Period

CONCEPTUAL MODEL FOR WET PERIOD
(APR - OCT)

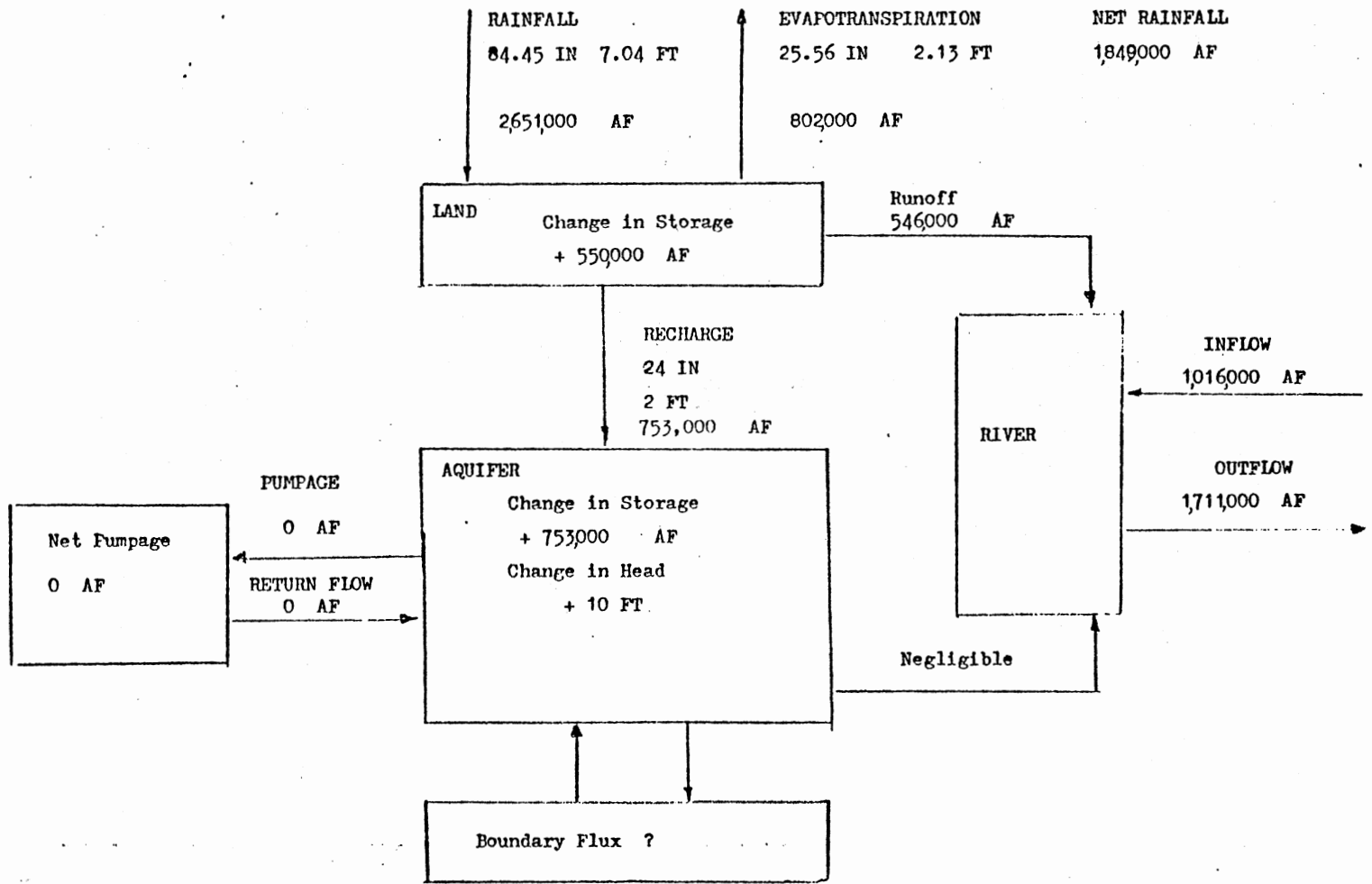


Figure 31. Conceptual Model (wet period)

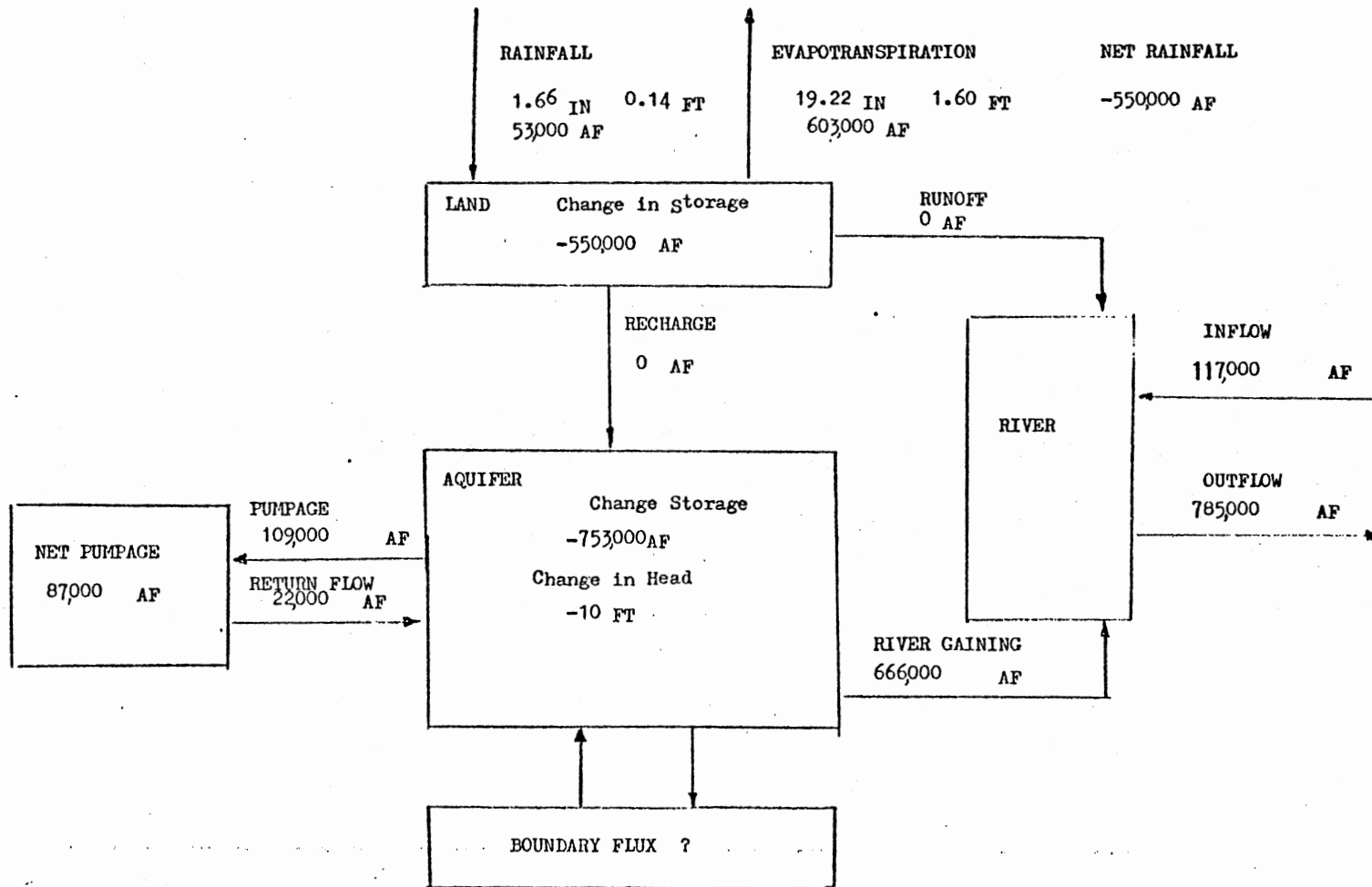


Figure 32. Conceptual Model (dry period)

outflow as being equal and is indicated by negligible fluctuations in the water table elevations.

After the initial calibration, using constant recharge, the discharge was calibrated to set the aquifer to the recharge-discharge equilibrium. The initial one year simulation resulted in an appreciable rise in the water table. Apparently the water could not be sufficiently drained. It was noted from the model that ground-water drainage concided with perennial rivers flowing over this area. The water which rises up to ten feet due to recharge during wet period was discharged fully to the river during the dry period. During calibration water was not shown sufficiently discharged into the rivers and removed from the ground-water system. In order to increase this discharge into perennial rivers, minor adjustment of river elevation was made. Other excessively rising nodes did not respond to river discharge due to their distant location from the river. Finally, the model was modified to allow for river discharge on all nodes in order to represent intermittent streams throughout the area. After making final adjustments, an equilibrium condition was achieved and model calibration was completed.

CHAPTER VII

RESULTS

A 20-year computer simulation was conducted for the 1977 to 1997 period for entire area using pumping rates of prior irrigation pumpage. This simulation was repeated with allocation pumping in conjunction with prior irrigation pumping. The allocation pumping was used when it was greater than the prior irrigation pumping for a node.

The model using one year simulation runs to achieve equilibrium, a 20-year simulation was conducted using prior irrigation pumpage. The mass balance is shown in Table XIV. The 1977 prior pumpage water head is shown in Figure 33. When comparing the 1997 water elevation map (Figure 33) to the corresponding 1977 (Figure 12) a slight fluctuation in head was noted and was considered negligible. Repeated runs were made using various allocation to achieve a maximum yield where no more than 50% of the nodes would be expected to go below critical depth (22 ft). Table XV shows the simulation results for different allocation with corresponding water depth, drawdowns and the percentage of nodes which are predicted to occur below the critical depth of 22 feet. The total maximum annual yield

TABLE XIV
 MASS BALANCE FOR PRIOR IRRIGATION PUMPING
 FROM 1977 to 1997

	: Average Annual		: Twenty-year total	
	: (Acre-feet)		: (Acre feet)	
	: Inflow	: Outflow	: Inflow	: Outflow
Recharge	: 753,216	: ...	: 15,064,313	:
Pumpage	: ...	: 87,112	: ...	: 1,742,235
River leakage	: 4,124	: 651,172	: 82,486	: 13,023,437
Subsurface flow:	4,852	: 23,506	: 97,037	: 470,127
Total	: 762,192	: 761,790	: 15,243,834	: 15,235,798
Net storage change		+402		+8036

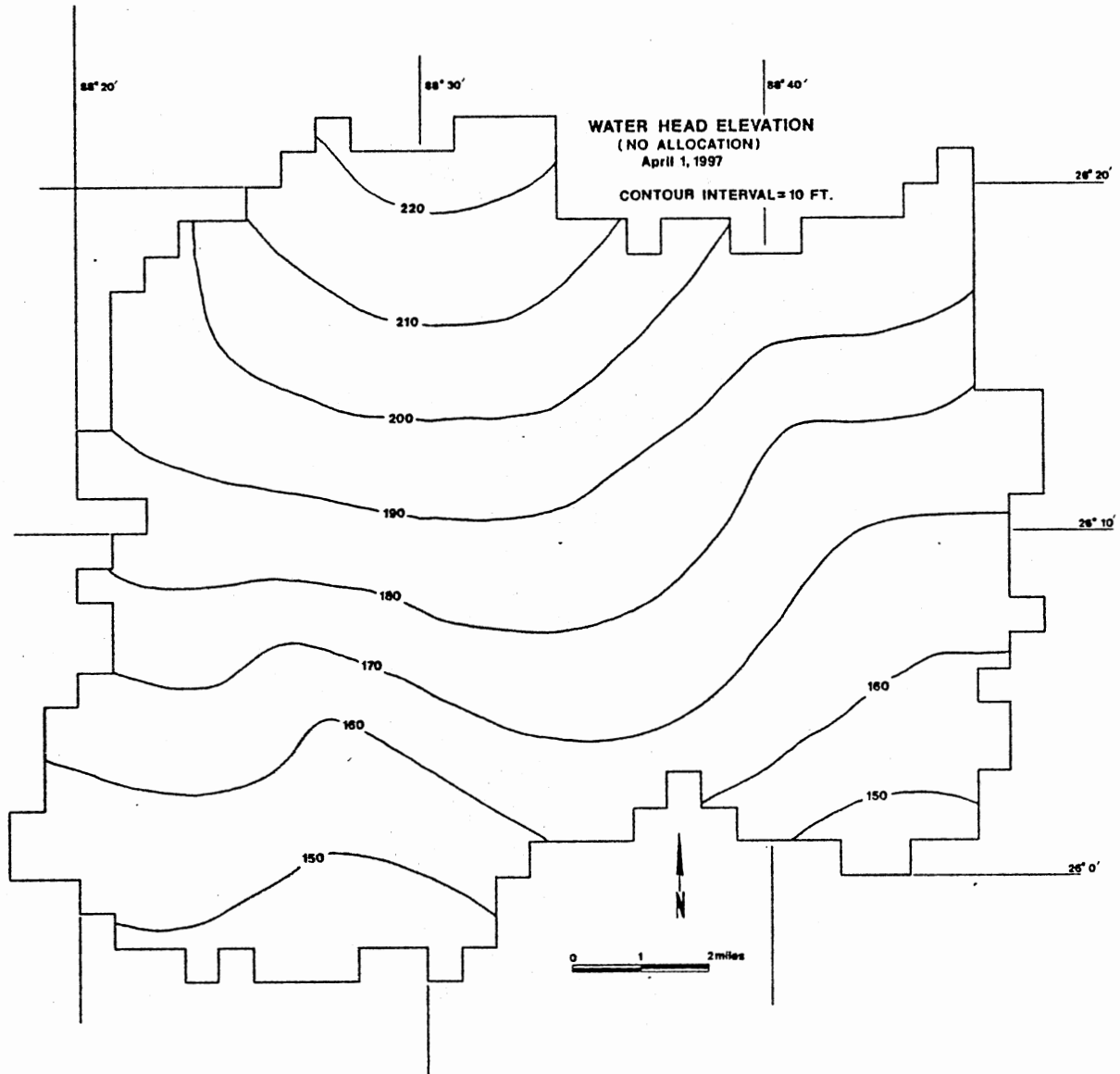


Figure 33. 1997 Water-table Contour Map (Prior Irrigation)

TABLE XV
 SUMMARY OF SIMULATION RESULTS
 WITH VARIOUS ALLOCATION

Allocation of pumping rate	: Water withdrawal : from storage : (Acre-feet)	: Drawdown : (ft)	: Depth of : water from : surface : (ft)	: No. of : nodes below : 22 feet : (Critical : depth)	: Percent : of nodes : below 22 : feet
cfs/acre : Acre-ft/ : acre	:	:	:	:	:
0.0034	: 0.5	: -50,000	: 0.6	: 13.0	: 0
0.0068	: 1.0	: -147,000	: 2.1	: 14.8	: 0
0.010	: 1.5	: -270,000	: 3.6	: 16.27	: 0
0.015	: 2.23	: -685,000	: 8.4	: 21.03	: 200
0.016	: 2.38	: -935,000	: 11.31	: 23.94	: 352
0.020	: 3.00	: -4,314,000	: 44.0	: 80.0	: 535
					: 40%
					: 66%
					: 100%

was determined to be 843,000 acre-feet per year using a pumping allocation of 2.23 acre-feet per acre per year. This yield was produced by dividing the total pumpage (1997) by the period of simulation of 20 years. The mass balance is shown in Table XVI. A 20-year sequence of maps showing areas which had crossed the depth limit (critical depth) are shown in Figures 34, 35, 36, 37, and 38. The final water table map of 1997 with allocation is shown in Figure 39. A 20-year ground-water budget was computed for the final computer allocation runs of the area is shown in Figure 40.

TABLE XVI

MASS BALANCE FOR PRIOR IRRIGATION PUMPING
AND 2.23 ACRE-FT/ACRE ALLOCATION FROM
1977 to 1997

	: Average Annual		: Twenty-year total	
	: (Acre-feet)		: (Acre-feet)	
	: Inflow	: Outflow	: Inflow	: Outflow
Recharge	: 753,216	:	:15,064,313:	
Pumpage	:	: 674,159	:	: 13,483,187
River leakage	: 9,626	: 104,630	: 193,910:	2,092,603
Subsurface flow:	4,697	: 23,049	: 93,951:	460,973
Total	: 767,609	: 801,838	:15,352,173:	16,036,762
Net storage change		-34,229		-684,589

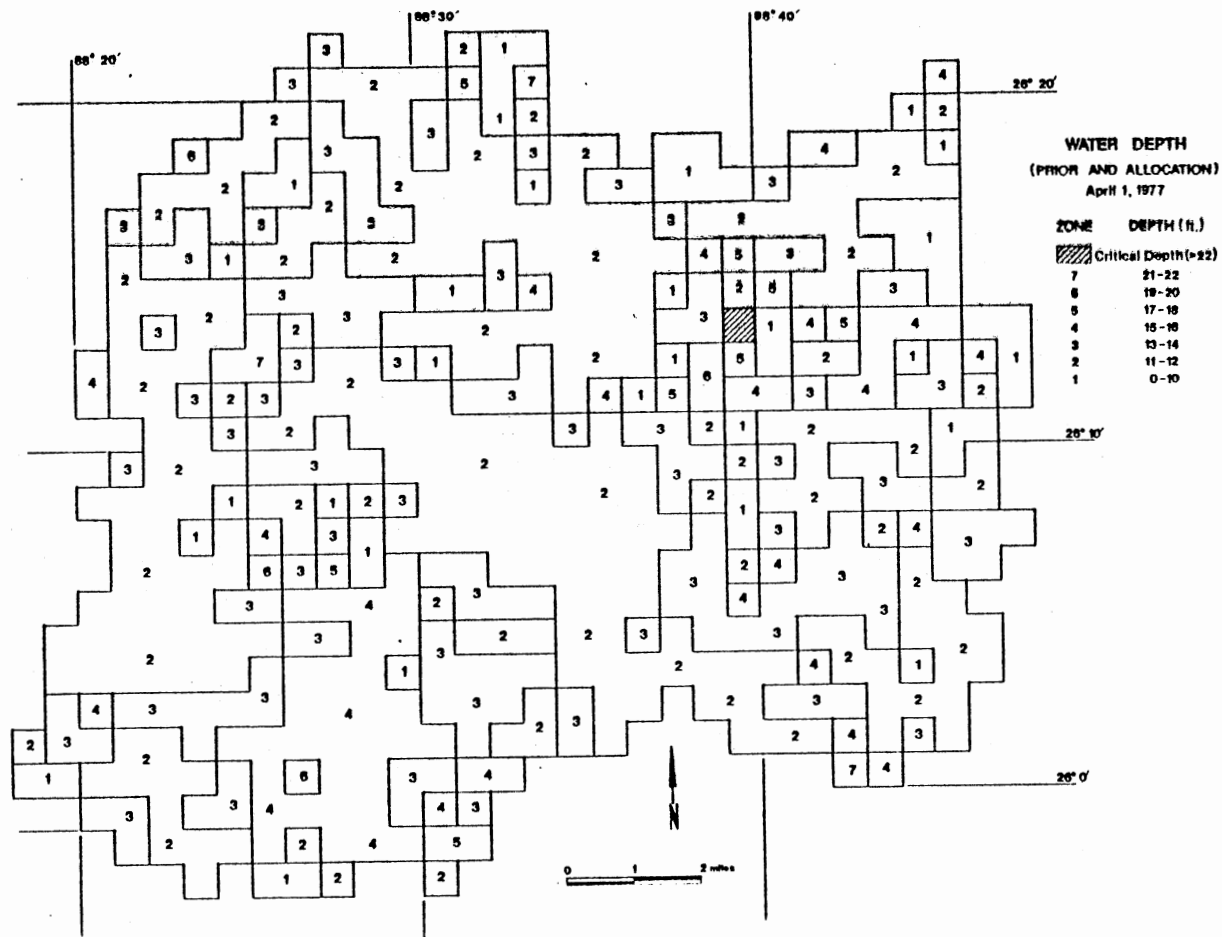


Figure 34. 1977 Water Depth Map (Allocation)

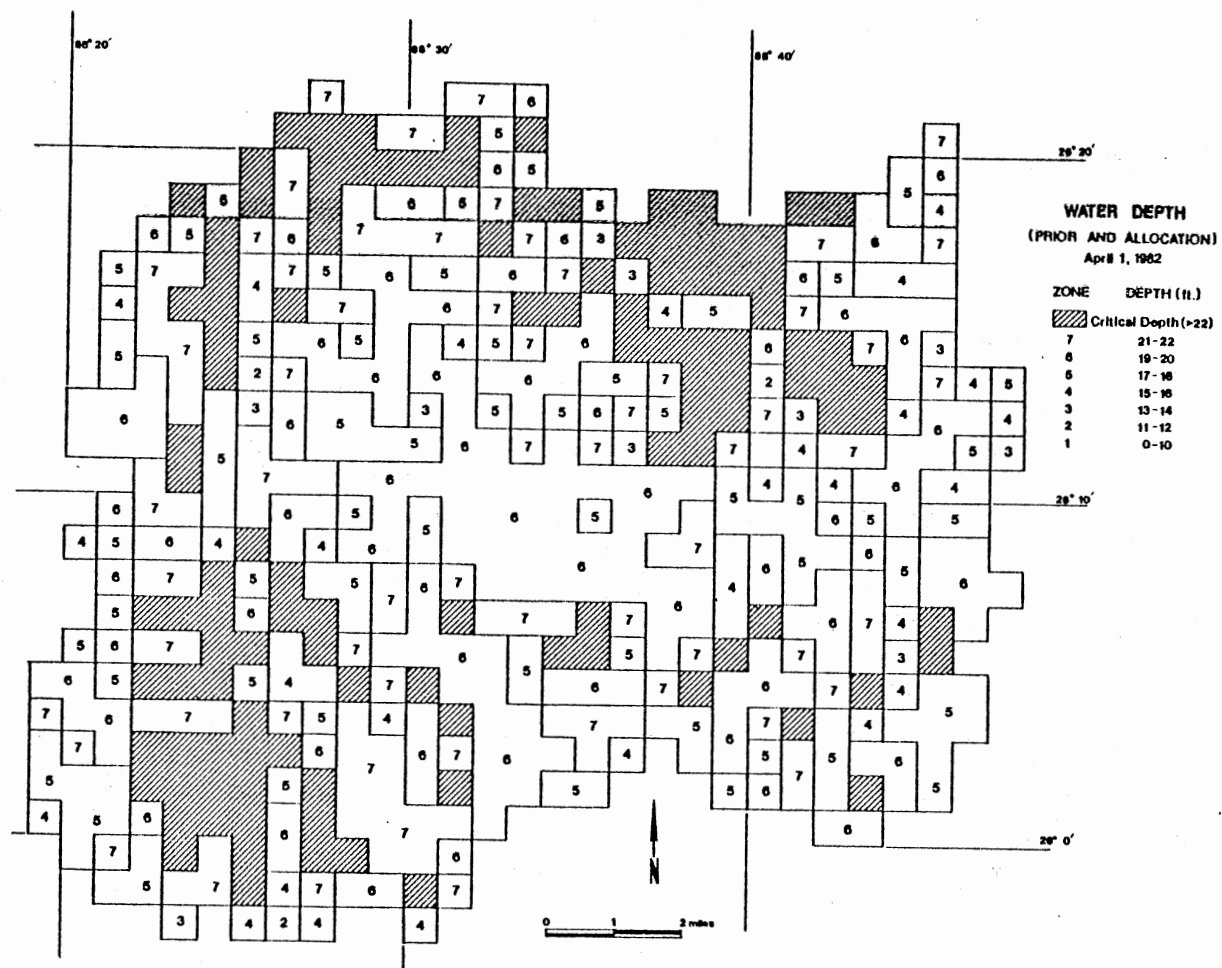


Figure 35. 1982 Water Depth Map (Allocation)

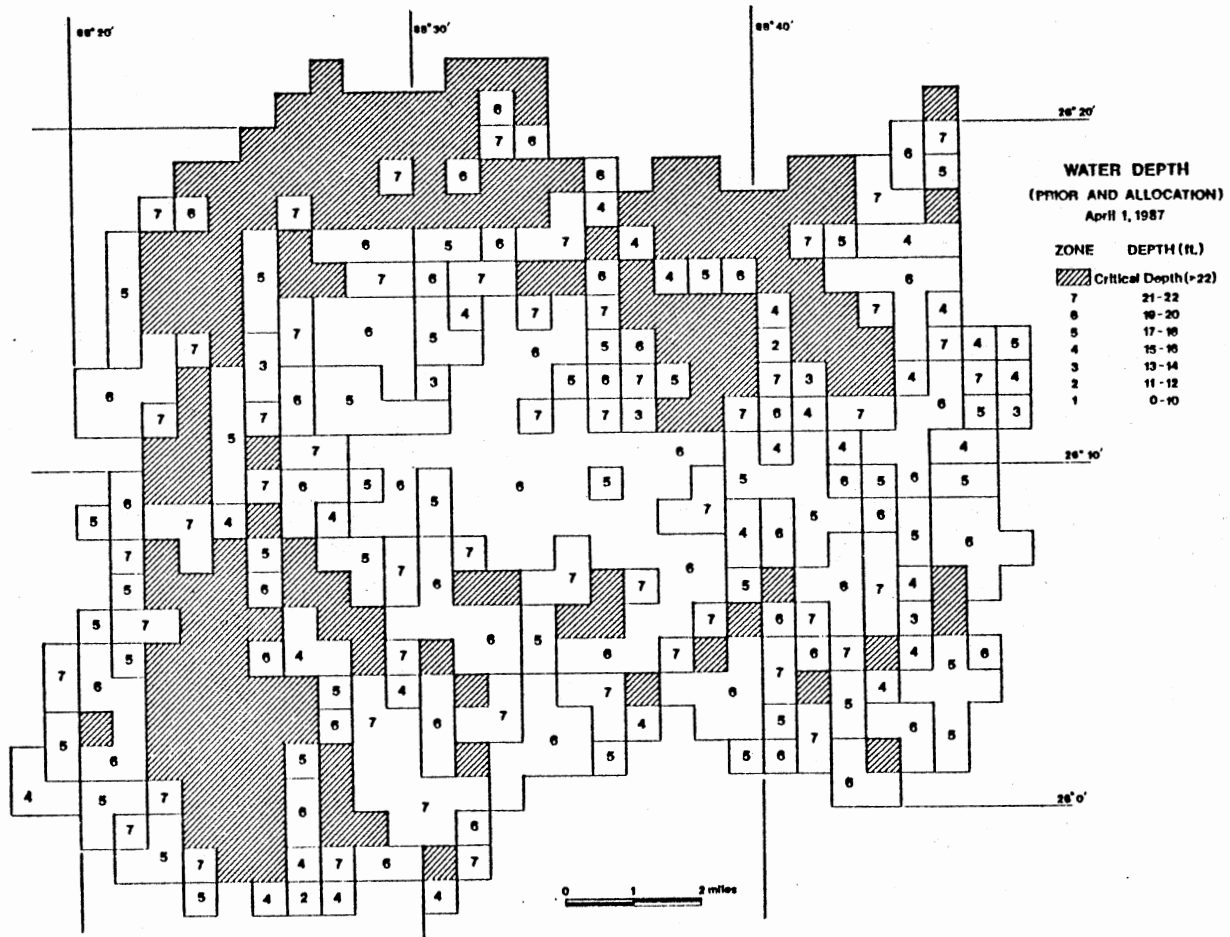


Figure 36. 1987 Water Depth Map (Allocation)

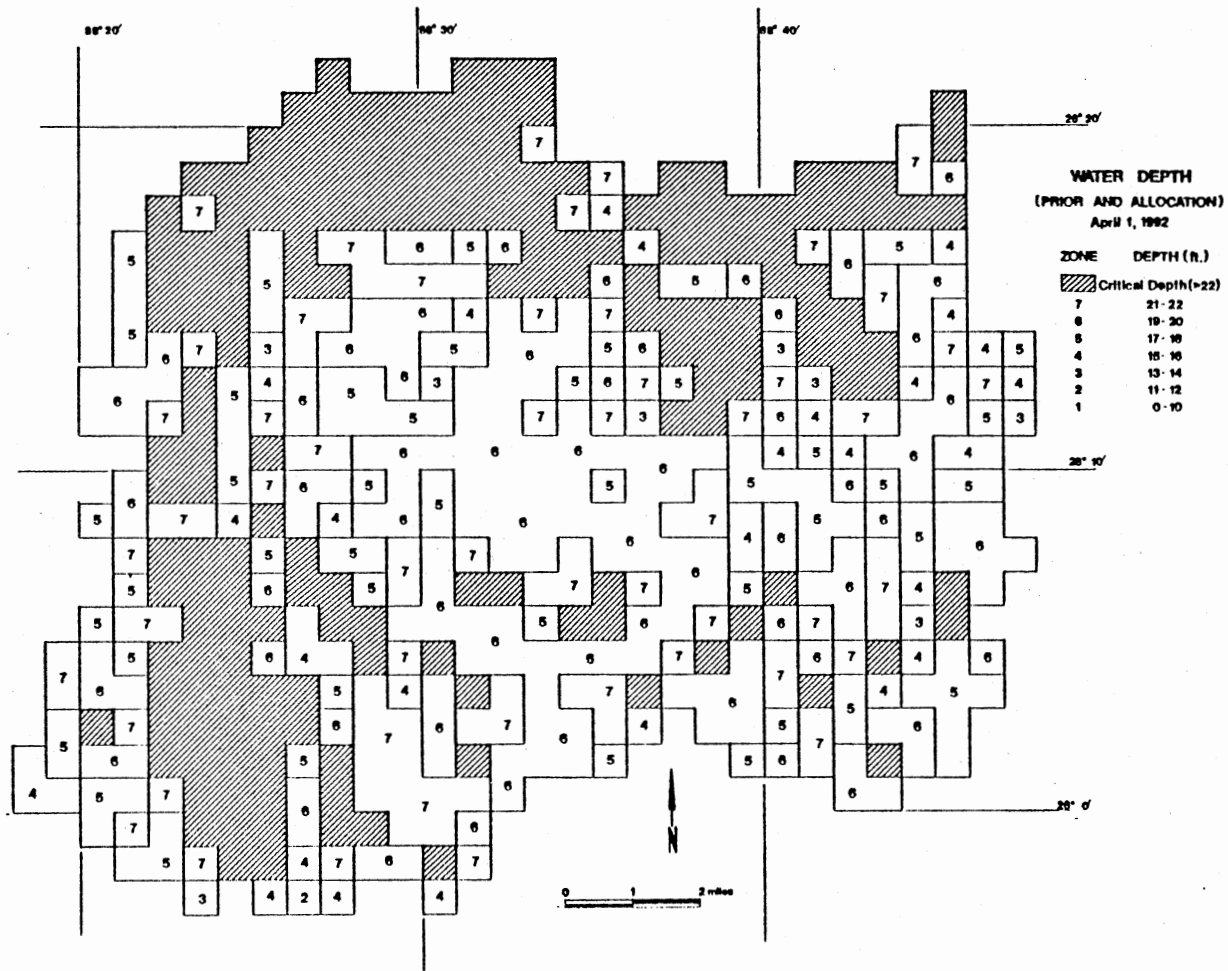


Figure 37. 1992 Water Depth Map (Allocation)

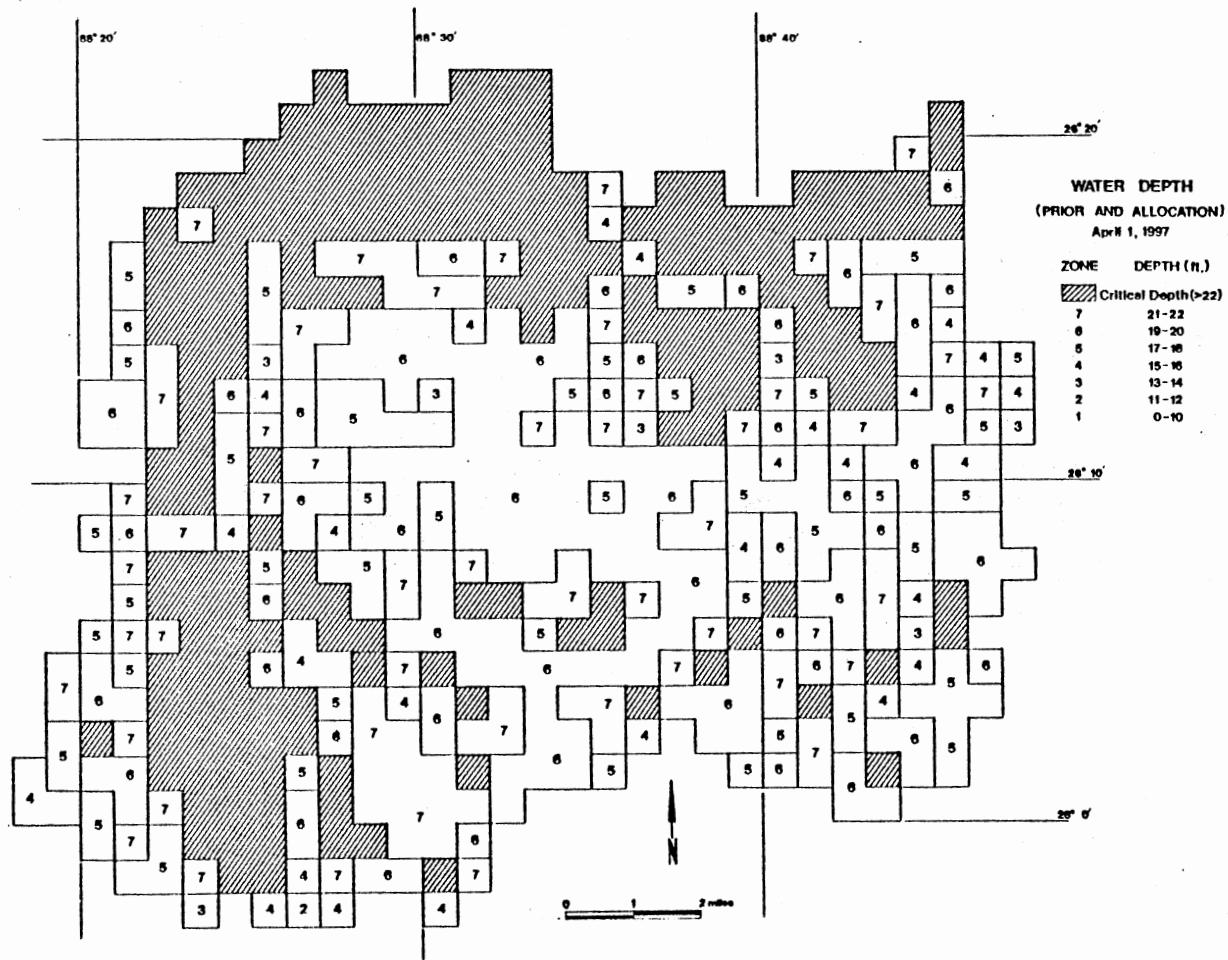


Figure 38. 1997 Water Depth Map (Allocation)

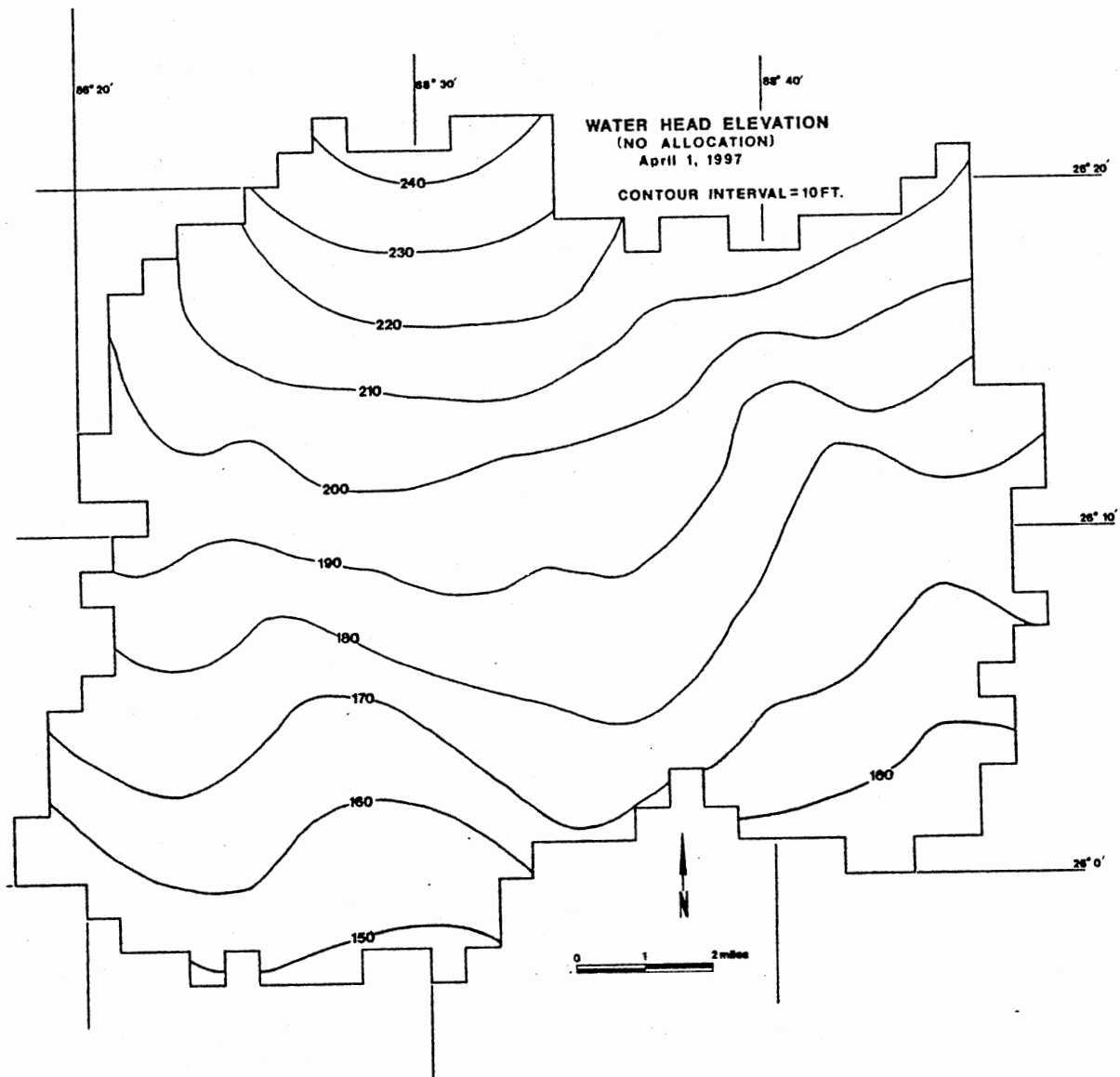


Figure 39. 1997 Water-table Contour Map (Allocation)

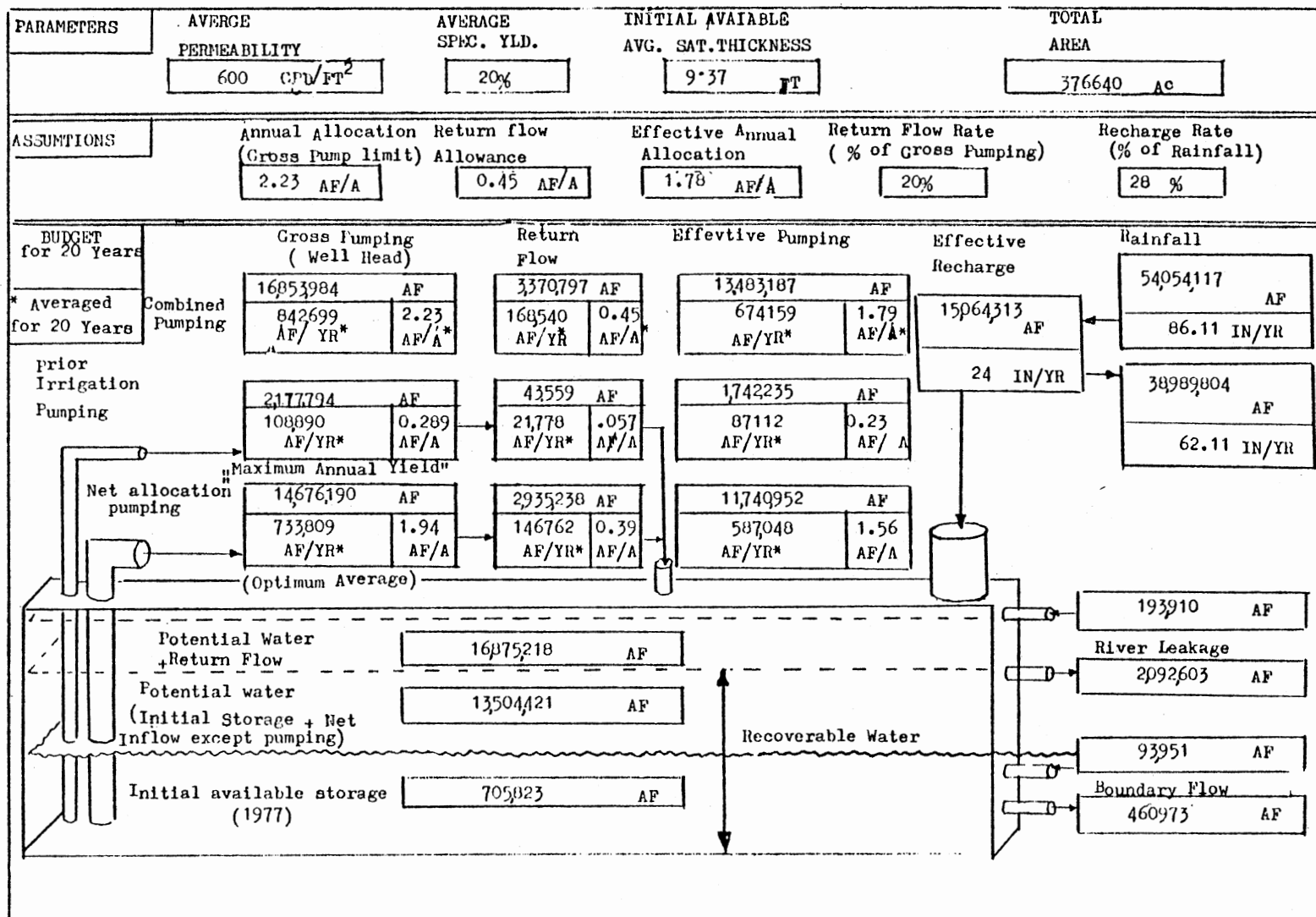


Figure 40. 20 Years Ground-Water Budget of the Study Area

CHAPTER VIII

SUMMARY AND CONCLUSIONS

Computer simulation is an effective tool for determining the maximum annual yield with limited draw-down for the ground-water basins in the central part of the Dinajpur district. The reliability of the output results of the model, however sophisticated, can only be as good as the data input upon which they are based. It is, therefore, essential in the modeling process to devote considerable care to the collection, interpretation, and validation of these data.

The principal parameters from which the annual yield was determined are:

1. The total land area is 676,640 acres overlying the Piedmont deposits in the aquifer;
2. The volume of water within 22 feet from surface storage in the aquifer as of 1977 is 705,823 acre-feet; this cumulative volume of water in storage for 20 years is 16,875,000 acre-feet;
3. The estimated rate of natural recharge is 24 inches per year;
4. The average specific yield in the upper part of the aquifer is 0.20; and

5. An average permeability is 600 gpd/ft².

With the prior irrigation pumpage rate the total water can be used at a rate of 109,000 acre-feet per year between 1977 to 1997. The mass balance is summarized in Figure 40. A total volume of 16,854,000 acre-feet represents the cumulative amount of water pumped from storage within 22 feet from the surface at the discharge rate of 2.23 acre-feet per acre during a 20-year period. A cumulative volume of 1,742,000 acre-feet is pumped at the prior irrigation pumpage rate during the same period. A cumulative volume of 16,875,000 acre-feet is stored within 22 feet from surface over the 20-year period. A groundwater storage within 22 feet of approximately 705,823 acre-feet is computed to have existed in 1977. An additional 16,169,000 acre-feet was accumulated due to recharge and return flow, especially recharge during the non-pumping periods (7 months per year).

The optimum pumping rate (2.23 acre-feet per acre) is almost half of the existing crop demand as discussed in Chapter III (4 acre-feet per acre). Therefore, only fifty percent of the total area can be used for irrigation when using this rate. The pumping rate would be one cfs for twelve hours continuous pumping per day during the irrigation season. Therefore, ten wells of one cfs capacity or five wells of two cfs capacity can be allotted per square mile (640 acres). The result of modeling

allow a choice of actions to produce various predictive results. A pumping limit of 1.5 acre-feet per acre is expected to prevent any shallow hand pump wells from being affected. A pumping limit of 2.23 acre-feet per acre is expected to affect 40% of the shallow wells. If the entire area is irrigated at the crop demand level of 4 acre-feet per acre, all shallow wells will be expected to be inoperative.

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APPENDIXES

APPENDIX A

LISTING OF COMPUTER PROGRAM

```

*****
DIGITAL MODEL FOR AQUIFER SIMULATION
BY P.C. TRESGOTT AND G.F. PINDER
JANUARY, 1974
- FOR U.S. GEOLOGICAL SURVEY USE ONLY -
*****
SUBPROGRAMS AND ENTRIES:

```

- | | |
|---|---|
| 1. MNPROG | 4. COEF
CLAY
TRANS
TCCF
ETRATE
STCRAGE
LEAKAGE
SCUPE
WELLHD |
| 2. DATAI
DATAIN
ITER
MAP
NEWPER | 5. CHECK I
CHECK
CWRITE |
| 3. COMPUT
NEWSTP
NEWITI
NEWITO
ROW
COLUMN
STEADY
CUTPUT
CRON
CRY | 6. PRNTAI
PRNTA |
| | 7. BLOCK DATA |

```

*****
MAIN PROGRAM TO DIMENSION DIGITAL MODEL

```

SPECIFICATIONS:

```

C*CM01*
C*CM02*
C*CM03*
C*CM04*
C*CM05*
CJMMON / PLTCC / PHE, KEEP, STRT, ISUR, BOTTOM, TOP, LAND, RIVER
* , M, S, SY, PERM, T, TR, TC, RATE, Q, QRE, WELLD, WELL, RRRR9
* , KKLAY, TLAY1, TLAY, RRRR8
C*DIM01*
DIMENSION BE(60), G(60), TEMP(60), PHI(50,60),
1 KEEP(50,60), PHE(50,60), STRT(50,60), ISUR(50,60), T(50,60),
2 TR(50,60), TC(50,60), S(50,60), CON(60), DELX(60), DELY(60),
3 PERM(50,60), BOTTOM(50,60), SY(50,60),
4 RATE(50,60), RIVER(50,60), M(50,60), Q(50,60),
5 TOP(50,60), LAND(50,60), QRE(50,60), WELLD(50,60), WELL(50,60),
6 KKLAY(50,60), TLAY1(50,60), TLAY(50,60,8),
7 NR(10), NWR(10,2)
C*DIM02*
DIMENSION RRRR(50,60,40), RRRR9(50,60,5), RRRR3(50,60,5)
DIMENSION IIII(50,60,40)
C*TYP01*
REAL *4KEEP,M,ISUR,LAND
C*TYP02*
REAL *3PHI,G,SE,TEMP
C*TYP03*
C*DTA01*
EQUIVALENCE (PHE, RRRR, IIII)
---INITIALIZE PARAMETERS DEFINING ARRAY SIZE---
DATA IZ,IP,IR,IC,IL,IQ,IW,IH /50,50,50,50,50,50,50,10/
DATA JZ,JP,JR,JC,JL,JQ,JW,IMAX/60,60,60,60,60,60,60,60/
C*DTA02*
C*DTA03*
DATA MNR, MNV / 40, 30 /, MLAY / 7 /
C*END01*
C
WRITE(5,100)
100 FORMAT(' *****', 'PROGRAM DIM IS EXECUTED', '*****')
9999 FORMAT(' GWMDL 5/25/79 MCD 20, 21, 25F, 26, 27A')
WRITE(6,9999)
---PASS DIMENSIONS OF PROBLEM TO SUBROUTINES---
CALL DATAI(PHI,KEEP,PHE,STRT,ISUR,T,TR,TC,S,DELX,DELY,Q,RATE,M,RIV
IER,WELL,SY,TCR,LAND,PERM,BOTTOM,QRE,IZ,JZ,IR,JP,IW,JW,IP,JP,IL,JL,
2IC,JC,IQ,JQ,NR,NWF,IH,WELLD,KKLAY,TLAY1,TLAY,MLAY)
CALL COMPUT(PHI,KEEP,PHE,STRT,ISUR,T,TR,TC,S,DELX,DELY,DDN,G,SE,TE
1MP,IMAX,IZ,JZ,TCR,IC,JC,BCTT,CM,IP,JP,WELL,IW,JW,KKLAY,TLAY1,TLAY
2,MLAY,PERM,SY)
CALL COEF(PHI,KEEP,PHE,STRT,ISUR,T,TR,TC,S,DELX,DELY,Q,RATE,M,RIVE

```



```

1R,WELL,SY, TOP, LAND, PERM, BCTTCM, CRE, IZ, JZ, IR, JR, IW, JW, IP, JP, IL, JL, I
2C, JC, IJ, JU, NR, NRR, IH, KKLAY, TLAY1, TLAY, MLAY)
CALL CHCKI(PHI, KEEP, PHE, STRT, ISUR, T, TR, TC, S, DELX, DELY, Q, RATE, M, RI
1VER, WELL, SY, TOP, LAND, PERM, BCTTCM, CRE, IZ, JZ, IR, JR, IW, JW, IP, JP, IL, JL
2, IC, JC, IJ, JU)
CALL PRINTAI(PHI, ISUR, S, DELX, DELY, WELL, IZ, JZ, IW, JW)
CALL P-TAI(S, RRRR, IZ, JZ, MNR, MNV, DELX, DELY, PHI, I, IIII)
WRITE(5, 9598) IZ, JZ
9998 FORMAT('DOMAIN DIMENSIONS:', 2I5)
C
C
C      ---START COMPUTATIONS---
CALL MNPRUG
STOP
END

SUBROUTINE MNPRUG
-----
C
C
C      SPECIFICATIONS:
C*CM01*
COMMON /DARRAY/ RHOP(20), CHK(10), VF4(11)
C*CM02*
COMMON /OPARAM/ WATER, CONVRT, EVAP, CHCK, FNCH, NUM, HEAD, CONTR, EROR, LE
1AK, RECH
C*CM03*
COMMON /SPARAM/ SLEAK, U, SS, TT, TMIN, ETDIST, QET, IFINAL, TMAX, COLT, DEL
1T, SUM, SUMP, NUMT, KT, KP, NPER, KTH, ITMAX, LENGTH, NWEL, NW, ERR, DIML, DIMW,
2JNU1, INU1, R, P, PU, SUBS, STORE, TEST, ETQB, ETQO, FACTX, FACTY, IERR,
3DAYS, YRS, SSRIV, CFLEAK, QSUM, KEDIT, MESSG, IPRDON, IPRHD, ISVHD, ISVFLX
4, IFILE(10), KOUNT, KSTEP, NHYDR, IHYDR(13), JHYDR(13), HYDR(13)
C*CM04*
C*CM05*
C*CM06*
COMMON / PLTC / LPLT, MPLT, IPLT, IRUN, IPER, ISTOP, ITRY, IVAP
* , TI, TPI
C*DIM01*
C*DIM02*
C*TYP01*
C*TYP02*
REAL *DOUBLE, RHOP, CHK, WATER, CONVRT, EVAP, CHCK, PNCH, NUM, HEAD, CONTR, ER
1OR, LEAK, RECH
C*TYP03*
INTEGER DIML, DIMW, R, P, PU
C*DTA01*
C*DTA02*
C*DTA03*
C*END00*
C
C      .....
C      ---READ AND WRITE DATA FOR A NEW PROBLEM---
10 IPER = 0
ISTP = 0
ISTPP = 0
ITRY = 0
IPI = 0
CALL DATAIN
C
C
C      ---INITIALIZE TRANSMISSIVITY VALUES IN WATER TABLE PROBLEM---
IF( WATER.EQ.CHK(2)) CALL TRANS --- INITIAL TRANS. NOW CALC. IN
SUBROUTINE DATAIN (REV. BY O.B. SAPIK).
C
C
C      ---COMPUTE ITERATION PARAMETERS---
CALL ITER
C
C
C      ---INITIALIZE PARAMETERS FOR ALPHAMERIC MAP---
IF (CONTR.EQ.CHK(3)) CALL MAP
C
C
C      ---COMPUTE T COEFFICIENTS FOR ARTESIAN PROBLEM---
IF (WATER.NE.CHK(2)) CALL TCOF
IPLT = -1
IRUN = IRUN + 1
IF(IPLT .GE. LPLT) CALL PLTX
C
C
C      ---READ TIME PARAMETERS AND PUMPING DATA FOR A NEW PUMPING PERIOD---
KSTEP=0
20 CALL NEWPER

```

```

C      KT=J
C      IFINAL=0
C      IERR=0
C      IPLT = -2
C      IPER = KP
C      ISTPP = 0
C      ITRY = 0
C      IF(IPLT .GE. LPLT) CALL PLTX
C
C      ---START NEW TIME STEP COMPUTATIONS---
C      30 CALL NEWSTP
C      IPLT = -3
C      ISTP = ISTP + 1
C      ISTPP = ISTPP + 1
C      ITRY = 0
C      TI = SUM
C      TPI = SUMP
C      IF(IPLT .GE. LPLT) CALL PLTX
C
C      ---COMPUTE LEAKAGE COEFFICIENTS---
C      IF (LEAK.EQ.CHK(9)) CALL CLAY
C
C      ---START NEW ITERATION IF MAXIMUM NO. ITERATIONS NOT EXCEEDED ---
C      CALL NEWITO
C      GO TO 30
C      40 CALL NEWITI
C
C      50 IPLT = -4
C      ITRY = ITRY + 1
C      IF(IPLT .GE. LPLT) CALL PLTX
C      ---COMPUTE TRANSMISSIVITY IN WT OR WT-ARTESIAN CONVERSION PROBLEM---
C      IF(WATER .NE. CHK(2) ) GO TO 70
C      CALL TRANS
C      IF (IERR.GT.0) GO TO 30
C
C      ---COMPUTE T COEFFICIENTS IN WATER TABLE PROBLEM---
C      60 CALL TCOF
C
C      ---COMPUTE IMPLICITLY ALONG ROWS---
C      70 CALL ROW
C
C      ---COMPUTE IMPLICITLY ALONG COLUMNS---
C      CALL COLUMN
C
C      IPLT = 4
C      IF(IPLT .LE. MPLT) CALL PLTX
C      ---IF SOLUTION NOT OBTAINED START NEW ITERATION---
C      IF (TEST.EQ.1.) GO TO 40
C
C      ---CHECK FOR STEADY STATE---
C      CALL STEADY
C
C      IPLT = 3
C      IF(IPLT .LE. MPLT) CALL PLTX
C      ---PRINT OUTPUT AT DESIGNATED TIME STEPS---
C      IF (MOD(KT,KTH).NE.0.AND.IFINAL.NE.1) GO TO 30
C      CALL OUTPUT
C      IF (IFINAL.NE.1) GO TO 30
C
C      IPLT = 2
C      IF(IPLT .LE. MPLT) CALL PLTX
C      ---CHECK FOR NEW PUMPING PERIOD---
C      IF (KP.LT.NPER) GO TO 20
C
C      IPLT = 1
C      IF(IPLT .LE. MPLT) CALL PLTX
C      PRINT HYDROGRAPHS ---
C      30 IF (KT.LE.0) GO TO 90
C      CALL DRY
C      IF (KP.NE.NPER) GO TO 90
C
C      ---CHECK FOR NEW PROBLEM---
C      READ (R,100.END=90) NEXT
C      IF (NEXT.EQ.0) GO TO 10
C      90 RETURN
C
C      FORMAT:

```

```

100 FORMAT (110)
END

```

```

SUBROUTINE DATAI(PHI,KEEP,PHE,STRT,ISUR,T,TR,TC,S,DELX,DELY,Q,RATE
1,M,RIVER,WELL,SY,TOP,LAND,PERM,BOTTOM,QRE,IZ,JZ,IR,JR,IW,JW,IP,JP,
2IL,JL,IC,JC,IG,JC,WR,NWR,IH,WELLD,KKLAY,TLAY1,TLAY,MLAY)
-----

```

```

1. REVISIONS BY D.B. SAPIK (USGS - WRO, OKLA. CITY) - DEC. 1975.

```

- A. EDIT INPUT DATA.
- B. READ PROGRAM OPTION CARD.
- C. READ HYDROGRAPH OPTION CARD.
- D. READ THE FOLLOWING PARAMETERS FROM DISK FILE:
 - INITIAL MASS BALANCE PARAMETERS
 - HEAD (PHI)
 - HEAD (STRT)
 - RECHARGE
- E. WRITE THE FOLLOWING PARAMETERS ON DISK FILE:
 - LEAKAGE RATES COMPUTED AT END OF FIRST TIME STEP
 - HEAD AT THE END OF A PUMPING PERIOD
 - CUMULATIVE MASS BALANCE PARAMETERS AT THE END OF SIMULATION
 - HEAD (PHI) AT THE END OF SIMULATION

```

-----
SPECIFICATIONS:

```

```

C*CM01*
COMMON /DARRAY/ RHOP(20),CHK(10),VF1(11)
C*CM02*
COMMON /DPARAM/ WATER,CONVRT,EVAP,CHCK,PNCH,NUM,HEAD,CCNTR,EROR,LE
1AK,RECH
C*CM03*
COMMON /SPARAM/ SLEAK,U,SS,TT,TMIN,ETDIST,GET,IFINAL,TMAX,CDLT,DEL
1T,SJM,SJMP,NUMT,KT,KP,NPER,KTH,ITMAX,LENGTH,NWEL,NW,ERP,DIML,DIMW,
2JN01,IN01,R,P,PU,SUBS,STORE,TEST,ETQB,ETQD,FACTX,FACTY,IERR,
3JAYS,YRS,SSRIV,CFLEAK,QSUN,KEDIT,MESSG,IPRDCN,IPRHEC,ISVFEI,ISVFLX
4,IFILE(13),KOUNT,KSTEP,NHYDR,IHYDR(13),JHYDR(13),HYDR(13)
* ,WELBOT,WELTCP,SYB
C*CM04*
COMMON /CK/ ETLXNT,QRET,QRETN,FLUXT,FLXNT,CHST,CHOT
* ,CFLXPT,CFLXNT,PUMPT,PUMPPT,STORT
C*CM05*
COMMON /PR/ XLABEL(3),YLABEL(6),TITLE(4),XN1,SYM(28),PRNT(122),BLA
1NK(50),DIGIT(122),VF1(5),VF2(6),VF3(7),NA(4),XN(100),YN(13),XSF,NX
2J,WIDTH,SPACNG,N1,N2,N3,N4,N6,N8,NC
C*CM06*
COMMON / COPYC / ICPYW, KCPY
COMMON / LAYER / SATL(20), PRMSY(10), SYPRM(10), SYC(10)
* , NLAY, NLAY0, MSY, NSY, NSY0
C NOTE MSY MUST BE SET TO DIMENSION OF SY LIST AT END OF ENTRY DATAI
C*DIM01*
DIMENSION PHI(IZ,JZ),KEEP(IZ,JZ),PHE(IZ,JZ),STRT(IZ,JZ),ISUR(I
1Z,JZ),T(IZ,JZ),TR(IZ,JZ),TC(IZ,JZ),S(IZ,JZ),DELX(JZ),DELY(IZ
2),J(IX,JR),RATE(IR,JR),M(IR,JR),RIVER(IR,JR),WELL(IW,JW),SY(
3IP,JP),TOP(IC,JC),LAND(IL,JL),PERM(IP,JP),BOTTOM(IP,JP),QRE(I
4J,JZ),WR(IH),NWR(IH,2),WELLD(IW,JW)
5 ,KKLAY(IZ,JZ),TLAY1(IZ,JZ),TLAY(IZ,JZ,MLAY)
C*DIM02*
DIMENSION SETIC(20)
C*TYP01*
REAL *4KEEP,M,ISUR,LAND
C*TYP02*
REAL *8PHI,DBLE,RHOP,CHK,*WATER,CONVRT,EVAP,CHCK,PNCH,NUM,HEAD,CCNTR
1R,EROR,XLABEL,YLABEL,TITLE,XN1,HEADNG(15),MESUR,LEAK,RECH
C*TYP03*
INTEGER DIML,DIMW,R,P,PU
C*DTA01*
DATA SETID/4HSTRT, 1HS, 1HT, 4HPERM, 4HBOTT, 2HSY,
1 3HTCP, 4HRATE, 4HRIVE, 1HM, 4HLAND, 3HQRE,
2 4HDELX, 4HDELY, 4HWELL, 5*1H /
C*DTA02*
DATA EPS1, EPS2/1.0E-10, 1.0E-20/
DATA THIN / .02 /

```

```

C*DTA03*
C*END00*
9999 FORMAT(' SUB DATA 12/19/78 MOD 26, 27A')
WRITE(P, 9999)
  KCPY = 3
  KPLC = 3
  MSY = 10
  RETURN
*****
ENTRY DAIN
*****

---DEFINE DISK (OR TAPE) FILES---

IFILE(1) = FILE NO. FOR WRITING LEAKAGE RATES COMPUTED AT THE END
           OF THE FIRST TIME STEP (IF ISVFLX = 1).
IFILE(2) = FILE NO. FOR READING RECHARGE RATES AT THE START OF
           SIMULATION (IF IRDRCH = 1).
IFILE(3) = FILE NO. FOR WRITING HEAD (SINGLE PRECISION PHI) AT THE
           END OF A PUMPING PERIOD (IF ISVHED = 1).
IFILE(4) = FILE NO. FOR READING STARTING HEAD (STRT) AT THE
           BEGINNING OF SIMULATION (IF IRDHED = 1).
IFILE(5) = FILE NO. FOR WRITING CUMULATIVE MASS BALANCE PARAMETERS
           AND FINAL HEAD (PHI) AT THE END OF SIMULATION
           (IF PNCH = 'PUNCH').
IFILE(6) = FILE NO. FOR READING CUMULATIVE MASS BALANCE PARAMETERS
           AND HEAD (PHI) SAVED AT THE END OF A PREVIOUS
           SIMULATION (IF IRDINI = 1).
IFILE(7) = FILE NO. FOR WRITING HYDROGRAPHS OF HEAD AT SELECTED
           NODES (IF NHYDR .GT. 0).

IFILE(1)=11
IFILE(2)=12
IFILE(3)=13
IFILE(4)=14
IFILE(5)=15
IFILE(6)=16
IFILE(7)=17

READ PRINT/PLOT PARAMETERS
READ(R, 9000) ICPY, ICPY2, ICPYW, K1, MPRN, KPLT, K2
IF(K1 .NE. 0) KCPY = K1
IF(K2 .NE. 0) KPLC = K2
IF(ICPY .GE. 1) WRITE(KCPY, 9012) ICPY, ICPY2, ICPYW, K1, MPRN
* , KPLT, K2
IF(ICPY .GE. 2) WRITE(KCPY, 9013) ICPY, ICPY2, ICPYW, KCPY, MPRN
* , KPLT, KPLC

---READ GROUP 1 DATA---
READ (R, 910) HEADNG
IF(ICPY .GE. 1) WRITE(KCPY, 9020) HEADNG
WRITE (P, 900) HEADNG

READ (R, 940) WATER, LEAK, CONVRT, EVAP, RECH, CHCK, PNCH, NUM, HEAD
IF(ICPY .GE. 1) WRITE(KCPY, 9030) WATER, LEAK, CONVRT, EVAP, RECH
* , CHCK, PNCH, NUM, HEAD

READ (R, 950) CONTR, SCALE, DINCH, SPACNG, MESUR
IF(ICPY .GE. 1) WRITE(KCPY, 9040) CONTR, SCALE, DINCH, SPACNG, MESUR

IF(CONVRT.EQ.CHK(7)) WATER=CHK(2)
WRITE (P, 1100) WATER, LEAK, CONVRT, EVAP, RECH, CHCK, PNCH, NUM, HEAD, CONT
L2
IF (CONTR.EQ.CHK(3)) WRITE (P, 1110) SCALE, MESUR, MESUR, DINCH, SPACNG

.....

---READ PROGRAM OPTION CARD---
READ (R, 941) KEDIT, NHYDR, MBRES, ISVFLX, IRDINI, IRDHED, IRDRCH
CARD DELETED
IF(ICPY .GE. 1) WRITE(KCPY, 9050) KEDIT, NHYDR, MBRES, ISVFLX
* , IRDINI, IRDHED, IRDRCH

IF (KEDIT.LT.0 .OR. KEDIT.GT.19) KEDIT=0
KED=KEDIT
IF (KEDIT.LT.12 .AND. KEDIT.GT.5) KED=KED-6
MESSG=1
IF (KED.EQ.4 .OR. KED.EQ.5) MESSG=0
IF(ICPY .GE. 2) WRITE(KCPY, 9050) KEDIT, NHYDR, MBRES, ISVFLX

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* , IRDINI, IRDHED, IRDRCH
.....
--- READ HYDROGRAPH OPTION CARD ---
IF(NHYDR .EQ. 0) GO TO 6
--- READ NODE COORDINATES FOR A MAXIMUM OF 13 HYDROGRAPHS ---
IF (NHYDR.GT.13) NHYDR=13
IF(NHYDR .LT. -13) NHYDR = -13
NHYDR2 = IABS(NHYDR)
READ(R, 341) (IHYDR(J), JHYDR(J), J = 1, NHYDR2)
IF(ICPY .GE. 1 .AND. NHYDR .GE. 0) WRITE(KCPY, 9060)
* (IHYDR(J), JHYDR(J), J = 1, NHYDR2)
IF(ICPY .GE. 1 .AND. NHYDR .LT. 0) WRITE(KCPY, 9062)
* (IHYDR(J), JHYDR(J), J = 1, NHYDR2)
JMI=IFILE(7)
IF(NHYDR .GT. 0) REWIND JMI
CONTINUE
.....
---READ GROUP II DATA---
READ (R,340) NPER,DIML,DIMW,KTH,LENGTH,ERR,HMAX,ITMAX,EROR,SS,GET,
1 ETDIST,FACTX,FACTY,SSRIV
IF(ICPY .GE. 1) WRITE(KCPY, 9070) NPER, DIML, DIMW, KTH, LENGTH
* , ERR, HMAX, ITMAX, EROR, SS, GET, ETDIST, FACTX, FACTY, SSRIV
IF (ITMAX.GT.100) ITMAX=100
IF (FACTX.LE.0.0) FACTX=1.0
IF (FACTY.LE.0.0) FACTY=1.0
IF (ETDIST.LE.0.0) ETDIST=1.0
IF(ICPY .GE. 2) WRITE(KCPY, 9072) NPER, DIML, DIMW, KTH, LENGTH
* , ERR, HMAX, ITMAX, EROR, SS, GET, ETDIST, FACTX, FACTY, SSRIV
INDI=DIML-1
JNDI=DIMW-1
*RIE (P,880) NPER,DIML,DIMW,KTH,ERR,ITMAX,EROR,SS,SSRIV,GET,
1 ETDIST,FACTX,FACTY
IF(DIML.LE.IZ .AND. DIMW.LE. JZ) GO TO 7
*RITE(P, 7007)
GO TO 600
.....
---READ CUMULATIVE MASS BALANCE PARAMETERS FOR CONTINUATION OF
A PREVIOUS SIMULATION (GROUP II DATA)---
7 IF(IRDINI .GT. 0) GO TO 8
READ(R, 1090) SUM, SUMP, ETLXPT, QRET, QRETN, FLUXT, FLXNT
* , CHST, CHDT, CFLXPT, CFLXNT, PUMPT, PUMPPT, STORT
IF(ICPY .GE. 1) WRITE(KCPY, 9080) SUM, SUMP, PUMPT, CFLXPT, QRET
* , QRETN, CHST, CHDT, CFLXPT, CFLXNT, PUMPT, PUMPPT, STORT
GO TO 20
9 JMI=IFILE(5)
READ(JMI) SUM, SUMP, ETLXPT, QRET, QRETN, FLUXT, FLXNT
* , CHST, CHDT, CFLXPT, CFLXNT, PUMPT, PUMPPT, STORT
IF(ICPY .GE. 2) WRITE(KCPY, 9080) SUM, SUMP, PUMPT, CFLXPT, QRET
* , QRETN, CHST, CHDT, CFLXPT, CFLXNT, PUMPT, PUMPPT, STORT
*RITE (P,830) SUM
.....
---READ GROUP III DATA---
.....PHI (HEAD AT THE END OF A PREVIOUS SIMULATION).....
DO 10 I=1,DIML
READ (JMI) (PHI(I,J), J=1,DIMW)
10 *RITE (P,912) I, (PHI(I,J), J=1,DIMW)
.....
.....STRT (STARTING HEAD) .....
20 (ADD 20,000 TO STARTING HEAD AT CONSTANT FLUX BOUNDARY NODES)
IERR=0
IERR2=0
READ(R, 342) SETNAM, FACT, IVAR, IPRN, NOWRNH
IF(ICPY .GE. 1) WRITE(KCPY, 9420) SETNAM, FACT, IVAR, IPRN,NCWRNH
IF(IPRN .GT. 1) IPRN = 1
IF(IPRN .LT. 0) IPRN = 0
IF(ICPY .GE. 2) WRITE(KCPY, 9422) SETNAM, FACT, IVAR, IPRN,NCWRNH
SET=SETID(1)
IF(SETNAM.NE.SET) GO TO 485
IF(IVAR .EQ. 0) WRITE(P, 660) FACT
A2=FACT

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LIST=0
JMI=(FILE(4))
IF (IRJHEQ.EQ.1) IVAR=2
IF (IVAR.GT.0 .AND. IPRN.NE.1) LIST=1
IF (LIST.EQ.1) WRITE(P,820)
DO 50 I=1,DIML
IF (IVAR.EQ.1) READ (R,950) (STR(I,J), J=1,DIMW)
IF (ICPY2.GE.1 .AND. IVAR.EQ.1) WRITE(KCPY,9950) (STR(I,J), J=1,DIMW)
IF (IRJHEQ.EQ.1) READ (JMI) (STR(I,J), J=1,DIMW)
DO 50 J=1,DIMW
IF (IVAR.GT.0) A2=STR(I,J)*FACT
ISUR(I,J)=A2
IF (A2.LT.2.0E4) GO TO 43
C .....CHECK FOR ERRORS IN DATA SPECIFICATIONS.....
IF (I.GT.1 .AND. I.LT.DIML .AND. J.GT.1 .AND. J.LT.DIMW) GO TO 47
IF (MESSG.EQ.1) WRITE(P,7010) I,J
IERR2=1
47 A2=A2-2.0E4
48 IF (A2.GT.EPS1) GO TO 49
WRITE(P,7012) I, J
IERR=1
49 STR(I,J)=A2
IF (SUM.LT.EPS2) PHI(I,J)=A2
50 CONTINUE
IF (ICPY2.GE.3-IVAR) WRITE(KCPY,9952) (STR(I,J), J=1,DIMW)
IF (LIST.EQ.1) WRITE(P,912) I, (ISUR(I,J), J=1,DIMW)
50 CONTINUE
C WRITE (MOVED) BEFORE LOOP
C ..... S (STORAGE COEFFICIENT) .....
READ (R,942) SETNAM, FACT, IVAR, IPRN
IF (ICPY .GE. 1) WRITE(KCPY, 9420) SETNAM, FACT, IVAR, IPRN
IF (MPRN .GT. 1) IPRN = 1
IF (MPRN .LT. 0) IPRN = 0
IF (ICPY .GE. 2) WRITE(KCPY, 9422) SETNAM, FACT, IVAR, IPRN
SET=SETID(2)
IF (SETNAM.NE.SET) GO TO 485
IF (IVAR .EQ. 0) WRITE(P, 670) FACT
A2=FACT
LIST=0
IF (IVAR.EQ.1 .AND. IPRN.NE.1) LIST=1
IF (LIST.EQ.1) WRITE(P,930)
DO 90 I=1,DIML
IF (IVAR.EQ.1) READ (R,860) (S(I,J),J=1,DIMW)
IF (ICPY2.GE.1 .AND. IVAR.EQ.1) WRITE(KCPY,9860) (S(I,J),J=1,DIMW)
DO 30 J=1,DIMW
IF (IVAR.EQ.1) A2=S(I,J)*FACT
S(I,J)=A2
IF (A2.GE.0.0) GO TO 80
C .....CHECK FOR ERRORS IN DATA SPECIFICATIONS.....
IF (I.GT.1 .AND. I.LT.DIML .AND. J.GT.1 .AND. J.LT.DIMW) GO TO 72
IF (MESSG.EQ.1) WRITE(P,7015) I,J
IERR2=1
DO TO 80
72 IF (ISUR(I,J).LT.2.0E4) GO TO 80
IF (MESSG.EQ.1) WRITE(P,7020) I,J
IERR2=1
30 CONTINUE
IF (ICPY2.GE.3-IVAR) WRITE(KCPY,9864) (S(I,J), J=1,DIMW)
IF (LIST.EQ.1) WRITE(P,916) I, (S(I,J), J=1,DIMW)
50 CONTINUE
C ..... T (TRANSMISSIVITY), CR .....
C ..... PERM (HYDRAULIC CONDUCTIVITY) .....
C (READ TRANSMISSIVITY IF IPERM=0, CP
C READ HYDRAULIC CONDUCTIVITY IF IPERM=1)
READ(R, 942) SETNAM, FACT, IVAR, IPRN, IPERM, NLAY, PSCAL
IF (ICPY .GE. 1) WRITE(KCPY, 9420) SETNAM, FACT, IVAR, IPRN, IPERM
* , NLAY, PSCAL
IF (MPRN .GT. 1) IPRN = 1
IF (MPRN .LT. 0) IPRN = 0
IF (MPRN .LT. -1) IPRN = 2
IF (ICPY .GE. 2) WRITE(KCPY, 9422) SETNAM, FACT, IVAR, IPRN, IPERM
* , NLAY, PSCAL
SET=SETID(3)
IF (IPERM.EQ.1) SET=SETID(4)
IF (SETNAM.NE.SET) GO TO 435

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IF(PSCAL .EQ. 0.) PSCAL = 1.
FACT1 = FACT
FACT = FACT*PSCAL
IF(IVAR .EQ. 0 .AND. IPERM .NE. 1) WRITE(P, 720) FACT
IF(IVAR .EQ. 0 .AND. IPERM .EQ. 1) WRITE(P, 730) FACT
-IST2=0
IVPRM = IVAR
IF(IVAR.NE.1 .OR. IPRN.EQ.1) GO TO 132
LIST2=1
IF(IPERM.NE.1) WRITE(P,390)
IF(IPERM.EQ.1) WRITE(P,960)
132 DO 100 I=1,DIML
IF(IVAR.EQ.1) READ(R,850) (T(I,J), J=1,DIMW)
IF(ICPY2.GE.1.AND.IVAR.EQ.1)WRITE(KCPY,9830) (T(I,J),J=1,DIMW)
DO 100 J=1,DIMW
IF(NLAY .GT. 1) KKLAY(I, J) = 0
TR(I,J)=0.0
TC(I,J)=0.0
A2=FACT
IF(IVAR.EQ.1) A2=T(I,J)*FACT
IF(I.EQ.1 .OR. I.EQ.DIML .OR. J.EQ.1 .OR. J.EQ.DIMW) GO TO 148
IF(A2.GT.0.0) GO TO 150
C .....CHECK FOR ERRORS IN DATA SPECIFICATIONS.....
IF(3(I,J).GE.0.0 .AND. ISUR(I,J).LT.2.0E4) GO TO 150
WRITE(P,7025) I, J
IERR=1
148 A2=0.0
150 T(I,J)=A2
IF(ICPY2.GE.3-IVAR) WRITE(KCPY,9864) (T(I,J), J=1,DIMW)
IF(-IST2.EQ.1) WRITE(P,900) I, (T(I,J), J=1,DIMW)
150 CONTINUE
C WRITE MOVED BEFORE LOOP
C WRITE MOVED BEFORE LOOP
IF(IPRN.EQ.2) LIST2=1
NNX=1
IF(-IST2.EQ.1) NNX=0
C .....
C ..... TLAY .....
C ..... LAYER T OR PERM .....
SAT = 0.
IF(NLAY .EQ. 0) GO TO 179
IF(WATER .NE. CHK(2) ) WRITE(P, 7100)
IF(WATER .NE. CHK(2) ) GO TO 486
NLAY0 = NLAY
IF(NLAY .LT. 0) NLAY = -NLAY
IF(NLAY .GT. MLAY) WRITE(P, 7007)
IF(NLAY .GT. MLAY) GO TO 486
KLAY1 = 0
IVAR1 = IVAR
IPRN1 = IPRN
IPRM1 = IPRM
SR = 1.
SD0 = 10.
SDJ1 = 0.
SD1 = 0.
KSET1 = IVAR
DO 173 KLAY = 1, NLAY
SAT1 = SAT
READ(R, 842) SETNAM, FACT, IVAR, IPRN, IPRML, SD
IF(ICPY .GE. 1) WRITE(KCPY, 9420)
* SETNAM, FACT, IVAR, IPRN, IPRML, SD
IF(IPRN .GT. 1) IPRN = 1
IF(4P4N .LT. 0) IPRN = 0
IPRM10 = IPRML
IF(IPRM1 .GE. 2) IPRML = IPRML - 2
IF(FACT .NE. 0) GO TO 172
FACT = FACT1
IVAR = IVAR1
IPRN = IPRN1
IPRM1 = IPRM1
172 CONTINUE
FACT1 = FACT
IVAR1 = IVAR
IPRN1 = IPRN
IPRM1 = IPRML
FACT = FACT*PSCAL
C
C SAT, SD SET TO MATCH S2, S
OF PROGRAM (G808) PSEUDO-

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HYDROGRAPH GENERATION
 IF IPRML LT 2,
 SD, PERM/T FOR INTERVAL
 IF IPRML GE 2,
 SD, PERM/T CUMULATIVE

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IF(SD .LE. 0.) SD = SD1 + SJD*SR
SDD = SD - SD1
IF(SDD1 .GT. 0.) SR = SDD/SDD1
SD1 = SD
SDD1 = SDD
IF(ICPY .GE. 2) WRITE(KCPY, 9422)
* SETNAM, FACT, IVAR, IPRN, IPRML, SAT
SET = SETID(3)
IF(IPRML .EQ. 1) SET = SETID(4)
IF(SETNAM .NE. SET) GO TO 485
SAT = SD
IF(IPRML0 .LT. 2) SAT = SAT1 + SAT
SATL(KLAY) = SAT
SD = SAT - SAT1
IF(IVAR .EQ. 0 .AND. IPRML .NE. 1) WRITE(P, 720) FACT
IF(IVAR .EQ. 0 .AND. IPRML .EQ. 1) WRITE(P, 730) FACT
LIST = 0
IF(IVAR .EQ. 1 .AND. IPRN .NE. 1) LIST = 1
IF(LIST .EQ. 1 .AND. IPRML .NE. 1) WRITE(P, 860)
IF(LIST .EQ. 1 .AND. IPRML .EQ. 1) WRITE(P, 960)
IF(IPRML .EQ. 1) FACT = FACT*SD
KSET = 0
IF(KSET1 .EQ. 0 .AND. IVAR .EQ. 1) KSET = 1
DO 177 I = 1, DIML
      BORROW DELX FOR TEMP
IF(IVAR .EQ. 1) READ(R, 860) (DELX(J), J = 1, DIMW)
IF(ICPY2 .GE. 1 .AND. IVAR .EQ. 1) WRITE(KCPY, 9860)
* (DELX(J), J = 1, DIMW)
DO 175 J = 1, DIMW
A2 = FACT
IF(IVAR .EQ. 1) A2 = DELX(J)*FACT
IF(KLAY1 .GT. 0) A2 = A2 + TLAY(I, J, KLAY1)
IF(A2 .EQ. 0) GO TO 173
IF(T(I, J) .GT. 0.) GO TO 173
A2 = J.
IF(IVAR .NE. 1) GO TO 173
WRITE(P, 7105) I, J
IERR = 1
173 CONTINUE
      TLAY(I, J, KLAY) = A2
IF(KSET .GT. 0 .AND. A2 .EQ. 0.) T(I, J) = 0.
175 CONTINUE
IF(ICPY2 .GE. 2 - IVAR) WRITE(KCPY, 9864)
* (TLAY(I, J, KLAY), J = 1, DIMW)
IF(LIST .EQ. 1) WRITE(P, 900) I, (TLAY(I, J, KLAY), J = 1, DIMW)
177 CONTINUE
      KLAY1 = 0
IF(IPRML0 .LT. 2) KLAY1 = KLAY
IF(KSET .GT. 0) KSET1 = 1
178 CONTINUE
179 CONTINUE
      SAT1 = SAT
      SAT = SAT1
      ..... BOTTOM (AQ, BOTTOM EL.) .....
      (CODE ISATHK=1 TO SUPPRESS PRINTING A SAT, THKNS, MAP)
ISATHK=1
ND=J
<TOP>=0
IF(WATER.NE.CHK(2).AND.IPERM.EQ.0) GO TO 224
READ (R,842) SETNAM, FACT, IVAR, IPRN, ISATHK
* , WELBOT
IF(ICPY .GE. 1) WRITE(KCPY, 9420) SETNAM, FACT, IVAR, IPRN, ISATHK
* , WELBOT
IF(4PRN .GT. 0) ISATHK = 1
IF(4PRN .GT. 1) IPRN = 1
IF(4PRN .LT. 0) IPRN = 0
IF(4PRN .LT. -1) ISATHK = 0
IF(WELBOT .EQ. 0.) WELBOT = 5.
IF(ICPY .GE. 2) WRITE(KCPY, 9422) SETNAM, FACT, IVAR, IPRN, ISATHK
* , WELBOT
SET=SETID(5)
IF(SETNAM.NE.SET) GO TO 485
IF(IVAR .EQ. 0) WRITE(P, 740) FACT

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A2=FACT
LIST=0
IF (IVAR.EQ.1 .AND. IPPN.NE.1) LIST=1
IF (LIST.EQ.1) WRITE(P,970)
DO 190 I=1,DIML
IF (IVAR.EQ.1) READ (R,860) (BOTTOM(I,J),J=1,DIMW)
IF(ICPY2.GE.1.AND.IVAR.EQ.1)WRITE(KCPY,9860)(BOTTOM(I,J),J=1,DIMW)
DO 190 J=1,DIMW
IF(IVAR.EQ.1) A2=BOTTOM(I,J)*FACT
BOTTOM(I,J)=A2
180 CONTINUE
IF(ICPY2.GE.3-IVAR) WRITE(KCPY,9862) (BOTTOM(I,J), J=1,DIMW)
IF(LIST.EQ.1) WRITE(P,912) I, (BOTTOM(I,J), J=1,DIMW)
190 CONTINUE
C WRITE MOVED BEFORE LCOF
C ..... SY (SPECIFIC YIELD) .....
IF(AATER.NE.CHK(2)) GO TO 224
READ(R,842) SETNAM, FACT, IVAR, IPPN, NSY, SYR, SYB
IF(ICPY.GE.1) WRITE(KCPY,9420) SETNAM, FACT, IVAR, IPPN
* . NSY, SYR, SYB
IF(IPRN.GT.1) IPPN = 1
IF(IPRN.LT.0) IPPN = 0
IF(SYR.EQ.0.) SYR = 0.1
IF(SYR.LT.0.) SYR = 0.
FACT2 = SYR*ALOG10(PSCAL)
IF(SYB.EQ.0) SYB = .01
IF(ICPY.GE.2) WRITE(KCPY,9422) SETNAM, FACT, IVAR, IPPN
* . NSY, SYR, SYB
SET=SETID(6)
IF(SETNAM.NE.SET) GO TO 435
C OPTION MOVED TO 13352
IF(IVAR.EQ.0) FACT = FACT + FACT2
IF(IVAR.EQ.1) WRITE(P,680) FACT
C INITIALIZE MOVED TO 13685
LIST=0
IF (IVAR.EQ.1 .AND. IPPN.NE.1) LIST=1
IF (LIST.EQ.1) WRITE(P,1120)
PRMSY(1) = 0.
IF(NSY.EQ.0) GO TO 209
NSY0 = NSY
IF(NSY.LT.0) NSY = -NSY
IF(NSY.EQ.1) NSY = 2
READ(R,840) (PRMSY(I), SYPRM(I), I = 1, NSY)
IF(ICPY.GE.1) WRITE(KCPY,9950) (PRMSY(I), SYPRM(I), I = 1, NSY)
A2 = PRMSY(1)
SD = SYPRM(1)
DO 203 I = 2, NSY
A3 = A2
A2 = PRMSY(I)
SD1 = SD
SD = SYPRM(I)
IF(A3.LE.0.) WRITE(P,7110)
IF(A3.LE.0.) GO TO 486
SYPRM(I) = SD1
SY(I) = (SD - SD1)/ALOG10(A2/A3)
208 CONTINUE
209 CONTINUE
A2 = FACT
DO 220 I = 1, DIML
IF (IVAR.EQ.1) READ (R,860) (SY(I,J),J=1,DIMW)
IF(ICPY2.GE.1.AND.IVAR.EQ.1)WRITE(KCPY,9868) (SY(I,J),J=1,DIMW)
DO 210 J=1,DIMW
IF(IVAR.EQ.1) A2 = SY(I, J)*FACT + FACT2
SY(I,J)=A2
210 CONTINUE
IF(ICPY2.GE.3-IVAR) WRITE(KCPY,9864) (SY(I,J), J=1,DIMW)
IF(LIST.EQ.1) WRITE(P,916) I, (SY(I,J), J=1,DIMW)
220 CONTINUE
C WRITE MOVED BEFORE LCOF
C ..... TOP (AQ. TCP ELEVATION) .....
VALUES OF TOP ARE REQUIRED FOR SIMULATION OF THE FOLLOWING:
1. ARTESIAN AQUIFERS WITH OR WITHOUT LEAKAGE,
2. N.T.-ARTESIAN SYSTEMS WITH OR WITHOUT LEAKAGE,
3. N.T. AQUIFERS WITH LEAKAGE FROM STREAMS.
IF(LJNVRT.NE.CHK(7)) GO TO 254
224 KTOP=1

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      READ(R, 942) SETNAM, FACT, IVAR, IPRN
      IF(ICPY .GE. 1) WRITE(KCPY, 9420) SETNAM, FACT, IVAR, IPRN
      IF(IPRM .GT. 1) IPRN = 1
      IF(IPRM .LT. 0) IPRN = 0
      IF(ICPY .GE. 2) WRITE(KCPY, 9422) SETNAM, FACT, IVAR, IPRN
      SET=SET10(7)
      IF(SETNAM.NE.SET) GO TO 485
      IF(IVAR .EQ. 0) WRITE(P, 750) FACT
      A2=FACT
      LIST=0
      IF (IVAR.EQ.1 .AND. IPRN.NE.1) LIST=1
      IF (LIST.EQ.1) WRITE(P,980)
      DO 250 I=1,DIML
      IF (IVAR.EQ.1) READ (R,950) (TOP(I,J),J=1,DIMW)
      IF (IVAR.EQ.1) READ (R,950) (TOP(I,J),J=1,DIMW)
      IF(ICPY2.GE.1.AND. IVAR.EQ.1)WRITE(KCPY,9950) (TOP(I,J),J=1,DIMW)
      DO 240 J=1,DIMW
      IF(IVAR.EQ.1) A2=TOP(I,J)*FACT
      TOP(I,J)=A2
      C .....CHECK FOR ERRORS IN DATA SPECIFICATIONS.....
      IF(.NOT.(PHI(I,J)).GT.A2 .OR. WATER.EQ.CHK(2)) GO TO 240
      WRITE(P,7030) I, J
      IERR=1
      240 CONTINUE
      IF(ICPY2.GE.3-IVAR) WRITE(KCPY,9952) (TOP(I,J), J=1,DIMW)
      IF(.IST.EQ.1) WRITE(P,912) I, (TOP(I,J), J=1,DIMW)
      250 CONTINUE
      C WRITE (MVE) BEFORE LOOP
      C .....CALCULATE TRANSMISSIVITY FOR WATER-TABLE OR ARTESIAN AQUIFER...
      C (NEW PROCEDURE - ADDED BY D.B. SAPIK)
      254 IF (IPERM.EQ.0) GO TO 168
      IF(.LIST2.EQ.1) WRITE(P,892)
      DO 134 I=1,DIML
      DO 162 J=1,DIMW
      A2=PHI(I,J)
      A3 = ABS(T(I, J))
      IF(A3 .LE. EPS1) GO TO 159
      IF(A2 .GE. BOTTOM(I, J)+THIN) GO TO 256
      IF(.NOT.(HMIN .LE. 0) .AND. WATER.EQ.CHK(2)) WRITE(P, 7032) I, J
      A2 = BOTTOM(I, J) + THIN
      IERR2 = 1
      255 IF(.NOT.(TOP.NE.1)) GO TO 161
      A2 = AMINI(A2, TOP(I, J))
      IF(A2 .GT. BOTTOM(I, J)) GO TO 161
      C .....CHECK FOR ERRORS IN DATA SPECIFICATIONS.....
      C CARD DELETED
      IF(4ESSG .EQ. 1 .AND. IPRM .EQ. 1) WRITE(P, 7034) I, J
      IERR2=1
      NJ=3
      159 A3=0.0
      161 IF(WATER.EQ.CHK(2)) PERM(I,J)=A3
      HMIN = A2 - BOTTOM(I, J)
      PHE(I, J) = HMIN
      T(I,J)=A3*HMIN
      IF(HMIN .GT. SAT) SAT = HMIN
      162 CONTINUE
      IF(.LIST2.EQ.1) WRITE(P,900) I, (T(I,J), J=1,DIMW)
      164 CONTINUE
      IF(NNX.EQ.1) WRITE(P,894)
      GO TO 258
      C .....CALCULATE HYDRAULIC COND. FOR WATER-TABLE AQUIFER...
      C (NEW PROCEDURE - ADDED BY D.B. SAPIK)
      168 IF(WATER.NE.CHK(2)) GO TO 250
      IF(.LIST2.EQ.1) WRITE(P,962)
      DO 196 I=1,DIML
      DO 194 J=1,DIMW
      A2=STR(I,J)
      TPA=TOP(I,J)
      IF(.NOT.(TPA.EQ.1)) A2=AMINI(A2,TPA)
      HMIN=A2-BOTTOM(I,J)
      PHE(I,J)=HMIN
      A3=ABS(T(I,J))
      IF (HMIN.GT.1.001) GO TO 193
      C .....CHECK FOR ERRORS IN DATA SPECIFICATIONS.....
      IF(A3.LE.EPS1) GO TO 192
      IF(4ESSG .EQ. 1 .AND. IPRM .EQ. 1) WRITE(P, 7036) I, J

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IERK2=1
ND=3
192 T(I,J)=0.0
A3=0.0
1MIN=1.0
193 PERM(I,J)=A3/HMIN
IF(1MIN.GT.SAT) SAT = HMIN
194 CONTINUE
IF(_LIST2.EQ.1) WRITE(P,900) I, (PERM(I,J), J=1,DIMW)
196 CONTINUE
IF(NNX.EQ.1) WRITE(P,964)
IF(SUM.GT.0.0) ISATHK=1

C
C ..... PRINT SATURATED THICKNESS MAP FOR WATER-TABLE OR .....
C ..... WATER-TABLE/ARTESIAN AQUIFER .....
258 CONTINUE
IF(.NOT.(ISATHK.EQ.0 .OR. (ND.EQ.3 .AND. MESSG.EQ.1))) GO TO 260
WRITE(P,974)
DO 220 I=1,DIML
WRITE(P,912) I, (PHE(I,J), J=1,DIMW)
220 CONTINUE

C
C ..... RATE (CONF. BED CONDUCTIVITY) .....
260 IF (LEAK.NE.CHK(9)) GO TO 350
READ (R,842) SETNAM, FACT, IVAR, IPRN
IF(ICPY.GE.1) WRITE(KCPY, 9420) SETNAM, FACT, IVAR, IPRN
IF(MPRN.GT.1) IPRN = 1
IF(MPRN.LT.0) IPRN = 0
IF(ICPY.GE.2) WRITE(KCPY, 9422) SETNAM, FACT, IVAR, IPRN
SET=SETID(8)
IF(SETNAM.NE.SET) GO TO 435
IF(IVAR.EQ.0) WRITE(P, 590) FACT
A2=FACT
_LIST=J
IVRAT = IVAR
IF (IVAR.EQ.1 .AND. IPRN.NE.1) LIST=1
IF (_LIST.EQ.1) WRITE(P,370)
DO 290 I=1,DIML
IF (IVAR.EQ.1) READ (R,860) (RATE(I,J), J=1,DIMW)
IF(ICPY2.GE.1.AND.IVAR.EQ.1) WRITE(KCPY,9360) (RATE(I,J), J=1,DIMW)
DO 290 J=1,DIMW
R(I,J)=0.0
IF(IVAR.EQ.1) A2=RATE(I,J)*FACT
RATE(I,J)=A2
280 CONTINUE
IF(ICPY2.GE.3-IVAR) WRITE(KCPY,9864) (RATE(I,J), J=1,DIMW)
IF(_LIST.EQ.1) WRITE(P,900) I, (RATE(I,J), J=1,DIMW)
290 CONTINUE
WRITE (P,912) BEFORE LOOP

C
C ..... RIVER (HEAD IN RIVER) .....
C ..... (CODE ISTEDEY=1 TO SET RIVER HEAD EQUAL TO STARTING
C ..... AQUIFER HEAD FOR STEADY-STATE SIMULATION)
READ (R,842) SETNAM, FACT, IVAR, IPRN, ISTEDEY
IF(ICPY.GE.1) WRITE(KCPY, 9420) SETNAM, FACT, IVAR, IPRN, ISTEDEY
IF(MPRN.GT.1) IPRN = 1
IF(MPRN.LT.0) IPRN = 0
IF(ICPY.GE.2) WRITE(KCPY, 9422) SETNAM, FACT, IVAR, IPRN, ISTEDEY
SET=SETID(9)
IF(SETNAM.NE.SET) GO TO 435
IF(IVAR.EQ.0 .AND. ISTEDEY.NE.1) WRITE(P, 700) FACT
A2=FACT
IVRIV = IVAR
LIST=0
IF ((IVAR.EQ.1 .OR. ISTEDEY.EQ.1) .AND. IPRN.NE.1) LIST=1
IF (_LIST.EQ.1) WRITE(P,1040)
DO 320 I=1,DIML
IF (IVAR.EQ.1) READ (R,860) (RIVER(I,J), J=1,DIMW)
IF(ICPY2.GE.1.AND.IVAR.EQ.1) WRITE(KCPY,9360) (RIVER(I,J), J=1,DIMW)
DO 310 J=1,DIMW
IF(IVAR.EQ.1) A2=RIVER(I,J)*FACT
IF(ISTEDEDY.EQ.1) A2=STRT(I,J)+FACT
RIVER(I,J)=A2
310 CONTINUE
IF(ICPY2.GE.3-IVAR) WRITE(KCPY,9862) (RIVER(I,J), J=1,DIMW)
IF(_LIST.EQ.1) WRITE(P,912) I, (RIVER(I,J), J=1,DIMW)
320 CONTINUE
WRITE (P,912) BEFORE LOOP
IF (ISTEDEDY.EQ.1) WRITE (P,1041) FACT

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C ..... M (CONF, BED THICKNESS) .....
C (CODE NEGATIVE VALUES FOR STREAM BED THICKNESS)
READ(R, 342) SETNAM, FACT, IVAR, IPRN
IF(ICPY .GE. 1) WRITE(KCPY, 9420) SETNAM, FACT, IVAR, IPRN
IF(IPRN .GT. 1) IPRN = 1
IF(IPRN .LT. 0) IPRN = 0
IF(ICPY .GE. 2) WRITE(KCPY, 9422) SETNAM, FACT, IVAR, IPRN
SET=SETID(10)
IF(SETNAM.NE.SET) GO TO 435
IF(IVAR.EQ. 0) WRITE(P, 710) FACT
A2=FACT
ND=0
LIST=0
IF (IVAR.EQ.1 .AND. IPRN.NE.1) LIST=1
IF (LIST.EQ.1) WRITE(P,1030)
DO 350 I=1,DIML
IF (IVAR.EQ.1) READ (R,360) (M(I,J),J=1,DIMW)
IF (ICPY2.GE.1 .AND. IVAR.EQ.1) WRITE(KCPY,9360) (M(I,J),J=1,DIMW)
DO 340 J=1,DIMW
A2 = FACT
IF(IVAR.EQ.1) A2=M(I,J)*FACT
IF(IVAR.EQ. 0 .AND. RATE(I, J).EQ. 0.) A2 = 0,
M(I,J)=A2
IF(A2.LT.0.0) ND=1
IF(IVRAT.EQ. 0 .AND. A2.EQ. 0.) RATE(I, J) = 0.
IF(IVRIV.EQ. 0 .AND. A2.EQ. 0.) RIVER(I, J) = 2E4
.....CHECK FOR ERRORS IN SPECIFICATION OF VALUES FOR RATE, M,
C RIVER, TOP, ISUR, S, AND T.
C
A3=0.0
IF(CONVRT.EQ.CHK(7)) A3=TOP(I,J)
IF(RATE(I, J).EQ. 0.) GO TO 340
333 HMIN=RIVER(I,J)
IF (ISUR(I,J).GE.2.0E4) GO TO 340
IF(A2.EQ.0.0 .OR. HMIN.EQ.0.0 .OR. S(I,J).LT.0.0 .OR.
1 ISUR(I,J).GE.2.0E4 .OR. T(I,J).EQ.0.0) GO TO 333
IF(A3.EQ.0.0 .OR. (A3.LT.2.0E4 .AND. HMIN.GT.A3)) GO TO 340
333 IERR=1
WRITE(P,7045) I, J
340 CONTINUE
IF(ICPY2.GE.3-IVAR) WRITE(KCPY,9862) (M(I,J), J=1,DIMW)
IF(LIST.EQ.1) WRITE(P,912) I, (M(I,J), J=1,DIMW)
350 CONTINUE
C WRITE MVED BEFORE LOOP
IF(.NOT. (ND.EQ.1 .AND. WATER.EQ.CHK(2) .AND. CONVRT.NE.CHK(7)))
1 GO TO 360
WRITE(P,7040)
IERR=1
C
C ..... LAND (LAND ELEVATION) .....
300 IF(EVAP.NE.CHK(6) .OR. WATER.NE.CHK(2)) GO TO 400
READ(R, 342) SETNAM, FACT, IVAR, IPRN, NOWRN
* * * * * WELTOP
IF(ICPY .GE. 1) WRITE(KCPY, 9420) SETNAM, FACT, IVAR, IPRN, NOWRN
* * * * * WELTOP
IF(IPRN .GT. 1) IPRN = 1
IF(IPRN .LT. 0) IPRN = 0
IF(WELTOP .EQ. 0.) WELTOP = 2E4
IF(ICPY .GE. 2) WRITE(KCPY, 9422) SETNAM, FACT, IVAR, IPRN, NOWRN
* * * * * WELTOP
SET=SETID(11)
IF(SETNAM.NE.SET) GO TO 435
IF(IVAR.EQ. 0) WRITE(P, 760) FACT
A2=FACT
LIST=0
IF (IVAR.EQ.1 .AND. IPRN.NE.1) LIST=1
IF (LIST.EQ.1) WRITE(P,990)
DO 350 I=1,DIML
IF (IVAR.EQ.1) READ (R,840) (LAND(I,J),J=1,DIMW)
IF (ICPY2.GE.1 .AND. IVAR.EQ.1) WRITE(KCPY,9950) (LAND(I,J),J=1,DIMW)
DO 380 J=1,DIMW
IF(IVAR.EQ.1) A2=LAND(I,J)*FACT
LAND(I,J)=A2
IF(A2.GE.2.0E4) GO TO 380
.....CHECK FOR ERRORS IN DATA SPECIFICATIONS.....
A3=0.0
IF(CONVRT.EQ.CHK(7)) A3=TOP(I,J)
HMIN=0.0
IF(LAND.NE.CHK(9)) GO TO 376

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MMIN=M(I,J)
IF(RATE(I,J).EQ.0.0) GO TO 376
IF(MMIN) 372, 376, 374
372 IF(MESSG.EQ.1.AND.NOWRN.EQ.0) WRITE(P,7058) I, J
IERR2=1
IF(A3.EQ.0.OR.A2.GT.A3) GO TO 376
IF(MESSG.EQ.1) WRITE(P,7057) I, J
IERR2=1
GO TO 370
374 WRITE(P,7059) I, J
IERR=1
LAND(I,J)=2.0E4
GO TO 360
370 IF(START(I,J).LE.A2) GO TO 380
IF(A3.GT.0.AND.A2.GE.A3) GO TO 380
WRITE(P,7060) I, J
IERR=1
380 CONTINUE
IF(ICPY2.GE.3-IVAR) WRITE(KCPY,9952) (LAND(I,J), J=1,DIMW)
IF(_IST.EQ.1) WRITE(P,912) I, (LAND(I,J), J=1,DIMW)
390 CONTINUE
WRITE MOVED BEFORE LOOP
C ..... QRE (RECHARGE RATE) .....
400 IF (RECH.NE.CHK(10)) GO TO 440
READ(R, 842) SETNAM, FACT, IVAR, IPRN, NOWRN
IF(ICPY.GE.1) WRITE(KCPY, 9420) SETNAM, FACT, IVAR, IPRN, NOWRN
IF(IPRN.GT.1) IPRN = 1
IF(IPRN.LT.0) IPRN = 0
IF(ICPY.GE.2) WRITE(KCPY, 9422) SETNAM, FACT, IVAR, IPRN, NOWRN
SET=SETID(12)
IF(SETNAM.NE.SET) GO TO 485
IF(IVAR.EQ.0) WRITE(P, 770) FACT
A2=FACT
-IST=0
JMI=IFILE(2)
IF (IRDRCH.EQ.1) IVAR=2
IF (IVAR.GT.0.AND.IPRN.NE.1) LIST=1
IF (_IST.EQ.1) WRITE(P,1000)
DO +30 I=1,DIML
IF(IVAR.GT.0) READ(R, 860) (QRE(I, J), J = 1, DIMW)
IF(ICPY2.GE.1.AND.IVAR.EQ.1) WRITE(KCPY,9360) (QRE(I, J), J=1,DIMW)
IF (IRDRCH.EQ.1) READ (JMI) (QRE(I, J), J=1,DIMW)
DO +20 J=1,DIMW
IF(IVAR.EQ.1) A2=QRE(I, J)*FACT
IF(IVAR.EQ.2) A2 = QRE(I, J) + FACT
JRE(I, J)=A2
IF(A2.EQ.0) GO TO 420
C .....CHECK FOR ERRORS IN DATA SPECIFICATIONS.....
IF(ISJR(I, J).LT.2.0E4.AND.S(I, J).GE.0.0.AND.T(I, J).GT.0.0)
L GO TO 404
IF (ISJR(I, J).GE.2.0E4) GO TO 420
IF(MESSG.EQ.1.AND.IVAR.EQ.1) WRITE(P, 7065) I, J
IERR2=1
JRE(I, J)=0.0
GO TO 420
404 IF(LEAK.NE.CHK(9).OR.CONVRT.NE.CHK(7)) GO TO 420
IF(RATE(I, J).EQ.0.0) GO TO 420
IF(W(I, J).GT.0.0) GO TO 406
IF(MESSG.EQ.1.AND.NOWRN.EQ.0) WRITE(P, 7066) I, J
IERR2=1
GO TO 420
406 IF(MESSG.EQ.1) WRITE(P,7067) I, J
IERR2=1
420 CONTINUE
IF(ICPY2.GE.3-IVAR) WRITE(KCPY,9864) (QRE(I, J), J=1,DIMW)
IF(_IST.EQ.1) WRITE(P,900) I, (QRE(I, J), J=1,DIMW)
430 CONTINUE
C ..... WELLD .....
440 IF(JW.LE.1) GO TO 450
C CARD DELETED
C CARD DELETED
DO 441 I = 1, DIML
DO 441 J = 1, DIMW
441 WELLD(I, J) = 0.
READ(R, 842) SETNAM, FACT, IVAR, IPRN, IWCUM, WSCALE, CFSCAL
IF(ICPY.GE.1) WRITE(KCPY, 9420) SETNAM, FACT, IVAR, IPRN, IWCUM
* , WSCALE, CFSCAL

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IF(SETNAM .NE. SETID(15)) GO TO 452
IF(WSCALE .EQ. 0.) WSCALE = 1.
IF(CFSCAL .EQ. 0.) CFSCAL = 1.
C
C
CARD DELETED
CARD DELETED
IF(IVAR .GT. 0) GO TO 444
IF(ICPY .GE. 2) WRITE(KCPY, 9422) SETNAM, FACT, IVAR, IPRN, INCUM
* * WSCALE, CFSCAL
WRITE(P, 775) FACT
DO 443 I = 1, DIML
DO 442 J = 1, DIMW
IF(T(I, J) .GT. 0.) WELLD(I, J) = FACT
442 CONTINUE
IF(ICPY2 .GE. 3) WRITE(KCPY, 9864) (WELLD(I, J), J = 1, DIMW)
443 CONTINUE
GO TO 450
444 IF(IPRN .GT. 1) IPRN = 1
IF(IPRN .LT. 0) IPRN = J
IF(ICPY .GE. 2) WRITE(KCPY, 9422) SETNAM, FACT, IVAR, IPRN, INCUM
* * WSCALE, CFSCAL
IF(IPRN .EQ. 0) WRITE(P, 1150)
DO 445 I = 1, DIML
READ(R, 300) (WELLD(I, J), J = 1, DIMW)
IF(ICPY2 .GE. 1) WRITE(KCPY, 9860) (WELLD(I, J), J = 1, DIMW)
DO 447 J = 1, DIMW
A2 = WELLD(I, J)*FACT
IF(ISUR(I, J) .GE. 2E4) A2 = WELLD(I, J)*CFSCAL
IF(A2 .EQ. 0. .OR. T(I, J) .GT. 0.) GO TO 446
IF(MESS .EQ. 1) WRITE(P, 3015) I, J
IERR2 = 1
A2 = 0.
446 CONTINUE
WELLD(I, J) = A2
447 CONTINUE
IF(ICPY2 .GE. 2) WRITE(KCPY, 9864) (WELLD(I, J), J = 1, DIMW)
IF(IPRN .EQ. 0) WRITE(P, 900) I, (WELLD(I, J), J = 1, DIMW)
448 CONTINUE
C
..... DELX, DELY .....
450 READ(R, 342) SETNAM, FACT, IVAR, IPRN
IF(ICPY .GE. 1) WRITE(KCPY, 9420) SETNAM, FACT, IVAR, IPRN
452 SET = SETID(13)
IF(SETNAM .NE. SET) GO TO 485
A2 = FACT
IF(IVAR .EQ. 1) READ(R, 840) (DELX(J), J = 1, DIMW)
IF(ICPY2 .GE. 1 .AND. IVAR .EQ. 1) WRITE(KCPY, 9950) (DELX(J), J = 1, DIMW)
DO 453 J = 1, DIMW
IF(IVAR .EQ. 1) A2 = DELX(J)*FACT
DELX(J) = A2
450 CONTINUE
IF(ICPY2 .GE. 3 - IVAR) WRITE(KCPY, 9952) (DELX(J), J = 1, DIMW)
IF(IVAR .EQ. 1 . AND. IPRN .NE. 1) WRITE(P, 1020) (DELX(J), J = 1, DIMW)
IF(IVAR .EQ. 0) WRITE(P, 780) FACT
C
READ (R,342) SETNAM, FACT, IVAR, IPRN
IF(ICPY .GE. 1) WRITE(KCPY, 9420) SETNAM, FACT, IVAR, IPRN
SET=SETID(14)
IF(SETNAM.NE.SET) GO TO 485
A2=FACT
IF (IVAR.EQ.1) READ (R,840) (DELY(I),I=1,DIML)
IF(ICPY2.GE.1.AND.IVAR.EQ.1)WRITE(KCPY,9950) (DELY(I), I=1,DIML)
DO 480 I=1,DIML
IF(IVAR.EQ.1) A2=DELY(I)*FACT
DELY(I)=A2
480 CONTINUE
IF(ICPY2.GE.3-IVAR) WRITE(KCPY,9952) (DELY(I), I=1,DIML)
IF(IVAR.EQ.1.AND.IPRN.NE.1) WRITE(P,1030) (DELY(I), I=1,DIML)
IF (IVAR.EQ.0) WRITE (P,790) FACT
C
IF (KED.EQ.3) GO TO 484
IF (IERR1.GT.0 .AND. (KED.LT.2 .OR. KED.EQ.4)) GO TO 486
IF (IERR2.GT.0 .AND. KED.EQ.0) GO TO 486
C
.....
C
... CALCULATE THE INITIAL MASS BALANCE RESIDUAL AT EACH NODE AND ADD
TJ RECHARGE.
IF (MBRES.NE.1) GO TO 482

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WRITE (P,1085)
IF (RECH.EQ.CHK(10)) WRITE (P,1087)
WRITE (P,945)
SUMRES=0.0
DO 1230 I=1,DIML
YVAL=DELY(I)
DO 1230 J=1,DIMW
PHE(I,J)=0.0
IF (T(I,J).LT.EPS1 .OR. S(I,J).LT.0.0) GO TO 1230
IM1=I-1
IP1=I+1
JM1=J-1
JP1=J+1
XVAL=DELX(J)
TM1=STRT(I,J)
TT=T(I,J)
TM=T(I,JM1)
RES= 2.*TT*TM*FACTX*(STRT(I,JM1)-HMIN)/((TT*DELX(JM1)+TM*XVAL)*
5 XVAL)
TM=T(I,JP1)
RES=RES+2.*TT*TM*FACTX*(STRT(I,JP1)-HMIN)/((TT*DELX(JP1)+TM*XVAL)*
5 XVAL)
TM=T(IM1,J)
RES=RES+2.*TT*TM*FACTY*(STRT(IM1,J)-HMIN)/((TT*DELY(IM1)+TM*YVAL)*
5 YVAL)
TM=T(IP1,J)
RES=RES+2.*TT*TM*FACTY*(STRT(IP1,J)-HMIN)/((TT*DELY(IP1)+TM*YVAL)*
5 YVAL)
PHE(I,J)=RES
SUMRES=SUMRES+RES
IF (RECH.EQ.CHK(10)) QRE(I,J)=QRE(I,J)+RES
1230 CONTINUE
WRITE (P,900) I, (PHE(I,J), J=1,DIMW)
1250 CONTINUE
WRITE (P,1086) SUMRES
C
C.....
C---INITIALIZE VARIABLES---
482 CONTINUE
ETQ3=0.0
ETQJ=0.0
SLEAK=0.0
SUBS=0.0
JT=0.0
TT=0.0
IM=MIN(0*DIMW+4,124)
IM=(102-IM)/2
VF4(3) = DIGIT(IM)
VF4(3) = DIGIT(IM + 5)
IF(NLAY .EQ. 0) GO TO 4829
IF(NLAY .GE. MLAY) WRITE(P, 7007)
IF(NLAY .GE. MLAY) GO TO 486
NLAY1 = NLAY
NLAY = NLAY + 1
SAT = SAT + 1.
SAT(NLAY) = SAT
DO 4823 I = 1, DIML
DO 4823 J = 1, DIMW
A2 = PERM(I, J)*SAT
IF(A2 .LE. TLAY(I, J, NLAY1) ) A2 = TLAY(I, J, NLAY1)
* + PERM(I, J)*(SAT - SAT1)
TLAY(I, J, NLAY) = A2
IF(A2 .GT. 0.) KKLAY(I, J) = NLAY + 1
4823 CONTINUE
4829 CONTINUE
IF(KPLT .GT. 0) CALL PLTXI(KPLT, KPLC, DIML, DIMW,DELX(1),DELY(1))
IF(NLAY0 .LT. 0) CALL NEWSTP
IF(NLAY0 .LT. 0) NLAY = 0
RETURN
C
C---TERMINATE PROGRAM EXECUTION---
484 WRITE(P,7001)
STOP
485 WRITE(P,7002) SET, SETNAM
486 WRITE(P,7003)
STOP 10
C

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C C C C C .....
C C C C C ---COMPUTE AND PRINT ITERATION PARAMETERS---
C C C C C *****
C C C C C ENTRY ITER
C C C C C *****
C C C C C HMIN=2.
C C C C C XVAL=3.1415**2/(2.*DIMW**2)
C C C C C YVAL=3.1415**2/(2.*DIML**2)
C C C C C DO 490 I=2,DIML
C C C C C DO 490 J=2,DIMW
C C C C C IF (T(I,J).EQ.0.) GO TO 490
C C C C C XPART=XVAL*(1/(1+DELX(J)**2*FACTX/DELY(I)**2*FACTX))
C C C C C YPART=YVAL*(1/(1+DELY(I)**2*FACTX/DELX(J)**2*FACTX))
C C C C C HMIN=AMINI(HMIN,XPART,YPART)
490 C C C C C CONTINUE
C C C C C ALPHA=EXP(ALOG(HMAX/HMIN)/(LENGTH-1))
C C C C C RHOP(1)=HMIN
C C C C C DO 500 NTIME=2,LENGTH
500 C C C C C RHOP(NTIME)=RHOP(NTIME-1)*ALPHA
C C C C C *RITE(P,1010) LENGTH,(RHOP(J),J=1,LENGTH)
C C C C C RETURN
C C C C C .....
C C C C C ---INITIALIZE DATA FOR ALPHAMERIC PLOT---
C C C C C *****
C C C C C ENTRY MAP
C C C C C *****
C C C C C *IOTH=0.
C C C C C DO 510 J=2,JNO1
510 C C C C C *IOTH=*IOTH+DELX(J)
C C C C C YDIM=0.
C C C C C DO 520 I=2,INO1
520 C C C C C YD(I)=YD(I)+DELY(I)
530 C C C C C XSF=DINCH*SCALE
C C C C C NYD=YDIM/XSF
C C C C C IF (NYD*XSF.LE.YDIM-DELY(INO1)/2.) NYD=NYD+1
C C C C C IF (NYD.LE.12) GO TO 540
C C C C C JINCH=YDIM/(12.*SCALE)
C C C C C *RITE(P,1130) DINCH
C C C C C IF (SCALE.LT.1.0) WRITE(P,1140)
C C C C C DO 540
540 C C C C C NXD=WIDTH/XSF
C C C C C IF (NXD*XSF.LE.WIDTH-DELX(JNO1)/2.) NXD=NXD+1
C C C C C N4=NXD*N4+1
C C C C C N5=NXD+1
C C C C C N6=NYD+1
C C C C C N3=N4*N5+1
C C C C C NA(1)=N4/2-1
C C C C C NA(2)=N4/2
C C C C C NA(3)=N4/2+3
C C C C C NC=(N3-N6-10)/2
C C C C C ND=NC+N6
C C C C C NE=MAX(N5,N6)
C C C C C VF1(3)=DIGIT(ND)
C C C C C VF2(3)=DIGIT(ND)
C C C C C VF3(3)=DIGIT(NC)
C C C C C XLABEL(3)=MESUR
C C C C C YLABEL(3)=MESUR
C C C C C DO 550 I=1,NE
550 C C C C C VNX=N5-I
C C C C C VNY=I-1
C C C C C IF (VNY.GE.N6) GO TO 550
C C C C C VN(I)=XSF*VNY/SCALE
560 C C C C C IF (VNX.LT.J) GO TO 560
C C C C C VN(I)=XSF*VNX/SCALE
560 C C C C C CONTINUE
C C C C C RETURN
C C C C C .....
C C C C C ---READ TIME PARAMETERS AND PUMPING DATA FOR A NEW PUMPING PERIOD---
C C C C C *****
C C C C C ENTRY NEWPER
C C C C C *****
C C C C C SET=SETID(15)
C C C C C KED=KEDIT
C C C C C IF (KEDIT.GT.11) KED=KED-12

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IF (KEDIT.LT.6) GO TO 568
MESSG=1
IF (KED.EQ.4 .OR. KED.EQ.5) MESSG=0
IERR=0
IERR2=0
C
563 READ (R,343,END=654) SETNAM, KP, KPM1, NWEL, TMAX, NUMT, CDLT,
* DELT, NW, WMULT, IPRDDN, IPRHED, ISVHED, KTHP
IF (ICPY.GE.1) WRITE(KCPY, 9430) SETNAM, KP, KPM1, NWEL, TMAX
* , NUMT, CDLT, DELT, NW, WMULT, IPRDDN, IPRHED, ISVHED, KTHP
IF (KTHP.NE.0) KTH = KTHP
IF (SETNAM.NE.SET) GO TO 655
C
C ---COMPUTE ACTUAL DELT AND NUMT---
DT=DELT/2+
TM=J,0
DO 570 I=1,NUMT
DT=CDLT*DT
TM=TM+DT
J=1
IF (TM.GE.TMAX) GO TO 580
570 CONTINUE
GO TO 590
580 DELT=TMAX/TM*DELT
NUMT=J
590 CONTINUE
IF (ICPY.GE.2) WRITE(KCPY, 9430) SETNAM, KP, KPM1, NWEL, TMAX
* , NUMT, CDLT, DELT, NW, WMULT, IPRDDN, IPRHED, ISVHED, KTH
WRITE(P, 1050) KP, TMAX, NUMT, DELT, CDLT
DELT=DELT*3600.
TMAX=TMAX*86400.
C
C ---READ AND WRITE WELL PUMPING RATES---
WRITE (P,1058) NWEL, KP
IF (NWEL.GT.0) WRITE(P,1060)
IF (KP.GT.KPM1) SUMP=0.
A2 = 0.
DO 605 J = 1, DIMW
IF (NW.LT.0) READ(R, 360) (WELL(I, J), J = 1, DIMW)
IF (NW.LT.0 .AND. ICPYW.GE.1) WRITE(KCPY,9360)(WELL(I,J),J=1,DIMW)
DO 600 J=1,DIMW
IF (KP.GT.KPM1) STRT(I,J)=PHI(I,J)
IF (JW.LE.1) GO TO 600
IF (NW.LT.0) A2 = WELL(I, J)
IF (ISUR(I, J) .GE. 2E4) GO TO 598
FLUX = WELLD(I, J) + A2*WSCALE
IF (INCUM.GT.0) WELLD(I, J) = FLUX
WELL(I, J) = FLUX*WMULT
GO TO 600
598 WELL(I, J) = WELLD(I, J) + A2*CFSCAL
600 CONTINUE
IF (NW.LT.0 .AND. ICPYW.GE.2) WRITE(KCPY,9364)(WELLD(I, J), J=1, DIMW)
605 CONTINUE
IF (JW.LE.1) GO TO 650
IF (NW.LE.0) GO TO 620
DO 610 I=1,NW
610 WR(I)=0.
620 IF (NWEL.LE.0) GO TO 650
C
C <#>=J
CARD DELETED
DO 640 II=1,NWEL
READ (R,840,END=655) I, J, FLUX, RADIUS
IF (ICPYW.GE.1) WRITE(KCPY, 9400) I, J, FLUX, RADIUS
IF (ISUR(I, J) .LT. 2E4) FLUX = WELLD(I, J) + FLUX*WSCALE
IF (ISUR(I, J) .GE. 2E4) FLUX = WELLD(I, J) + FLUX*CFSCAL
IF (RADIUS .LT. 0.) FLUX = 0.
IF (ICPYW.GE.2) WRITE(KCPY, 9402) I, J, FLUX, RADIUS
IF (ISUR(I, J) .GE. 2E4) GO TO 621
IF (INCUM.GT.0) WELLD(I, J) = FLUX
CARD DELETED
FLUX = FLUX*WMULT
621 CONTINUE
WELL(I, J) = FLUX
IF (ICPYW.GE.3) WRITE(KCPY, 9402) I, J, FLUX, RADIUS
C
IF (ABS(FLUX).GT.0.0) GO TO 622
IF (ISUR(I,J).LT.2.0E4) GO TO 622

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      IF (MESSG.EQ.1) WRITE (P,3010) I, J
      IERR=1
      GO TO 525
022 IF (I(I,J).GT.0.0) GO TO 523
      WRITE(P,3015) I, J
      IERR=1
      GO TO 528
023 IF (S(I,J).GE.0.0) GO TO 624
      WRITE(P,3020) I, J
      IERR=1
      GO TO 523
024 IF (I.GT.1 .AND. I.LT.DIML .AND. J.GT.1 .AND. J.LT.DIMW) GO TO 623
      WRITE(P,3030) I, J
      IERR=1
023 CONTINUE
C
      IF (RADIUS .LE. 0.) GO TO 630
      KW=K+1
      IF (KW.GT.NW) GO TO 630
      NWR(KW,1)=I
      NWR(KW,2)=J
      WR(KW)=RADIUS
      WRITE (P,1070) I,J,WELL(I,J),WR(KW)
      IF (ISUR(I,J).GE.2.0E4) WRITE (P,1072)
      GO TO 640
030 WRITE (P,1070) I,J,WELL(I,J)
      IF (ISUR(I,J).GE.2.0E4) WRITE (P,1072)
040 CONTINUE
C
      IF (KEDIT.GT.17) GO TO 568
      IF (KED.EQ.3) GO TO 558
      IF (IERR.GT.0 .AND. (KED.LT.2 .OR. KED.EQ.4)) GO TO 657
      IF (IERR2.GT.0 .AND. KED.EQ.0) GO TO 557
050 RETURN
CC
      ---TERMINATE PROGRAM EXECUTION---
054 WRITE(P,7003)
      IF (KEDIT.LT.18) GO TO 657
056 WRITE (P,7001)
      STOP
055 WRITE (P,7004) KP
      GO TO 657
058 WRITE(P,7002) SET, SETNAM
057 WRITE(P,7000)
      STOP 10
CCCC
      FORMATS:
060 FORMAT ('0',63X,'STARTING HEAD =',G15.7)
070 FORMAT ('0',57X,'STORAGE COEFFICIENT =',G15.7)
080 FORMAT ('0',62X,'SPECIFIC YIELD =',G15.7)
090 FORMAT ('0',37X,'HYDRAULIC CONDUCTIVITY OF CONFINING BED =',G15.7)
100 FORMAT ('0',66X,'RIVER HEAD =',G15.7)
110 FORMAT ('0',53X,'CONFINING BED THICKNESS =',G15.7)
120 FORMAT ('0',62X,'TRANSMISSIVITY =',G15.7)
130 FORMAT ('0',46X,'AQUIFER HYDRAULIC CONDUCTIVITY =',G15.7)
140 FORMAT ('0',60X,'BOTTOM ELEVATION =',G15.7)
150 FORMAT ('0',63X,'TOP ELEVATION =',G15.7)
160 FORMAT ('0',62X,'LAND ELEVATION =',G15.7)
170 FORMAT ('0',63X,'RECHARGE RATE =',G15.7)
180 FORMAT ('0',64X,'PUMPING RATE =',G15.7)
190 FORMAT ('0',72X,'DELX =',G15.7)
200 FORMAT ('0',72X,'DELY =',G15.7)
210 FORMAT (1H1,16A8)
220 FORMAT (10A3)
230 FORMAT(1H1,56X, 20HSTARTING HEAD MATRIX/6H ROW)
240 FORMAT(1H1,15X, '---CONTINUATION OF SIMULATION--- HEAD AFTER ',
1 F13.2, ' SECONDS OF PREVIOUS SIMULATION'/
2 61 ROW)
250 FORMAT (3G10.0)
260 FORMAT (10G5.0)
270 FORMAT(A4, 6X, 7G10.0)
280 FORMAT (A4, 1X, 15G5.0)
290 FORMAT (A3,2X,3G10.0,A8)
300 FORMAT (20F4.0)
310 FORMAT(1H1,36X, 52HHYDRAULIC CONDUCTIVITY OF CONFINING BED OR RIVE

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      *R 000/ 0H ROW)
880 FORMAT ('-',51X,'NUMBER OF PUMPING PERIODS =',I5/63X,'NUMBER OF ROW
13 =',I5/60X,'NUMBER OF COLUMNS =',I5/19X,'TIME STEPS BETWEEN PRINT
23UTS =',I5/51X,'ERROR CRITERIA FOR CLOSURE =',G15.7/35X,'MAXIMUM
3PERMITTED NUMBER OF ITERATIONS =',I5/41X,' STEADY STATE ER
4ROR CRITERIA =',G15.7/44X,'SPECIFIC STORAGE OF CONFINING BED =',G
515.7/ 48X,' SPECIFIC STORAGE OF RIVER BED =',G15.7/
634X,'EVAPOTRANSPIRATION RATE =',G15.7/56X,'EFFECTIVE DEPTH OF
7BET =',G15.7/22X,'MULTIPLICATION FACTOR FOR TRANSMISSIVITY IN X D
8IRECTION =',G15.7/63X,'IN Y DIRECTION =',G15.7)
890 FORMAT (1H1,56X,21HTRANSMISSIVITY MATRIX/ 6H ROW)
892 FORMAT (1H1,50X,32HTRANSMISSIVITY MATRIX (COMPUTED)/ 3H ROW)
894 FORMAT(// 46X,40HTRANSMISSIVITY VALUES HAVE BEEN COMPUTED)
900 FORMAT(1H0,15,2X,10G11.4/ (3X,10G11.4))
910 FORMAT(1H0,15,2X,10F11.0/ (3X,10F11.0))
912 FORMAT(1H0,15,2X,10F11.2/ (3X,10F11.2))
915 FORMAT(1H0,15,2X,10F11.6/ (3X,10F11.6))
930 FORMAT(1H1,54X,26HSTORAGE COEFFICIENT MATRIX/ 6H ROW)
940 FORMAT (A8)
945 FORMAT(0H ROW)
950 FORMAT (3F10.0)
960 FORMAT (1H1,42X,29HHYDRAULIC CONDUCTIVITY MATRIX/ 6H ROW)
962 FORMAT (1H1,46X,40HHYDRAULIC CONDUCTIVITY MATRIX (COMPUTED)/
1 3H ROW)
964 FORMAT(// 42X,48HHYDRAULIC CONDUCTIVITY VALUES HAVE BEEN COMPUT
ED)
970 FORMAT(1H1,51X,30HELEVATION AT BOTTOM OF AQUIFER/
1 0H ROW)
974 FORMAT(1H1,52X,28HSTARTING SATURATED THICKNESS/ 6H ROW)
980 FORMAT(1H1,40X,53HELEVATION AT TOP OF AQUIFER OR AT BOTTOM OF LEA
1KY 3EJ/ 0H ROW)
990 FORMAT(1H1,54X,25HELEVATION AT LAND SURFACE/ 6H ROW)
1000 FORMAT(1H1,50X,13HRECHARGE RATE/6H ROW)
1010 FORMAT (//1H0,15,22H ITERATION PARAMETERS: 8D12.3//6X,10D12.3)
1020 FORMAT(1H1,40X,40HGRID SPACING IN PROTOTYPE -- X DIRECTION//
1 (3X,10F12.0)
1030 FORMAT(1H1,40X,40HGRID SPACING IN PROTOTYPE -- Y DIRECTION//
1 (3X,10F12.0)
1040 FORMAT(1H1,31X,'ELEV. OF W.S. IN RIVER OR HEAD IN OVERLYING (OR
UNDERLYING) AQUIFER' / 5H ROW)
1041 FORMAT(// 3X,'HEAD IN THE OVERLYING (OR UNDERLYING) AQUIFER IS
COMPUTED BY ADDING ',F10.3,' TO STARTING HEAD VALUE AT EACH N
ODE.//)
1050 FORMAT ('-',50X,'PUMPING PERIOD NO.',I4,':',F10.2,' DAYS'/51X,38('
1-')//53X,'NUMBER OF TIME STEPS =',I5//59X,'DELTA IN HOURS =',F10.3//
253X,'MULTIPLIER FOR DELTA =',F10.3)
1055 FORMAT(// 50X, I4, ' WELLS FOR PUMPING PERIOD NO. ', I4/
1 48X, 42(1H-))
1060 FORMAT(/50X, 1H1, 9X, 30HJ PUMPING RATE WELL RADIUS/)
1070 FORMAT (41X,2(10,2F13.2)
1072 FORMAT(1H+,50X, '*** CONSTANT FLUX BOUNDARY')
1080 FORMAT(1H1,45X,39HTHICKNESS OF CONFINING BED OR RIVER BED/
1 0H ROW)
1085 FORMAT(1H1, 20X, '*** MASS BALANCE RESIDUALS (FT/SEC) AT SIMULATIO
N TIME = 0 ***')
1086 FORMAT(1H-, 'TOTAL RESIDUAL = ',1PE12.4 )
1087 FORMAT(1H0,35X, '(RESIDUALS ARE ADDED TO RECHARGE)')
1090 FORMAT(2G10.0, 3G20.0 / (4G20.0) )
1100 FORMAT ('-SIMULATION OPTIONS: ',10(A8,3X))
1110 FORMAT ('0',40X,'ION ALPHAMERIC MAP: '/45X,'MULTIPLICATION FACTOR FO
R LENGTH =',G15.7/55X,'MAP SCALE IN UNITS OF ',A11/50X,'NUMBER OF
2 ',I3,' PER INCH =',G15.7/31X,'CONTOUR INTERVAL =',G15.7)
1120 FORMAT(1H1,56X,21HSPECIFIC YIELD MATRIX/6H ROW)
1130 FORMAT('0',25X,10('*'), ' TO FIT MAP WITHIN 12 INCHES, D INCH REVISE
10 TO ',G15.7,1X,10('*'))
1140 FORMAT('0',45X,'NOTE: GENERALLY SCALE SHOULD BE > OR = 1.0')
1150 FORMAT('1', 30X, 'PUMPING RATE'/' ROW)
C
7000 FORMAT(// 76H ***** PROGRAM EXECUTION IS TERMINATED BECAUSE OF ER
RORS IN INPUT DATA ***** //)
7001 FORMAT(// 29H ***** END OF DATA EDIT ***** //)
7002 FORMAT(// 1X, 11H***ERROR***, ' WRONG DATA SET IDENTIFIER READ F
ROM PARAMETER CARD.' // 10X,
2 'LOOKING FOR IDENTIFIER = ',A4, ' BUT READ IDENTIFIER = ',
3 A4)
7003 FORMAT (//1X, '***** END OF FILE FOR PUMPAGE DATA *****//)
7004 FORMAT(// 1X, 11H***ERROR***, ' END OF FILE BEFORE READING ALL
PUMPAGE DATA FOR PUMPING PERIOD NO. ', I4, 1H./)

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7007 FORMAT(/ 1X, '***ERROR*** DIMENSIONS EXCEED MAXIMUM')
7010 FORMAT(/ 1X, 13H***WARNING***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' A CONSTANT FLUX BOUNDARY IS SPECIFIED ON THE NOFLOW BORDER
2 SURROUNDING' / 10X, ' THE MODEL (CONSTANT FLUX AT THIS NODE IS IG
3 NORED DURING SIMULATION). ' /)
7012 FORMAT(/ 1X, 11H***ERROR***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' STARTING HEAD VALUE IS ZERO.' /)
7015 FORMAT(/ 1X, 13H***WARNING***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' A CONSTANT HEAD BOUNDARY IS SPECIFIED ON THE NOFLOW BORDER
2 SURROUNDING' / 10X, ' THE MODEL (CONSTANT HEAD AT THIS NODE IS IG
3 NORED DURING SIMULATION). ' /)
7020 FORMAT(/ 1X, 13H***WARNING***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' BOTH CONSTANT HEAD AND CONSTANT FLUX BOUNDARIES ARE' /
2 1X, ' SPECIFIED (CONSTANT HEAD IS USED AT THIS NODE DURING SIMU
3 LATION). ' /)
7025 FORMAT(/ 1X, 11H***ERROR***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' TRANSMISSIVITY (OR HYDRAULIC CONDUCTIVITY) IS ZERO FOR A CONS
2 TANT HEAD OR A CONSTANT FLUX BOUNDARY.' /)
7030 FORMAT(/ 1X, 11H***ERROR***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' STARTING HEAD IS BELOW TOP OF ARTESIAN AQUIFER (IF THIS IS T
2 HE CONTINUATION' / 10X, ' OF A PREVIOUS SIMULATION, THE STARTING
3 HEAD IS PHI). ' /)
7032 FORMAT(/ 1X, 13H***WARNING***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' HEAD IS BELOW BOTTOM. HEAD CHANGED TO BOTTOM + THIN.' /)
7034 FORMAT(/ 1X, 13H***WARNING***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' SATURATED THICKNESS IS ZERO OR NEGATIVE, BUT HYDRAULIC CONDUCT
2 IVITY' / 15X, ' IS GREATER THAN ZERO (PROGRAM SETS PERM AND T TO Z
3 ZERO). ' /)
7035 FORMAT(/ 1X, 13H***WARNING***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' SATURATED THICKNESS IS ZERO OR NEGATIVE, BUT TRANSMISSIVITY I
2 S' / 15X, ' GREATER THAN ZERO (PROGRAM SETS PERM AND T TO ZERO). '
3 /)
7040 FORMAT(/ 1X, 11H***ERROR***, ' CONVERSION IS NOT SPECIFIED FOR
1 SIMULATION OF A W.T. AQUIFER WITH LEAKAGE FROM AN OVERLYING RIVER
2 SIMULATION RESULTS' / 10X, ' WILL BE IN ERROR (CANNOT COMPUTE
3 THE CORRECT VALUES FOR LEAKAGE AND TRANSMISSIVITY). THE DATA SET
4 SPECIFYING ELEVATION' / 10X, ' AT TOP OF AQUIFER MUST BE READ AND
5 CONVERT MUST BE SPECIFIED.' /)
7045 FORMAT(/ 1X, 11H***ERROR***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' VALUES FOR RIVER, RATE, M, TOP, STRT, S AND T ARE NOT CONSIS
2 TENT.' /)
7050 FORMAT(/ 1X, 13H***WARNING***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' ELEV. OF LAND SURFACE IS BELOW BOTTOM OF RIVER BED (THIS DOES
2 NOT AFFECT' / 10X, ' THE RESULTS OF SIMULATION). ' /)
7055 FORMAT(/ 1X, 13H***WARNING***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' BOTH EVAPOTRANSPIRATION AND LEAKAGE FROM A RIVER MAY OCCUR D
2 URING SIMULATION.' /)
7059 FORMAT(/ 1X, 11H***ERROR***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' BOTH EVAPOTRANSPIRATION AND LEAKAGE FROM AN OVERLYING AQUIFE
2 R ARE SPECIFIED (LAND(I,J) IS' / 10X, ' SET TO 20,000 AT THIS NODE
3 TO PREVENT EVAPOTRANSPIRATION). ' /)
7060 FORMAT(/ 1X, 11H***ERROR***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' HEAD IS ABOVE LAND SURFACE FOR A W.T. AQUIFER.' /)
7065 FORMAT(/ 1X, 13H***WARNING***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' RECHARGE IS SPECIFIED FOR A CONSTANT HEAD, CONSTANT
2 FLUX, OR' / 10X, ' IMPERMEABLE BOUNDARY (ZERO RECHARGE IS ASSIGNE
3 D TO THIS NODE). ' /)
7066 FORMAT(/ 1X, 13H***WARNING***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' RECHARGE IS SPECIFIED WHERE VERTICAL LEAKAGE OCCURS
2 FROM AN OVERLYING' / 10X, ' RIVER (RECHARGE IS USED DURING SIMUL
3 ATION). ' /)
7067 FORMAT(/ 1X, 13H***WARNING***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' RECHARGE IS SPECIFIED WHERE VERTICAL LEAKAGE OCCURS
2 FROM AN OVERLYING' / 10X, ' AQUIFER (RECHARGE IS USED DURING SIM
3 ULATION). ' /)
7100 FORMAT(/ ' ***** ERROR ***** LAYER OPTION INVALID FOR ARTESIAN'
* ' AQUIFER.' /)
7105 FORMAT(' *** ERROR *** ROW ', I3, ' COL ', I3
* ' LAYER PERM OR T OUTSIDE PREVIOUS BOUNDARY.')
7110 FORMAT(' *** ERROR *** INVALID PERM (IN SY CURVE)')
8010 FORMAT(/ 1X, 13H***WARNING***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' WELL FLUX IS SPECIFIED AS ZERO FOR A CONSTANT FLUX BOUNDARY
2 (ZERO FLUX IS USED IN SIMULATION). ' /)
8015 FORMAT(/ 1X, 11H***ERROR***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' WELL FLUX IS SPECIFIED FOR AN IMPERMEABLE BOUNDARY.' /)
8020 FORMAT(/ 1X, 11H***ERROR***, ' AT ROW ', I3, ' COL ', I3,
1 ' ', ' WELL FLUX IS SPECIFIED FOR A CONSTANT HEAD BOUNDARY.' /)
8030 FORMAT(/ 1X, 11H***ERROR***, ' AT ROW ', I3, ' COL ', I3,

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1      , WELL FLUX IS SPECIFIED ON THE NOFLCW BORDER SURROUNDING THE
240DE..')
C
C      CARD DELETED
9000 FORMAT(16I5)
9012 FORMAT(81X, 'ICPY,ICPY2,ICPYW,KCPY,MPRN,KPLT,KPLC' / 1X, 16I5)
9013 FORMAT(81X, 'WITH DEFAULTS' / 1X, 16I5)
9020 FORMAT(81X, 'HEADING' / 1X, 10A8 / 1X, 10A8)
9030 FORMAT(1X, A8)
9040 FORMAT(81X, 'CONTR,SCALE,DINCH,SPACNG,MESUR'
* / 1X, A4, 2X, 3G15.7, A8)
9050 FORMAT(81X, 'KEDIT,NHYDR,MGRES,ISVFLX,IRDINI,IRDHED,IRDORCH'
* / 1X, 16I5)
9060 FORMAT(81X, 'HYDRO NODES' / 1X, 16I5)
9062 FORMAT(81X, 'MASS BALANCE NODES' / 1X, 16I5)
9070 FORMAT(81X, 'NPER,DIML,DIMW,KTH,LENGTH,ERR,HMAX,ITMAX' / 1X, 8G15.7
* / 81X, 'EROR,SS,QET,ETDIST,FACTX,FACTY,SSRIV' / 1X, 3G15.7)
9072 FORMAT(81X, 'WITH DEFAULTS' / 1X, 3G15.7 / 1X, 5G15.7)
9080 FORMAT(81X, 'INITIAL MASS BAL' / 1X, 2G15.7, 3G30.16 / (1X, 4G30.16))
9420 FORMAT(81X, 'PARAMETER CARD (A8,7G10.0)'
* / 1X, A4, 11X, G15.7, 3I15, 3G15.7)
9422 FORMAT(81X, 'WITH DEFAULTS' / 1X, A4, 11X, G15.7, 3I15, 3G15.7)
9950 FORMAT('0', 8G15.7 / (1X, 3G15.7) )
9952 FORMAT(81X, 'WITH DEFAULTS' / (1X, 3G15.7) )
9800 FORMAT('0', 20F6.0 / (1X, 20F6.0) )
9802 FORMAT(81X, 'WITH DEFAULTS' / (1X, 20F6.0) )
9804 FORMAT(81X, 'WITH DEFAULTS' / (1X, 3G15.7) )
9806 FORMAT(1X, 20F6.3 / (1X, 20F6.3) )
9430 FORMAT(81X, 'KP,KPM1,NWEL,TMAX,NUMT,CDLT,DELT',
* / 81X, 'N,MULT,IPRDDN,IPRHED,ISVHED,KTH'
* / 1X, A4, 1X, 3I5, F10.2, 15, F10.4, F10.2, 15, F10.4, 4I5)
9400 FORMAT('0', 2I10, 2F10.4)
9402 FORMAT(81X, 'WITH DEFAULTS' / 1X, 2I10, 2F10.4)
END

SUBROUTINE COMPUT(PHI,KEEP,PHE,STRT,ISUR,T,TR,TC,S,DELX,DELY,DDN,G
* ,BE,TEMP,IMAX,IZ,JZ,ICP,IC,JC,BOTTOM,IP,JP,WELL,IW,JW
2 ,KALAY,TLAY1,TLAY,MLAY,PERM,SY)
-----
C
C      SPECIFICATIONS:
C*COM01*
COMMON /DARRAY/ RHOP(20),CHK(10),VF4(11)
C*COM02*
COMMON /OPARAM/ WATER,CONVRT,EVAP,CHCK,PNCH,NUM,HEAD,CCNTR,ERDR,LE
1AK,RECH
C*COM03*
COMMON /SPARAM/ SLEAK,U,SS,TT,TMIN,ETDIST,QET,IFINAL,TMAX,CDLT,DEL
1T,SUM,SUMP,NUMT,KT,KP,NPER,KTH,ITMAX,LENGTH,NWEL,NW,ERR,DIML,DIMW,
2JN01,IN01,R,P,PU,SUBS,STORE,TEST,ETQB,ETQD,FACTX,FACTY,IERR,
3DAYS,YRS,SSRIV,CFLEAK,QSUM,KEDIT,MESSG,IPRDDN,IPRHED,ISVHED,ISVFLX
4,IFILE(10),KOUNT,KSTEP,NHYDR,IHYDR(13),JHYDR(13),HYDR(13)
* ,WELBOT,WELTCP
C*COM04*
COMMON /CK/ ETFLXT,QRET,QRETN,FLUXT,FLXNT,CHST,CHDT
* ,CFLXPT,CFLXNT,PUMPT,PJMPPT,STORT
C*COM05*
C*CD03*
COMMON /COPYC / ICPYW, KCPY
COMMON / LAYER / SATL(20), PRMSY(10), SYPRM(10), SYD(10)
* , NLAY, NLAY0, MSY, NSY, NSY0
C*DIM01*
DIMENSION BE(IMAX), G(IMAX), TEMP(IMAX), PHI(IZ,JZ),
1 KEEP(IZ,JZ), PHE(IZ,JZ), STRT(IZ,JZ), ISUR(IZ,JZ), T(IZ,JZ),
2 TR(IZ,JZ), TC(IZ,JZ), S(IZ,JZ), DELX(JZ), DELY(IZ), DDN(JZ)
3 , TJP(IC,JC), BOTTOM(IP,JP), WELL(IW,JP)
4 , KALAY(IZ,JZ), TLAY1(IZ,JZ), TLAY(IZ,JZ,MLAY)
5 , PERM(IP,JP), SY(IP,JP)
C*DIM02*
C*TYP01*
REAL *4MINS,TEST3(102),KEEP,ISUR
C*TYP02*
REAL *8PHI,DBLE,RHOP,CHK,WATER,CONVRT,EVAP,CHCK,PNCH,NUM,HEAD,CONT
1R,ERDR,XLABEL,YLABEL,TITLE,G,BE,TEMP,IMK, DABS,D,W,T1,T2,T3,T4,RH
2J,A,B,C,PARAM,TEST2,DMAX1,LEAK,RECH

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```

C DELETED
C DELETED
C*TYPO3*
      INTEGER DIML,DIMW,R,P,PU
C*END33*
9999 =FORMAT(' SUB COMPUT 2/12/79 MCD 26, 27A')
      WRITE(P, 9999)
      RETURN
C .....
C ---START A NEW TIME STEP---
C *****
C ENTRY NEWSTP
C *****
      IF(NLAY .EQ. 0) GO TO 1590
      DO 1580 I = 1, DIML
      DO 1580 J = 1, DIMW
      K = KKLAY(I, J)
      IF(K .LE. 0) GO TO 1580
      HED = PHI(I, J)
      IF(CONVRT .EQ. CHK(7) ) HED = AMINI(HED, TOP(I, J) )
      SAT = HED - BOTTOM(I, J)
      IF(K .LE. 1) GO TO 1520
      IF(SATL(K - 1) .LT. SAT) GO TO 1520
      S1 = 0.
      T1 = 0.
1510 K = K - 1
      IF(K .LE. 1) GO TO 1550
      IF(SATL(K - 1) .LT. SAT) GO TO 1540
      GO TO 1510
1520 IF(K .GE. NLAY) GO TO 1580
      IF(SATL(K) .GE. SAT) GO TO 1580
1530 K = K + 1
      IF(K .GE. NLAY) GO TO 1540
      IF(SATL(K) .GT. SAT) GO TO 1540
      GO TO 1530
1540 S1 = SATL(K - 1)
      T1 = TLAY(I, J, K - 1)
1550 CONTINUE
      KKLAY(I, J) = K
      TLAY(I, J) = T1
      A2 = (TLAY(I, J, K) - T1)/(SATL(K) - S1)
      IF(NLAY0 .LT. 0 .AND. SAT .GT. 0.) A2 = (T1 + A2*(SAT - S1) )/SAT
      PERI(I, J) = A2
      PO = PRMSY(1)
      IF(PO .EQ. 0.) GO TO 1580
      DO 1560 JSY = 2, NSY
      ISY = JSY
      PI = PO
      PO = PRMSY(ISY)
      IF(PO .GT. A2) GO TO 1569
1560 CONTINUE
1569 SY(I, J) = SYPRM(ISY) + SYD(ISY)*ALOG10(A2/PI)
1530 CONTINUE
      IF(NLAY0 .LT. 0) RETURN
1590 CONTINUE
      DELT = CDLT*DELT
      SUM = SUM + DELT
      SUMP = SUMP + DELT
      DAYSP = SUMP/86400.
      YRSP = DAYSP/360.
      HRS = SUM/3600.
      MINS = HRS*60.
      DAYS = HRS/24.
      YRS = DAYS/360.
      KI = KI + 1
      KSTEP = KSTEP + 1
      ISTEY = 0
      KOUNT = 0
      DO 1880 I = 1, DIML
      DO 1880 J = 1, DIMW
1800 KEEP(I, J) = PHI(I, J)
      RETURN
C
C ---INITIALIZE DATA FOR A NEW ITERATION---
C *****
C ENTRY NEWITI
C *****
      IF (KOUNT.LT.ITMAX) GO TO 20

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```

      KUJNT=KUJNT+1
      *RITE(P,410) XT, DAYS
      GO TO 260
20  KUJNT=KUJNT+1
      IF (MOD(KUJNT,LENGTH)) 30,30,40
C     *****
C     ENTRY NEWITO
C     *****
30  NTH=0
40  NTH=NTH+1
      PARAM=RHQP(NTH)
      TEST3(KUJNT+1)=0.
      TEST=0.
      DO 50 I=2,INOI
      DO 50 J=2,JNOI
50  PHE(I,J)=PHI(I,J)
      RETJRN
C
C     ---COMPUTE IMPLICITLY ALONG ROWS---
C     *****
C     ENTRY RWJ
C     *****
      DO 50 J=1,DIMW
      BE(J)=0.0
      G(J)=0.0
60  TEMP(J)=PHI(1,J)
      DO 140 I=2,DIWL
      DO 100 J=2,JNOI
C
C     ---SKIP COMPUTATIONS IF NODE IS OUTSIDE AQUIFER BOUNDARY---
70  IF (T(I,J)) 70,100,70
      T1=TR(I,J-1)/DELX(J)
      T2=TR(I,J)/DELX(J)
      T3=TC(I-1,J)/DELY(I)
      T4=TC(I,J)/DELY(I)
      QCDF=0.
      R=0.
      IF (S(I,J).LT.0.) GO TO 80
C
C     ---COMPUTE ET RATE (ETQ), STEADY AND TRANSIENT LEAKAGE FACTOR
C     (SLEAK), STORAGE COEFFICIENT, WELL AND RECHARGE RATES---
      IF (EVAP.EQ.CHK(6)) CALL STRATE(I,J)
      IF (LEAK.EQ.CHK(9)) CALL LEAKAG(I,J,QCCF)
      CALL SOURCE(I,J,RW)
      CALL STORAG(I,J)
C
      RHO=STURE/DELT
      GO TO 90
80  RHO=1.0E+0
C
C     ---CALCULATE VALUES FOR PARAMETERS USED IN THOMAS ALGORITHM ---
90  IMK=PARAM*(T1+T2+T3+T4)
      A=T1
      B=-T1-T2-RHO-IMK-QCDF*U-ETQ3
      C=T2
      W=0-A*BE(J-1)
      IF (DABS(W) .GT. 1.E-20) GO TO 95
      *RITE(P, 94) I, J, W, T1, T2, T3, T4
94  FORMAT(' ***** IN ENTRY ROW, ROW', I3, ', COL', I3,
* ', JENDM W =', G15.7, ' / 7X, 'T1, T2, T3, T4 =', 4G13.7)
      W = 1.0/W
95  CONTINUE
      BE(J)=C/W
      D=-T3*PHI(I-1,J)+(T4+T3-IMK)*PHI(I,J)-T4*PHI(I+1,J)-RHC*KEEP(I,J)-
      ISL=AK+R*ETQD-SUBS
      G(J)=(D-A*G(J-1))/W
100 CONTINUE
C
C     ---CALCULATE HEAD VALUES FOR ROWS OF MATRIX AND PLACE THEM IN
C     TEMPORARY LOCATION TEMP; IF (I.GT.2) FIRST MAKE PHI(I-1,NO4)=
C     TEMP(NO4)---
      NO3=DIW-2
      DO 130 KNO4=1,NC3
      NO4=DIW-KNO4
      PHI(I-1,NO4)=TEMP(NO4)
      IF (T(I,NO4)) 120,110,120
110  TEMP(NO4)=PHI(I,NO4)
      GO TO 130

```

```

120 TEMP(N04)=G(N04)-BE(N04)*TEMP(N04+1)
130 CONTINUE
140 CONTINUE
    RETURN
C
C      ---COMPUTE IMPLICITLY ALONG COLUMNS---
C      *****
C      ENTRY COLUMN
C      *****
C      DO 150 I=1, DIML
C      BE(I)=0.0
C      G(I)=0.0
150  TEMP(I)=PHI(I,1)
C      DO 230 J=2, DIMW
C      DO 190 I=2, INCI
C
C      ---SKIP COMPUTATIONS IF NODE IS OUTSIDE AQUIFER BOUNDARY---
160  IF (I(I,J).LT.190.190.160)
C      T1=TR(I,J-1)/DELTX(J)
C      T2=TR(I,J)/DELTX(J)
C      T3=TC(I-1,J)/DELY(I)
C      T4=TC(I,J)/DELY(I)
C      QCCF=0.
C      R#=0.
C      IF (S(I,J).LT.0.) GO TO 170
C
C      ---COMPUTE SEEPAGE RATE (ETQ), STEADY AND TRANSIENT LEAKAGE FACTOR
C      (S-LEAK), STORAGE COEFFICIENT, WELL AND RECHARGE RATES---
C      IF (EVAP.EQ.0.) IMK(6) CALL ETRATE(I,J)
C      IF (-LEAK.EQ.0.) IMK(9) CALL LEAKAG(I,J,QCCF)
C      CALL SOURCE(I,J,RW)
C      CALL STORAGE(I,J)
C
C      RHO=STORE/DELT
C      GO TO 130
170  RHO=1.0E+0
C
C      ---CALCULATE VALUES FOR PARAMETERS USED IN THOMAS ALGORITHM---
180  IMK=PARAM*(T1+T2+T3+T4)
C      A=T3
C      B=-T3-T4-RHO-IMK-QCCF*U-ETQB
C      C=T4
C      D=A*B*(I-1)
C      IF (ABS(D).GT.1.E-20) GO TO 185
C      WRITE(7,13) I, J, W, T1, T2, T3, T4
184  FORMAT(' ***** IN ENTRY CCL, ROW', I3, ', CCL', I3,
C      * ', DENUM W = ', G15.7, ', ' / 7X, 'T1, T2, T3, T4 =', 4G15.7)
C      W = 1.00
135  CONTINUE
C      BE(I)=C/D
C      D=-T1*PHI(I, I-1)+(T1+T2-IMK)*PHI(I,J)-T2*PHI(I,J+1)-RHO*KEEP(I,J)-
C      SLEAK+R#+ETQ-SLBS
C      G(I)=(D-A*G(I-1))/W
190  CONTINUE
C
C      ---CALCULATE HEAD VALUES FOR COLUMNS OF MATRIX AND PLACE IN TEMP-
C      ORARY LOCATION TEMP; IF (J.GT.2) FIRST MAKE PHI(N04,J-1)=TEMP(N04)---
C      NU3=JIML-2
C      A2=0.0
C      DO 220 KNU4=1, NC3
C      NU4=JIML-KNU4
C      PHI(N04,J-1)=TEMP(N04)
C      IF (I(N04,J).LT.210.200.210)
200  TEMP(N04)=PHI(N04,J)
C      GO TO 220
210  TEMP(N04)=G(N04)-BE(N04)*TEMP(N04+1)
C      TCHK=ABS(SNGN(TEMP(N04))-PHE(N04,J))
C      IF (TCHK.GT.1.E-08) TEST=1.
C      A2=A2+TCHK
220  CONTINUE
C      TEST3(KCOUNT+1)=TEST3(KCOUNT+1)+A2
230  CONTINUE
    RETURN
C
C      *****
C      ---CHECK FOR STEADY STATE---
C      *****

```



```

ENTRY STEADY
*****
TEST2=0.
DO 240 I=2,INO1
DO 240 J=2,JNO1
240 TEST2=)MAX1(TEST2,DABS(DBLE(KEEP(I,J))-PHI(I,J)))
IF (TEST2.GE.EPCR) GO TO 250
*WRITE(P,360) KT, DAYS
IFINAL=1
ISTEDY=1
DO 250 I=1,INO1
250 IF (KT.EQ.NUMT) IFINAL=1
260 IF (CHK.EQ.CHK(5)) CALL CHECK
C
C --- SAVE HYDROGRAPHS FOR SELECTED NODES ---
IF (NHYDR.LE.J) GO TO 258
DO 254 J=1,NHYDR
IM1=IHYDR(J)
JM1=JHYDR(J)
254 HYDR(J)=PHI(IM1,JM1)
JM1=IFILE(7)
*WRITE (JM1) DAYS, (HYDR(J), J=1,NHYDR)
256 CONTINUE
C
IF (KOUNT.LE.ITMAX) RETURN
KOUNT=KOUNT+1
C
C ---PRINT OUTPUT AT DESIGNATED TIME STEPS---
*****
ENTRY OUTPUT
*****
*WRITE (P,390) KT,DELT,SUM,MIN,S,HRS,DAYS,YRS,DAYSP,YRSP,KCUNT
IF (CHK.EQ.CHK(5)) CALL CWRITE
IF (JW.LE.1 .OR. (WATER.NE.CHK(2) .AND. EVAP.NE.CHK(6))) GO TO 5090
DO 5050 I = 1, DIML
DO 5070 J = 1, DIMW
IF (ISUR(I, J) .GE. 2E4 .OR. WELL(I, J) .LE. 0.) GO TO 5070
IF (WATER .NE. CHK(2) ) GO TO 5050
IF (PHI(I, J) .LT. BOTTOM(I, J) + WELBOT) *WRITE(P, 500) I, J
5050 IF (EVAP .NE. CHK(6) ) GO TO 5070
IF (PHI(I, J) .LT. LAND(I, J) - WELTOP) *WRITE(P, 510) I, J
5070 CONTINUE
5080 CONTINUE
5090 CONTINUE
IF (WATER .NE. CHK(2) ) GO TO 2609
IDRY = 0
DO 2608 I = 1, DIML
DO 2607 J = 1, DIMW
IF (PHI(I, J) .GE. BOTTOM(I, J) ) GO TO 2607
IDRY = IDRY + 1
2607 CONTINUE
2608 CONTINUE
*WRITE(P, 530) IDRY
2609 CONTINUE
IF (IT.NE.0.) *WRITE (P,370) TMIN,IT
*WRITE (P,340) TEST2
KOUNT=KOUNT+1
*WRITE (P,350) (TEST3(J),J=1,KCUNT)
C
IF (CONTR.EQ.CHK(3) .AND. .NOT.(KT.EQ.NUMT .AND. (PRDN.LT.0)))
CALL PRNTA
C
IF (KT.NE.NUMT .OR. ISVHED.NE.1) GO TO 266
C
C --- SAVE HEAD AT THE END OF A PUMPING PERIOD ---
JM1=IFILE(3)
DO 264 I=1,DIML
DO 263 J=1,DIMW
263 PHE(I,J)=PHI(I,J)
264 *RITE (JM1) (PHE(I,J), J=1,DIMW)
C
C ---PRINT HEAD MATRIX---
266 IF (HEAD.NE.CHK(8) .OR. (KT.EQ.NUMT .AND. (PRHED.LT.0)) GO TO 280
*WRITE (P,350) KT, DAYS
IF (ISTEDY.EQ.1) *WRITE (P,334)
*RITE (P,336)
DO 270 I=1,DIML
270 *RITE(P,329) I, (PHI(I,J), J=1,DIMW)
C

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C      ---PRINT DRAWDOWN---
230 IF (NUM.NE.CHK(4) .OR. (KT.EQ.NUMT .AND. (PRODN.LT.0))) GO TO 310
    WRITE (P,330) KT, DAYS
    IF (ISTEDY.EQ.1) WRITE (P,334)
    WRITE (P,336)
C      *****
C      ENTRY JRN
C      *****
    DO 300 I=1,DIML
    DO 290 J=1,DIMW
    A2=ISUR(I,J)
    IF(A2.GE.2.0E4) A2=A2-2.0E4
290 DDN(J) = PHI(I, J) - A2
300 WRITE(P,331) I, (DDN(J), J = 1, DIMW)
C
    IF(IPRODN .LT. 1) GO TO 310
    WRITE(P, 302)
302 FORMAT(1H1, 41X, 'SATURATED THICKNESS')
    WRITE(P, 336)
    DO 303 I = 1, DIML
    DO 304 J = 1, DIMW
304 DDN(J) = PHI(I, J) - EOTTM(I, J)
305 WRITE(P, 308) I, (DDN(J), J = 1, DIMW)
308 FORMAT(1H0, 15, 2X, 10F12.3 / (2X, 10F12.3) )
C LINE 2342+ CONTAINS MOD 17
310 IF(KT .LT. NUMT .OR. (PRODN .LT. 2) GO TO 315
    IF(1CPY# .GT. 0) WRITE(KCPY, 511)
    WRITE(P, 512)
    WRITE(P, 335)
511 FORMAT(31X, 'CALIBRATION HEAD')
512 FORMAT(1H1, 40X, 'CALIBRATION RESIDUAL')
513 FORMAT(3F10.0)
514 FORMAT(1H0, 8G15.7 / (1X, 8G15.7) )
    DO 513 I = 1, DIML
    READ(R, 514) (DCN(J), J = 1, DIMW)
    IF(1CPY# .GT. 0) WRITE(KCPY, 516) (DDN(J), J = 1, DIMW)
    DO 514 J = 1, DIMW
    IF(DDN(J) .GE. 2E4) DDN(J) = DDN(J) - 2E4
514 DDN(J) = PHI(I, J) - DDN(J)
515 WRITE(P, 331) I, (DDN(J), J = 1, DIMW)
315 IF(NW .GT. 0) .AND. IERR .NE. 1) CALL WELLD
    IF (KOUNT.LE.ITMAX) RETURN
C
C      --- SAVE FINAL MASS BALANCE PARAMETERS, FINAL HEAD, AND
C      PRINT HYDROGRAPHS ---
C      *****
C      ENTRY JRY
C      *****
    IF (PNCH.NE.CHK(1)) GO TO 323
    JMI=IFILE(5)
    WRITE(JMI) SUM, SUMP, ETFLXT, GRET, GRETN, FLUXT, FLXNT
    * , CHST, CHDT, CFLXPT, CFLXNT, PUMPT, PUMPTT, STORT
    DO 320 I=1,DIML
320 WRITE (JMI) (PHI(I,J), J=1,DIMW)
    ENDFILE JMI
C
C      --- PRINT HYDROGRAPHS FOR SELECTED NODES ---
C
323 IF (NHYDR.E.0) GO TO 328
    JMI=IFILE(7)
    ENDFILE JMI
    REWIND JMI
    WRITE (P,430)
    WRITE (P,434) (IHYDR(I), I=1,NHYDR)
    WRITE (P,435) (JHYDR(J), J=1,NHYDR)
    WRITE (P,405)
325 READ (JMI,END=328) DAYS, (HYDR(J), J=1,NHYDR)
    WRITE (P,440) DAYS, (HYDR(J), J=1,NHYDR)
    GO TO 325
C
323 CONTINUE
    JMI=IFILE(3)
    IF (ISVHD.EQ.1 .AND. KT.EQ.NUMT) ENDFILE JMI
C
C      IF (KJUNT.GT.ITMAX) STOP
C
C      RETURN
C
C      .....

```



```

INTEGER DIML,DIMW,R,P,PU
C*DTA01*
  DATA P1E/3.141593/
  DATA TMIN / .02 /
C*DTA02*
  DATA QREB / 0. /
C*DTA03*
C*END03*
9999 PUR4AT(' SUB COEF 12/05/79 MOD 26, 27')
  WRITE(P, 9999)
  RETURN
C
C *****
C --- COMPUTE Q COEFFICIENTS ---
C *****
C ENTRY CLAY
C *****
C TMIN=1.040
C TT=0.0
C RATE=0.
C DO 50 I=1,DIML
C DO 50 J=1,DIMW
C
C --- SKIP COMPUTATIONS IF T, RATE OR M = 0, OR IF CONSTANT
C HEAD BOUNDARY ---
C IF (RATE(I,J).LE.0..OR.T(I,J).EQ.0..OR.M(I,J).EQ.0)..CR.S(I,J).LT.0
C L.) GO TO 50
C
C --- CHECK FOR SS = 0 ---
C IF (SS.NE.0.) GO TO 10
C SUMN=0.0
C DENUM=1.0
C X2=ABS(M(I,J))
C GO TO 50
C
C --- CHECK WHETHER VALUE FOR Q(I,J) WILL EQUAL VALUE FOR PREVIOUS
C NODE ---
C 10 X2=ABS(M(I,J))
C IF (RATE(I,J)*X2.EQ.PRATE) GO TO 50
C DIMT=RATE(I,J)*SUMP/(X2*X2*SS*3)
C IF (DIMT.GT.TT) TT=DIMT
C IF (DIMT.LT.TMIN) TMIN=DIMT
C PPT=PIE*PIE*DIMT
C
C --- RECOMPUTE PPT IF DIMT WITHIN RANGE FOR SHORT TIME COMPUTATION ---
C IF (DIMT.LT.1.0E-03) PPT=1.0/DIMT
C CK=(2.3-PPT)/(2.*PPT)
C SUMN=0.0
C DO 30 K=1,200
C POWER=K*K*PPT
C IF (POWER.LE.150.) GO TO 20
C POWER=150
C 20 PEX=EXP(-POWER)
C SUMN=SUMN+PEX
C IF (PEX.GT.0.00009) GO TO 30
C IF (K.GT.CK) GO TO 40
C 30 CONTINUE
C
C --- COMPUTE DENOMINATOR DEPENDING ON VALUE OF DIMT ---
C 40 DENUM=1.0
C IF (DIMT.LT.1.0E-03) DENOM=SQRT(PIE*DIMT)
C
C --- HEAD VALUES ARE NOT INCLUDED IN COMPUTATION OF Q FACTOR SINCE
C LEAKAGE IS CONSIDERED IMPLICITLY ---
C 50 Q1=RATE(I,J)/(X2*DENOM)
C Q(I,J)=Q1+2.0*Q1*SUMN
C PRATE=RATE(I,J)*X2
C 60 CONTINUE
C TMIN=TMIN*3.0
C TT=TT*3.0
C RETURN
C
C --- COMPUTE TRANSMISSIVITY IN WT OR WT-ARTESIAN CONVERSION PROBLEM ---
C *****
C ENTRY TRANS
C *****
C DO 30 I=1,DIML
C DO 30 J=1,DIMW
C IF (PERM(I,J).EQ.0.) GO TO 30
C HD=PHI(I,J)

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```

IF(CONVRT.EQ.CHK(7)) HED = AMINI(HED, TOP(I, J))
IF(HED.LI.BOTTCM(I, J) + THIN) GO TO 70
IF(NLAY.EQ.0) GO TO 659
K = KKLAY(I, J)
IF(K.LE.1) GO TO 659
T(I, J) = TLAY(I, J) + PERM(I, J)*(HED - BOTTCM(I, J)-SATL(K-1))
GO TO 30
659 CONTINUE
T(I, J)=PERM(I, J)*(HED-BOTTCM(I, J))
GO TO 30
70 T(I, J) = PERM(I, J)*THIN
C DRY MODE MESSAGE DELETED
30 CONTINUE
RETURN

C
C ---COMPUTE T COEFFICIENTS---
C *****
C ENTRY TCOF
C *****
DO 150 I=1,INC1
DO 150 J=1,JNC1
DENOM=(T(I, J)*DELX(J+1)+T(I, J+1)*DELX(J))
IF(DENOM.NE.0.) GO TO 120
TR(I, J)=0.
GO TO 130
120 TR(I, J)=(2.*T(I, J+1)*T(I, J))/DENOM*FACTX
130 DENJM=(T(I, J)*DELY(I+1)+T(I+1, J)*DELY(I))
IF(DENOM.NE.0.) GO TO 140
TC(I, J)=0.
GO TO 150
140 TC(I, J)=(2.*T(I+1, J)*T(I, J))/DENOM*FACTY
150 CONTINUE
RETURN

C
C ---COMPUTE ET RATE---
C *****
C ENTRY ETRATE(I, J)
C *****
ETQB=0.0
ETQJ=0.0
X=LAND(I, J)
IF(X.GT.2E4) X = X - 2E4
IF(PHE(I, J).LE.X-ETDIST) GO TO 160
ETQB=QET/ETDIST
ETQJ=ETQB*(ETDIST-X)
160 RETURN

C
C ---COMPUTE STORAGE COEFFICIENT---
C *****
C ENTRY STORAG(I, J)
C *****
SUBS=0.0
IF(WATER.NE.CHK(2)) GO TO 220
IF(CONVRT.NE.CHK(7)) GO TO 200
X=KEEP(I, J)-PHE(I, J)
IF(X) 170, 180, 180
170 HED1=PHE(I, J)
HED2=KEEP(I, J)
GO TO 190
180 HED1=KEEP(I, J)
HED2=PHE(I, J)
190 X2=TOP(I, J)
IF(X2.GT.2E4) X2 = X2 - 2E4
IF(HED1-X2) 200, 200, 210
200 STORAE=SY(I, J)
IF(KEEP(I, J).LT.BOTTCM(I, J).AND.SYB.GT.0) STORE = SYB
GO TO 240
210 IF(X2-HED2) 220, 220, 230
220 STORE=S(I, J)
GO TO 240
230 STORAE=SY(I, J)
SUBS=(HED1-X2)*(S(I, J)-SY(I, J))/DELT
IF(X.LT.0.) SUBS=-SUBS
240 RETURN

C
C ---COMPUTE STEADY AND TRANSIENT LEAKAGE FACTOR---
C *****
C ENTRY LEAKAG(I, J, QCOF)

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```

C *****
HED1=STRT(I,J)
J=1.
HED2=0.
X2=TOP(I,J)
IF(X2.GE.2E4) GO TO 272
IF(CONVRT.EQ.CHK(7)) HED1=AMAX1(STRT(I,J),X2)
IF(CONVRT.NE.CHK(7)) GO TO 250
IF(PHE(I,J).GE.X2) GO TO 250
HED2=X2
J=0.
250 X=0.
X2=ABS(X(I,J))
IF(X2.GT.1.0E-10) X=RATE(I,J)/X2
270 SLEAK=X*(RIVER(I,J)-HED1)+G(I,J)*(HED1-HED2)
QCUF=Q(I,J)
RETURN
272 SLEAK = J.
QCUF = 0.
RETURN

C ---COMPUTE WELL AND RECHARGE RATES---
*****
ENTRY SOURCE(I,J,RW)
*****
IF(JW.LT.2) GO TO 278
IF(WELL(I,J).EQ.0.) GO TO 278
IF(ISUR(I,J).GE.2E4) GO TO 276
XWEL = 0.
IF(WATER.EQ.CHK(2)) XWELL = BOTTOM(I,J) + WELBOT
IF(EVAP.NE.CHK(6)) GO TO 274
XTOP = LAND(I,J)
IF(XTOP.GT.2E4) XTOP = XTOP - 2E4
XTOP = XTOP - WELTOP
IF(XTOP.GT.XWELL) XWELL = XTOP
274 IF(KEEP(I,J).LT.XWELL) GO TO 278
276 RW = RW - WELL(I,J)/(DELX(J)*DELY(I))
278 CONTINUE
IF(RECH.NE.CHK(10)) GO TO 2798
X = JRE(I,J)
IF(X.GE.0. OR WATER.NE.CHK(2)) GO TO 2795
IF(KEEP(I,J).LT.BOTTOM(I,J)) X = X*QRES
2795 R = RW - X
2798 CONTINUE
RETURN

C ---COMPUTE APPROXIMATE HEAD FOR PUMPING WELLS---
*****
ENTRY WELLD
*****
WRITE(P,380)
DO 320 K=1,NW
IF(WR(K).EQ.0.) GO TO 320
I=NWR(K,1)
J=NWR(K,2)
RE=(DELX(J)+DELY(I))/9.62
IF(WATER.NE.CHK(2)) GO TO 280
IF(CONVRT.NE.CHK(7)) GO TO 290
IF(PHI(I,J).LT.X2) GO TO 290
280 HW=PHI(I,J)+WELL(I,J)*ALOG(RE/WR(KW))/(2.*PIE*T(I,J))
GO TO 310
290 ARG=HED*HED+WELL(I,J)*ALOG(RE/WR(KW))/(PIE*PERM(I,J))
IF(ARG.GT.0.) GO TO 300
WRITE(P,390) I,J
GO TO 320
300 HW=SQRT(ARG)+BOTTOM(I,J)
310 DRA=ISUR(I,J)-HW
WRITE(P,370) I,J,WR(KW),HW,DRAW
320 CONTINUE
RETURN

C ---FORMATS---
340 FORMAT ('1',50X,'DRAWDOWN WHEN WELL WENT DRY')
350 FORMAT ('1',32X,'DRAWDOWN FOR TIME STEP ',I4,' (SIMULATION TIME =
. ',F8.2,' GH DAYS) )

```

```

370 FORMAT (' ',43X,2I5,3F11.2)
380 FORMAT ('-',50X,'HEAD AND DRAWDOWN IN PUMPING WELLS'/51X,34('-')//
143X,'I      J      WELL RADIUS      HEAD      DRAWDOWN'//)
390 FORMAT (' ',43X,2I5,' WELL IS DRY')
END

```

```

SUBROUTINE CHECKI(PHI,KEEP,PHE,STRT,ISUR,T,TR,TC,S,DELX,DELY,Q,RAT
1E,M,RIVER,WELL,SY,TOP,LAND,PERM,BOTTOM,GR,IZ,JZ,IR,JR,IW,JW,IP,JP
2,IL,JL,IC,JC,IQ,JQ)

```

```

C-----THIS SUBROUTINE COMPUTES A MASS BALANCE-----
C
C
C SPECIFICATIONS:
C*COM1*
COMMON /DARRAY/ RHOP(20),CHK(10),VF4(11)
C*COM2*
COMMON /OPARAM/ WATER,CONVRT,EVAP,CHCK,PNCH,NUM,HEAD,CONT,EROR,LE
1AK,RECH
C*COM3*
COMMON /SPARAM/ SLEAK,U,SS,TT,TMIN,ET)(ST,QET,IFINAL,TMAX,CDLT,DEL
1T,SJM,SJMP,NUMT,KT,KP,NPER,KTH,ITMAX,LENGTH,NWEL,NW,ERR,DIML,DIMW,
2JNUL,INUL,R,P,PL,SUBS,STORE,TEST,ETQB,ETOD,FACTX,FACTY,IERR,
3JAYS,YRS,SSRIV,CFLKAK,QSUM,KEDIT,MESSG,IPOON,IPPHED,ISVHED,ISVFLX
4,IFILE(10),KOUNT,KSTEP,NHYDR,IHYDR(13),JHYDR(13),HYDR(13)
* ,WELBOT,WELTOP,SYB
C*COM4*
COMMON /CK/ ETLX, QRET, QRETN, FLUX, FLXNT, CHST, CHDT
* , CFLXPT, CFLXNT, PUMPT, PUMPT, STORT
C*COM5*
C*COM6*
C*DIM1*
DIMENSION PHI(IZ,JZ), KEEP(IZ,JZ), PHE(IZ,JZ), STRT(IZ,JZ), ISUR(
1Z,JZ), T(IZ,JZ), TR(IZ,JZ), TC(IZ,JZ), S(IZ,JZ), DELX(JZ), DELY(IZ
2), J(IR,JR), RATE(IR,JR), M(IR,JR), RIVER(IR,JP), WELL(IW,JW), SY(
3IP,JP), TOP(IC,JC), LAND(IL,JL), PERM(IP,JP), BOTTOM(IP,JP), GR(
4I,JJ)
C*DIM2*
DIMENSION SAVE(32), SAVER(32)
C*TYP1*
REAL **KEEP,M,ISUR,LAND
C*TYP2*
REAL *3PHI,DOUBLE,RHOP,CHK,*ATER,CONVRT,EVAP,CHCK,PNCH,NUM,HEAD,CONT
1R,EROR,LEAK,RECH
REAL*8 HED2
C*TYP3*
INTEGER DIML,DIMW,R,P,PU
C*DTA01*
CARD DELETED
DATA CHKTR /'ITER' /
DATA QREB / 0. /
C*DTA2*
C*DTA3*
C*ENDJ*
9999 FORMAT(' SUB CHECKI 10/11/78 MOD 26, 27')
WRITE(P,9999)
C
C
C D3 CONVERTS FT**3 TO ACRE FT
D3PT CONVERTS FT**3/SEC TO
ACRE FT PER YEAR
C
C
C D3 = 1./43560.
D3PT = 3157600.*D3
D3PTS = D3PT
D3PTR = D3PT
RETURN
C
C*****
C ENTRY CHECK
C*****
C
C-----INITIALIZE VARIABLES-----
JG 10 ISV = 1, 32
SAVE(ISV) = 0.
10 SAVER(ISV) = 0.
PJM=0.
PUMPP = 0.
STJR=0.

```



```

GO TO 120
115 X = TC(I-1, J)*(PHI(I-1, J) - PHI(I, J))*DELX(J)
    IF(X .GT. 0.) SAVE(31) = SAVE(31) + X
    IF(X .LT. 0.) SAVE(32) = SAVE(32) + X
120 IF(S(I+1, J) .GE. 0.) GO TO 145
    X=TC(I, J)*(STRT(I+1, J)-PHI(I, J))*DELX(J)
    IF (X) 130,150,140
130 CHD1=CHD1+X
    GO TO 150
140 CHD2=CHD2+X
    GO TO 150
145 X = TC(I, J)*(PHI(I+1, J) - PHI(I, J))*DELX(J)
    IF(X .GT. 0.) SAVE(31) = SAVE(31) + X
    IF(X .LT. 0.) SAVE(32) = SAVE(32) + X
150 SAVE(9) = CHD2 - SAVE(9)
    SAVE(10) = CHD1 - SAVE(10)
C
    IF(RECH .NE. CHK(10) ) GO TO 160
    X = QRE(I, J)*AREA
    IF(X) 153, 160, 156
150 QREFLX = QREFLX + X
    SAVE(3) = X
    SAVE(4) = 0.
    GO TO 150
158 IF(WATER .NE. CHK(2) ) GO TO 159
    IF(KEEP(I, J) .LT. BOTTOM(I, J) ) X = X*QREB
159 QREFN = QREFN + X
    SAVE(3) = 0.
    SAVE(4) = X
160 CONTINUE
C
    ---COMPUTE ET RATE---
    IF (EVAP.NE.CHK(6)) GO TO 170
    SAVE(1) = 0.
    X = LAND(I, J)
    IF(X .GT. 2E4) X = X - 2E4
    IF(PHI(I, J) .LT. X - ETDIST) GO TO 170
C DELETED
C DELETED
    ETQ = GET/ETDIST*(PHI(I, J) + ETDIST - X)
    ETFLUX = ETFLUX - ETQ*AREA
    SAVE(1) = -ETQ*AREA
C
    ---COMPUTE LEAKAGE RATE---
170 IF (LEAK.NE.CHK(9)) GO TO 180
    SAVE(5) = 0.
    SAVE(6) = 0.
    IF (M(I, J).EQ.0) GO TO 180
    IF(TOP(I, J).GE.2.E4) GO TO 180
    HED1=STRT(I, J)
    IF (CONVRT.EQ.CHK(7)) HED1=AMAX1(STRT(I, J), TOP(I, J))
    HED2=PHI(I, J)
    IF(CONVRT .NE. CHK(7)) GO TO 175
    IF(TOP(I, J) .GT. HED2) HED2 = TOP(I, J)
175 CONTINUE
    XX=ABS(M(I, J))
    XX=RATE(I, J)*(RIVER(I, J)-HED1)*AREA/XX
    YY=M(I, J)*(-HED1-HED2)*AREA
    FLUX=FLUX+XX
C LEAKAGE FROM PREVIOUS PERIOD CONSIDERED TOGETHER WITH CURPENT
    XX = XX + YY
    FLUXS = FLUXS + XX
    IF(XX .LT. 0.) FLXN = FLXN + XX
    IF(XX .GT. 0.) SAVE(5) = XX
    IF(XX .LT. 0.) SAVE(6) = XX
    IF(ISVFLX .EQ. 1) PHE(I, J) = XX/AREA
C
    ---COMPUTE VOLUME FROM STORAGE---
180 STORES(I, J)
    IF(WATER .NE. CHK(2) ) GO TO 185
    STORE = SY(I, J)
    IF(KEEP(I, J) .LT. BOTTOM(I, J) .AND. SYB .GT. 0.) STORE = SYB
185 CONTINUE
    IF (CONVRT.NE.CHK(7)) GC TO 220
    X=KEEP(I, J)-PHI(I, J)
    IF(X) 190, 220, 200
190 HED1=PHI(I, J)
    HED2=KEEP(I, J)

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```

ZLK5 = U3PT*FLUX
ZCH1 = U3PT*CHD2
ZCH2 = U3PT*CHD1
ZCH3 = U3 *CHST
ZCH4 = U3 *(-CHOT)
ZCF1 = U3PT*CONFXP
ZCF2 = U3PT*CONFXN
ZCF3 = U3 *CFLXPT
ZCF4 = U3 *(-CFLXNT)
ZP1 = U3PT*PUMPP
ZP2 = U3PT*(PUMP - PUMPP)
ZP3 = U3 *PUMPPT
ZP4 = U3 *(-PUMPT - PUMPPT)
ZT1 = ZRE1 + ZLK1 + ZCH1 + ZCF1 + ZP1
ZT2 = ZRE2 + ZLK2 + ZCH2 + ZCF2 + ZP2
* + ZRE2
ZT3 = ZRE3 + ZLK3 + ZCH3 + ZCF3 + ZP3
ZT4 = ZRE4 + ZLK4 + ZCH4 + ZCF4 + ZP4
* + ZRE4
ZN1 = ZT1 + ZT2
ZN3 = ZT3 + ZT4
ZST2 = U3PT*STOR
ZST4 = U3 *(-STORT)
ZE1 = ZN1 - ZST2
ZE3 = ZN3 - ZST4
ZPC1 = 100.*ZE1/AMAX1(ZT1, ZT2, 1E-30)
ZPC3 = 100.*ZE3/AMAX1(ZT3, ZT4, 1E-30)
*WRITE(P, 240)
IF(ZP3 - ZP4 .GT. 0.) WRITE(P, 2410) ZP1, ZP2, ZP3, ZP4
IF(ZLK3 - ZLK4 .GT. 0.) WRITE(P, 2411) ZLK1, ZLK2, ZLK3, ZLK4
IF(ZCF3 - ZCF4 .GT. 0.) WRITE(P, 2412) ZCF1, ZCF2, ZCF3, ZCF4
IF(ZCH3 - ZCH4 .GT. 0.) WRITE(P, 2413) ZCH1, ZCH2, ZCH3, ZCH4
IF(ZRE3 - ZRE4 .GT. 0.) WRITE(P, 2414) ZRE1, ZRE2, ZRE3, ZRE4
*WRITE(P, 242) ZT1, ZT2, ZT3, ZT4, ZN1, ZN3
* , ZST2, ZST4, ZE1, ZE3, ZPC1, ZPC3
C
--- WRITE ON DISK FILE THE LEAKAGE RATE AT EACH NODE ---
IF (ISVFLX.NE.1) GO TO 310
ISVFLX=0
WRITE (P,9110) KT, DAYS
JMI=IFILE(1)
DO 250 I=1,DIML
DO 279 J=1,DIMW
IF (T(I,J).LT.1.0E-10 .OR. S(I,J).LT.0.0) PHE(I,J)=0.0
279 CONTINUE
*WRITE (JMI) (PHE(I,J), J=1,DIMW)
*WRITE (P,9100) I, (PHE(I,J), J=1,DIMW)
230 CONTINUE
ENDFILE JMI
C
310 CONTINUE
RETURN
C
C
C
C
FORMATS:
240 FORMAT('0', 25X, 'M A S S B A L A N C E' / 1X, 72('-')),
* / ' TYPE OF FLOW', 4X, 'CURRENT RATE (ACRE FT/YR)',
* 3X, 'CUMULATIVE (ACRE FT)' / 20X, 'INFLOW', 6X, 'OUTFLOW',
* 3X, 'INFLOW', 8X, 'OUTFLOW' / 1X, 72('-'))
241 FORMAT(' EVAPOTRANS.', 10X, F20.4, 10X, F20.4
* / ' RECHARGE', F19.4, 10X, F20.4
* / ' LEAKAGE', 6X, 2F14.4, ' * ', 2F14.4
* / ' CONSTANT HEAD', 2F14.4, 2X, 2F14.4
* / ' CONSTANT FLUX', 2F14.4, 2X, 2F14.4
* / ' PUMPING', 6X, 2F14.4, 2X, 2F14.4 )
2410 FORMAT(' PUMPING ', 2F14.0, 2X, 2F14.0)
2411 FORMAT(' LEAKAGE ', 2F14.0, 2X, 2F14.0)
2412 FORMAT(' CONSTANT FLUX', 2F14.0, 2X, 2F14.0)
2413 FORMAT(' CONSTANT HEAD', 2F14.0, 2X, 2F14.0)
2414 FORMAT(' EVAPOTRANS.', 16X, F14.0, 16X, F14.0)
2415 FORMAT(' RECHARGE ', 2F14.0, 2X, 2F14.0)
242 FORMAT(10X, 12('-'), 2X, 12('-'), 4X, 12('-'), 2X, 12('-'))
* / ' TOTAL', 8X, 2F14.0, 2X, 2F14.0
* / ' ONEI INFLOW', 3X, F14.0, 16X, F14.0
* / ' STORAGE INCR.', F14.0, 16X, F14.0
* / 15X, 12('-'), 18X, 12('-')
* / ' ERROR', 8X, F14.0, 16X, F14.0

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      * / ' PERCENT ERROR', F14.2, '% ', 14X, F14.2, '%'
C      DELETE CARD
      * / 1X, 72(' ') )
C      DELETE CARD
244  FORMAT(' LATERAL FLOW ', 2F14.4)
250  FORMAT('-', 27X, 'NODE', 2I4)
251  FORMAT('-', 27X, 'RIVER NODES')
9100 FORMAT (1H0, IS, 2X, 1P10E12.4 / (3X, 1P10E12.4))
9110 FORMAT(1H1, 34X, 'LEAKAGE RATE (FT/SEC) COMPUTED AT THE END OF TI
      ME STEP NO. ', I4, 21H (SIMULATION TIME = , F3.2, 6H DAYS) /
      5 64  RO# )
C
      END

      SUBROUTINE PRNTAI(PHI, ISUR, S, DELX, DELY, WELL, IZ, JZ, IW, JW)
C
C
C      SPECIFICATIONS:
C*COM1*
C*COM2*
C*COM3*
      COMMON /SPARAM/ SLEAK,U,SS,FT,TMIN,ETD IST,DET,IFINAL,TMAX,CDLT,DEL
      IT,SUM,SUMP,NUMT,KT,KP,NPER,KTH,ITMAX,LENGTH,NWEL,NW,ERR,DIML,DIMW,
      2JNO1,INO1,R,P,PU,SUBS,STORE,TEST,ETQB,ETOD,FACTX,FACTY,IERR,
      3DAYS,YRS,SSRIV,CFLEAK,QSUM,KEDIT,MESSG,IPRODN,IPRFD,ISVHD,ISVFLX
      +,IFILE(10),KOUNT,KSTEP,NHYDR,IHYDR(13),JHYDR(13),HYDR(13)
C*COM4*
C*COM5*
      COMMON /PR/ XLABEL(3),YLABEL(6),TITLE(4),XN1,SYM(23),PRNT(122),BLA
      1NK(5),DIGIT(122),VF1(6),VF2(6),VF3(7),NA(4),XN(100),YN(13),XSF,NX
      2J,NIDTH,SPACNG,N1,N2,N3,N4,N6,N8,NC
C*COM6*
C*DIM1*
      DIMENSION PHI(IZ,JZ), ISUR(IZ,JZ), S(IZ,JZ), DELX(JZ), DELY(IZ), W
      1EL(I,J)
C*DIM2*
C*TYP1*
      REAL *4K, ISUR
C*TYP2*
      REAL *8XLABEL, YLABEL, TITLE, XN1, Z, PHI
C*TYP3*
      INTEGER DIML, DIMW, R, P, PU
C*DTA1*
C*DTA2*
C*DTA3*
C*ENDJ*
      RETJRN
C
C
C      *****
C      ENTRY PRNTA
C      *****
C      ---INITIALIZE VARIABLES---
      JIST=WIDTH-DELX(JNO1)/2.
      JJ=JNO1
      LL=1
      Z=NXD*KSF
      WRITE (P,150) (TITLE(I),I=1,4)
      DO 140 I=1,N4
C
C
C      ---LOCATE X AXES---
      IF (I.EQ.1.OR.I.EQ.N4) GO TO 10
      PRNT(1)=SYM(23)
      PRNT(N3)=SYM(23)
      IF ((I-1)/N1*N1.NE.I-1) GO TO 30
      PRNT(1)=SYM(25)
      PRNT(N3)=SYM(25)
      GO TO 30
C
C
C      ---LOCATE Y AXES---
      DO 20 J=1,N3
      IF ((J-1)/N2*N2.EQ.J-1) PRNT(J)=SYM(25)
      IF ((J-1)/N2*N2.NE.J-1) PRNT(J)=SYM(24)
C
C
C      ---COMPUTE LOCATION OF NODES AND DETERMINE APPROPRIATE SYMBOL---
      DO 30 IF (DIST.LT.0..OR.DIST.LT.Z-XN1*XSF) GO TO 30

```

```

      YLEN=DELY(2)/2.
      DO JJ L=2,IND1
      J=YLEN*N2/XSF+1.5
      K=(ISUR(L,JJ)-PHI(L,JJ))/SPACNG
      IF (K) 30,50,40
40  N=AMOD(K,20.)
      N=N
      PRNT(J)=SYM(N+1)
      GO TO 70
50  PRNT(J)=SYM(26)
      GO TO 70
60  PRNT(J)=SYM(22)
70  IF (S(L,JJ).LT.0.) PRNT(J)=SYM(27)
      IF (J#CJ.1) GO TO 30
      IF (NE(L,JJ).NE.0.) PRNT(J)=SYM(28)
60  YLEN=YLEN+(DELY(L)+DELY(L+1))/2.
      J(IST=UIST-(DELX(JJ)+DELX(JJ-1))/2.
      JJ=JJ-1
90  CONTINUE
C
C      ---PRINT AXES, LABELS, AND SYMBCLS---
      IF (I-NA(L).EQ.0) GO TO 110
      IF ((I-1)/N1*N1-(I-1)) 120,100,120
100  WRITE (P,VF1) (BLANK(J),J=1,NC),(PRNT(J),J=1,N6),XN(1+(I-1)/6)
      GO TO 130
110  WRITE (P,VF2) (BLANK(J),J=1,NC),(PRNT(J),J=1,N6),XLABEL(LL)
      LL=LL+1
      GO TO 130
120  WRITE (P,VF2) (BLANK(J),J=1,NC),(PRNT(J),J=1,N6)
C
C      ---COMPUTE NEW VALUE FOR Z AND INITIALIZE PRNT---
130  Z=Z-2.*XN1*XSF
      DO I=0 J=1,N6
140  PRNT(J)=SYM(11)
C
C      ---NUMBER AND LABEL Y AXIS AND PRINT LEGEND---
      WRITE (P,VF3) (ELANK(J),J=1,NC),(YN(I),I=1,N6)
      WRITE (P,170) (YLABEL(I),I=1,6)
      WRITE (P,160) SPACNG
      RETURN
C
C      ---FORMATS---
150  FORMAT ('1',46X,4A8//)
160  FORMAT ('-LEGEND-'// '-----'// ' R = CONSTANT HEAD BOUNDARY'// ' W = W
1  WELL LOCATION'// ' 0 = NO-FLOW BOUNDARY'// ' * = CONE OF IMPRESSION'// '
2  CONTOUR INTERVAL =',F10.2// ' THE FOLLOWING 20 SYMBCLS, STARTING #
3  WITH BLANK, ARE CYCLED: 1 2 3 4 5 6 7 8 9 1 3 3 D S F 7 H 9')
170  FORMAT ('0',39X,6A3)
      END

```

```

BLOCK DATA
-----
C
C*COM1*
COMMON /DARRAY/ RHOP(20), CHK(10), VF4(11)
C*COM2*
COMMON /SPARAM/ SLEAK,U,SS,TT,TMIN,ETDIST,GET,IFINAL,TMAX,CDLT,DEL
1F,SJM,SJMP,NUMT,KT,KP,NPER,<TH,ITMAX,LENGTH,NWEL,NW,ERR,DI ML,DIMW,
2JNUI,INUI,R,P,PU,SUBS,STORE,TEST,ETQB,ETQD,FACTX,FACTY,IERR,
3DAY,YRS,SSRIV,CFLEAK,QSUM,<EDIT,MESSG,IPRODN,IPRHED,ISVHED,ISVFLX
4,IFILE(13), KOUNT, KSTEP, NHYDR,IHYDR(13),JHYDR(13),HYDR(13)
* , WELBUT, WELTCP, SYB
C*COM4*
C*COM5*
COMMON /PR/ XLABEL(3),YLABEL(6),TITLE(4),XN1,SYM(28),PRNT(122),BLA
NK(66),DIGIT(122),VF1(6),VF2(6),VF3(7),NA(4),XN(100),YN(13),XSF,NX
2D,DI TH,SPACNG,N1,N2,N3,N4,N6,N8,NC
C*COM6*
C*TPJ1*
C*TPJ2*
REAL *BRHOP,CHK,XLABEL,YLABEL,TITLE,XN1
C*TPJ3*
INTEGER DIML,DIMW,R,P,PU
C
*****
C*DTA01*
DATA CHK/'PUNCH','WATERTAB','CCNTCUR','NUMERIC','CHECK','EVAPOTRA'
1,'CONVERT','HEAD','LEAKAGE','RECHARGE'/,R,P,PU/5.6,7/
C*DTA02*
DATA SYM/1H,1H1,1H2,1H3,1H4,1H5,1H6,1H7,1H8,1H9,1H,1H1,1H8,1H3,1
1H0,1H5,1HF,1H7,1HH,1H9,1H,1H*,1H|,1H-,1H+,1H0,1HR,1HW/
C*DTA03*
DATA PRNT/122*' /,N1,N2,N3,XN1/6,10,133,,0833333333D0/,BLANK/60*'
1' /,NA(4)/1000/
C*DTA04*
DATA XLABEL/' X DIS-', 'TANCE IN', ' MILES ',YLABEL/'O ISTANCE', '
1FROM OR', 'IGIN IN ', 'Y DIRECT', 'IGN, IN ', 'MILES ',TITLE/'ALPHA
2MER', 'IC CNTD', 'URS OF D', 'RAWDOWN '/
C*DTA05*
DATA DIGIT/'1','2','3','4','5','6','7','8','9','10','11','12','13'
1,'14','15','16','17','18','19','20','21','22','23','24','25','25',
2,'27','28','29','30','31','32','33','34','35','36','37','38','39',
3,'40','41','42','43','44','45','46','47','48','49','50','51','52','5
43','54','55','56','57','58','59','60','61','62','63','64','65','66
5,'67','68','69','70','71','72','73','74','75','76','77','78','79
6,'80','81','82','83','84','85','86','87','88','89','90','91','92'
7,'93','94','95','96','97','98','99','100','101','102','103','104'
8,'105','106','107','108','109','110','111','112','113','114','115'
9,'116','117','118','119','120','121','122'/
C*DTA06*
DATA VF1/'(1H ',',',', ' ', 'A1,F', '10.2', ')'/
C*DTA07*
DATA VF2/'(1H ',',',', ' ', 'A1,1', 'X,A3', ')'/
C*DTA08*
DATA VF3/'(1H0',',',', ' ', 'A1,F', '3.1', ', '12F1', '0.2')'/
C*DTA09*
C*COM3*
DATA VF4/'(1H0',',',', ' ', 'X,I2', ',2X', ',20F6', ',,1/(', ' ', 'X,2
10', 'F0.1', ')')'/
C*DTA10*
C*ENDJJ*
C
*****
END

```

```

3420 IF(VUTJ .GE. 10) CALL PLTTQ( 3420)
      RETURN
C                                     3.4 CQ EXIT = 2000 LOOPSQ
C                                     1.5 CX EOD
3500 IF(VUTJ .GE. 10) CALL PLTTQ( 3500)
      IE = IES
      GO TO 2100
C                                     2.5 CM
3520 IF(VUTJ .GE. 10) CALL PLTTQ( 3520)
      IF(VUTX .GE. 5) WRITE(UVC, 352)
352  FORMAT(' EOD ON CONTROL INPUT')
      IF(NW .GE. LW) GO TO 3530
      IF(NAB .GE. LAB) GO TO 3530
      IF(NSAD .GT. 0) GO TO 3530
      IF(LE .NE. 0) LPLT = LE
      IF(KE .NE. 0) MPLT = KE
      IF(KE .NE. 0) IES = IIE(MOD(KE, MNIE) + 1)
C                                     STORE EXIT COMMAND
      JE = 4
      CALL PLTEG
      NE = NE - 1
C                                     START EXECUTION
      VQ = 1
      RETURN
3530 CALL PLTEE(3, 3530, 70)
      WRITE(JVC, 353)
353  FORMAT(' EXECUTION INHIBITED DUE TO ERRORS. ')
      GO TO 3900
C                                     3.5 CQ EOD
3540 CALL PLTEE(4, 3540, 80)
      WRITE(JVC, 354)
354  FORMAT(' MISSING END ')
      GO TO 3900
C                                     1.6 CX TRACEM = SAB
C                                     2.6 CM TRACEM
C                                     3.6 CQ TRACEM
C                                     4.3 SX TRACE)
3600 IF(VUTJ .GE. 20) CALL PLTTQ( 3600)
      LE = MOD(LE, 5) + 1
      GO TO (3610, 3620, 3630, 3640, 3650), LE
      GO TO 9000
C                                     6.0 LC, MQ, KQ, IIE
3610 IF(VUTJ .GE. 10) CALL PLTTQ( 3610)
      IF(VE .NE. 0) VUTI = VE
      IF(WE .NE. 0) VUTJ = WE
      IF(XE .NE. 0) VUTX = XE
      IF(ME .NE. -1) GO TO 3614
      WRITE(JVC, 361) ILQ, LQ, (LLQ(I), I = 1, MNLQ)
      WRITE(JVC, 361) ILQ, MQ, (MMQ(I), I = 1, MNLQ)
C                                     361  FORMAT(' LQ, MQ', T10, 215, (T20, 2015) )
      WRITE(JVC, 361) ILQ, KQ, (KKQ(I), I = 1, MNLQ)
3614 IF(KE .EQ. 1) WRITE(UVC, 130) LPLT, MPLT, (IIO(I), I = 1, 9)
      IF(KE .NE. -1) GO TO 3616
      WRITE(JVC, 362) IE, IES, (IIE(I), I = 1, MNIE)
362  FORMAT(' IIE', T10, 215, (T20, 2015) )
3615 IF(KE .EQ. 1) WRITE(UVC, 353) IE, YE
363  FORMAT(' TRACE AT', I4, ' Y =', F10.4)
      GO TO 2100
C                                     6.1 FLTET
3620 IF(VUTJ .GE. 10) CALL PLTTQ( 3620)
      CALL PLTET(ME, KE, VE)
      GO TO 2100
C                                     6.2 PLTAT
3630 IF(VUTJ .GE. 10) CALL PLTTQ( 3630)
      CALL PLTAT(ME, KE, VE)
      GO TO 2100
C                                     6.3 FLTUT
3640 IF(VUTJ .GE. 10) CALL PLTTQ( 3640)
      CALL PLIUT(ME, KE, VE)
      GO TO 2100
C                                     6.4 PLTFT
3650 IF(VUTJ .GE. 10) CALL PLTTQ( 3650)
      CALL PLIFT(ME, KE, VE)
      GO TO 2100
C                                     6.5 PLTPT
3660 IF(VUTJ .GE. 10) CALL PLTTQ( 3660)
      CALL PLIPT(ME, KE, VE)
      GO TO 2100

```

APPENDIX B

PRINT - PLOT PACKAGE LISTING


```

C
                                G*PLT
IMPLICIT LOGICAL*4 (B)
IMPLICIT REAL*8 (C-D)
IMPLICIT INTEGER (F-G, U-V)
IMPLICIT INTEGER*2 (H)
DIMENSION RRRR(54, 60, 40), DDC(54, 60), XXDEL(50), YYDEL(54)
EQUIVALENCE (RRRR, I111)
DATA MNI, MNJ, MNP, MNV / 54, 60, 40, 5 /
DATA UVC / 5 /
*WRITE(UVC, 1) MNI, MNJ
1  FORMAT('          GWPLT  2/11/73 MCD 27A'
* , 2JA, 'MAXIMUM DIMENSIONS', 2I5)
CALL PLTA(UVC, RRRR, MNI, MNJ, MNP, MNV, XXDEL, YYDEL, DDC, MND
* , I111)
*WRITE(UVC, 2)
2  FORMAT('1 PRINT/PLOT PROGRAM')
CALL PLTX(5, 5, 10, 10, 10, 10)
*WRITE(UVC, 300)
300  FORMAT('1-PRINT/PLOT RETURNED TO MAIN PROGRAM')
STOP
END

```

```

SUBROUTINE PLTX(UC0, UVC0, NI0, NJ0, XDEL0, YDEL0)
IMPLICIT LOGICAL*4 (B)
IMPLICIT REAL*8 (C-D)
IMPLICIT INTEGER (F-G, U-V)
IMPLICIT INTEGER*2 (H)
COMMON / PLTC / LPLT, MPLT, IIDO(9)
COMMON / PLTX / UC, UC0, SCC, UVC, SW, VUTI, VUTQ, WUTX
* , VV, MW, NAB, MAB, NSAB, KAB
* , IMAP, LI, MI, KI, VI, NI, JMAP, LJ, MJ, KJ, VJ, NJ
* , VG, JUP, KOP, IE, NE, MNE, JE, LE, ME, KE, VE, WE, XE, YE
* , ADEL, YDEL
DIMENSION JJJQ(10, 3), LLQ(10), MMQ(10), KKQ(10), IIE(20)
EQUIVALENCE (IIDO(1), IPLT), (IIDO(7), IVAR)
EQUIVALENCE (IIDO(3), TI ), (IIDO(9), TPI )
                                VERSION AND CORRECTION DATE
                                *** PLEASE MAINTAIN ***
DATA VERS, TCCR / 0, 77.1108 /
DATA LLQ, MMQ, KKQ / 30*0 /
DATA MNIJUP, MNVC, MNLQ, MNIE / 10, 3, 10, 20 /
DATA IIE / 20*0 /
DATA NEAB / 0 /
MJJ(I, N) = IABS(I + N - ((I + N)/N)*N)
                                STOPE PARMS
JC = UC0
SW = UVC0 .GE. 0
IF(UVC0 .GT. 0) UVC = UVC0
NI = NI0
NJ = NJ0
XDEL = XDEL0
YDEL = YDEL0
*WRITE(UVC, 101) VERS, TCCR
101  FORMAT('1, T30, 'PRINT/PLOT PACKAGE - VERSION', I3, ' CORRECTED'
* , F10.4 ///)
                                INIT COMMON
UC0 = JC
KAB = 0
VAB = 2
LW = 10
MW = 100
NW = 0
LAB = 1
TAB = 10
VAB = 0
NSAB = 0
IMAP = 1
LI = 1
MI = NI
KI = 1
VI = NI
JMAP = 1
LJ = 1
MJ = NJ
KJ = 1

```

```

VJ = NJ
NE = J
IE = 0
IES = 0
JE = 1
C
NEAS = MVE
C
CALL PLTTI(UVC)
CALL PLTTM(1000)
C
INIT LCCAL
INIT TRACE
LOAD TABLES
121 FORMAT(16I5)
122 FORMAT(' TABLE', T10, 16I5)
123 FORMAT(30I2)
124 FORMAT(' TABLE', T10, 30I2)
READ(JC, 121) LE, VE, VUTI, VUTC, VUTX, ME
IF(VE .GT. 0) WRITE(UVC, 122) LE, VE, VUTI, VUTC, VUTX, ME
IF(LE .GT. 0) JC = LE
BCC = VE .GE. 10
CALL PLTEI
READ(JC, 121) NJOP, NVQ
IF(VE .GE. 10) WRITE(UVC, 122) NJOP, NVQ
IF(NJOP .LT. 0) GO TO 1450
READ(JC, 123) ( (JJJQ(JCP, VQ), VQ = 1, NVQ), JOP = 1, NJOP)
IF(VE .GE. 20) WRITE(UVC, 124)
* ( (JJJQ(JOP, VQ), VQ = 1, NVQ), JOP = 1, NJOP)
GO TO 1490
1450 CONTINUE
NJOP = -NJOP
GO 1480 JOP = 1, NJOP
READ(JC, 121) (JJJQ(JOP, VQ), VQ = 1, NVQ)
IF(VE .GE. 20) WRITE(UVC, 122) (JJJQ(JCP, VQ), VQ = 1, NVQ)
1480 CONTINUE
1490 CONTINUE
IF(ME .GT. 0) WRITE(ME, 121) NJOP, NVQ
IF(ME .GT. 0) WRITE(ME, 123)
* ( (JJJQ(JOP, VQ), VQ = 1, NVQ), JOP = 1, NJOP)
C
RESTART
1600 IF(VJTX .GE. 40) CALL PLTTQ( 1600)
ILQ = J
LJ = J
MW = 0
KJ = 0
VQ = 2
NEV = J
GO TO 2100
C
C
ENTRY PLTX
IF(VJTX .GT. 0) CALL PLTTM(1800)
IF(VUTI .GE. 10) WRITE(UVC, 130) LPLT, MPLT, IIDC
1800 FORMAT(' TIME', T10, 2I5, 7I10, 2F15.3)
IF(KAS) 9000, 2200, 8900
C
LCOPEQ
2000 IF(VJTX .GE. 40) CALL PLTTQ( 2000)
CALL PLTEQ
C
LOOPER
2100 IF(VJTX .GE. 40) CALL PLTTQ( 2100)
IF(KAS) 9000, 2120, 8900
2120 CONTINUE
CALL PLTER
C
LOOPJO
2200 CONTINUE
JJ = JJJQ(JOP, VQ)
IF(VJTX .GE. 100) WRITE(UVC, 240) VQ, JCP, JJ
2400 FORMAT(' JQ', T10, 16I5)
2500 CONTINUE
GO TO (2510, 2520, 2530, 2540, 2000, 2550, 2570, 2580, 2590, 2600
* , 2610), JJ
CALL PLTTQ(2500)
GO TO 9000
C
FIRST LEVEL EXITS
1.1/1 CX CONTRJL
C
2510 IF(VUTQ .GE. 40) CALL PLTTQ( 2510)
GO TO (3100, 3200, 3300, 3400, 3500, 9000, 3700, 3800, 9000, 4000
* , 1000, 4400, 9000), KDP
GO TO 9000
C
1.2/2 CH

```

```

2520 IF(VUT2 .GE. 40) CALL PLTTQ( 2520)
      SU TO (3120, 3220, 3300, 3420, 3520, 3600, 3720, 3820, 3920, 4020
      * , 4120, 5720, 9000), KOP
      GO TO 9000
C
2530 IF(VUT2 .GE. 40) CALL PLTTQ( 2530)
      SU TO (3120, 3220, 3300, 3400, 3540, 3600, 3740, 3840, 3920, 2000
      * , 2000, 3740, 9000), KOP
      GO TO 9000
C
2540 IF(VUT2 .GE. 40) CALL PLTTQ( 2540)
      SU TO (3100, 2100, 3600, 5400, 5600, 5700, 5700, 5700, 5700
      * , 3700, 6200, 6300, 6400, 6500), KOP
      GO TO 9000
C
2550 IF(VUT2 .GE. 40) CALL PLTTQ( 2550)
      CALL PLTAX
      SU TO 2100
C
2570 IF(VUT2 .GE. 40) CALL PLTTQ( 2570)
      CALL PLFJM
      SU TO 2100
C
2580 IF(VUT2 .GE. 40) CALL PLTTQ( 2580)
      CALL PLTUX
      SU TO 2100
C
2590 IF(VUT2 .GE. 40) CALL PLTTQ( 2590)
      CALL PLTUF
      SU TO 2100
C
2600 IF(VUT2 .GE. 40) CALL PLTTQ( 2600)
      CALL PLTFX
      SU TO 2100
C
2610 IF(VUT2 .GE. 40) CALL PLTTQ( 2610)
      CALL PLTFX
      SU TO 2100
C
SECOND LEVEL EXITS
1.1 CX UNRECOGNIZED (JE = 1)
C
3100 CALL PLTEE(5, 3100, 10)
      WRITE(JVC, 310)
310  FORMAT(' ERROR IN STORED PROGRAM')
      GO TO 8000
C
3120 CALL PLTEE(3, 3120, 20)
      WRITE(JVC, 312)
312  FORMAT(' INVALID COMMAND CODE')
      GO TO 2100
C
3140 CALL PLTEE(3, 3140, 20)
      WRITE(JVC, 312)
      GO TO 2000
C
3200 CALL PLTEE(5, 3200, 30)
      WRITE(JVC, 320)
320  FORMAT(' UNDEFINED LABEL')
      GO TO 8000
C
3220 CALL PLTEE(2, 3220, 40)
      WRITE(JVC, 322)
322  FORMAT(' UNSUPPORTED OP CODE')
      GO TO 2100
C
3300 IF(VUT2 .GE. 10) CALL PLTTQ( 3300)
      IF(VUTX .GE. 5) WRITE(UVC, 330)
330  FORMAT(' ABORT COMMAND')
      GO TO 8000
C
3400 IF(VUT2 .GE. 10) CALL PLTTQ( 3400)
      SET EOD
      KOP = 5
      RETURN
C

```

```

C
3700 IF(VUTJ .GE. 10) CALL PLTTQ( 3700) 1.7 CX BEGIN
C
IF(ILQ .GE. MNLQ) GO TO 3710 PUSH Q = BEGIN, END, WAIT
ILQ = ILQ + 1
LLQ(ILQ) = LQ
MMQ(ILQ) = MQ
LQ = LE
MQ = VE
C
KJ = MIN(KQ, KE)
GO TO 2100
3710 CALL PLTEE(5, 3710, 100)
WRITE(JVC, 371)
371 FORMAT(' EXCESSIVE BEGINS FOR RUN TIME STACK')
GO TO 2100
C
3720 IF(VUTJ .GE. 10) CALL PLTTQ( 3720) 2.7 CM BEGIN
VQ = 3
C
3740 IF(VUTJ .GE. 10) CALL PLTTQ( 3740) 3.7 CQ BEGIN
C
IF(ILQ .GE. MNLQ) GO TO 3750
ILQ = ILQ + 1
LLQ(ILQ) = LQ
MMQ(ILQ) = MQ
C
LQ = LCC WHERE BEGIN WILL BE
LQ = NE + 1
MQ = 0
C
KJ = 0
C
KE = 0
VE = 0
GO TO 2000
3750 CALL PLTEE(4, 3750, 100)
WRITE(JVC, 371)
GO TO 2000
C
3800 IF(VUTJ .GE. 10) CALL PLTTQ( 3800) 1.3 CX END
IF(ILQ .EQ. 0) GO TO 3810
LQ = LLQ(ILQ)
MQ = MMQ(ILQ)
ILQ = ILQ - 1
GO TO 2100
3810 CALL PLTEE(5, 3810, 110)
WRITE(JVC, 381)
381 FORMAT(' UNMATCHED END')
GO TO 3900
C
3820 CALL PLTEE(3, 3820, 110) 2.8 CM END
WRITE(JVC, 381)
GO TO 2100
C
3840 IF(VUTJ .GE. 10) CALL PLTTQ( 3840) 3.8 CQ END
IF(ILQ .EQ. 0) GO TO 9000
STORE END ADDRESS IN BEGIN
CALL PLTEV(LQ, NE)
LQ = LLQ(ILQ)
MQ = MMQ(ILQ)
ILQ = ILQ - 1
IF(ILQ .LE. 0) VQ = 2
GO TO 2000
C
C
C
1.9 CX LABEL = 9000 SAB
2.9 CM LABEL
3.9 CQ
C
3920 IF(VUTJ .GE. 10) CALL PLTTQ( 3920)
LE = MOD(LE, MNIE) + 1
IIE(LE) = NE
GO TO 2100
C
4000 IF(VUTJ .GE. 10) CALL PLTTQ( 4000) 1.10 CX GO TO
IE = IIE(MOD(LE, MNIE) + 1)
GO TO 2100
C
4020 IF(VUTJ .GE. 10) CALL PLTTQ( 4020) 2.10 CM GO TO
I = IIE(MOD(LE, MNIE) + 1)
IF(I .GT. MNE) GO TO 4030
NE = I
GO TO 2100
4030 CALL PLTEE(4, 4030, 30)

```



```

102 =FORMAT(' OP TABLE', T10, 1615)
103 =FORMAT(6(212, A3) )
104 =FORMAT(' OP TABLE', T10, 6(212, A8) )
    IF(VE .GE. 30 .AND. NOP1 .GT. 0) WRITE(UVC, 104)
    * (JJUP(IOP), KKCP(IOP), CCOP(IOP), IOP = 1, NOP1), LCP
    READ(UC, 101) NCP, JE, JCP
    IF(VE .GE. 10) WRITE(UVC, 102) NOP, JE, JOP
    IF(JE .GT. 0) LOP = JE
    IF(JOP .GT. 0) NOP1 = JOP - 1
    IF(NOP .LT. 0) GO TO 1240
    JE = NOP1 + 1
    MOP = NOP1 + NOP
    READ(JC, 103) (JJOP(IOP), KKOP(IOP), CCOP(IOP), IOP = JE, MOP)
    IF(VE .GE. 20) WRITE(UVC, 104)
    * (JJUP(IOP), KKCP(IOP), CCOP(IOP), IOP = JE, MOP)
    GO TO 1260
1240 CONTINUE
    JE = NOP1 + 1
    NOP = 0
    DO 1260 IOP = JE, MNOP
    READ(JC, 103) JJOP(IOP), KKOP(IOP), CCOP(IOP)
    IF(VE .GE. 20) WRITE(UVC, 104) JJCP(IOP), KKCP(IOP), CCOP(IOP)
    IF(JJUP(IOP) .EG. 0) GO TO 1270
    NOP = NOP + 1
1260 CONTINUE
1270 CONTINUE
    MOP = NOP1 + NOP
1280 CONTINUE
    JUP = 0
    IF(VE .GT. 0) WRITE(WE, 101) JOP, JOP, NOP
    IF(VE .GT. 0) WRITE(WE, 103)
    * (JJOP(IOP), KKCP(IOP), CCOP(IOP), IOP = JE, MOP)
    INIT EXEC TABLE
C
    DO 1480 I = 1, MNE
    JJE(I) = 1
1480 CONTINUE
    JJE(MNE + 1) = 1
    JJE(MNE + 2) = 2
    RETURN
                                ENTRY PLTER
    IF(VUTX .EQ. 1) GO TO 3100
    IF(VUTX .GE. 30) CALL PLTTX(22000)
    READ(JC, 210, END=2800) CC, COP, LE, ME, KE, VE, WE, XE, YE
210 =FORMAT(10A3, T1, A8, 2X, 4I5, 3E10.0)
    IET = NE + 1
    IF(JCC) WRITE(UVC, 220) IET, CC
220 =FORMAT(' ', I5, T10, 10A8, ' CARD')
2400 CONTINUE
    DO 2430 IOP = LOP, MOP
    JE = IOP
    IF(COP .EQ. CCOP(IOP) ) GO TO 3500
2430 CONTINUE
    JE = 1
    GO TO 3500
2600 CONTINUE
    *RITE(UVC, 280)
280 =FORMAT('0 *** END OF FILE ON CONTROL INPUT')
    *RITE(UVC, 281)
281 =FORMAT('0', T10, 'STOP', 10X, 'GENERATED STATEMENT')
    COP = CSTOP
    LE = 0
    GO TO 2400
                                ENTRY PLTEX
    IF(VUTX .GE. 35) CALL PLTTX(23000)
3100 CONTINUE
    IE = IE + 1
    IET = IE
    JE = JJE(IE)
    LE = LLE(IE)
    ME = MME(IE)
    KE = KKE(IE)
    VE = VVE(IE)
    WE = WVE(IE)
    XE = XVE(IE)
    YE = YVE(IE)
3500 CONTINUE
    JUP = JJUP(JE)
    KOP = KKOP(JE)

```



```

IF(VOTE .GE. 30) WRITE(UVC, 350) VQ, JE, JOP, KOP, IET, CCOF(JE)
* .LE. ME, KE, VE, WE, XE, YE
350 FORMAT(' TRACE EX', T10, S15, A3, 2X, 4I5, 3G15.7)
RETURN
                                ENTRY PLTEQ
IF(NE .GE. MNE) GO TO 4800
NE = NE + 1
IF(NE .GT. MNET) MNET = NE
JJE(NE) = JE
LLE(NE) = LE
MME(NE) = ME
KKE(NE) = KE
VVE(NE) = VE
WWE(NE) = WE
XXE(NE) = XE
YYE(NE) = YE
RETURN
4800 CONTINUE
WRITE(UVC, 480) IET, CCOF(JE)
480 FORMAT(' ***FATAL ER # 300(24800) AT', I5, ' ', A3
* / ' EXECUTE TABLE FULL')
NSAB = NSAB + 1
KAB = 1
RETURN
                                ENTRY PLTEV(NEO, VEO)
VVE(NEO) = VEO
RETURN
                                ENTRY PLTEE(KEE, IEE, IAB)
IF(VJT) .GT. 0) CALL PLTTQ(IEE)
IF(VJTX .GE. 10) CALL PLTTX(29000)
IF(VUTI .GE. 10) WRITE(UVC, 901) LPLT, MPLT, IIDC
901 FORMAT(' TIME', T10, 2I5, 7I10, 2F15.5)
IF(VUTE .GE. 10) WRITE(UVC, 350) VQ, JE, JOP, KOP, IET, CCOF(JE)
* .LE. ME, KE, VE, WE, XE, YE
WRITE(UVC, 902) CCEE(KEE), IAB, IEE, IET, CCOF(JE)
902 FORMAT(' *** ', A8, ' #', I4, '(', I5, ') AT', I5, ' ', A8)
GO TO (9100, 9200, 9300, 9400, 9500, 9600, 9700), KEE
WRITE(UVC, 909)
909 FORMAT(' DOUBLE FAULT')
GO TO 9700
9100 CONTINUE
RETURN
9200 CONTINUE
NW = NW + 1
IF(NW .GE. MW) KAB = 1
RETURN
9300 CONTINUE
NAB = NAB + 1
IF(NSAB + NAB .GE. MAB) KAB = 1
RETURN
9400 CONTINUE
NSAB = NSAB + 1
IF(NSAB + NAB .GE. MAB) KAB = 1
RETURN
9500 CONTINUE
NSAB = NSAB + 1
KAB = 1
RETURN
9600 CONTINUE
NSAB = NSAB + 1
KAB = -1
RETURN
9700 CONTINUE
WRITE(UVC, 970) NW, NAB, NSAB
970 FORMAT(' --PRINT/PLOT STOP', I5, ' WARNINGS', I5, ' ERRORS',
* , I5, ' SEVERE ERRORS.')
STOP
                                ENTRY PLTET(MO, KO, VO)
IF(VO .NE. 0) VUTE = VO
IF(KO .LE. 0) RETURN
M = KO
IF(M .LE. 0) M = MNET
DO 995 I = MO, M
995 FORMAT(' EXEC TABLE', T15, 4I5, 1X, A3, 1X, 4I5, 3G15.7)
J = JJE(I)
WRITE(UVC, 995) J, JJOP(J), KKCP(J), I, CCOF(J)
* .LE(I), MME(I), KKE(I), VVE(I), WWE(I), XE(I), YYE(I)

```

9953 CONTINUE
 RETURN
 END

```

SUBROUTINE PLTAI(UVCO, RRRR, MNI, MNJ, MNR, MNV
* , XXDEL, YYDEL, DDD, MND, IIII)
IMPLICIT LOGICAL*4 (B)
IMPLICIT REAL*8 (C-D)
IMPLICIT INTEGER (F-G, U-V)
IMPLICIT INTEGER*2 (H)
COMMON / PLTCX / UC, UCQ, SCC, UVC, BW, VUTI, VUTQ, VUTX
* , VB, MB, NAB, MAB, NSAB, KAB
* , IMAP, LI, MI, KI, VI, NI, JMAP, LJ, MJ, KJ, VJ, NJ
* , VJ, JOP, KOP, IE, NE, MNE, JE, LE, ME, KE, VE, WE, XE, YE
* , XDEL, YDEL
C
C          DIMENSION PARAMETERS
DIMENSION PPR(MNI, MNJ, MNR), XXDEL(MNJ), YYDEL(MNI), DDD(MNI, MNJ)
C
C          DIMENSION LOCAL
DIMENSION HHC(6)
C
C          DATA LOCAL
DATA HHC / ' ', ' ', ' ', '0', '-1', '1', '+1' /
DATA MNRK / 6 /
DATA MVDIV, MIDIV, MDIV / 10, 100, 10 /
DATA RLDIV, REDIV, RDIV / 0., 1E-20, 1E20 /
DATA MVLOG, MILCG, MLOG / 10, 100, 10 /
DATA RLLOG, RELCG, RLOG / 0., 1E-20, 1E20 /
MDD(1, N) = IABS(1 + N - ((1 + N)/N)*N)
C
C          ENTRY PLTAI
INIT COMMON
C
C          JVC = JVC0
1  FORMAT(' SJB PLTAI 12/17/73 MOD 27')
WRITE(JVC, 1)
VUIV = J
NLU = J
RLDIV = AMAX1(RLDIV, REDIV)
RMLJG = AMAX1(RLLOG, RELCG)
CALL PLTUI(RRRR, MNI, MNJ, MNR, MNV)
RETURN
C
C          6 PX ARITHMETIC
ENTRY PLTAX
IF(VUTQ .GE. 30) CALL PLTTQ(0, 20000)
SU TO (1000, 2000, 3000, 4000), KCP
CALL PLTEE(3, 20000, 0)
RETURN
C
C          6.1 PX ZDIV
1000 IF(VUTQ .GE. 20) CALL PLTTQ(21000)
ITRAC = 21000
IF(L - 1) 1100, 1200, 3000
1100 IF(VUTQ .GE. 10) CALL PLTTQ(21100)
IF(ME .NE. 0) MVDIV = ME
IF(KC .NE. 0) MIDIV = KE
IF(VE .NE. 0) MDIV = VE
IF(AE .NE. 0) RLDIV = WE
IF(XE .NE. 0) REDIV = XE
IF(YE .NE. 0) RDIV = YE
IF(RLDIV .EQ. -1) RLDIV = 0.
IF(REDIV .LT. 0) REDIV = 0.
RLDIV = AMAX1(RLDIV, REDIV)
RETURN
1200 IF(VUTQ .GE. 10) CALL PLTTQ(21200)
IF(ME .NE. 0) MVLOG = ME
IF(KC .NE. 0) MILCG = KE
IF(VE .NE. 0) MLOG = VE
IF(AE .NE. 0) RLLOG = WE
IF(XE .NE. 0) RELCG = XE
IF(YE .NE. 0) RLOG = YE
IF(RLLOG .EQ. -1) RLLOG = 0.
IF(RELCG .LT. 0) RELCG = 0.
RMLJG = AMAX1(RLLOG, RELCG)
RETURN
C
C          6.2 PX FUNCTION
2000 IF(VUTQ .GE. 20) CALL PLTTQ(22000)
NE = MDD(ME - 1, MNR) + 1

```

```

A = MOD(KE - 1, MNR) + 1
V = MOD(VE - 1, MNR) + 1
X = KE
Y = VE
IF(X .EQ. 0.) X = 1.
IF(Y .EQ. 0.) Y = 1.
L = ABS(L) + 1
GO TO (2100, 2200, 2300, 2400, 2500, 2600, 2700), L
ITRAC = 22000
GO TO 3000

C
2100 IF(VJTJ .GE. 10) CALL PLTTQ(22100)
IF(VE .NE. 0) GO TO 2170
IF(KE .NE. 0) GO TO 2140
DO 2120 I = 1, NI
DO 2120 J = 1, NJ
2120 RRRR(I, J, ME) = WE
RETURN
2140 CONTINUE
DO 2150 I = 1, NI
DO 2150 J = 1, NJ
2150 RRRR(I, J, ME) = RRRR(I, J, K)
RETURN
2170 CONTINUE
DO 2180 I = 1, NI
DO 2180 J = 1, NJ
2180 RRRR(I, J, ME) = RRRR(I, J, K) - RRRR(I, J, V)
RETURN

C
2200 IF(VJTJ .GE. 10) CALL PLTTQ(22200)
IF(VE .NE. 0) GO TO 2250
DO 2240 I = 1, NI
DO 2240 J = 1, NJ
2240 RRRR(I, J, ME) = WE + X*RRRR(I, J, K)
RETURN
2250 CONTINUE
IF(L .LT. 0) Y = -Y
DO 2280 I = 1, NI
DO 2280 J = 1, NJ
2280 RRRR(I, J, ME) = WE + X*RRRR(I, J, K) + Y*RRRR(I, J, V)
RETURN

C
2300 IF(VJTJ .GE. 10) CALL PLTTQ(22300)
IF(L .LT. 0) GO TO 2350
DO 2340 I = 1, NI
DO 2340 J = 1, NJ
2340 RRRR(I, J, ME) = WE + X*RRRR(I, J, K)*RRRR(I, J, V)
RETURN

C
2350 CONTINUE
IDIV = 0
DO 2380 I = 1, NI
DO 2380 J = 1, NJ
R = RRRR(I, J, V)
IF(ABS(X) .GT. RMDIV) GO TO 237E
IF(ABS(K) .GT. RLDIV) GO TO 2373
RRRR(I, J, ME) = 0.
GO TO 2380
2373 CONTINUE
IDIV = IDIV + 1
IF(IDIV .LE. MVDIV) WRITE(UVC, 237) K, I, J, R
237 FORMAT(' *** DIVISION BY VARIABLE', I3, ', ', POSITION', 2I4
* , ' VALUE', G15.7)
RRRR(I, J, ME) = RLOG
GO TO 2380
2375 CONTINUE
RRRR(I, J, ME) = WE + X*RRRR(I, J, K)/R
2380 CONTINUE
IF(IDIV .LE. 0) GO TO 2385
IF(IDIV .LT. MVDIV) WRITE(UVC, 238) K, IDIV
238 FORMAT('0*** DIVISION BY VARIABLE', I3, ', ', 110, ' ZEROES.')
NDIV = NDIV + 1
IF(IDIV .GE. MIDIV .OR. NDIV .GE. MDIV) GO TO 8200
2385 CONTINUE
RETURN

C
2400 IF(VJTJ .GE. 10) CALL PLTTQ(22400)
ITRAC = 22400
POWER/DEFER

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```

GO TO 3100
C
2500 IF(VUTQ .GE. 10) CALL PLTTQ(22500) 6.2.4 EXP
      ITRAC = 22500
      IF(YE .EQ. 0) YE = 10.
      IF(YE .LT. 1) GO TO 8000
      IF(YE .GT. 1) YE = ALOG(YE)
      IF(LE .LT. 0) GC TO 2550
      DO 2540 I = 1, NI
      DO 2540 J = 1, NJ
2540 RRRR(I, J, ME) = WE + X*EXP(YE*RRRR(I, J, K))
      IF(VE .NE. 0) GC TO 2900
      RETURN 6.2.-4 LQG
C
2550 CONTINUE
      ITRAC = 22550
      X = X/YE
      ILOG = 0
      DO 2580 I = 1, NI
      DO 2580 J = 1, NJ
      R = RRRR(I, J, K)
      IF(R .GT. RMLOG) GO TO 2560
      IF(ABS(R) .GT. RLLOG) GO TO 2555
      RRRR(I, J, ME) = 0.
      GO TO 2580
2555 CONTINUE
      ILOG = ILOG + 1
      IF(ILOG .LE. MVLOG) WRITE(UVC, 255) K, I, J, R
2555 FORMAT(' *** LOG OF VARIABLE ', I3, ', ', POSITION, 214
            * , ' VALUE ', G13.7)
      RRRR(I, J, ME) = RLOG
      GO TO 2580
2560 CONTINUE
      RRRR(I, J, ME) = WE + X*ALOG(R)
2560 CONTINUE
      IF(ILOG .LE. 0) GO TO 2585
      IF(ILOG .GT. MVLOG) WRITE(UVC, 256) K, ILOG
2560 FORMAT(' *** LOG OF VARIABLE ', I3, ', ', I10, ' ZEROS. ')
      NLOG = NLOG + 1
      IF(ILOG .GE. MILOG .OR. NLOG .GE. MLOG) GO TO 3300
2565 CONTINUE
      IF(VE .NE. 0) GC TO 2900
      RETURN
C
2600 IF(VUTQ .GE. 10) CALL PLTTQ(22600) 6.2.5 PHI
      DW = WE
      DX = X
      IF(LE .LT. 0) GC TO 2650
      IF(VE .NE. 0) GC TO 2630
      DO 2620 I = 1, NI
      DO 2620 J = 1, NJ
      DRK = RRRR(I, J, K)
2620 DJJ(I, J) = DW + DX*DRK
      RETURN
2630 CONTINUE
      DY = Y
      DO 2640 I = 1, NI
      DO 2640 J = 1, NJ
      DRK = RRRR(I, J, K)
      DRV = RRRR(I, J, V)
2640 DJJ(I, J) = DW + DX*DRK + DY*DRV
      RETURN
2650 CONTINUE
      IF(VE .NE. 0) GC TO 2670
      DO 2660 I = 1, NI
      DO 2660 J = 1, NJ
2660 RRRR(I, J, ME) = DW + DX*DDO(I, J)
      RETURN
2670 CONTINUE
      DY = Y
      DO 2680 I = 1, NI
      DO 2680 J = 1, NJ
      DRV = RRRR(I, J, V)
2680 RRRR(I, J, ME) = DW + DX*DDO(I, J) - DY*DRV
      RETURN
C
2700 CONTINUE 6.2.6 INTEGER
      IF(LE .LT. 0) GC TO 2750

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      DO 2740 I = 1, NI
      DO 2740 J = 1, NJ
2740 III(I, J, ME) = WE + X*RRRR(I, J, K)
      RETURN
C
      6.2.-6 REAL
2750 CONTINUE
      DO 2780 I = 1, NI
      DO 2780 J = 1, NJ
2780 RRRR(I, J, ME) = WE + X*FLOAT(III(I, J, K))
      RETURN
C
      DIVIDE BY P(V)
2900 CONTINUE
      ITRAC = 22900
      GO TO 3100
C
      6.3 PX COMPARE
3000 IF(VUTJ .GE. 20) CALL PLTTQ(23000)
      ME = MOD(ME - 1, MNR) + 1
      KE = MOD(KE - 1, MNR) + 1
      VE = MOD(VE - 1, MNR) + 1
      LE = MOD(LE + 3, 7) + 1
      GO TO (3350, 3250, 3150, 3050, 3100, 3200, 3300), L
      ITRAC = 23000
      GO TO 3000
C
      6.3.0 EQUAL
3050 IF(VUTJ .GE. 10) CALL PLTTQ(23050)
      DO 3060 I = 1, NI
      DO 3060 J = 1, NJ
3060 IF(RRRR(I, J, VE) .EQ. YE) RRRR(I, J, ME) = WE + X*RRRR(I, J, KE)
      RETURN
C
      6.3.1 GREATER OR EQUAL
3100 IF(VUTJ .GE. 10) CALL PLTTQ(23100)
      DO 3140 I = 1, NI
      DO 3140 J = 1, NJ
3140 IF(RRRR(I, J, VE) .GE. YE) RRRR(I, J, ME) = WE + X*RRRR(I, J, KE)
      RETURN
C
      6.3.-1 LESS OR EQUAL
3150 IF(VUTJ .GE. 10) CALL PLTTQ(23150)
      DO 3180 I = 1, NI
      DO 3180 J = 1, NJ
3180 IF(RRRR(I, J, VE) .LE. YE) RRRR(I, J, ME) = WE + X*RRRR(I, J, KE)
      RETURN
C
      6.3.2 GREATER
3200 IF(VUTJ .GE. 10) CALL PLTTQ(23200)
      DO 3240 I = 1, NI
      DO 3240 J = 1, NJ
3240 IF(RRRR(I, J, VE) .GT. YE) RRRR(I, J, ME) = WE + X*RRRR(I, J, KE)
      RETURN
C
      6.3.-2 LESS
3250 IF(VUTJ .GE. 10) CALL PLTTQ(23250)
      DO 3280 I = 1, NI
      DO 3280 J = 1, NJ
3280 IF(RRRR(I, J, VE) .LT. YE) RRRR(I, J, ME) = WE + X*RRRR(I, J, KE)
      RETURN
C
      6.3.3 MAX
3300 IF(VUTJ .GE. 10) CALL PLTTQ(23300)
      IF(KE .EQ. VE) GO TO 3400
      DO 3340 I = 1, NI
      DO 3340 J = 1, NJ
3340 RRRR(I, J, ME) = AMAX1(RRRR(I, J, KE), RRRR(I, J, VE))
      IF(KE .EQ. VE) GO TO 3400
C
      6.3.-3 MIN
3350 IF(VUTJ .GE. 10) CALL PLTTQ(23350)
      DO 3380 I = 1, NI
      DO 3380 J = 1, NJ
3380 RRRR(I, J, ME) = AMIN1(RRRR(I, J, KE), RRRR(I, J, VE))
3400 CONTINUE
      IF(KE .GE. YE) RETURN
      DO 3440 I = 1, NI
      DO 3440 J = 1, NJ
3440 RRRR(I, J, ME) = AMIN1(AMAX1(XE, RRRR(I, J, ME)), YE)
      RETURN
C
      6.4 PX STAT
4000 IF(VUTJ .GE. 20) CALL PLTTQ(24000)
      ME = MOD(ME - 1, MNR) + 1
      KE = MOD(KE - 1, MNR) + 1
      VE = MOD(VE - 1, MNR) + 1
      MC = HHC(MOD(IFIX(WE), MNHC) + 1)
      NTR = 0

```



```

SUBROUTINE PLTUI(RRRR, MNI, MNJ, MNR, MNV)
  IMPLICIT LOGICAL*4 (B)
  IMPLICIT REAL*8 (C-D)
  IMPLICIT INTEGER (F-G, U-V)
  IMPLICIT INTEGER*2 (H)
  COMMON / PLTC / LPLT, MPLT, IIDO(9)
  COMMON / PLTCX / UC, UCQ, BCC, UVC, BW, VUTI, VUTQ, VUTX
  * : V*, M*, NAB, MAB, NSAB, KAB
  * : JMAP, LI, MI, KI, VI, NI, JMAP, LJ, MJ, KJ, VJ, NJ
  * : VJ, JUP, KCP, IE, NE, MNE, JE, LE, ME, KE, VE, WE, XE, YE
  * : ADEL, YDEL
  C
  DIMENSION RRRR(MNI, MNJ, MNR)
  C
  DIMENSION LOCAL
  DIMENSION L
  DIMENSION BBUU(99), IIUU(99), NMJU(99), UUVV(99), VVUU(99)
  DIMENSION BBC(6), BEV(3), CCU(6), UU(5), UUV(6), IIU(10), JJU(10)
  DIMENSION CCV(50), JJDD(9), LLDD(9)
  C
  DIMENSION F
  DIMENSION CCHA(2), CCHI(25)
  DIMENSION MHA(3), MHC(6), MHI(100), MHT(10000)
  DIMENSION LLT(100), MMT(100), NNT(100), KKF(100), NNF(100)
  DIMENSION IIF(13), JJF(13), IIV(13), IIUF(13)
  C
  EQUIVALENCE (UU(5),UXR),(UUV(5),UVXR),(BBC(5),BCXR),(BBV(5),BVXR)
  EQUIVALENCE (UU(6),UXW),(UUV(6),UVXW),(BCC(6),BCXW),(BEV(6),BVXW)
  EQUIVALENCE (UU(1),UP),(IIDO(7),IVAR)
  * : (JJDD(1),JPLT),(JJDD(7),JVAR),(JJDD(8),TJ),(JJDD(9),TPJ)
  C
  EQUIVALENCE (MHA(1),CCHA(1)),(MHI(1),CCHI(1))
  C
  DATA LOCAL
  DATA U
  DATA CCU / 'PRINTER', 'CONTROL', 'DATA', 'PUNCH', 'INPUT', 'OUTPUT' /
  DATA CCV / 50*'LUUUUUUU' /
  DATA LLDD / 9*0 /
  DATA JJ / 6, 5, 0, 7, 20, 20 /
  DATA IIU / 1, 2, 3, 4, 5, 6, 3, 2, 3, 1 /
  DATA JJJ / 1, 2, 3, 4, 5, 6, 2, 2, 2, 4 /
  DATA MNV / 50 /
  DATA MLINE / 134 /
  C
  DATA F
  DATA CCHA / '(A1,(T9 ', ' ', 36A2))' /
  DATA CCHI / ' 0 1 2 3', ' 4 5 6 7', ' 8 9 10 11', '12 13 14 15', '16 17 18 19'
  * : '20 21 22 23', '24 25 26 27', '28 29 30 31', '32 33 34 35', '36 37 38 39'
  * : '40 41 42 43', '44 45 46 47', '48 49 50 51', '52 53 54 55', '56 57 58 59'
  * : '60 61 62 63', '64 65 66 67', '68 69 70 71', '72 73 74 75', '76 77 78 79'
  * : '80 81 82 83', '84 85 86 87', '88 89 90 91', '92 93 94 95', '96 97 98 99' /
  DATA MHC / ' ', ' ', ' ', '0', ' ', '1', ' ', '1', ' ', '1' /
  DATA JJF / 1, 2, 1, 2, 1, 3, 4, 5, 4, 5, 2 /
  I, I, A, G, G, G, E, E, F, F, G
  DATA IIF / 98, 98, 99, 95, 95, 55, 94, 94, 93, 93, 95 /
  DATA IIV / 11*95 /
  DATA IIUF / 6*1, 3, 3, 4, 4, 1 /
  DATA MHA, HLCCM / ' ', ' ', ' ', ' ', ' ', ' ' /
  DATA MHA, MHC, MHI, MNHT, MNT / 8, 6, 100, 10000, 100 /
  DATA MHT / 0 /
  MOD(I, N) = IABS(I + N - ((I + N)/N)*N)
  C
  ENTRY PLTUI
  *WRITE(JVC, 1)
  1 FORMAT(' SUB PLTUI 8/23/79 MCD 27A')
  DD 1020 I = 1, 9
  1020 IIDO(I) = 0
  C
  INIT LOCAL
  DD 1200 I = 1, 99
  IIUU(I) = 0
  VVUU(I) = 0
  BBUU(I) = .FALSE.
  JJVV(I) = UVC
  NMJU(I) = 0
  1250 CONTINUE
  DD 1300 I = 1, 6
  BBC(I) = .TRUE.
  BBV(I) = .FALSE.
  JJV(I) = UVC
  1300 CONTINUE
  DD 1400 I = 1, MNT
  LLT(I) = 0

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MMT(1) = 0
NNF(1) = 0
KKF(1) = -3
NNF(1) = 0
1480 CONTINUE
CALL PLTFI(RRRR, MNI, MNJ, MNR, MNV, CCV, MNCV)
C CALL PLTPI(RRRR, MNI, MNJ, MNR, MNV
C * , TIU, HMT, NHT, MNHT, LLT, NNT, KKF, MNT, CCV, MNCV)
C RETURN
7 UM FILE IMMEDIATE
ENTRY PLTUM
IF(VJTI .GE. 30) CALL PLTTO(32000)
GO TO (2100, 2200, 2300), KOF
CALL PLTEE(5, 32000, 0)
RETURN

7.1 TEXT
2100 IF(VJTI .GE. 10) CALL PLTTO(32100)
LE = MOD(LE - 1, MNT) + 1
IF(ME .LE. 0) ME = 72
LT = NHT + 1
L = LT
IF(NE .GE. 3) L = L + 3
M = L + (ME - 1)/2
IF(M .GT. MNHT) GO TO 2190
READ AND IGNORE/DEFER
210 READ(JC, 210) (HHT(I), I = L, M)
FORMAT(36A2)
IF(3CC) WRITE(UVC, 211) (HHT(I), I = L, M)
211 FORMAT(T10, 36A2, T90, ' CARD')
NHT = M
LLT(LE) = LT
MNT(LE) = M
NNT(LE) = ME
IF(VE .LE. 0) VE = 1
NNF(LE) = VE
KKF(LE) = MIN0(KF - 2, 0)
RETURN
2190 CALL PLTEE(5, 32190, 420)
WRITE(JVC, 219)
219 FORMAT(' TEXT STORAGE FULL')
RETURN

7.2 FORMAT
2200 IF(VJTI .GE. 10) CALL PLTTO(32200)
LE = MOD(LE - 1, MNT) + 1
ME = MOD(ME - 1, MNT) + 1
IF(KKF(ME) .LT. 0) GO TO 2290
IF(LE .EQ. ME) GO TO 2220
L = LLT(ME)
M = MNT(ME)
IF(NHT + M - L + 1 .GT. MNHT) GO TO 2291
LT = NHT + 1
DO 2210 I = L, M
NHT = NHT + 1
HHT(NHT) = HHT(I)
2210 CONTINUE
LLT(LE) = LT
MNT(LE) = NHT
NNT(LE) = NNT(ME)
KKF(LE) = KKF(ME)
NNF(LE) = NNF(ME)
REFORMAT
2220 CONTINUE
LT = LLT(LE)
SET T FORMAT
C KE = MOD(KE, MNHI)
IF(KE .GT. 0) HHT(LT + 9) = HHT(KE + 1)
SET REPETITION
C IF(VE .LE. 1) GO TO 2225
VE = MOD(VE - 1, MNHI) + 1
IF(VE .GT. 1) HHT(LT + 15) = HHT(VE)
+ 1 - 1
C NNF(LE) = VE
2225 CONTINUE
SET W.D
C IF(ME .LE. 0.) GO TO 2230
I = ME
J = MOD(IFIX(WE*100. + .5), 100)
IF(J .GE. 30) J = J/10

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MHT(LT + 19) = MHI(MOD(I, MNHI) + 1)
IF(MHT(LT + 21) .EQ. HLB) GO TO 2228
MHI(LT + 20) = MHI(MOD(J, MNHI) + 1)
IF(J .GT. 0) GO TO 2228
IF(MHT(LT + 19) .NE. HLCDM) GO TO 2228
MHT(LT + 19) = HLB
MHT(LT + 20) = HLB
MHT(LT + 21) = HLB
2223 CONTINUE
IF(XE .LE. 0.) GO TO 2235
C
2230 CONTINUE
IF(XE .LE. 0.) GO TO 2240
I = XE
J = MOD(IFIX(XE*100. + .5), 100)
IF(J .GE. 30) J = J/10
2235 CONTINUE
MHT(LT + 12) = MHI(MOD(I, MNHI) + 1)
IF(MHT(LT + 15) .EQ. HLB) GO TO 2240
MHT(LT + 14) = MHI(MOD(J, MNHI) + 1)
IF(J .GT. 0) GO TO 2240
IF(MHT(LT + 13) .NE. HLCDM) GO TO 2240
MHT(LT + 14) = HLB
MHT(LT + 15) = HLB
2240 CONTINUE
RETURN
2290 CALL PLTEE(3, 32290, 430)
WRITE(JVC, 229)
229 FORMAT(' FORMAT NOT AVAILABLE')
RETURN
2291 CALL PLTEE(3, 32291, 420)
WRITE(JVC, 219)
RETURN
C
2300 IF(VUT .GE. 10) CALL PLTTQ(32300)
LE = MOD(LE - 1, MNCV) + 1
ME = LE + ME - 1
IF(ME .GT. MNCV) GO TO 2390
READ(JC, 230) (CCV(I), I = LE, ME)
230 FORMAT(9A8)
IF(BCC) WRITE(UVC, 231) (CCV(I), I = LE, ME)
231 FORMAT(T10, 9A8, T90, ' CARD')
RETURN
2390 CALL PLTEE(5, 32390, 440)
WRITE(JVC, 239)
239 FORMAT(' END OF NAME TABLE')
RETURN
C
8 UX FILE EXECUTE
ENTRY PLTUX
IF(VJTG .GE. 30) CALL PLTTQ(34000)
GO TO (4100, 4200, 4300, 4400, 4500, 4600, 4700, 4800), KOP
CALL PLTEE(5, 34000, 0)
RETURN
C
8.1 UNIT
4100 IF(VJTG .GE. 10) CALL PLTTQ(34100)
LE = MOD(LE, 10) + 1
C
SET DEVICE IJ CN DEVICE JU
IU = IU(LE)
JU = JU(LE)
J = MOD(ME, 100)
IF(J .EQ. 0) U = UU(JU)
IF(LE .LT. 7 .OR. LE .GT. 3) GO TO 4110
J = JC2
IF(LE .EQ. 3) UC = U
C
INITIALIZE CONTROL AND CARD FILES
IF(LE .NE. 7) GO TO 4110
JU(1) = UVC
BCC(2) = BW
UUV(2) = UVC
IUJ(JC) = 2
IUJ(UVC) = 1
V = 0
IF(BW) V = 2
VUJ(J) = V
UUV(J) = UVC
BW = .TRUE.
4110 CONTINUE

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IF(11JJ(J) .EQ. 0) 11UU(U) = JU
IF(11UU(U) .NE. JU) GO TO 4190
V = VVJJ(U)
IF(J .EQ. UU(IU) ) GO TO 4120
UU(IU) = U
BBC(IU) = V .GE. 1
BBV(IU) = V .GE. 2
UVV(IU) = UVV(U)
C
4120 CONTINUE
IF(KE .EQ. 0) GO TO 4140
V = KE
BBC(IU) = V .GE. 1
BBV(IU) = V .GE. 2
IF(IU .EQ. JU) VVUU(U) = V
C
4140 CONTINUE
VE = MJD(VE, 100)
IF(VE .EQ. 0) GO TO 4160
IF(11UU(VE) .EQ. 0) 11UU(VE) = 1
IF(11JJ(VE) .NE. 1) GO TO 4160
UVV(IU) = VE
IF(IU .EQ. JU) UVV(U) = VE
4160 CONTINUE
UV = UVV(IU)
C
IF(KE .NE. 0) WRITE(UV, 416) HHC(MOD(IFIX(WE), MNHC) + 1)
* , CCU(IU), U
416 FORMAT(A1, T30, A8, ' FILE', I3 / )
C
HEADING
LITTLE OPEN
IF(KE .EQ. 0) GO TO 4170
IF(BBJJ(J) ) GO TO 4170
BBJJ(J) = .TRUE.
NNJJ(J) = 0
4170 CONTINUE
IF(YE .NE. 0) BW = YE .GT. 0
IF(IU .NE. 2) GO TO 4180
IF(J .NE. UC) UCQ = UC
JC = JJ(2)
BCC = BBC(2)
JVC = JVV(2)
4180 CONTINUE
RETURN
4190 CALL PLTEE(3, 34190, 500)
WRITE(JVC, 419)
419 FORMAT(' UNIT IS WRONG TYPE')
RETURN
C
8.2 OPENR
4200 IF(VJTD .GE. 10) CALL PLTTQ(34200)
N = 0
IF(11UU(UXR) .EQ. 0) 11UU(UXR) = 4
IF(11JJ(JX?) .NE. 5) GO TO 4294
C
STANDARD FILE HEADER
READ(UXR, END=4690) JJDD
N = 1
IF(BCXR) WRITE(UVXR, 420) HHC(MOD(VE, MNHC) + 1)
* , CCU(5), JXR, JJDD
420 FORMAT(A1, T30, A8, ' FILE', I3
* / 'U', T10, 'CCDE, IDENT, TITLE, NI, NJ, NZ, XDEL, YDEL'
* / T10, 7110, 2F20.6 / )
IF(JPLT .NE. -9) GO TO 4290
IF(KE .GE. 0 .AND. JJDD(2) .NE. ME) GO TO 4291
IF(JJDD(3) .LE. 0) GO TO 4220
KE = MOD(KE - 1, MNT) + 1
M = MHT + 1
M = - + (JJDD(3) - 1)/2
IF(M .GT. MNHT) GO TO 4292
C
IGNORE TITLE/DEFER
READ(JXR, END=4690) (HHT(I), I = L, M)
N = 2
IF(BCXR) WRITE(UVXR, 421) (HHT(I), I = L, M)
421 FORMAT('OHEADER', T10, 50A2)
MHT = M + 1
LLT(KE) = L
MMT(KE) = M
NNT(KE) = JJDD(3)
KKF(KE) = -2
4220 CONTINUE

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```

IF(ABS(LE) .GE. 2) GO TO 4230
NI = JJDD(4)
NJ = JJDD(5)
MI = NI
MJ = NJ
VI = NI
VJ = NJ
XDEL = TJ
YDEL = TPJ
GO TO 4240
4230 CONTINUE
IF(JJDD(4) .NE. NI) GO TO 4293
IF(JJDD(5) .NE. NJ) GO TO 4293
4240 CONTINUE
IF(LE .GT. 0) GO TO 4290
C
CALL PLTEE(5, 34240, 410)
WRITE(JWC, 424)
424 FORMAT(' UNSUPPORTED OPERATION')
RETURN
4230 CONTINUE
NNUJ(UJR) = N
BBUJ(UJR) = .TRUE.
RETURN
4290 CALL PLTEE(5, 34290, 510)
WRITE(JWC, 429)
429 FORMAT(' FILE HEADER INVALID')
IIJJ(UJ) = -1
RETURN
4291 CALL PLTEE(5, 34291, 520)
WRITE(JWC, 429)
4291 FORMAT(' FILE HEADER ID DOES NOT MATCH.')
IIJJ(UJ) = -1
RETURN
4292 CALL PLTEE(3, 34292, 420)
WRITE(JWC, 219)
IIJJ(UJ) = -1
RETURN
4293 CALL PLTEE(5, 34293, 530)
WRITE(JWC, 427)
427 FORMAT(' FILE HEADER DIMENSIONS INCOMPATIBLE.')
IIJJ(UJ) = -1
RETURN
4294 CALL PLTEE(3, 34294, 500)
WRITE(JWC, 419)
IIJJ(UJ) = -1
RETURN
C
4300 IF(VJTJ .GE. 10) CALL PLTTQ(34300)
IF(IIJJ(JX*) .EQ. 0) IIUU(UXW) = 5
IF(IIUU(UXW) .NE. 6) GO TO 4294
N = 0
JJDD(1) = -9
JJDD(2) = ME
JJDD(3) = 0
JJDD(4) = NI
JJDD(5) = NJ
JJDD(6) = NI*NJ
JJDD(7) = 0
TJ = XDEL
TPJ = YDEL
IF(KE .EQ. 0) GO TO 4320
KE = MOD(KE - 1, MNT) + 1
L = LLT(KE)
M = MMT(KE)
JJDD(3) = NNT(KE)
4320 CONTINUE
IF(LE .GT. 0) GO TO 4340
C
CALL PLTEE(5, 34320, 410)
WRITE(UVC, 424)
RETURN
4340 CONTINUE
IF(BCX*) WRITE(UVXW, 420) HHC(MCD(VE, MNHC) + 1)
* , CCU(0), UXW, JJDC
IF(BW) WRITE(UXW) JJDD
IF(BW) M = 1
IF(KE .EQ. 0) GO TO 4350

```

PACKED FILE/DEFER

S.3 OPENW

PACKED FILE/DEFER

```

IF(BCXW) WRITE(LVXW, 421) (HHT(I), I = L, M)
IF(BW) WRITE(UXW) (HHT(I), I = L, M)
IF(JW) N = 2
C 4350 CONTINUE
C                                     PACKED FILE/DEFER
      BBUJ(UXW) = .TRUE.
      NNUJ(UXW) = N
      RETURN
C                                     8.4 CLOSE
4400 IF(VUT) .GE. 10) CALL PLTTQ(34400)
      L = MOD(ME, 100)
      IF(LE .GT. 0) GC TO 4450
      M = L
      IF(L .GT. 0) GO TO 4410
      L = 1
      M = 99
4410 CONTINUE
      DU +440 U = L, M
      IU = IIU(U)
      IF(IU .LE. 0) GC TO 4440
      IF(IU .LT. 3 .AND. LE .GT. -2) GO TO 4435
      IF(NNUJ(U) .LE. 0) GO TO 4435
      WRITE(JVC, 442) CCU(IU), U, NNUJ(U)
442  FORMAT('0', T10, A3, ' FILE', I3, ' CLOSED AFTER', I6, ' RECORDS.')
```

```

      REWIND U
      NNUJ(U) = 0
4435 CONTINUE
      IF(MOD(LE, 2) .EQ. 1) IIU(U) = 0
4440 CONTINUE
      RETURN
4450 CONTINUE
      IU = IIU(L)
      WRITE(JVC, 445) CCU(IU), L, NNUJ(L)
445  FORMAT('0', T10, A3, ' FILE', I3, ' ENDED AFTER', I6, ' RECORDS.')
```

```

      ENDFILE L
      NNUJ(L) = 0
      RETURN
C                                     8.5 LIMITR
4500 IF(VUT) .GE. 10) CALL PLTTQ(34500)
      IF(LE .NE. 0) LLDO(2) = LE
      IF(ME .NE. 0) LLDO(3) = ME
      IF(KE .NE. 0) LLDO(4) = KE
      IF(VE .NE. 0) LLDO(5) = VE
      IF(AE .NE. 0) LLDO(6) = WE
      RETURN
C                                     8.6 READ
4600 IF(VUT) .GE. 10) CALL PLTTQ(34600)
      IF(IIU(UXR) .NE. 3) GO TO 4294
      -E = MOD(LE - 1, MNR) + 1
      HC = MHC(MOD(VE, MNHC) + 1)
      GO TO 4520
4610 CONTINUE
      READ(JXR, END = 4690)
      NNUJ(U) = NNUJ(U) + 1
4620 CONTINUE
      READ(JXR, END = 4690) JJDO
      NNUJ(U) = NNUJ(U) + 1
      IF(BCXR) WRITE(UVXR, 460) HC, CCU(5), UXR, JJDO
460  FORMAT(A1, A8, ' FILE', I3, 7I10, 2F15.5)
      DU +600 I = 2, 6
      IF(JJDO(I) .LT. LLDO(I)) GO TO 4610
4640 CONTINUE
      IF(JPLT .LT. LPLT) GO TO 4610
      IF(JPLT .GT. MPLT) GO TO 4610
      IF(ME .EQ. 0) GC TO 4650
      IF(JVAR .NE. ME) GO TO 4610
      GO TO 4550
4650 CONTINUE
      ME = JVAR
      DU +555 I = 1, 3
4655 IJU(I) = JJDO(I)
4660 CONTINUE
      READ(UXR, END = 4690) ( (RRRR(I, J, LE), J = 1, NJ), I = 1, NI)
      NNUJ(UXR) = NNUJ(UXR) + 1
      IF(VUT) BVXR) RETURN
      KUP = 11
      U = UVAR
      VE = WE
```

```

      GO TO 6130
4690 CALL PLTEE(5, 34690, 540)
      *RITE(JVC, 469) CCU(5), UXR, NNUU(UXR)
469 FORMAT(' END OF ', A8, ' FILE', I3, ' AFTER', I6, ' RECORDS. ')
      *BUU(UXR) = .FALSE.
      NNUU(UXR) = 0
      RETURN
C
      8.7 WRITE
4700 IF(VJTJ .GE. 10) CALL PLTTQ(34700)
      IF(11JJ(UXW) .NE. 6) GO TO 4294
      LE = MOD(LE - 1, MNR) + 1
      MC = MHC(MOD(VE, MNHC) + 1)
      IF(4E .EQ. 0) ME = LE
      I = IVAR
      IVAR = ME
      IF(UXW) WRITE(UVXW, 460) HC, CCU(5), UXW, IIDO
      IF(UW) WRITE(UXW) IIDC
      IVAR = I
      IF(UW) WRITE(UXW) ( (RRRR(I, J, LE), J = 1, NJ), I = 1, NI)
      IF(UW) NNUU(UXW) = NNUU(UXW) + 2
      IF(UW) *BUU(UXW) RETURN
      KOP = 11
      U = UVXW
      VE = 4E
      GO TO 6130
C
      8.8 TITLE
4800 IF(VJTJ .GE. 10) CALL PLTTQ(34800)
      LU = UP
      IF(4E .GT. 0) LU = WE
      MU = LU
C
      (9.12 TITLE1)
4810 CONTINUE
      MC = MHC(MOD(VE, MNHC) + 1)
      IF(LE .EQ. 0) GO TO 4890
      LE = MOD(LE - 1, MNT) + 1
      IF(.NOT.(LE) .LE. -3) GO TO 4890
      IF(4E .EQ. 0) ME = 10
      IF(4E .GT. 0) GO TO 4820
      ME = -ME - NNT(LE)/2
      IF(4E .LT. 2) ME = 2
4820 CONTINUE
      IF(4E .LT. 1) ME = 1
      IF(4E .GE. MNHI) ME = MNHI - 1
      IF(4E + KE .GT. MLINE) KE = 0
      IF(KE .LE. 0) KE = MLINE + KE - ME
      KE = (KE + 1)/2
      IF(KE .LT. 1) KE = 1
      IF(KE .GE. MNHI) KE = MNHI - 1
      MHA(4) = MHI(ME + 1)
      MHA(5) = MHI(KE + 1)
      L = LLT(LE)
      M = MMT(LE)
      DO 4850 J1 = LU, MU
      J = J1
      IF(11UU(0) .NE. 1) U = UP
4850 *RITE(J, MHA) HC, (HHT(I), I = L, M)
      RETURN
4860 CONTINUE
      DO 4880 J = LU, MU
4880 *RITE(J, 438) HC
4880 FORMAT(A1)
      RETURN
4890 CALL PLTEE(3, 34890, 550)
      *RITE(JVC, 489)
489 FORMAT(' TEXT NOT SET')
      RETURN
C
      9 UF FORMATTED I/O
      ENTRY PLTUF
      IF(VJTJ .GE. 30) CALL PLTTQ(36000)
      GO TO (6100, 6200, 6300, 6100, 6300, 6700, 6300, 6700, 6800
      * , 6100, 7200), KOP
      CALL PLTEE(6, 36000, 0)
      RETURN
C
      9.1 HEAD
      9.4 PRINT
      9.5 PRINTI
      9.11 VERIFY
6100 IF(VJTJ .GE. 10) CALL PLTTQ(36100)

```



```

209 #WRITE(JVC, 209)
    #FORMAT(' INVALID FORMAT')
    RETURN
C
    ENRY PLTFU(UF, KOPF, JF, KF, HMF)
    IF(VJTD .GE. 30) CALL PLTTQ(43000)
    IF(KF + 1) 2090, 3080, 3020
3020 CONTINUE
    IF(JF .EQ. KF) GO TO 3080
    KF = JF
    DO 3080 I = 1, MNHF
3080 HMF(I) = HMF(I, KF)
3080 CONTINUE
    V = VE
    IF(V .GE. 10) V = MOD(V, 10)
    HC = HHC(MOD(V, MNHC) + 1)
    DO TO (3100, 3200, 3300, 3400, 3500, 3600, 3700, 3800, 3900, 4000
    * , +100), KOPF
    CALL PLTEE(6, 43000, 0)
    RETURN
C
    9.1 HEAD
3100 IF(VJTD .GE. 20) CALL PLTTQ(43100)
    #RITE(JF, HMF) HC, CCV(ME), (J, J = LJ, MJ, KJ)
    RETURN
C
    9.2 HEADI
3200 IF(VJTD .GE. 20) CALL PLTTQ(43200)
    J = JF
    L = LJ
    V = (VJ - 1)*KJ
3220 CONTINUE
    M = MIN0(L + V, MJ)
    #RITE(J, HMF) HC, IMAP, (J, J = L, M, KJ)
    J = J + 1
    L = M + 1
    IF(L .LE. MJ) GO TO 3220
    RETURN
C
    9.3 HEADIJ
3300 IF(VJTD .GE. 20) CALL PLTTQ(43300)
    L = -E
    IF(L .EQ. 0) L = 2
    L = MOD(L - 1, MNKRJ) + 1
    M = NKRJ
    IF(ME .GT. 0) M = L + ME - 1
    IF(M .GT. MNKRJ) M = MNKRJ
    #RITE(JF, HMF) HC, CCV(KVJ), (CCV(KKVJ:IK)), IK = L, M)
    RETURN
C
    9.4 PRINT
3400 IF(VJTD .GE. 20) CALL PLTTQ(43400)
    DO 3480 I = LI, MI, KI
    IF(VE .LT. 30) GO TO 3450
    DO 3440 V = 30, VE, 30
3440 #RITE(JF, 340)
340 #FORMAT(' ')
3450 CONTINUE
3480 #RITE(JF, HMF) HC, I, (RRRR(I, J, LE), J = LJ, MJ, KJ)
    RETURN
C
    9.5 PRINTI
3500 IF(VJTD .GE. 20) CALL PLTTQ(43500)
    U = JF
    L = LJ
    V = (VJ - 1)*KJ
3520 CONTINUE
    M = MIN0(L + V, MJ)
    #RITE(J, HMF) HC, CCV(ME), (RRRR(IMAP, J, LE), J = L, M, KJ)
    U = U + 1
    L = M + 1
    IF(L .LE. MJ) GO TO 3520
    RETURN
C
    9.6 PRINTIJ
3600 IF(VJTD .GE. 20) CALL PLTTQ(43600)
    L = LE
    IF(L .EQ. 0) L = 2
    L = MOD(L - 1, MNKRJ) + 1
    M = NKRJ
    IF(ME .GT. 0) M = L + ME - 1
    IF(M .GT. MNKRJ) M = MNKRJ

```



```

C
DO 3680 I = LI, MI, KI
                                HEAD ROW / DEFER
DO 3650 J = LJ, MJ, KJ
IF(RRRR(I, J, KRJ), LE, WE) GO TO 3679
WRITE(UF, HMF) HC, I, J, (RRRR(I, J, KKRJ(IK)), IK = L, M)
3679 CONTINUE
3650 CONTINUE
RETURN

C
                                9.7 CARD
3700 IF(VOTS .GE. 20) CALL PLTTQ(43700)
DO 3760 I = LI, MI, KI
READ(UF, HMF, END = 3790) (RRRR(I, J, LE), J = LJ, MJ, KJ)
IF(SV) WRITE(UV, HHV) HC, I, (RRRR(I, J, LE), J = LJ, MJ, KJ)
3730 CONTINUE
SV = .FALSE.
RETURN
3790 CALL P-TEE(5, 43790, 541)
WRITE(UVC, 379) UF
379 FORMAT(' END OF CARD FILE', I3)
RETURN

C
                                9.8 CARDIJ
3800 CONTINUE
L = LE/100
LE = LE - L*100
IF(L .EQ. 0) L = 2
L = MOD(L - 1, MNKRJ) + 1
M = NKRJ
IF(LE .GT. 0) M = L + LE - 1
IF(M .GT. MNKRJ) M = MNKRJ
3810 CONTINUE
READ(UF, HMF, END=3790) I, J, (RRJ(IK), IK = L, M)
IF(SV) WRITE(UV, HHV) HC, I, J, (RRJ(IK), IK = L, M)
IF(I .EQ. 0) GO TO 3880
IF(I .GE. 1 .AND. I .LE. NI .AND. J .GE. 1 .AND. J .LE. NJ) GO TO 3830
CALL P-TEE(3, 43810, 560)
WRITE(UVC, 381) I, J
381 FORMAT(' CARDIJ, ELEMENT', I5, ' OUT OF RANGE.')
GO TO 3810
3830 CONTINUE
IF(WE .NE. 0.) RRRR(I, J, KRJ) = WE
DO 3850 IK = L, M
RRRR(I, J, KKRJ(IK)) = RRJ(IK)
GO TO 3810
3880 CONTINUE
SV = .FALSE.
RETURN

C
                                9.9 PUNCH
3900 CONTINUE
DO 3980 I = LI, MI, KI
IF(SV) WRITE(UV, HHV) HC, I, (RRRR(I, J, LE), J = LJ, MJ, KJ)
3980 IF(SW) WRITE(UF, HMF) (RRRR(I, J, LE), J = LJ, MJ, KJ)
SV = .FALSE.
RETURN

C
                                9.10 PUNCHIJ
4000 CONTINUE
L = LE/100
LE = LE - L*100
IF(L .EQ. 0) L = 2
L = MOD(L - 1, MNKRJ) + 1
M = NKRJ
IF(LE .GT. 0) M = L + LE - 1
IF(M .GT. MNKRJ) M = MNKRJ
DO 4080 I = LI, MI, KI
DO 4080 J = LJ, MJ, KJ
IF(RRRR(I, J, KRJ), LE, WE) GO TO 4079
IF(SV) WRITE(UV, HHV) HC, I, J, (RRRR(I, J, KKRJ(IK)), IK = L, M)
IF(SW) WRITE(UF, HMF) I, J, (RRRR(I, J, KKRJ(IK)), IK = L, M)
4079 CONTINUE
4080 CONTINUE
SV = .FALSE.
RETURN

C
                                9.11 VERIFY
4100 IF(VOTS .GE. 20) CALL PLTTQ(44100)
DO 4160 I = 1, NI
WRITE(UF, HMF) HC, I, (RRRR(I, J, LE), J = 1, NJ)
RETURN
C
C

```

```

C                                     10 FX FORMATTED EXECUTE
ENTRY PLTFX
IF(VJTD .GE. 30) CALL PLTTQ(46000)
SU TO (0100, 6200, 6300), KOP
CALL PLTEE(5, 40000, 0)
RETURN

C                                     10.1 IPRINT
6100 IF(VJTD .GE. 10) CALL PLTTQ(46100)
IMAP = MOD(LE - 1, NI) + 1
RETURN

C                                     10.2 SETIJ
6200 IF(VJTD .GE. 10) CALL PLTTQ(46200)
IF(LE .GT. 0) NKRJ = MOD(LE - 1, MNKRJ) + 1
IF(LE .LT. 0) NKRJ = 0
IF(ME .EQ. 0) RETURN
ME = MOD(ME - 1, MNKRJ) + 1
KKRJ(ME) = MOD(KE - 1, MNR) + 1
KKVJ(ME) = MOD(VE - 1, MNCV) + 1
RETURN

C                                     10.3 VARIJ
6300 IF(VJTD .GE. 10) CALL PLTTQ(46300)
I = LE/100
J = LE
IF(I .NE. 0) J = MOD(IABS(J), 100)
IF(I .EQ. 0) I = J
IF(NKRJ .GE. MNKRJ) GO TO 6380
NKRJ = NKRJ + 1
KKRJ(NKRJ) = MOD(I - 1, MNR) + 1
KKVJ(NKRJ) = MOD(J - 1, MNCV) + 1
IF(ME .EQ. 0) GO TO 6380
I = ME/100
J = ME
IF(I .NE. 0) J = MOD(IABS(J), 100)
IF(I .EQ. 0) I = J
IF(NKRJ .GE. MNKRJ) GO TO 6380
NKRJ = NKRJ + 1
KKRJ(NKRJ) = MOD(I - 1, MNR) + 1
KKVJ(NKRJ) = MOD(J - 1, MNCV) + 1
IF(KE .EQ. 0) GO TO 6380
I = KE/100
J = KE
IF(I .NE. 0) J = MOD(IABS(J), 100)
IF(I .EQ. 0) I = J
IF(NKRJ .GE. MNKRJ) GO TO 6380
NKRJ = NKRJ + 1
KKRJ(NKRJ) = MOD(I - 1, MNR) + 1
KKVJ(NKRJ) = MOD(J - 1, MNCV) + 1
IF(VE .EQ. 0) GO TO 6380
I = VE/100
J = VE
IF(I .NE. 0) J = MOD(IABS(J), 100)
IF(I .EQ. 0) I = J
IF(NKRJ .GE. MNKRJ) GO TO 6380
NKRJ = NKRJ + 1
KKRJ(NKRJ) = MOD(I - 1, MNR) + 1
KKVJ(NKRJ) = MOD(J - 1, MNCV) + 1
SPLIT ME, XE, YE / DEFER

C 6380 CONTINUE
RETURN

C
C ENTRY PLTFT
RETURN
END

```

```
SUBROUTINE PLTTI(UVC)
INTEGER UVC
DIMENSION II(10)
DATA II / 10*0 /
DATA MNI, NI / 10, 0 /
RETURN

NI = 1
II(NI) = 1
RETURN

ENTRY PLTTM(I)

ENTRY PLTTG(I)

IF(NI .LT. MNI) GO TO 3800
GO 3780 J = 2, MNI
3780 II(J - 1) = II(J)
NI = NI - 1
3800 CONTINUE
NI = NI + 1
II(NI) = 1
RETURN

ENTRY PLTTX(I)

WRITE(JVC, 400) I, (II(J), J = 1, NI)
400 FORMAT(' TRACE PROG', T15, IS, (T20, 10I10) )
NI = 0
RETURN
END
```

APPENDIX C

INPUT DATA FOR MODEL

230	232	234	240	240	240	240	240
240	237	232	272	233	230	229	240
223	220	220	218	217	217	214	9999
9999	9999						
9999	9999	9999	9999	209	213	220	224
230	223	232	231	233	233	232	231
232	232	230	229	216	223	222	220
220	215	212	209	208	207	206	9999
9999	9999						
9999	9999	9999	9999	209	212	220	223
225	220	230	230	230	230	230	230
230	230	228	222	212	212	210	209
219	213	210	210	208	207	206	9999
9999	9999						
9999	9999	9999	9999	208	212	218	220
222	218	223	224	223	224	224	221
223	225	221	220	220	217	213	211
206	210	209	207	204	198	196	9999
9999	9999						
9999	9999	9999	9999	208	210	214	217
220	210	220	220	220	220	220	220
220	220	217	213	212	213	211	210
195	206	207	206	200	200	194	193
9999	9999						
9999	9999	9999	206	208	210	212	215
212	209	216	214	215	216	212	217
206	216	212	212	211	205	210	208
200	190	200	200	192	194	195	189
9999	9999						
9999	9999	9999	206	207	208	210	214
208	213	212	211	212	212	212	213
213	214	210	210	201	208	208	200
195	189	195	195	193	193	190	187
9999	9999						
9999	9999	9999	9999	9999	206	209	210
204	210	210	210	210	210	210	210
210	210	208	206	204	203	200	194
190	190	186	190	190	187	186	185
9999	9999						
9999	9999	9999	9999	199	204	206	205
200	205	204	204	203	205	204	208
208	206	206	202	202	201	200	192
190	188	189	185	188	186	188	185
9999	9999						
9999	9999	9999	197	199	200	202	201
195	202	200	195	200	203	202	204
204	204	204	202	200	200	198	189
190	186	186	186	183	186	186	9999
9999	9999						
9999	9999	9999	9999	196	199	200	199
200	192	198	193	194	200	200	202
202	202	202	200	198	197	194	187
202	202	202	185	181	184	184	184
186	186	186					
9999	9999						
9999	9999	9999	9999	9999	192	197	197
190	193	193	193	190	195	196	200
200	200	200	200	198	194	192	186
190	186	184	184	175	184	183	178
9999	9999						
9999	9999	9999	9999	185	190	192	192
193	193	180	190	190	190	192	193
190	193	188	197	192	192	191	190
194	182	182	181	171	180	9999	9999
9999	9999						
9999	9999	9999	184	184	184	190	190
190	176	176	172	185	186	190	190
190	192	192	192	191	190	190	184
190	180	180	180	170	172	172	169
9999	9999						
9999	9999	9999	182	182	182	186	186
182	130	172	172	180	176	184	188
180	130	130	190	190	185	182	180
180	172	172	169	171	170	170	167
9999	9999						
9999	9999	167	173	180	180	184	184
184	184	178	174	176	178	180	183
184	184	184	187	182	183	179	177
173	174	168	171	170	169	166	9999

WELL	33	32	0	210	9999	1.	240.	0	0	-1	-1
WELL	33	33	0	150	9999	1.	240.	0	1	-1	-1
WELL	34	34	0	210	9999	1.	240.	0	0	-1	-1
WELL	35	35	0	150	9999	1.	240.	0	1	-1	-1
WELL	36	36	0	210	9999	1.	240.	0	0	-1	-1
WELL	37	37	0	150	9999	1.	240.	0	1	-1	-1
WELL	38	38	0	210	9999	1.	240.	0	0	-1	-1
WELL	39	39	0	150	9999	1.	240.	0	1	-1	-1

VITA²

Syed Abul Hossain

Candidate for the Degree of
Master of Science

Thesis: APPLICATION OF NUMERICAL MODEL FOR GROUND-WATER
MANAGEMENT OF PIEDMONT AQUIFER IN CENTRAL
DINAJPUR, BANGLADESH

Major Field: Geology

Biographical:

Personal Data: Born in Bangladesh, March 1, 1937,
the son of Mr. Syed Kayem Ali.

Education: Graduated in Intermediate of Science
from Dacca Government College in 1957; received
Bachelor of Science in 1959 and Master of Science
in 1961, from University of Dacca, Dacca,
Bangladesh, with a major in Geology; completed
requirements for the Master of Science degree
at Oklanoma State University in July, 1981.

Professional Experience: Geologist, Groundwater
Circle, Bangladesh Water Development Board,
1961-67, and Deputy Director, 1967-79; attended
groundwater group training course in Tokyo, Japan
in 1973; graduate research assistant, Oklahoma
State University, Department of Geology, 1980-81.