

**SIMULATION AND 3D ANIMATION OF
A SIX-DEGREE-OF-FREEDOM
MOTION BASE SYSTEM FOR
FLIGHT SIMULATORS**

By

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CHAPTER I

INTRODUCTION

This is part of an ongoing research project at OSU funded by Flight Safety International to design and analyze a digital motion base system.

A flight simulator is used to train pilots. The object is to fool them into thinking they are flying in a real aircraft without ever getting off the ground. With an accurate simulation training can take place in a very realistic environment, without danger to the pilot.

In some simulators the only indication to the pilot that the aircraft is in motion is through the visual display and the instruments [1]. But the acceleration cues felt by the pilot in flight also affect his response, so many simulators attempt to reproduce these cues by mounting the simulator cockpit on a moving motion base [1].

A moving-base flight simulator consists of a motion base which has an upper moving platform and a fixed lower platform. The upper platform is attached to the lower platform by hydraulic cylinders or actuators that extend and retract, making possible the motion of the simulator. The cockpit is mounted on top of the moving upper platform.

Since the simulator is driven by cylinders that have constrained movement, it is confined to a fixed volume and is not able to move as much as the real aircraft [2]. This is the major difficulty of moving-base simulators [2]. To make this simulator effective we need to use this volume as best as possible.

Simulators are built with different degrees-of-freedom of movement of the motion base. The six-degree-of-freedom simulators have been adopted for most training simulators, although it has not been experimentally established why [1]. The motion base that was used has six cylinders. Therefore it has six-degrees-of-freedom and it can move in the directions of three mutually perpendicular axes and also rotate about these axes. The rotations are called roll (x axis), pitch (y axis) and yaw (z axis). A six-degree-of-freedom motion base is shown in Figure 1.1.

The points where the hydraulic cylinders attach to the platforms form an equilateral triangle in each platform as it can be seen in Figure 1.2. In this figure it is also shown how the axes described above are defined with respect to the simulator platform.

For the pilot to have the same sensations as if he were in the real aircraft a simulator attempts to produce the same accelerations as the real aircraft would produce in response to the pilot's commands [1].

To achieve these accelerations we designed a motion system consisting of the following blocks:

- primary motion
- special effects
- motion control
- servo

The primary motion block transforms the accelerations coming from the host computer, which has the main aircraft simulation, into accelerations of the motion base, taking into account its constraints of movement.

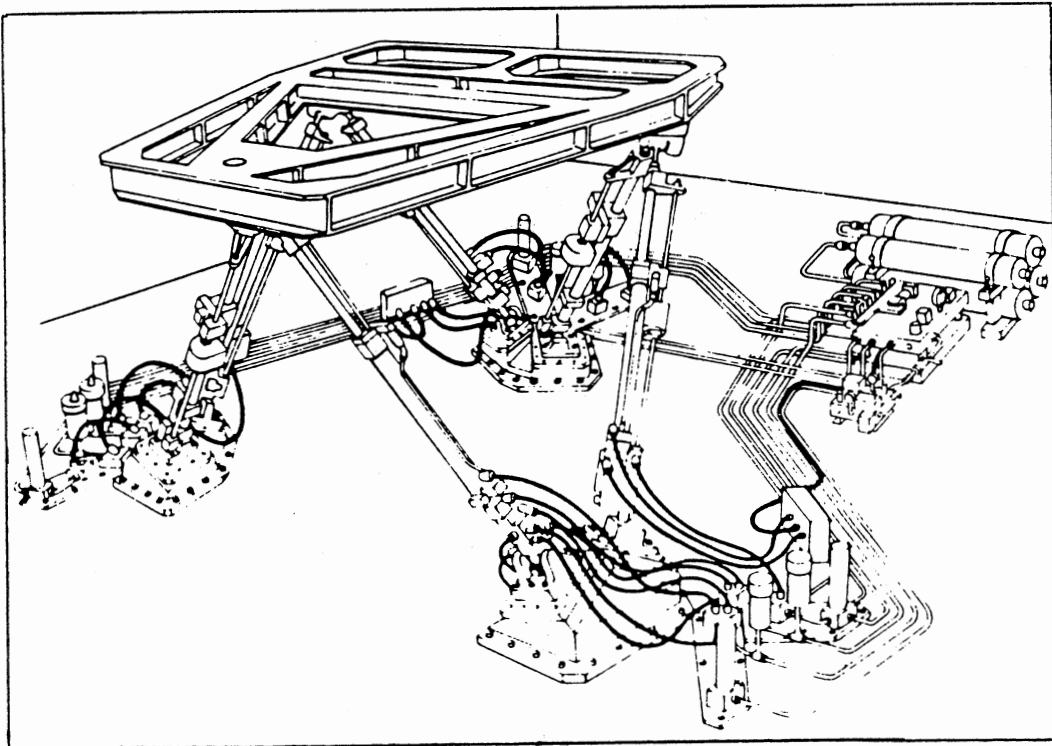


Figure 1.1. A Six Degree-of-Freedom Motion Base [1]

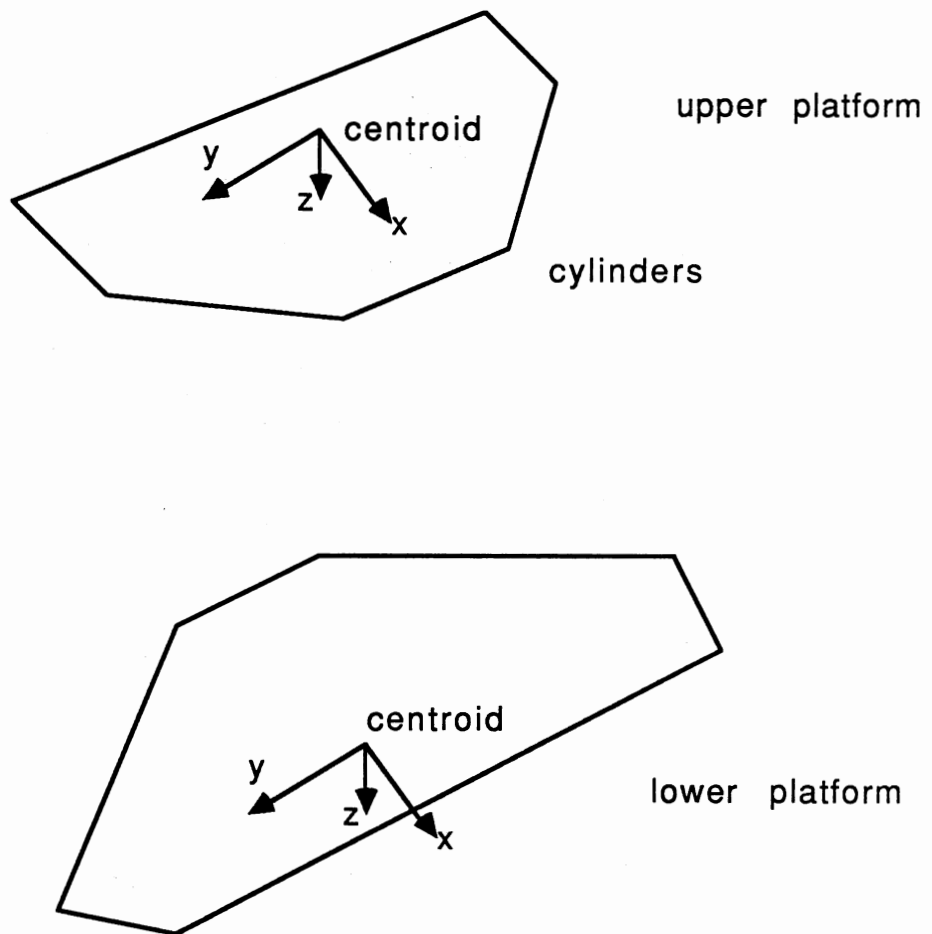


Figure 1.2. Definition of the Coordinate Systems

The special effects block creates additional accelerations which correspond to small disturbances that affect the aircraft, like runway bumps and landing gear movements.

The motion control block creates tests to be performed on the hydraulic cylinders, fades signals in and out on flight resets and crashes, brings the motion base to its neutral position, and also calibrates feedback position of the servo, given by position transducers, for better control. However, these functions of the motion control block do not need to be modeled. The parts of the motion control block that are of interest are the geometric transformation and the smoothing algorithm.

The geometric transformation, part of the motion control block, transforms upper platform positions and orientations into cylinder extensions. The smoothing algorithm prevents the cylinders from moving beyond their limits and also ensures that the cylinders reach their maximum extensions with zero acceleration.

The servo block takes the desired cylinder positions from the motion control block and attempts to move the cylinders smoothly to these positions.

The system operates with the host computer reading the pilot's commands given through controls such as the wheel, pedals and throttle. The host computer contains the flight simulation program, which produces aircraft attitudes, rates and accelerations. The host sends accelerations and rates to the primary motion block and flags to the special effects block. The special effects and primary motion, each independently, calculate a position and an angular orientation for the upper platform. The outputs of the special effects and the primary

motion are summed, filtered and transformed into cylinder extensions in the motion control block. The servo then commands the motion base with the desired cylinder extensions given by the motion control. A diagram of this system is shown in Figure 1.3.

A simulation of this motion system (MOTSIM) was developed in order to obtain a better understanding of the whole system, in order to be able to test the effects of various elements of the system on overall performance. With this simulation new designs can be tested without building hardware. This program will be used as a tool aiding engineers in the design of a motion base system for a flight simulator. The main object of this thesis is to describe the motion system simulation (MOTSIM).

To simulate the motion system it is necessary to simulate each of the blocks represented in Figure 1.3. A diagram of the simulated system (MOTSIM) is shown in Figure 1.4. Here we have almost the same diagram as Figure 1.3, except that the motion base is replaced by the valve/cylinder combination and the motion control block by the geometric transformation and smoothing algorithm block (the simulated functions of the motion control block). In addition, an inverse geometric transformation is performed to obtain true platform position and orientation from true cylinder lengths (as opposed to desired cylinder lengths).

In Chapter II the primary motion block is defined. In Chapter III the special effects are described, and a procedure for simulating them is developed. In Chapter IV the geometric transformation and the smoothing algorithm, which make up the motion control block, are discussed.

Chapter V explains the operation of the servo. Chapter VI discusses the simulation of the valve/cylinder combination. In Chapter VII the inverse geometric transformation is analyzed. Chapter VIII is a summary of the entire simulation. It explains how the various blocks interact with each other. A conclusion and suggestions for further improvements are presented in the final chapter.

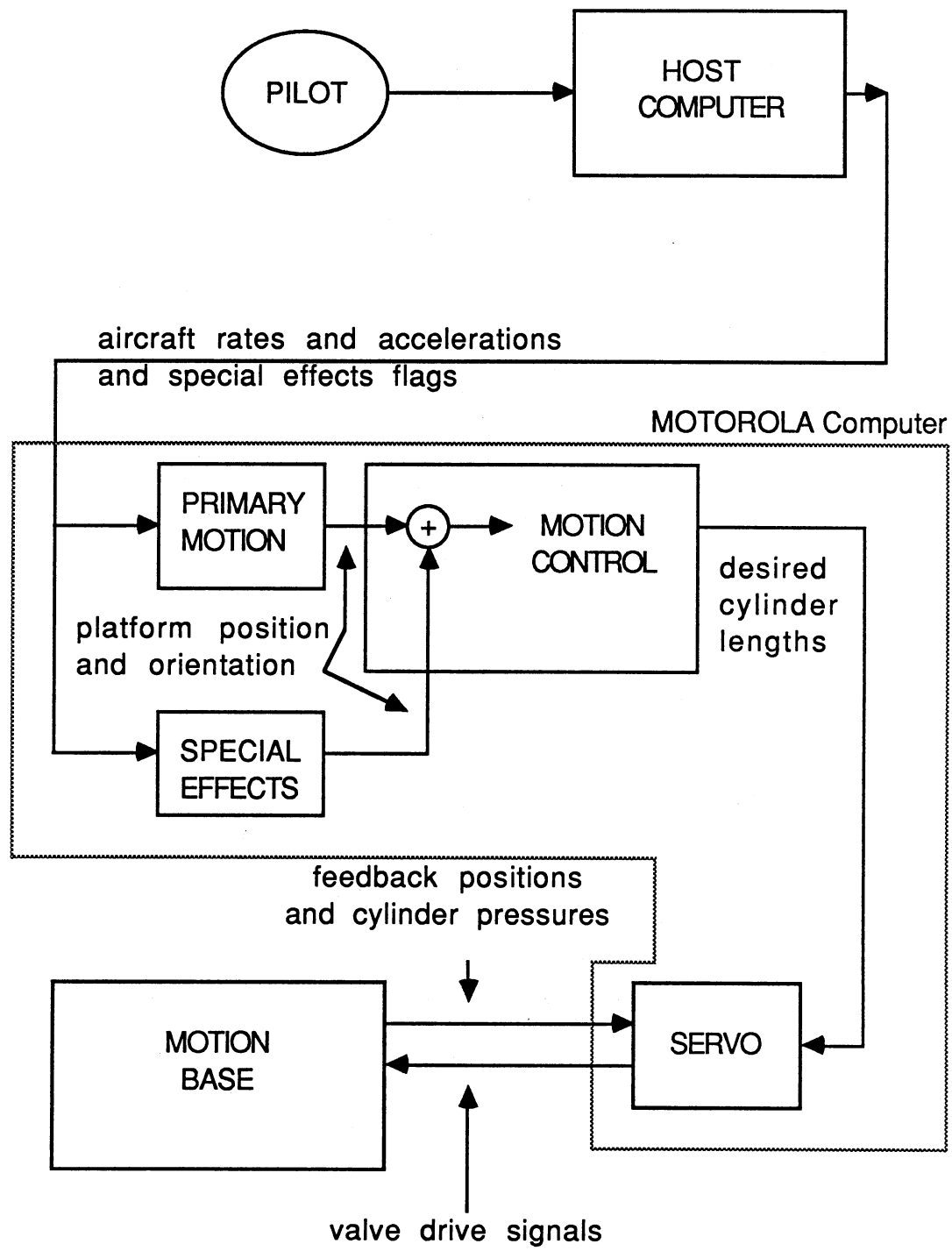
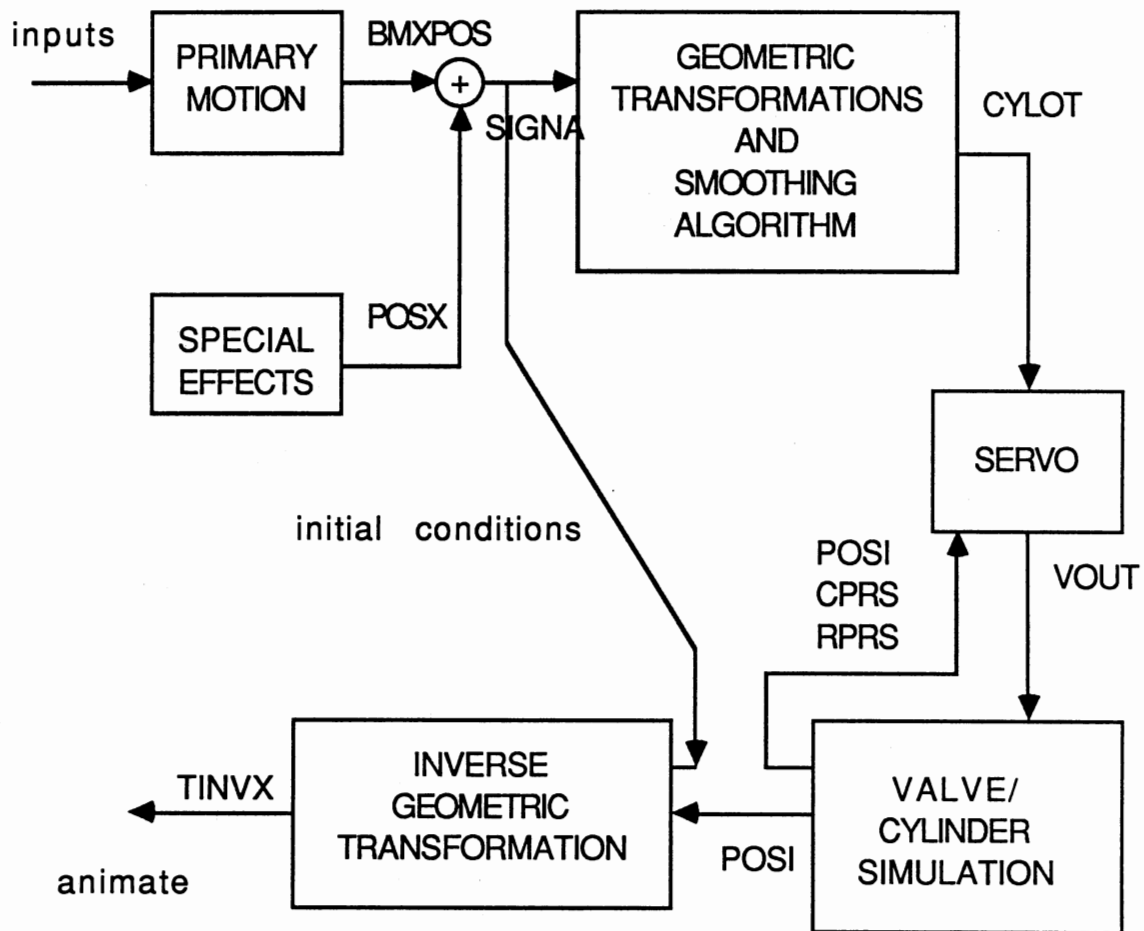


Figure 1.3. Digital Motion Base System



- BMXPOS - position and angles of orientation of centroid of upper platform
- POSX - position and angles of orientation of centroid of upper platform
- $SIGNA = BMXPOS + POSX$
- CYLOT - desired cylinder extensions
- POSI - actual cylinder extensions
- CPRS - cap pressure
- RPRS - rod pressure
- VOUT - voltage to drive valves
- TINVX - position and angles of orientation of centroid of upper platform

Figure 1.4 Diagram of Simulated System

CHAPTER II

PRIMARY MOTION

As was seen in Chapter I the output of the main aircraft simulation consists of signals representing its acceleration and attitude. These signals must be converted to platform positions in order to drive the motion platform. An acceptable perception of the real aircraft's motion must be preserved. There is not a one-to-one relationship since the motion platform is limited in movement and the real aircraft is not [1].

The primary motion is the block that transforms the aircraft accelerations into motion base accelerations and positions. It is composed of a coordinate transformation, a washout, and a gravity alignment as shown in Figure 2.1.

The coordinate transformation transforms accelerations from the aircraft axes to the moving motion-base axes [1]. The host computer generally computes the aircraft accelerations in a vehicle-based axis system. However, the motion platform has an earth-based system. Therefore, the coordinate transformation is required to determine the accelerations in this earth-based axes system [1]. So, the outputs of the coordinate transformation are motion platform accelerations.

Next, the motion platform accelerations go through the washout algorithm. The washout is mainly a high-pass filter so it excludes undesired low frequency signals from motion base input [3]. Low

frequency signals or constant inputs require a large movement of the motion base which might exceed the cylinder's travel limits. The washout is used to limit the movement of the motion base while best reproducing the accelerations of the simulated aircraft [1].

Gravity alignment is used to simulate the constant inputs or sustained accelerations [3]. There is a reorientation of the pilot with respect to gravity. This can be simulated by pitch and roll of the motion base platform. But these angles should be small enough so as not to reproduce a significant z component [4].

After aircraft accelerations are transformed into motion-base accelerations, motion-base positions need to be obtained. To transform the accelerations into positions a double-integration is performed. This is necessary since the inputs to the geometric transformation are the position and angular orientation of the moving platform, which drive the motion base. These inputs are the primary motion output added with the special effects output.

The position of the moving platform obtained from simulated aircraft accelerations is added to the position of the moving platform given by the special effects and is transformed into cylinder extensions by the geometric transformation described later in Chapter IV.

Emphasis on special effects will be given in the next chapter.

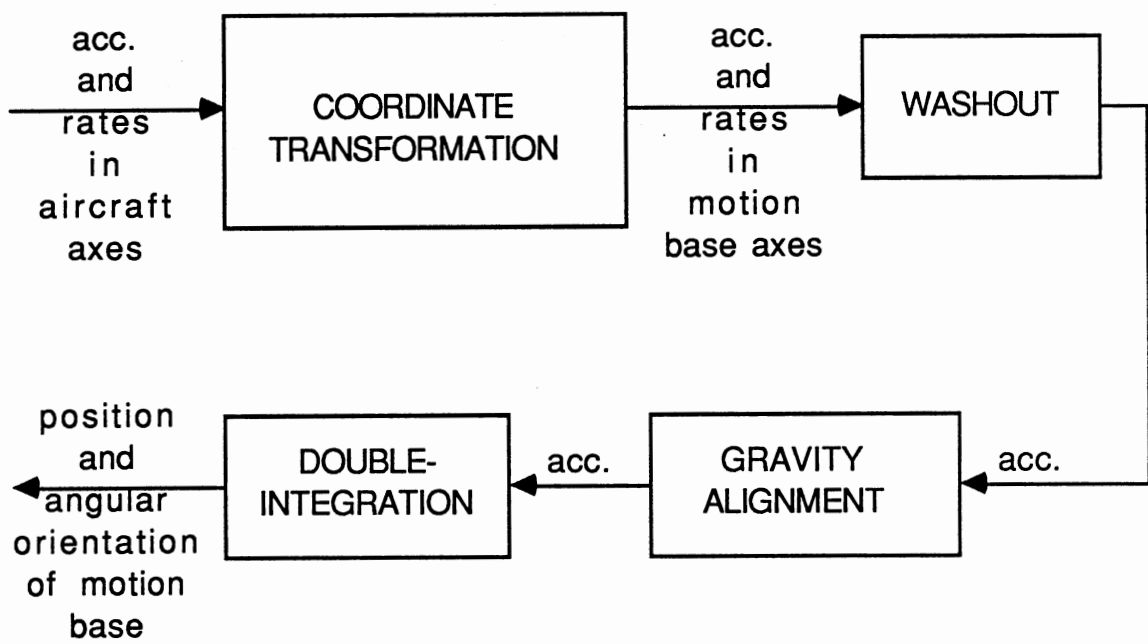


Figure 2.1. Primary Motion Block Diagram

CHAPTER III

SPECIAL EFFECTS

Special effects are any disturbances affecting the aircraft which are not caused by movement of the pilots controls. They range from simple bumps caused by cracks on the runway to turbulence vibrations. They are usually put into three categories: 1) bumps, 2) vibrations and 3) those effects that register on the instruments (turbulence and surge). There are many kinds of special effects and they are different for each aircraft in number and type.

Special effects vary depending on the type of aircraft being simulated and little documentation is available. The design of this package of subroutines was based on many discussions with personnel experienced in the simulation of special effects.

A traditional approach to create a special effect is empirical in nature. They are created on a trial and error basis which uses the subjective opinion of the pilot to reach an acceptable perception. This package will help in the design of special effects.

Special effects were all created with a small number of analog signal generators, making it difficult to achieve the complexity of the special effect being created. Currently sine wave generators with adjustable frequency and amplitude are used. In the digital implementation the number of generators that can be used for each special effect created is large. This gives more flexibility in tuning special effects.

The most complex special effect is turbulence because of its randomness and dependence on altitude and velocity of the aircraft, and also because it affects the readings on the instruments. A lot of research has been done on turbulence, but because of its complexity, it was not implemented in this project. Later it should be incorporated for improvements.

Another type of special effect is vibration, such as runway rumble and buffets. This is the type studied and implemented here. Vibrations are created by a combination of different generators, now digital generators, whose parameters can be changed quite easily.

The generators used here are of three kind: sine wave, first order filtered white noise and second order filtered white noise. As many as twelve generators can be combined together in any way to produce one special effect. Also, a combination of different special effects can be chosen to run simultaneously.

The special effects section of the motion base system simulation consists of two parts: set up and implementation. This chapter will describe the set up section first, then the implementation section.

Set Up Section

The structured diagram for the set up section of the special effects package is shown in Figure 3.1. It is menu driven, making it very easy to use. Next a description of each subroutine used in the package is given. The flowcharts of these subroutines can be found in Appendix A.

ADDSE: this subroutine is used to add special effects. It is mainly a menu that calls other specific subroutines as shown in Figure A.1.

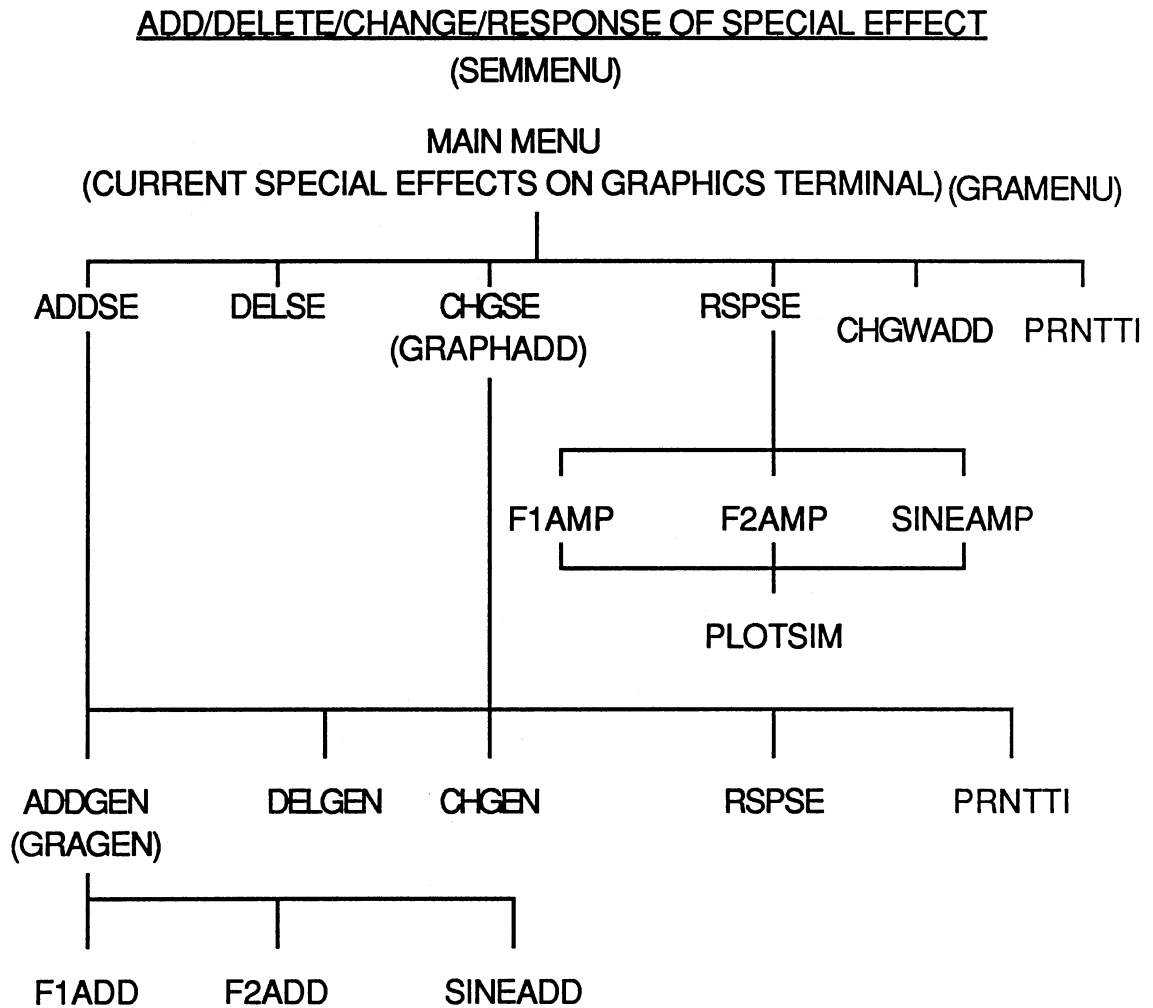


Figure 3.1. Special Effects Subroutine Simplified Diagram

DELSE: this subroutine deletes any unwanted special effects. Its flowchart is seen in Figure A.2.

CHGSE: this subroutine changes the specified special effect by adding generators, deleting generators, changing parameters of a generator and checking its response. Its flowchart is shown in Figure A.3.

GRAPHADD: this subroutine was written for the graphics terminal to show the type of generators that can be used to create a special effect.

RSPSE: this subroutine checks the special effect by plotting its response. Its flowchart is in Figure A.4. To calculate the response four other subroutines were called, they are:

E1AMP: calculates the first order filtered white noise. It is simply a first order filter with white noise input. In Figure A.5 the flowchart for the first order filtered white noise generator is shown. It calculates:

$$\begin{aligned}
 U &= (X-0.5)*V + M \\
 X_1 &= e^{-DT*2\pi*BW} *X_1 + [1- e^{-DT*2\pi*BW}]*U \\
 Y &= X_1
 \end{aligned}
 \tag{3.1}$$

where: Y - amplitude of generator

X₁ - state variable

DT - sampling interval

BW - bandwidth of filter (Hz)

U - uniformly distributed white noise with mean M and variance V [5].

X - seed for the random number generator

F2AMP: calculates the second order filtered white noise. It is simply a second order filter with white noise input. In Figure A.7 the basic flowchart for the second order filtered white noise generator is shown. Two sets of equations are used since the damping ratio (ξ) of the second order filter is between 0 and 1. The value of the conditional frequency $\left(\omega = BW * \sqrt{1 - \xi^2} \right)$ [6], where BW is the bandwidth of the filter, determines which set of equations is used. These equations are shown in Figure A.6 and they form the matrix AD and BD such that:

$$X = AD * X + BD * U \quad (3.2)$$

where: X - state vector variable = $[X_1 \ X_2]^T$

U - white noise defined as above

And the amplitude of the filter is given by: $Y = X_1$.

SINEAMP: calculates the amplitude of the sine wave. In Figure A.5 the flowchart for the sine wave generator is shown. It calculates:

$$Y = A * \sin(2\pi f T) \quad (3.3)$$

where: Y - amplitude

A - maximum amplitude

f - specified frequency (Hz)

T - sampling interval

PLOTSIM: plots the values of the output on the graphics terminal.

CHGWADD: this subroutine changes the name of the special effect selected or changes where to add the special effect. The special effects can be added in each of the degrees-of-freedom discussed in Chapter I: x, y, z directions and angles roll, pitch and yaw. Its flowchart is shown in Figure A.8.

PRNTTI: is a subroutine written to get hardcopies of the graphics

terminal.

ADDGEN: this subroutine adds generators to the special effect being created or changed. Its flowchart is shown in Figure A.9.

GRAGEN: this subroutine was written for the graphics terminal and it displays the generators and the parameters of each generator for the special effect selected. Its flowchart is shown in Figure A.10.

DELGEN: this subroutine deletes unwanted generators created for the special effect selected. Its flowchart is shown in Figure A.3.

CHGEN: this subroutine changes the parameters of a chosen generator. Its flowchart is shown in Figure A.3.

F1ADD. F2ADD. SINEADD: these subroutines add a filtered white noise first order, filtered white noise second order and sine wave generator respectively to the special effect being created or changed. Their flowcharts are shown in Figure A.9 as part of the flowchart for the subroutine ADDGEN.

GRAMENU: this subroutine written for the graphics terminal shows the name of the special effects already created, if any, and where they are being added in the simulation. Its flowchart is shown in Figure A.11.

All of the above routines are called by a main menu called SEMMENU and they are all used to create and simulate a special effect. The variables used in these various subroutines are described in Table I. Below a better description of the arrays PSTO and PAR is made.

Initial condition vector PSTO is:

For sine wave: $PSTO(I) = 0$

For filtered white noise first order: $PSTO(I) = 10000.$

$PSTO(I+1) = 0.$

For filtered white noise second order: $PSTO(I) = 10000.$

$PSTO(I+1) = 0.$

$PSTO(I+2) = 0.$

Parameter vector PAR is:

For sine wave: $PAR(I) = \text{amplitude}$

$PAR(I+1) = \text{frequency}$

For filtered white noise first order: $PAR(I) = \text{mean}$

$PAR(I+1) = \text{variance}$

$PAR(I+2) = \text{bandwidth}$

For filtered white noise second order: $PAR(I) = \text{mean}$

$PAR(I+1) = \text{variance}$

$PAR(I+2) = \text{bandwidth}$

$PAR(I+3) = \text{damping}$

Implementation Section

The special effects created using this package will later be used in the simulation of the motion-base system (MOTSIM). The flowchart of the subroutine that implements the special effect block seen in Figure 1.4 is shown in Figure 3.2. The subroutine is called SMSPEF, and it calls the already described subroutines F1AMP, F2AMP and SINEAMP.

The output of this block, which is upper platform position and orientation, is added to the output of the previously described primary motion block and is input to the geometric transformation and smoothing algorithm block which will be described in the next chapter.

TABLE I
VARIABLES USED IN SPECIAL EFFECTS

Variable Name	Description	Type and Dimension	Units
NAME	name of special effect	character (20x1)	
IEFF	number of special effect currently in use	integer	
WADD	number indicating where to add the amplitude of the special effect given by index number 1. position x axis 2. position y axis 3. position z axis 4. pitch angle 5. roll angle 6. yaw angle	integer (20x1)	
KEEP	keeps number of the generators for a specified special effect (only used in CHANGE S.E.)	integer (1000x1)	
MAXKEEP	twice total number of generators used in specified special effect (only used in CHANGE S.E.)	integer	
MAXGEN	total number of generators	integer	
MAXPAR	total number of parameters	integer	
MAXPSTO	total number of initial conditions	integer	
NGEN	type of generator (1,2,3) 1. 1st order filter 2. 2nd order filter 3. sine wave	integer (240x1)	
SPECIAL	indicates number of special effect the generator (given by index number) belongs to	integer (240x1)	
PAR	parameters of all generators	real (1000x1)	

TABLE I (Continued)

Variable Name	Description	Type and Dimension	Units
PSTO	stores the variables needed for next calculations of amplitudes of the generators and initial conditions	real (1000x1)	
POSX	output of special effects in real time	real (6x1)	in
DTSPEF	sampling interval	real	sec
IEFFLG	if true the special effect is on and its amplitude should be calculated	flag ^a (20x1)	
IFLGEN	if true the generator is on and its amplitude should be calculated	flag ^a (240x1)	

^aflag is true if equal to -1 and false if equal to 0

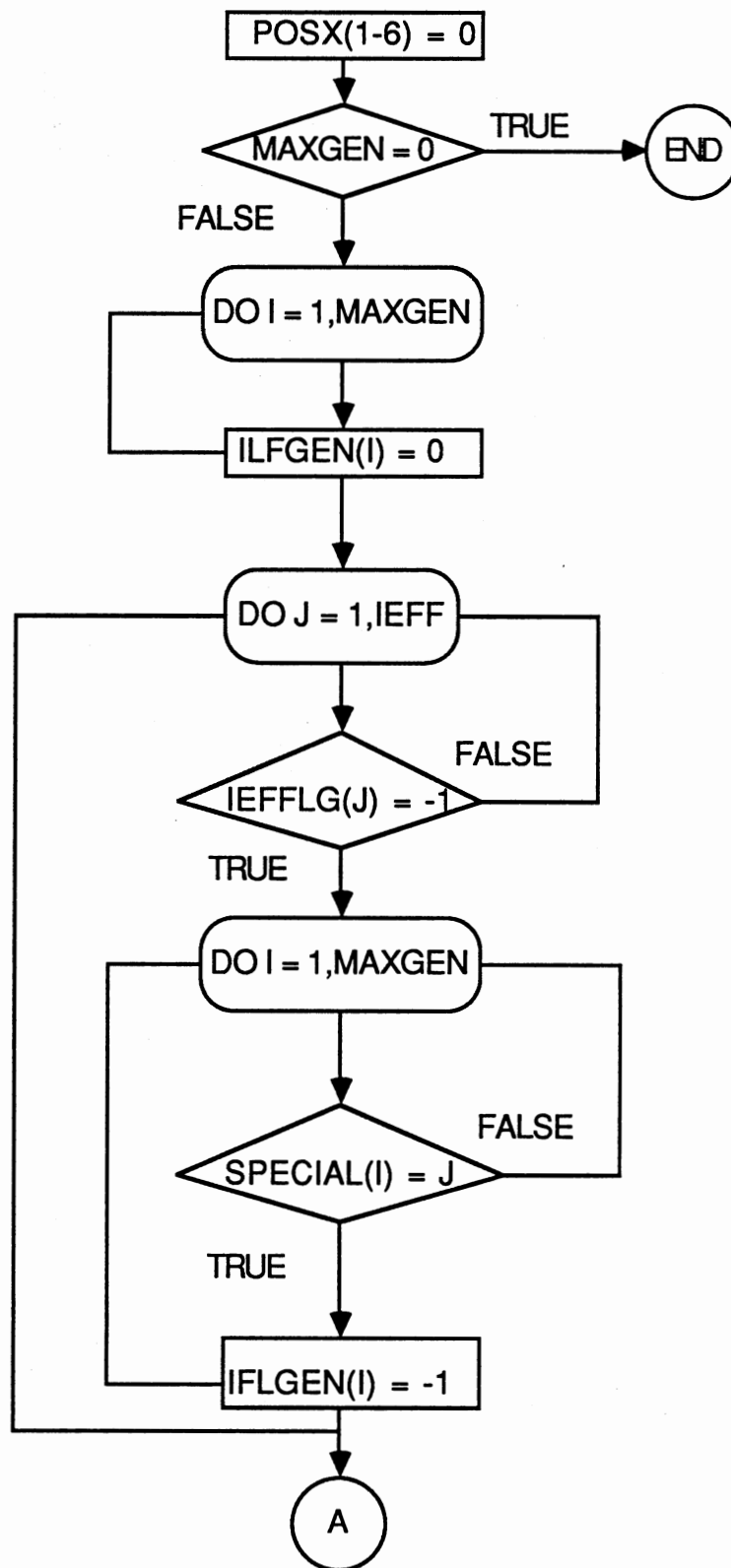


Figure 3.2. Flowchart for Subroutine SMSPEF

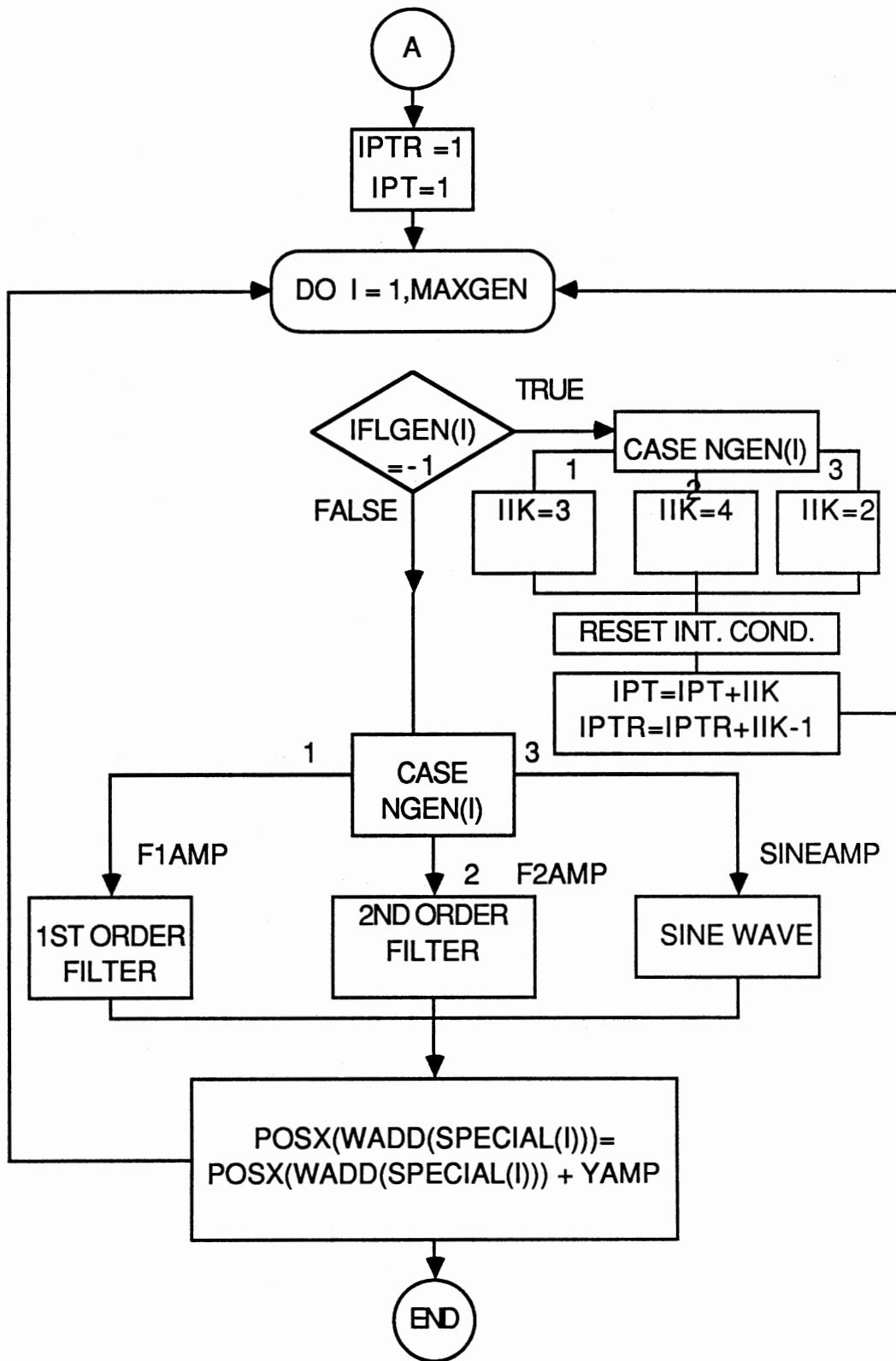


Figure 3.2. (Continued)

CHAPTER IV

GEOMETRIC TRANSFORMATION AND SMOOTHING ALGORITHM

The geometric transformation transforms the position and angular orientation of the upper platform into cylinder extensions, and the smoothing algorithm makes sure that the cylinders don't extend beyond their limits.

The geometric transformation is necessary since the motion base cannot be driven by the position and angular orientation of its center of gravity given by the aircraft simulation. It is driven by the actuators (cylinders) which from the combination of their extensions gives the position of the motion base [7].

The geometric transformation is based on the geometry of the motion base. Figure 4.1 shows the relationship between the centroid of each platform and the cylinder attachment point at each platform. The vectors are defined as:

z - from the centroid of the lower platform to the centroid of the upper platform

l_i - from cylinder i attachment point at the lower platform to cylinder i attachment point at the upper platform - cylinder i vector

B_i - from the centroid of the lower platform to cylinder i attachment point at the lower platform

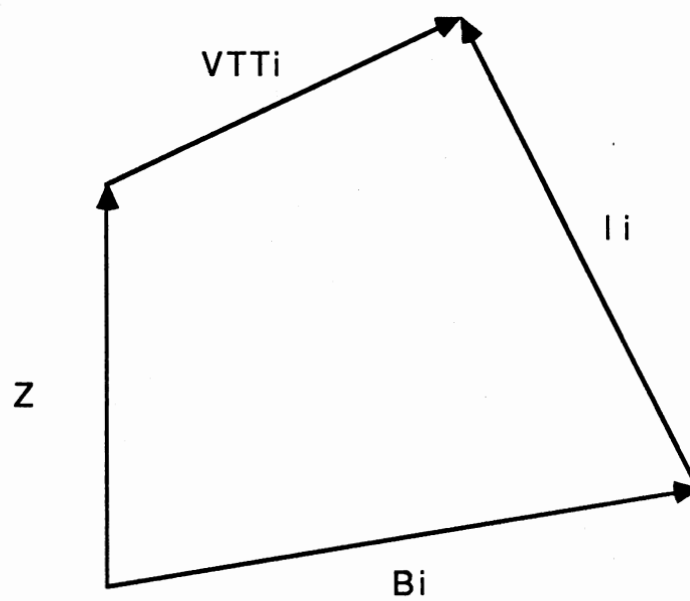


Figure 4.1. General Orientation Vector of Actuator i

VTT_i - from the centroid of the upper platform to cylinder i attachment point at the upper platform.

All coordinates are defined with respect to the lower platform coordinate system (defined in Chapter I Figure 1.2).

From Figure 4.1 the following vector equation is obtained:

$$I_i = VTT_i + Z - B_i \quad (4.1)$$

The vector VTT_i has its coordinates determined with respect to the lower platform coordinate system. The vectors given by special effects and primary motion are with respect to upper platform coordinate system. Therefore, a transformation must be performed in order to convert the vectors from the upper platform coordinate system to the lower platform coordinate system. This transformation is called an Euler angle transformation.

Let R be defined as the displacement vector of the upper platform and $A_{i,m}$ be defined as the vector going from the centroid of the upper platform to the i th cylinder attachment point at the upper platform.

The following equation results:

$$VT_i = R + A_{i,m} \quad (4.2)$$

which is the total displacement vector of the i th cylinder attachment point of cylinder i .

In order to define this vector in the coordinate system of the lower platform (VTT_i) the Euler angle transformation must be applied.

This is nothing more than a rotation of axes and the Euler's rotation matrix T is used. This transformation is defined as:

$$VTT_i = [T]^T VT_i \quad (4.3)$$

where vector VT_i is rotated by the movement of upper platform (pitch, roll and yaw angles). For more detail of this transformation see [7].

The order in which the given equations are calculated is:

1. $VT_i = R + A_{i,m}$
2. $VTT_i = [T]^T VT_i$
3. $l_i = VTT_i + Z - B_i$ (4.4)

And the cylinder extension is calculated as:

$$\|l_i\| = (l_i^T l_i)^{1/2} \quad (4.5)$$

Cylinder movement is limited to 18in extension or retraction (total cylinder length is 36in). Then, having the cylinder extensions, one must make sure that it was not overextended. This is the purpose of the smoothing algorithm. It is used as a safety device since the washout filter, in the primary motion block, should prevent the cylinders from hitting the end during normal maneuvers.

The smoothing algorithm input/output relationship (normalized) is shown in Figure 4.2. It is a linear relationship until the input reaches .83, after that it is a nonlinear (circular) relationship limiting the output to .9 of the maximum cylinder extension. This ensures that the cylinders stay within their limits.

The subroutine that simulates the geometric transformation and smoothing algorithm block is called GTRN2 and a simplified flowchart is shown in Figure 4.3. The variables used in the subroutine are described in Table II.

The output of this block - geometric transformation and smoothing algorithm - is input to the servo that commands the cylinder movement and stabilizes the system. A study of the servo is done in the next

chapter.

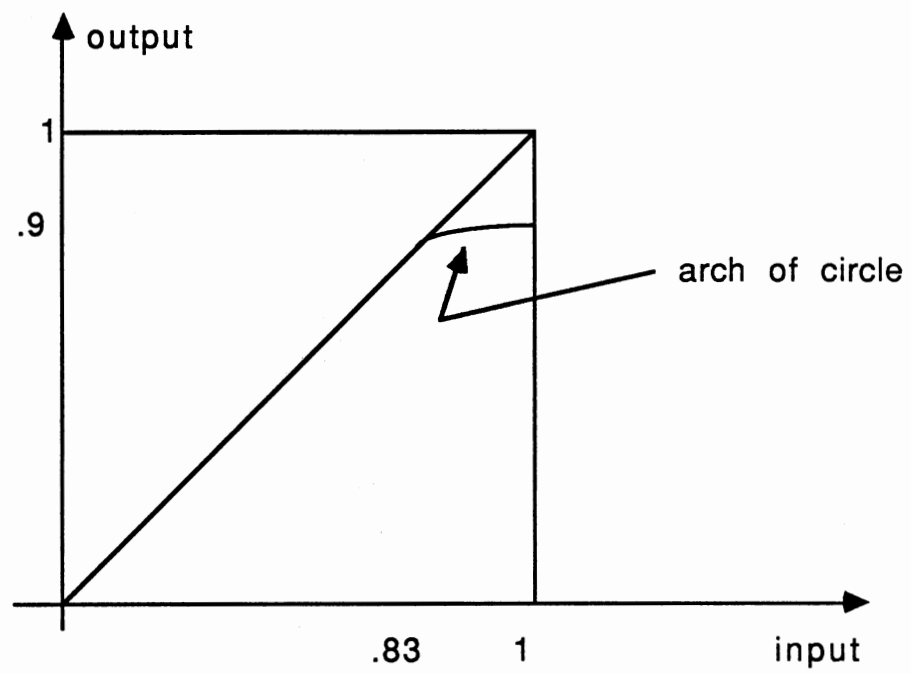


Figure 4.2. Input/Output Relationship of Smoothing Algorithm

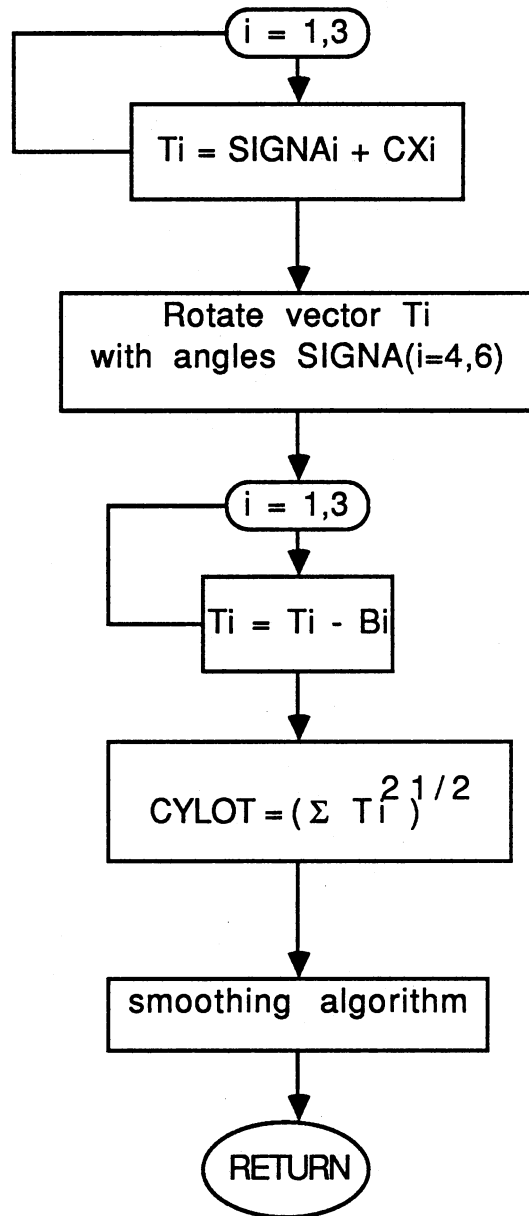


Figure 4.3. Flowchart of Subroutine GTRN2

TABLE II
 VARIABLES USED IN GEOMETRIC TRANSFORMATION
 AND SMOOTHING ALGORITHM

Variable Name	Description	Type and Dimension	Units
SIGNA	position and angle of orientation of upper platform	real (6x1)	in,rad
CYLOT	cylinder extension	real (6x1)	in
CX	x direction component of upper platform attachment point	real (6x1)	in
CY	y direction component of upper platform attachment point	real (6x1)	in
BX	x direction component of lower platform attachment point	real (6x1)	in
BY	y direction component of lower platform attachment point	real (6x1)	in
BZ	height difference between upper and lower platform	real	in

CHAPTER V

SERVO

Servo, short for servomechanism, is a feedback control system [8]. It is the controller of the model, making it stable while increasing response and accuracy. Its operation depends upon the difference between the actual position of the object and the desired position. The servo acts to reduce this difference to zero and make the actual position equal to the desired position, so it is a model follower [9]. It is a device that moves an object while expending the smallest amount of energy [8].

In this study the object to be controlled is the piston of the hydraulic cylinder and the servo will track its position.

A servo is composed of [8]:

- error detector
- amplifiers
- compensation

The error detector measures the difference between the actual and desired positions. The amplifiers are used to better control the actual position. And the compensation is used to stabilize the system if cannot be stabilized by position feedback alone [6]. Usually mechanical systems become unstable because of resonances in the mechanical linkages [8].

A block diagram of the servo is shown in Figure 5.1. The feedback is composed of position feedback and compensation. If position

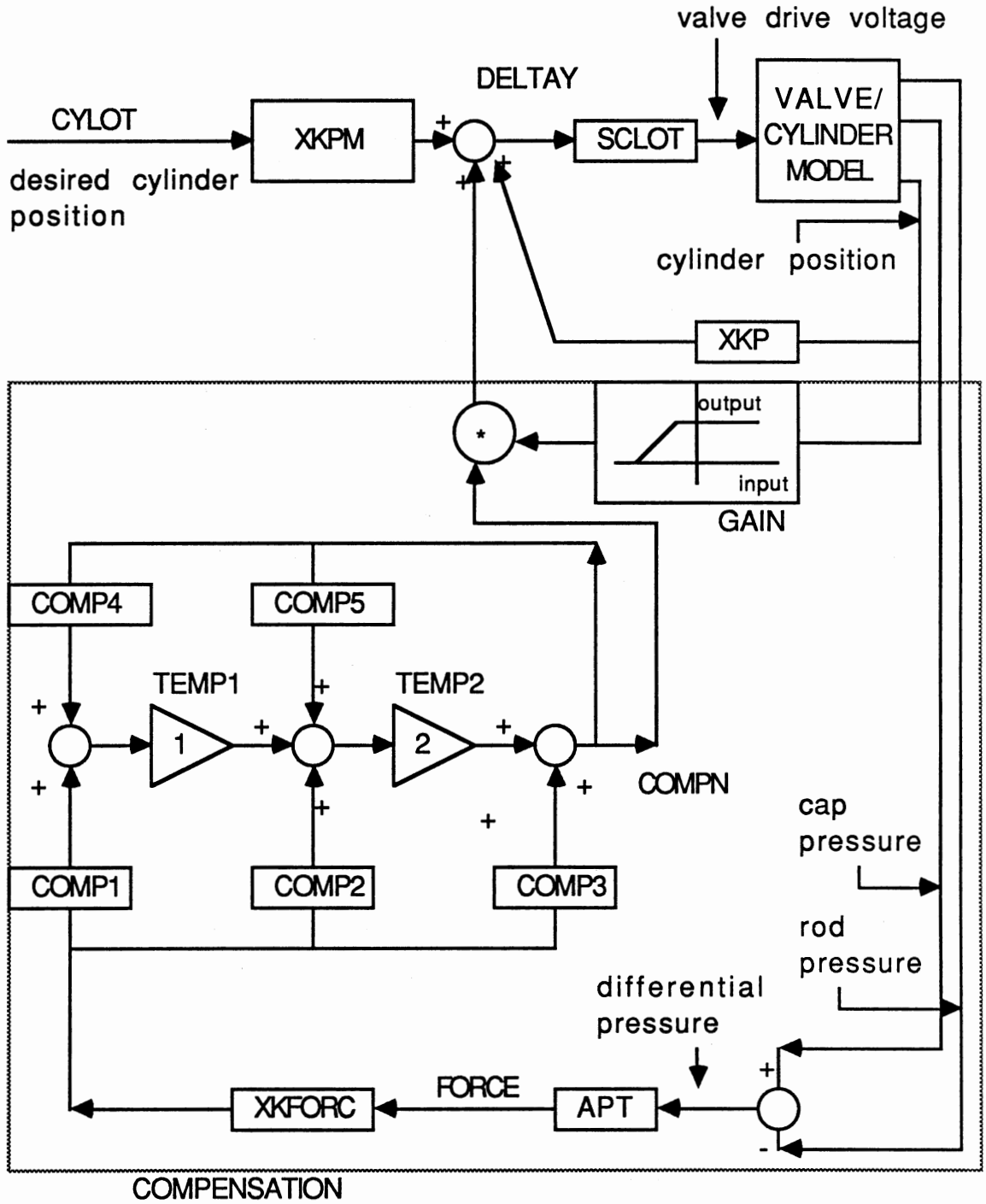


Figure 5.1. Servo Block Diagram

feedback alone is used and the gains are made high enough so that the servo will track the desired position the system becomes unstable because of resonances of the motion base. So the compensation is needed to make the system stable.

The compensation consists of pressure feedback. The pressure feedback is an approximate measure of the acceleration of the piston, which is the main compensation element. It goes through a second-order filter and is multiplied by a gain which is determined by piston position. This gain is necessary since the compensation is taken out when the piston is at the cushion, i.e., when the piston is totally retracted. When the cylinders are totally retracted the pressures measured do not represent acceleration of the piston, so if pressure feedback is used it will give an undesired output. The gain is determined by element GAIN in the servo block diagram, Figure 5.1.

The flowchart for the servo subroutine is shown in Figure 5.2. The description of the variables used in the subroutine are in Table III.

As can be seen from the servo block diagram, Figure 5.1, the output of the servo (which is the voltage to the valve that drives the cylinders) is input to the valve/cylinder model. Position and pressures obtained from the valve/cylinder model are input to the servo as feedback elements (compensation).

In the next chapter an analysis of the valve/cylinder model is made.

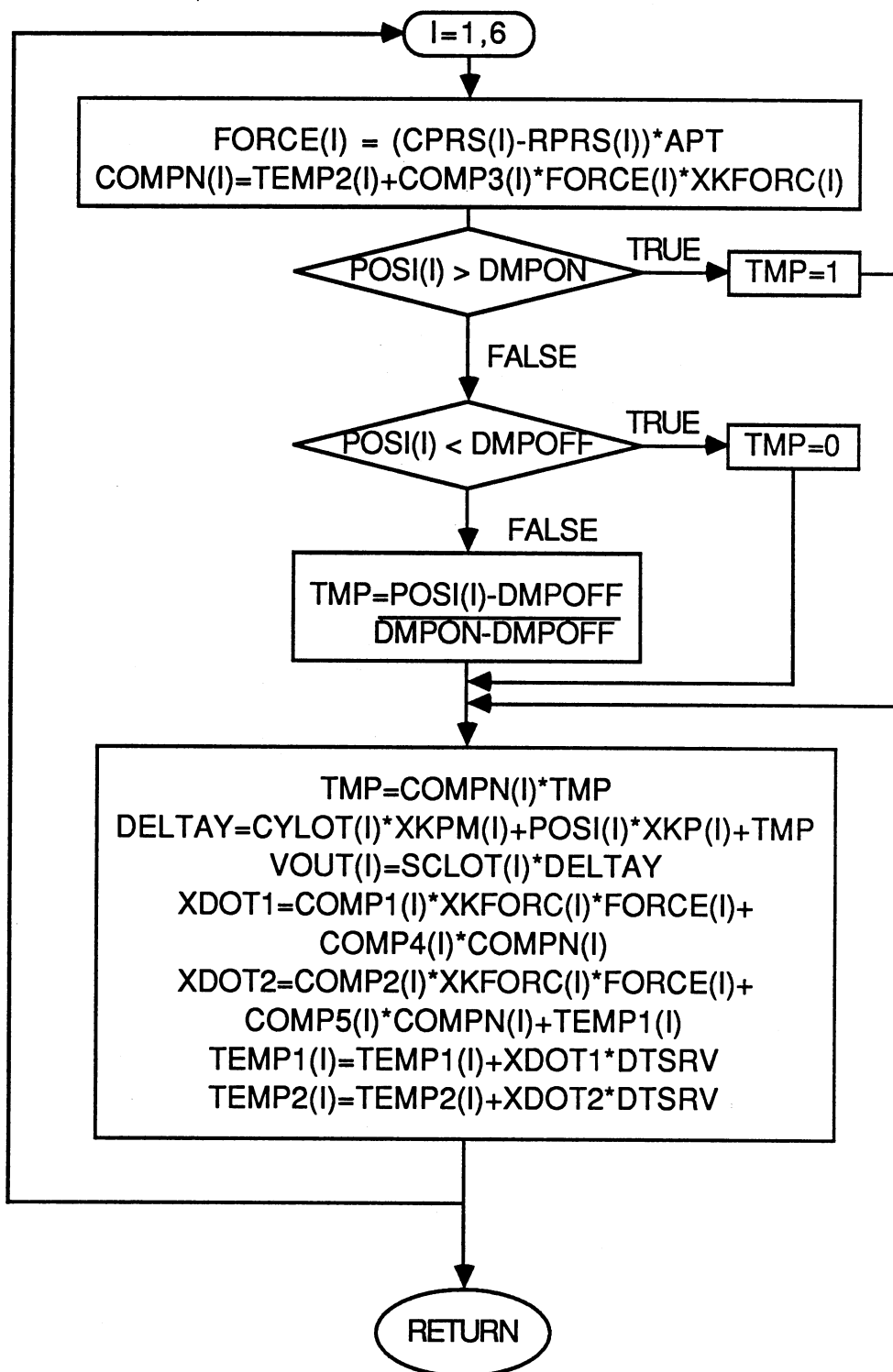


Figure 5.2. Flowchart of Subroutine SMSRV

TABLE III
VARIABLES USED IN SERVO

Variable Name	Description	Type and Dimension	Units
XKPM	desired position gain	real (6x1)	
XKP	actual (feedback) position gain	real (6x1)	
SCLOT	scale for valve voltage	real (6x1)	mV/in
XKFORC	differential pressure gain	real (6x1)	lb/psi
COMP1	compensation gain #1	real (6x1)	
COMP2	compensation gain #2	real (6x1)	
COMP3	compensation gain #3	real (6x1)	
COMP4	compensation gain #4	real (6x1)	
COMP5	compensation gain #5	real (6x1)	
DMPON	higher damping fade limit	real	in
DMPOFF	lower damping fade limit	real	in
FORCE	differential force	real (6x1)	lb
TEMP1	storage variable for integration initial condition of compensation	real (6x1)	
TEMP2	storage variable for integration initial condition of compensation	real (6x1)	
APT	area of piston	real	in ²
VOU	input current to drive valve	real (6x1)	mA
CPRS	cap pressure	real (6x1)	psi
RPRS	rod pressure	real (6x1)	psi
DTSRV	sampling interval	real	sec

CHAPTER VI

VALVE/CYLINDER MODEL

The valve is commanded by the servo, which was described in the previous chapter, and measurements are transferred to the servo as feedback elements for compensation. Now a closer look at how the valve/cylinder model is made.

The valve/cylinder combination is a hydraulic system which is composed of the following: hydraulic fluids with a reservoir, valves, and an actuator (piston) to convert hydraulic energy into mechanical energy [10]. Ogata [10] explains many types of hydraulic systems, their equations and how they work.

The valves are used to control the direction of the fluid flow [10]. They are classified by types and by the number of ways that the flow can enter and leave the valve [10]. Having this in mind, the valve used is a sliding-spool four-way valve. The equations for the movement of the valve are nonlinear. The valve is assumed to be zero-lapped, i.e., there is no overlap when the port and the spool are aligned, so the area of the port is given by $A = k \cdot x$ (x -spool displacement) as shown in Figure 6.1. The movement of the spool causes a flow through the valve orifices (see Figure 6.3).

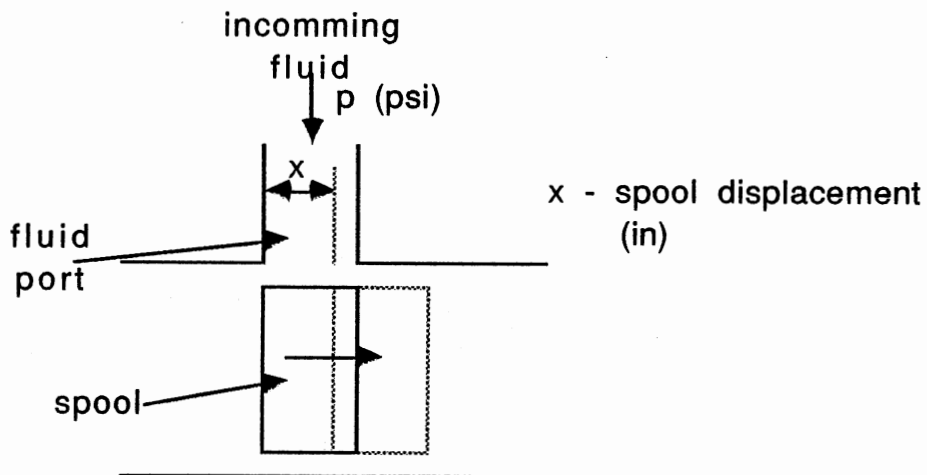


Figure 6.1. Spool Movement

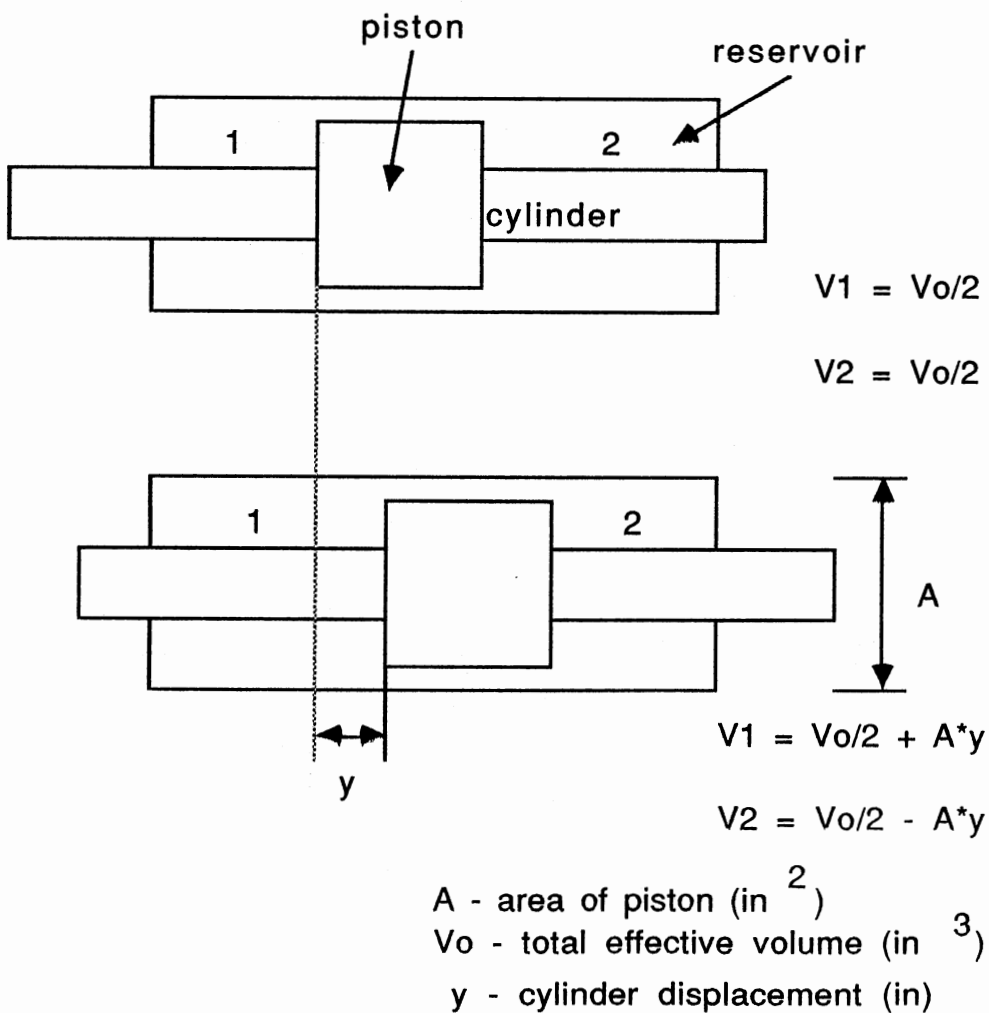


Figure 6.2. Piston Movement

These flows can be calculated by [10]:

$$\begin{aligned} \text{orifice 1: } Q_1 &= cA\sqrt{(2g/\gamma)(p_s-p_1)} = ck\sqrt{2g/\gamma}\sqrt{p_s-p_1} x = C\sqrt{p_s-p_1} x \\ \text{orifice 2: } Q_2 &= cA\sqrt{(2g/\gamma)(p_2-p_r)} = ck\sqrt{2g/\gamma}\sqrt{p_2-p_r} x = C\sqrt{p_2-p_r} x \end{aligned} \quad (6.1)$$

where: k - proportional area constant

x - spool displacement

p_1 - cap pressure

p_2 - rod pressure

p_s - supply pressure

p_r - return pressure

g - gravity

$\gamma = g \cdot \rho$ - specific weight of oil

ρ - mass density

c - discharge coefficient

$$C = ck \sqrt{2g/\gamma} \quad (\text{see Appendix B})$$

The flow of the hydraulic fluid into reservoir 1 compresses the hydraulic fluid in reservoir 1 (Figure 6.2). The compressibility is determined by the bulk modulus of the fluid [10]. As the fluid is compressed, the pressure increases which gives the compressibility flow as:

$$\frac{dV}{dt} = \frac{-V}{\beta} \frac{dp}{dt} \quad (6.2)$$

where: p - pressure

V - volume

β - bulk modulus, which is defined as:

$$\beta = \frac{dp}{-dV/V} \quad (6.3)$$

The change in pressure creates a force which causes the piston to move. The change in volume is expressed by $V_1 = V_0/2 + A*y$ and $V_2 = V_0/2 - A*y$ where A - area of piston, y - displacement of piston and V_0 - total effective volume. This is shown in Figure 6.2.

Because of imperfect fabrication of the cylinders some leakage of the oil occurs (Q_3 , Q_4 and Q_5 in Figure 6.3). The leakage is proportional to the pressures of the two parts involved, so the leakage flow is defined as:

$$Q_L = L*\Delta p \quad (6.4)$$

where: L - leakage proportional constant

Δp - differential pressure

When the piston moves an additional flow of $A*v$ (area of piston * velocity of piston) is created as if it were flowing from side 1 to side 2 (see Figure 6.3). The total flow in each side of the cylinder will be:

$$\begin{aligned} \text{in} &= \text{out} \\ \text{side 1: } Q_1 &= Q_3 + Q_4 + Q_6 + A*v \\ \text{side 2: } Q_3 + A*v &= Q_2 + Q_5 + Q_7 \end{aligned} \quad (6.5)$$

The equation characterizing the piston's movement comes from Newton's Law: $F = ma$. These equations are shown in Figure 6.4. The state variable representation of the system [11] is:

$$w' = A*w + B \quad (6.6)$$

where: $w' = dw/dt$

$$w = [y_1 \ y'_1 \ y_2 \ y'_2]^T$$

$$w' = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -\frac{K}{M_1} & -\frac{B}{M_1} & \frac{K}{M_1} & \frac{B}{M_1} \\ 0 & 0 & 0 & 1 \\ \frac{K}{M_2} & \frac{B}{M_2} & -\frac{K}{M_2} & -\frac{B}{M_2} \end{bmatrix} w + \begin{bmatrix} 0 \\ \frac{A}{M_1}(p_1 - p_2) \\ 0 \\ 0 \end{bmatrix} \quad (6.7)$$

The motor that moves the spool can also be mathematically modeled and linearized [6]. The motor equation is given in Figure 6.5. The state variable model representation of the motor system [11] is given by:

$$w' = dw/dt = A^*w + B^*u \quad (6.8)$$

where: $w = [x \ x']^T$

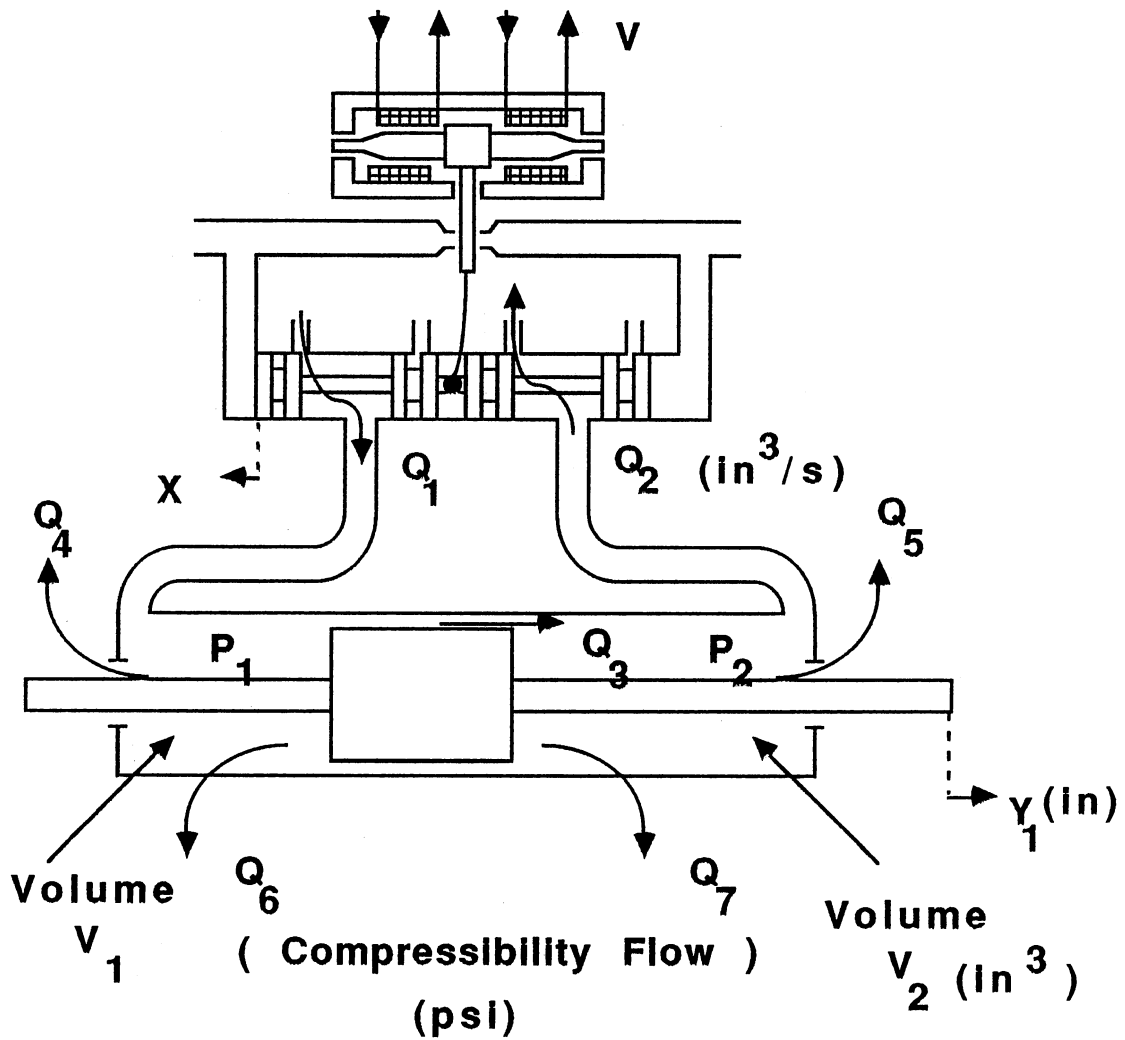
$$w' = \begin{bmatrix} 0 & 1 \\ -\omega_n^2 & -2\xi\omega_n \end{bmatrix} w + \begin{bmatrix} 0 \\ \frac{K_m \omega_n^2}{R} \end{bmatrix} V \quad (6.9)$$

In the MOTSIM program the differential equations are integrated numerically using Euler's method:

$$w(t+\Delta t) = w(t) + w'(t) \cdot \Delta t \quad (6.10)$$

where Δt is the integration interval.

Now that all of the equations necessary to simulate the valve/cylinder model are known, the order in which they shall be executed must be determined. The following paragraph explains how the order, in which the equations are calculated, was obtained. This order is also given in Figure 6.6 and the equations referred in the paragraph below are from that figure. Table IV relates the variables seen in Figure 6.6 to the variables used in the subroutine that simulates the valve/cylinder combination.



$$V_o = V_1 + V_2 \text{ (total effective volume) (in}^3\text{)}$$

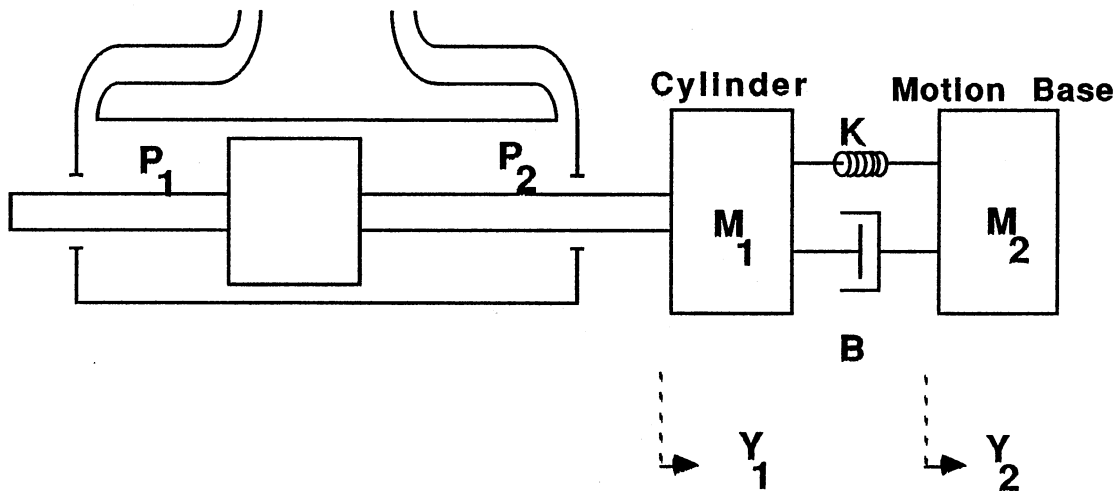
$$A = \text{APT} - \text{are of piston (in}^2\text{)}$$

β = BETAO - bulk modulus of fluid

P_1 = CPRS - cap pressure

P_2 = RPRS - rod pressure

Figure 6.3. Valve/Cylinder



$$M_1 \frac{d^2}{dt^2} y_1 = A(p_1 - p_2) - K(y_1 - y_2) - B \left(\frac{d}{dt} y_1 - \frac{d}{dt} y_2 \right)$$

$$M_2 \frac{d^2}{dt^2} y_2 = K(y_1 - y_2) + B \left(\frac{d}{dt} y_1 - \frac{d}{dt} y_2 \right)$$

M_1 - mass of cylinder (slugs)

M_2 - mass of motion base on each cylinder (slugs)

g - gravity ($=32.2 \text{ ft/s}^2$ or $32.2 \cdot 12 \text{ in/s}^2$)

So the given mass in pounds (lb) has to be divided by g to be in mass units (slugs), the program does this.

K - spring constant (lb/in)

B - damping coefficient (lb/(in/s))

y_1 - displacement of cylinder (in)

y_2 - displacement of motion base (in)

Figure 6.4. Newton's Law for the Piston

TORQUE MOTOR EQUATION

$$\frac{d^2}{dt^2} x + 2\xi\omega_n \frac{d}{dt} x + \omega_n^2 x = \frac{K_m \omega_n^2}{R} V$$

ξ = DAMPM – damping ratio

ω_n = 2 π BANDM – angular velocity

K_m = GAINM – gain (in/mA)

R = VRST – motor resistance (Ω)

V = VOUT – input voltage (mV)

x – output displacement (in)

Figure 6.5. Torque Motor Equation

The order in which the equations are executed is determined by the way the system operates. To drive the cylinders, a voltage is applied to the valve which moves the spool (equation 1). This opens the orifices 1 and 3 or 2 and 4 (see Figure 6.3) letting the fluid pass through the ports (equation 2). In addition to this flow, there is a leakage flow around the piston (equation 3). If orifices 1 and 3 are open $p_1 > p_2$, the piston moves forward. If orifices 2 and 4 are open $p_1 < p_2$, the piston moves backward. As was seen above the pressure difference causes the piston to move (equation 4). The flow into the cylinder creates a compressibility flow (equation 5) causing a change in pressures (equation 6). These are the steps used to simulate the valve/cylinder combination and the subroutine in which they are implemented is called SMVALVE. The variables used in the subroutine are described in Table V.

The servo block diagram (Figure 5.1) shows pressures and positions of the cylinders, derived from this block (valve/cylinder model block), being sent to the servo as feedback to stabilize the system.

To make sure that the actual cylinder lengths are correct, given the desired cylinder lengths (outputs of the geometric transformation), another transformation is used, the inverse geometric transformation. The inverse geometric transformation will be described in the next chapter.

① $\frac{d^2}{dt^2}X + 2\zeta\omega_n\frac{d}{dt}X + \omega_n^2X = K_m\omega_n^2i$ } Torque Motor Equation

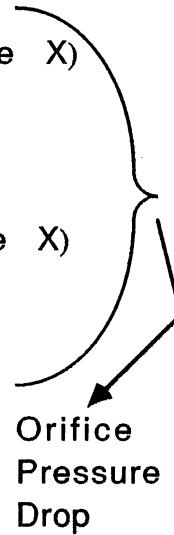
$Q_1 = cA_1\sqrt{\frac{2g}{\gamma}(p_s-p_1)} = C\sqrt{(p_s-p_1)} X$ (for positive X)

$Q_1 = C\sqrt{(p_1-p_r)} X$ (for negative X)

②

$Q_2 = cA_2\sqrt{\frac{2g}{\gamma}(p_2-p_r)} = C\sqrt{(p_2-p_r)} X$ (for positive X)

$Q_2 = C\sqrt{(p_s-p_2)} X$ (for negative X)



$Q_3 = L_1(p_1-p_2)$

$Q_4 = L_2(p_1-p_r)$

$Q_5 = L_3(p_2-p_r)$

③

Leakage Flow

④

Newton's Law for the Piston (See Figure 6.4)

$Q_6 = Q_1 - Q_3 - Q_4 - A\frac{d}{dt}Y_1$

⑤

$Q_7 = Q_2 - Q_5 + A\frac{d}{dt}Y_1$

$V_1 = V_0/2 + A \times Y_1$

$V_2 = V_0/2 - A \times Y_1$

Volumetric Flow

⑥

$\frac{V_1}{\beta} \frac{d}{dt}p_1 = Q_6$

$\frac{V_2}{\beta} \frac{d}{dt}p_2 = Q_7$

[p_1 and p_2 saturate at p_s (high) and p_r (low)]

Compressibility Flow

Figure 6.6. Valve/Cylinder Equations

TABLE IV
PROGRAM NAMES FOR VARIABLES
SEEN IN FIGURE 6.6

Variable Name in figure	Program Name
C	FRC
p_1	CPRS
p_2	RPRS
A	APT
y	PD
$\frac{dy}{dt}$	PDOT
β	BETAO
p_s	PS
p_r	PR
L_1	XL1
L_2	XL2
L_3	XL3
$Q\#$	Q#
$V\#$	V#
V_o	VO

TABLE V
VARIABLES USED IN VALVE/CYLINDER

Variable Name	Description	Type and Dimension	Units
MOTOR SPECIFICATIONS			
DAMPM	damping	real	
BANDM	bandwidth	real	Hz
GAINM	gain	real	in/mA
VRST	resistance	real	Ω
VALVE SPECIFICATIONS			
PS	supply pressure	real	psi
PR	return pressure	real	psi
XL1	leakage flow constant #1	real	$\text{in}^3/(\text{s} \cdot \text{psi})$
XL2	leakage flow constant #2	real	$\text{in}^3/(\text{s} \cdot \text{psi})$
XL3	leakage flow constant #3	real	$\text{in}^3/(\text{s} \cdot \text{psi})$
APT	area of piston	real	in^2
VO	total effective volume of cylinder	real	in^3
XLIMIT	limit of spool position	real	in
FRC	flow rate constant	real	see App. B
XM1	mass of cylinder	real	lb
OIL SPECIFICATIONS			
BETAO	bulk modulus	real	psi
MODEL OF MOTION BASE			
XM2	mass on top of each cylinder because of motion base	real (6x1)	lb
XK	spring const. for each cylinder	real (6x1)	lb/in
B	damping coeff. for each cylinder	real (6x1)	lb/(in/s)

TABLE V (Continued)

Variable Name	Description	Type and Dimension	Units
SIMULATION VARIABLES			
X	spool position	real (6x1)	in
XDOT	spool velocity	real (6x1)	in/s
VOUT	input current to drive valve	real (6x1)	mA
XMOTOR	continuous time motor matrix	real (2x3)	see eq. 6.9
Q1	orifice flow	real (6x1)	in ³ /s
Q2	orifice flow	real (6x1)	in ³ /s
Q3	leakage flow	real (6x1)	in ³ /s
Q4	leakage flow	real (6x1)	in ³ /s
Q5	leakage flow	real (6x1)	in ³ /s
Q6	compressibility flow	real (6x1)	in ³ /s
Q7	compressibility flow	real (6x1)	in ³ /s
CPRS	cap pressure	real (6x1)	psi
RPRS	rod pressure	real (6x1)	psi
PISTON	continuous time piston matrix	real (4x5)	see eq. 6.7
UIN	differential pressure	real (6x1)	psi
PD	piston displacement	real (6x1)	in
PDOT	piston velocity	real (6x1)	in/s
V1	volume on cap side	real (6x1)	in ³
V2	volume on rod side	real (6x1)	in ³
POSI	cylinder position	real (6x1)	in

CHAPTER VII

INVERSE GEOMETRIC TRANSFORMATION

The inverse geometric transformation is used to check the simulation. Its inputs are the actual cylinder extensions and the outputs are the positions and angular orientations of the upper platform. They are compared to the positions and angular orientations given as input to the geometric transformations (described in Chapter IV) to measure how well the system behaved [1].

The objective is then to find the actual positions and angles of orientation of the centroid of the upper platform of the motion base knowing only the six cylinder extensions given by potentiometers. So the root of the following equation must be found:

$$f(x) = 0 \quad (7.1)$$

where: f - vector formed by $f_i(x) = c_i^T(x) c_i(x) - m_i^2$

$c_i(x)$ - calculated cylinder position (3 dimensional vector)

m_i - measured cylinder lengths

x - positions and angles of orientation of the centroid of the upper platform (6 dimensional vector).

To find the root of equation 7.1 an iterative numerical method was applied. The first numerical method used was Newton-Raphson [12] whose iterative formula has the form:

$$x(n+1) = x(n) - J^{-1}f \quad (7.2)$$

where: J - Jacobian of f with respect to x

$$f - \text{vector formed by } f_i(x) = c_{l_i}^T(x) c_{l_i}(x) - m_{l_i}^2$$

x - positions and angles of orientation of the centroid of the upper platform (6 dimensional vector).

The Newton-Raphson method for iteration suggested by Dieudonne [7] gave a very slow convergence and problems occurred when the determinant of J was near zero. Since the algorithm depends on the inverse of J another algorithm is required. The Marquarot algorithm was chosen since the inverse matrix that it calculates always exists [13].

The iteration formula has the form:

$$x(n+1) = x(n) - [J^T J + \mu I]^{-1} J^T f \quad (7.3)$$

where: J - Jacobian of f with respect to x

$$f - \text{vector formed by } f_i(x) = c_{l_i}^T(x) c_{l_i}(x) - m_{l_i}^2$$

$c_{l_i}(x)$ - calculated cylinder position (3 dimensional vector)

m_{l_i} - measured cylinder lengths

x - positions and angles of orientation of the centroid of the upper platform (6 dimensional vector).

μ - adjustable constant

I - identity matrix.

This algorithm has a faster convergence and it certainly gives an inverse for the matrix in brackets (eq. 7.3) since the constant μ is adjustable.

With the appropriate initial conditions equation 7.3 is repeated until the criterion for convergence is met. Two criteria for convergence are used:

$$\begin{aligned}
 &1. \sum (J^T f)_i < \varepsilon \\
 &2. \sum [x(n+1) - x(n)]^2 < \text{TOL}
 \end{aligned}
 \tag{7.4}$$

where ε and TOL are tolerances defined by the user.

The Marquarot algorithm adjusts μ at each iteration. If the value of $\sum f_i^2(x(n+1))$ is less than $\sum f_i^2(x(n))$ then μ is decreased by some factor ($1/r$). Otherwise μ is increased by some factor (r). As μ gets small the algorithm approaches the Gauss-Newton method. As μ gets large the algorithm approaches the steepest descent method [13].

The detailed equations for the implementation of the inverse geometric transformation - IGT - can be found in [7]. The subroutine that implements IGT is called SMIGT and its flowchart is shown in Figure 7.1. The variables used in the subroutine are in Table VI.

The order of the positions and angles in array variables TINVX and TINVXI are different than those in array variables TINVXL and TINVXN so a rearrangement of the arrays is necessary in the beginning and end of the routine (see Table VII).

In the next chapter an analysis of the whole system, and the integration of the various subroutines described in the previous chapters is discussed.

TABLE VI
VARIABLES USED IN INVERSE
GEOMETRIC TRANSFORMATION

Variable Name	Description	Type and Dimension	Units
EPSILON	tolerance for convergence of MARQUAROT algorithm	real	
TOL	tolerance for change in TINVX	real	
CEXT (POSI)	actual cylinder lengths	real (6x1)	in
TINVX	position and angular orientation of platform	real (6x1)	in,rad
TINVXI	initial condition of position and angular orientation (last saved position and angular orientation)	real (6x1)	in,rad
FI	identity matrix	real (6x6)	
TINVXN	new values of position and angular orientation	real (6x1)	in,rad
TINVXL	old values of position and angular orientation	real (6x1)	in,rad
F	difference between calculated length and actual length	real (6x1)	in
DF	gradient with respect to TINVX of vector F	real (6x6)	
DFINV	inverse of DF	real (6x6)	
DECTIV	decrement to approach correct value of TINVX	real (6x1)	in
CX	x direction component of upper platform attachment point	real (6x1)	in
CY	y direction component of upper platform attachment point	real (6x1)	in
BX	x direction component of lower platform attachment point	real (6x1)	in

TABLE VI (Continued)

Variable Name	Description	Type and Dimension	Units
BY	y direction component of lower platform attachment point	real (6x1)	in
BZ	height difference between upper and lower platform	real	in
ERFO	square of the norm of old F	real	
ERRN	square of the norm of new F	real	
RNORM	square of the norm of H (test for convergence)	real	
SUM	square of the norm of DECTIV (test for convergence)	real	

TABLE VII
 ORDER OF POSITIONS AND ANGLES IN ARRAYS
 TINVX, TINVXI, TINVXL AND TINVXN

TINVX and TINVXI	TINVXL and TINVXN	DIMENSION
x direction	x direction	in
y direction	y direction	in
z direction	z direction	in
pitch angle	yaw angle	rad
roll angle	pitch angle	rad
yaw angle	roll angle	rad

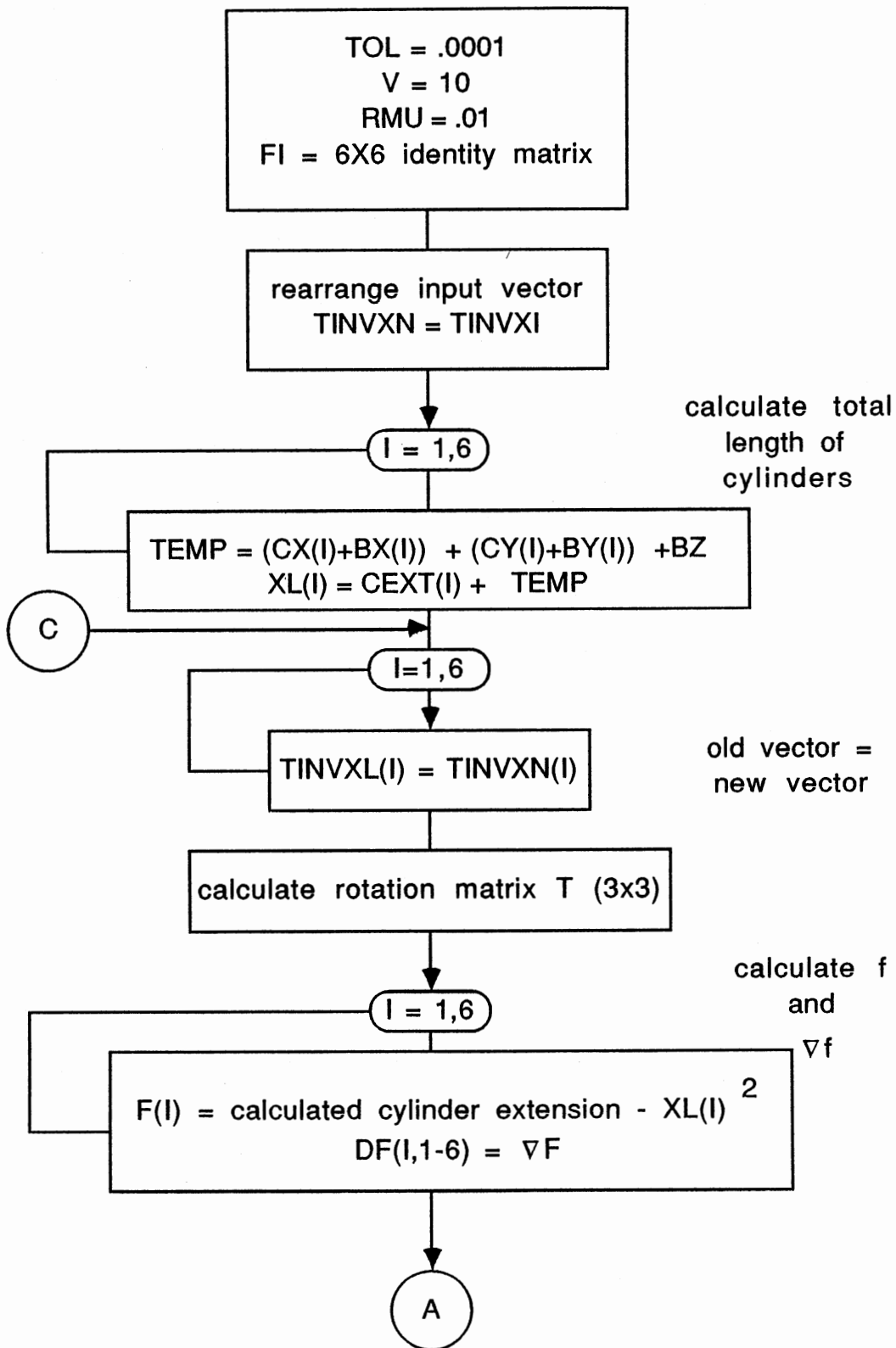


Figure 7.1. Flowchart for Subroutine SMIGT

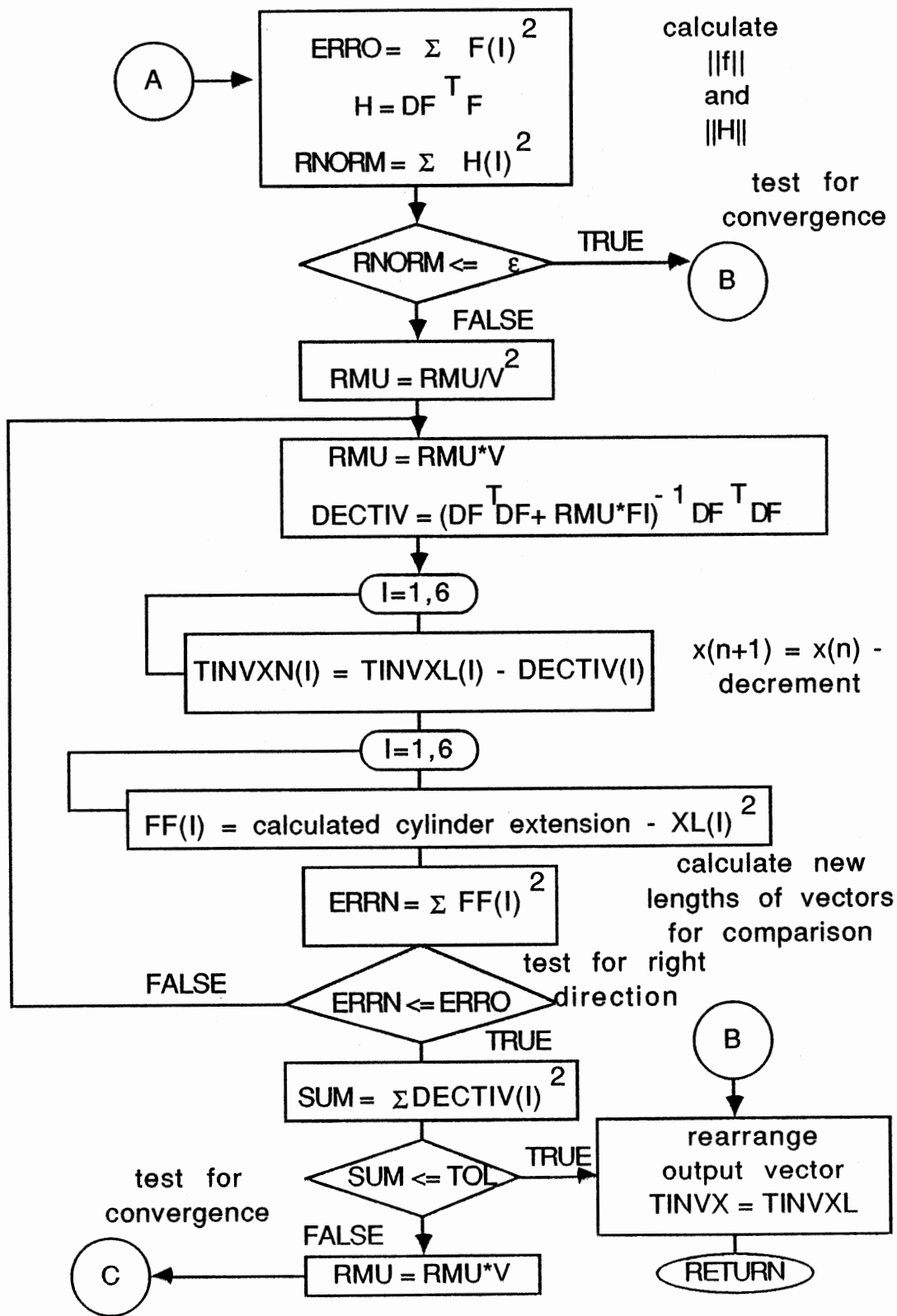


Figure 7.1. (Continued)

CHAPTER VIII

COMPUTER PROGRAM

In the previous chapters a description of the blocks that form the motion base system simulation (MOTSIM) was given. In this chapter the structure of MOTSIM is presented along, with a description of the subroutines and some sample runs.

The structured diagram of MOTSIM is shown in Figure 8.1. As one can see this program, not only executes the motion base system simulation, but also sets up and changes the parameters used in the blocks (see Figure 1.4), prepares the inputs, displays results, and shows an animation of the motion base system. Separate subroutines for each of these tasks were written. A brief description of the subroutines used in program MOTSIM is presented next. The program MOTSIM is menu driven, making it user-friendly.

Subroutine Descriptions

SEMMENU - this subroutine makes it possible to create special effects. It calls the various subroutines described in Chapter III and Appendix A.

SERVO - sets up the parameters for the servo.

VALVE - sets up the parameters that are used in the subroutine to simulate the valve/cylinder combination.

FILERD - reads the four files of parameters used in the program.

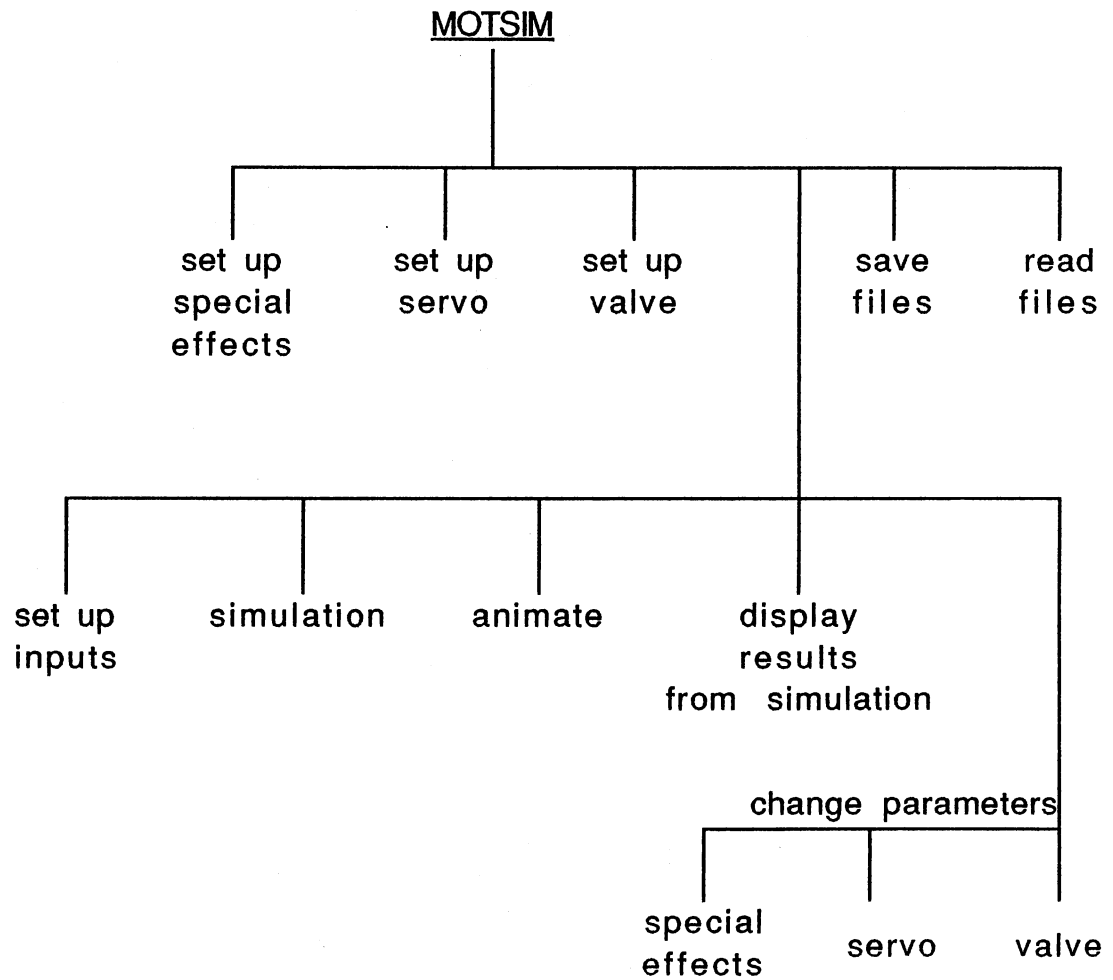


Figure 8.1. MOTSIM Structure Diagram

FILESV - saves three of the files of parameters used in the program.

INPUTS - this subroutine prepares the inputs to the simulation.

SIMULATE - this subroutine simulates the motion base system, and will be described later in this chapter.

ANIMATE - this subroutine shows the results of the simulation representing a motion base in movement in a graphics terminal.

DISRES - this subroutine is used to plot, display or print the results of the simulation.

CHGSE - this subroutine makes it possible to change or view parameters of the special effects.

CHGSRV - this subroutine makes it possible to change or view parameters of the servo.

CHGVAL - this subroutine makes it possible to change or view parameters used to simulate the valve/cylinder combination.

Subroutine SIMULATE

The most important subroutine is SIMULATE, the one that executes the simulation - the objective of the program MOTSIM. The basic flowchart for the SIMULATE subroutine is shown in Figure 8.2. As one can see it contains the blocks (see Figure 1.4) defined in the previous chapters, that is, primary motion, special effects, geometric transformation and smoothing algorithm, servo, valve/cylinder combination and inverse geometric transformation blocks. They are simulated by subroutines OSUONE, SMSPEF, GTRN2, SMSRV, SMVALVE and SMIGT respectively.

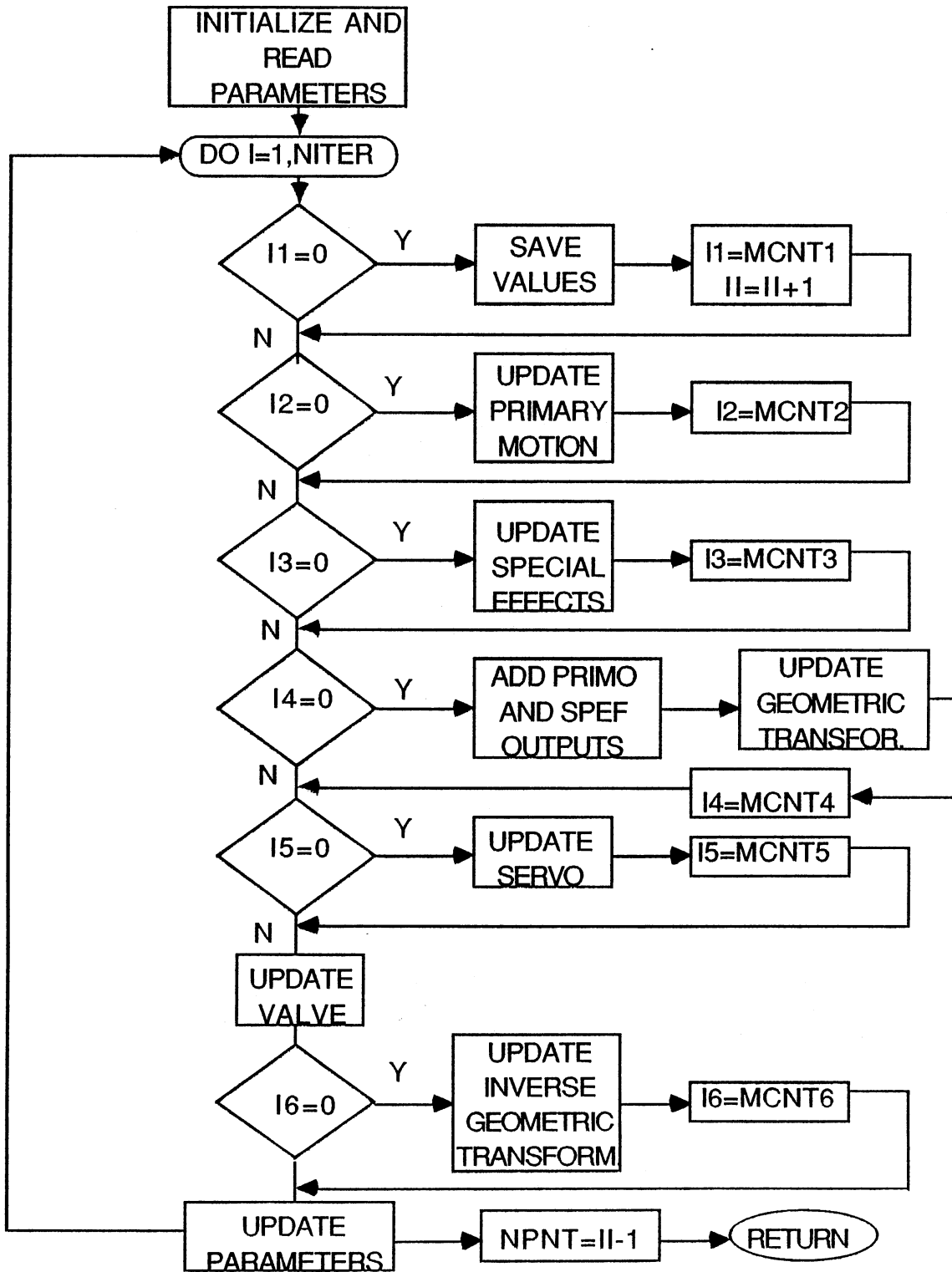


Figure 8.2. Basic Flowchart for Subroutine SIMULATE

SAVEVAL - save values- is the only subroutine seen in Figure 8.2 which has not been described yet. The SAVEVAL subroutine saves the variables chosen in subroutine SIMULATE in array variable PLOTV for plotting, displaying or printing after the simulation of the motion base system is completed. The variables can be chosen from file TABLE.SA. A maximum of 17 variables can be chosen per execution of the simulation.

All the subroutines used in SIMULATE have been described. A description of how the subroutine SIMULATE is executed follows now.

The first step to start execution of subroutine SIMULATE is to select option #2 (EXECUTE) from "SIMULATION MENU". The second step is to enter, in ascending order, the number of the variables the user wants to be saved, if any. These variables shall be entered by their corresponding number found in file TABLE.SA. The next step is to enter the sampling rates for the following SIMULATE blocks: valve/cylinder, primary motion, special effects, servo and save values. The rate for the geometric transformation and smoothing algorithm block is derived from the rates of primary motion and special effect blocks. The rate for the inverse geometric transformation block is derived from the rate of save values block. After these steps the integration intervals and the update counters will be calculated from the given rates. Table VIII below shows the blocks used in SIMULATE and the corresponding update variable and integration interval variable. These variables are also described in Table IX along with some other variables used in MOTSIM. Afterward, enter if the inverse geometric transformation block is to be executed. Finally, the total time for the simulation is entered.

TABLE VIII
COMMANDING VARIABLE PER
PROGRAM UNIT

Block	Variable Update	Integration Variable
valve	every iteration	DT
servo	MCNT5	DTSRV
primary motion	MCNT2	DTPRMO
special effects	MCNT3	DTSPEF
IGT [*]	MCNT6	
GT [*]	MCNT4	
SAVE [*]	MCNT1	DTSAVE

*Where IGT stands for inverse geometric transformations, GT for geometric transformations and smoothing algorithm and SAVE for the routine that saves variables to be plotted, printed or displayed.

After the simulation is complete the results can be plotted, displayed or printed. An animation of the motion base can also be seen. The three dimensional picture of the moving motion base on the graphics terminal is drawn using the outputs of the inverse geometric transformation (positions and angular orientations of the centroid of the upper platform). However, the animation can only be performed when the inverse geometric transformation is executed. The animation of the motion base can be viewed from various angles: an angled view from the front, a straight front view, a straight top view and a straight right side view.

Additional observations must be made with respect to using the program. First, if a block is not to be executed zero must be entered as the RATE for that block, as described in Table VIII. Only the RATE for the valve cannot be zero. Second, the execution of some blocks depend

on other blocks. The inverse geometric transformation is only executed if the saving values (SAVEVAL) and the servo blocks are also executed. The geometric transformation and smoothing algorithm block is executed if the primary motion block and/or the special effects block are also executed. Next, the simulation is complete when the number of iterations, defined by $TMAX/DT$ where $TMAX$ is the total time of simulation and DT is the integration interval of the valve, is reached. Finally, if the primary motion block and the special effects block are not executed, then the desired position of the cylinders is a unit step. This way, the response of the valve/cylinder combination can be tested.

In the next section some examples are presented.

TABLE IX
VARIABLES USED IN SIMULATE

Variable Name	Description	Type and Dimension	Units
I1	counters for SAVEVAL to be executed	integer	
I2	counters for OSUONE to be executed	integer	
I3	counters for SMSPEF to be executed	integer	
I4	counters for GTRN2 to be executed	integer	
I5	counters for SMSRV to be executed	integer	
I6	counters for SMIGT to be executed	integer	
NVS	total number of chosen variables to save	integer	
NVAR	number of chosen variable to save	integer (17x1)	
MCNT1	number of iterations for SAVEVAL variables update	integer	
MCNT2	number of iterations for OSUONE variables update	integer	
MCNT3	number of iterations for SMSPEF variables update	integer	
MCNT4	number of iterations for GTRN2 variables update	integer	
MCNT5	number of iterations for SMSRV variables update	integer	
MCNT6	number of iterations for SMIGT variables update	integer	
NPNT	number of points saved for plotting	integer	
MITER	number of iterations	integer	
T	time counter	real	sec
DT	integration interval of valve	real	sec
DTPRMO	integration interval of primary motion	real	sec

TABLE IX (Continued)

Variable Name	Description	Type and Dimension	Units
DTSPEF	integration interval for special effects	real	sec
DTSRV	integration interval for servo	real	sec
DTSAVE	integration interval for SAVE	real	sec
TMAX	total time of simulation	real	sec

Examples

Several examples were prepared in order to illustrate some of the program features. The examples were divided into 6 categories: washout, special effects, geometric transformation, valve/cylinder model, inverse geometric transformation and animation.

Washout

The washout category illustrates the washout block (see Figure 2.1) part of the primary motion block.

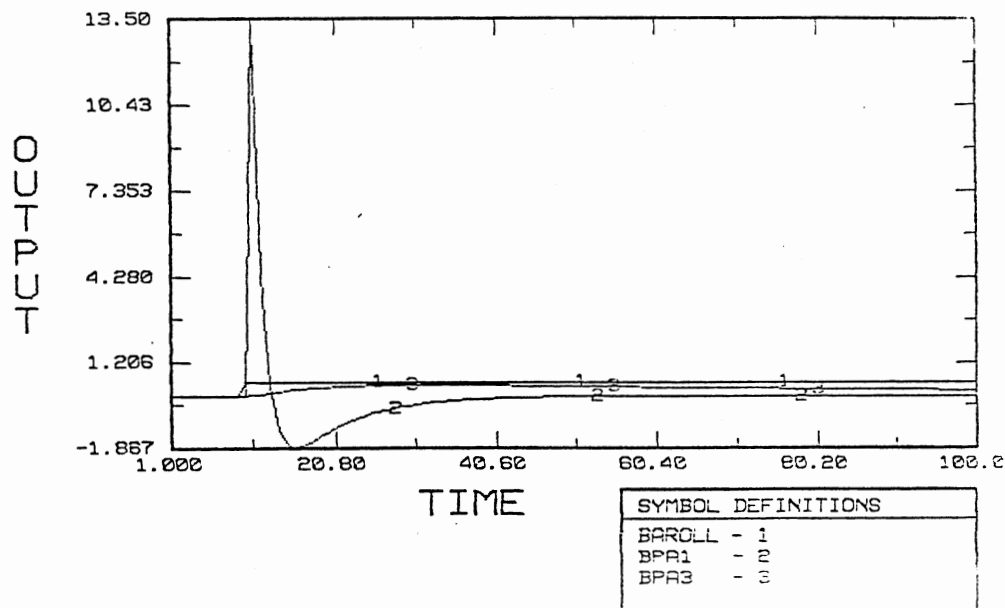


Figure 8.3. Input/Output of Washout

The figure above shows the input/output relationship of the washout block. The input BAROLL is a step roll acceleration in the motion base axes. The outputs are BPA1 (roll acceleration) and BPA3 (roll angle). The constant roll acceleration input is scaled, washed out and integrated to get the roll angle (BPA3). The roll angle decays to zero as the acceleration is washed out.

Special Effects

The special effects category illustrates the set up of special effects.

```

PAGE      1      LIST VER  122084 4   11/14/88  18:56:14  SYS:0064..TEST.SA

 9
SINEX          SINEY          SINEZ          SINE_PITCH
SINE_ROLL      SINE_YAW      FILT_1ST_ORDER FILT_2ND_ORDER
COMBINATION
 1 2 3 4 5 6 2 4 6
11
 1 2 3 4 5 6 7 8 9 9 9
 3 3 3 3 3 3 1 2 1 2 3
28
1.000 1.000 1.000 1.000 1.000 1.000 .1000 .5000 .1000 .5000 .1000
.5000 .0000 1.000 10.00 .0000 1.000 15.00 .1000 .0000 1.000 10.00
.0000 1.000 15.00 .2000 2.000 5.000
17
.0000 .0000 .0000 .0000 .0000 .0000 1.0000E+04 .0000 1.0000E+04 .0000 .0000
1.0000E+04 .0000 1.0000E+04 .0000 .0000 .0000

```

Figure 8.4. Example of a Special Effect Data File

Figure 8.4 shows an example of a special effect data file after 9 special effects have been created. The values used here are for demonstration purposes only and do not represent true special effects.

CURRENT SPECIAL EFFECTS

```

01. SINEX          /AT: POS X
02. SINEY          /AT: POS Y
03. SINEZ          /AT: POS Z
04. SINE_PITCH    /AT: PITCH
05. SINE_ROLL     /AT: ROLL
06. SINE_YAW      /AT: YAW
07. FILT_1ST_ORDER /AT: POS Y
08. FILT_2ND_ORDER /AT: PITCH
09. COMBINATION   /AT: YAW

```

Figure 8.5. "Current Special Effects" Screen

The above figure shows one of the graphics screens - "CURRENT SPECIAL EFFECTS" - when the data file of Figure 8.4 is used. The "/AT:" denotes where the output of the special effect is going. Example: Special effect 1, SINEX, is going to affect the position of the motion base in the x axis.

ADD GENERATORS

SPECIAL EFFECT: COMBINATION

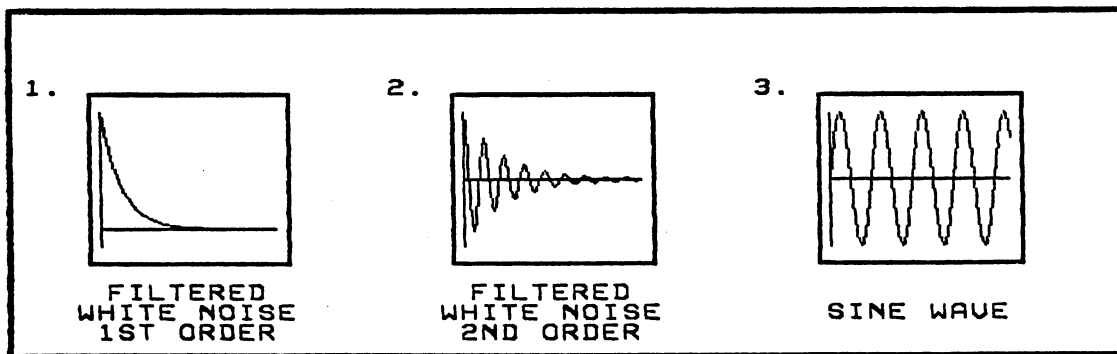


Figure 8.6. "Add Generators" Screen

Figure 8.6 shows the graphics screen that appears when the user wants to add generators to a specified special effect. The special effect specified here is "COMBINATION", selection 9 from Figure 8.5. Three types of generators can be chosen: first order filtered white noise, second order filtered white noise and sine wave. They are represented by an impulse response to a first order filter, an impulse response to a second order filter and a sine wave respectively.

```

COMBINATION
ADD OUTPUT AT: YAW
-----
01.  FILT. WHITE NOISE-1ST ORD
      MEAN = +0.0000E+00
      VARIANCE = +0.1000E+01
      BANDWIDTH = +0.1000E+02
02.  FILT. WHITE NOISE-2ND ORD
      MEAN = +0.0000E+00
      VARIANCE = +0.1000E+01
      BANDWIDTH = +0.1500E+02
      DAMPING = +0.2000E+00
03.  SINE WAVE
      AMPLITUDE = +0.2000E+01
      FREQUENCY = +0.5000E+01

```

Figure 8.7. Special Effect "COMBINATION" with Generators

The figure above shows an example of the view option for a specified special effect. It illustrates the special effect "COMBINATION", selection 9 from Figure 8.5. From this screen one can tell that the special effect "COMBINATION" is going to affect the position of the motion base in the yaw angle. One can also see the generators that form the special effect. This special effect is composed of:

- 1) first order filtered white noise. The white noise has mean zero and variance 1. The bandwidth of the filter is 10 Hz.
- 2) second order filtered white noise. The white noise has mean zero and variance 1. The bandwidth of the filter is 15 Hz and the damping is 0.2.
- 3) sine wave with amplitude 2 and frequency 5 Hz.

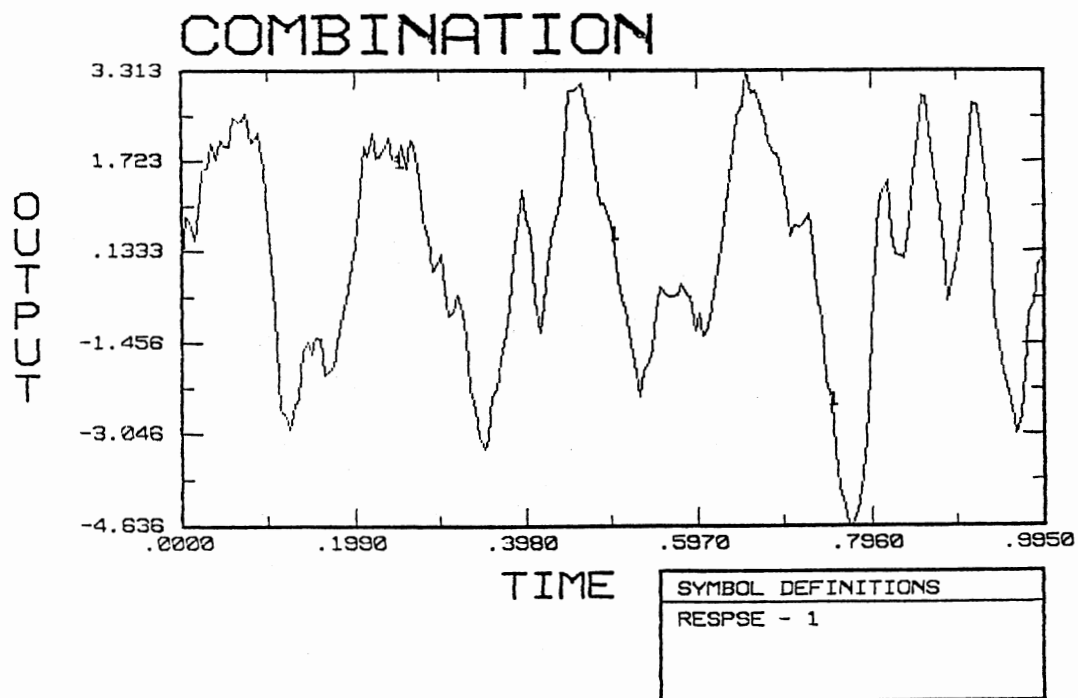


Figure 8.8. Response of Special Effect COMBINATION

The figure above illustrates the response of a special effect. This figure shows how the special effect COMBINATION is going to affect the yaw angle of the motion base in the time length of 1 second.

Geometric Transformation

The geometric transformation category illustrates the geometric transformation and smoothing algorithm block. The input to this block is SIGNA, which represents the position and angular orientation of the motion base. The output is CYLOT, the cylinder extensions.

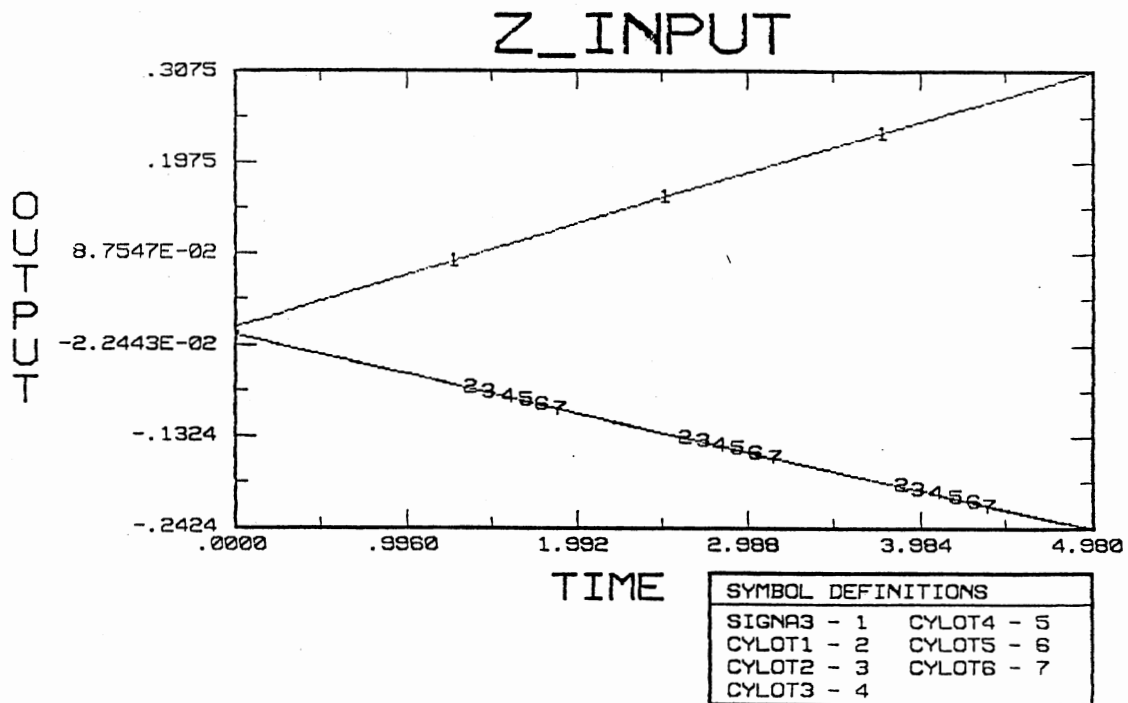


Figure 8.9. Input/Output of Geometric Transformation (Pure Z)

Figure 8.9 shows a pure z input (only SIGNA3). The outputs are cylinders 1-6 extension (CYLOT1 - CYLOT6). As expected all the cylinders move the same amount in the same time interval. This allows the motion base to move vertically. The position in the z axis is positive so all cylinders retract moving the motion base down (positive z direction).

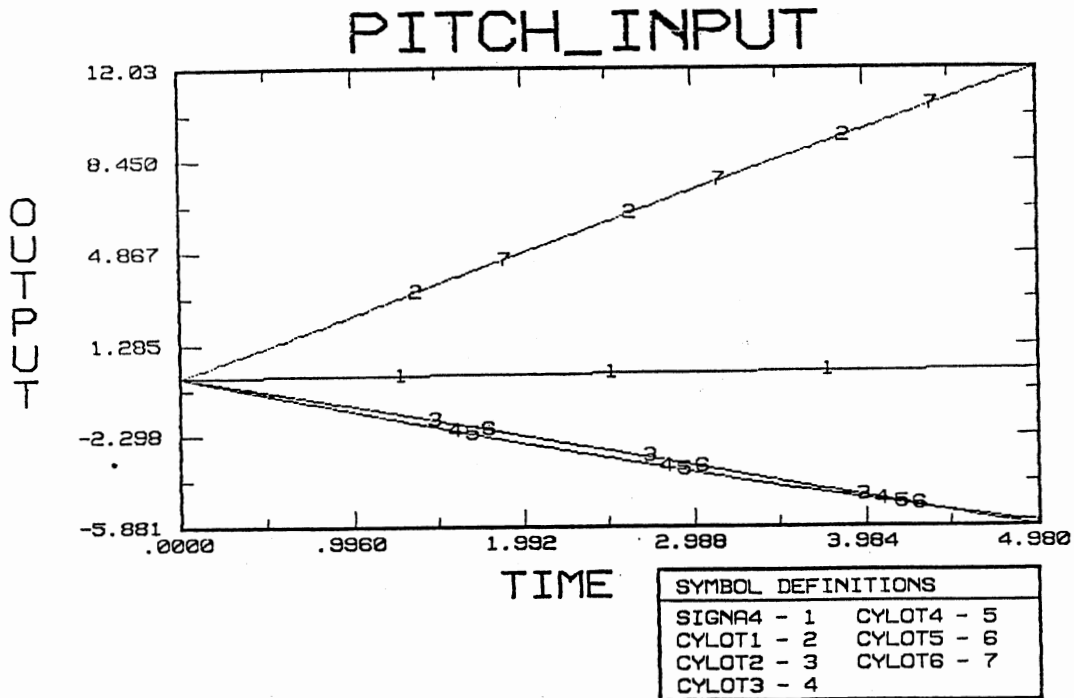


Figure 8.10. Input/Output of Geometric Transformation (Pure Pitch)

Figure 8.10 shows a pure pitch input (only SIGNA4). The outputs are cylinders 1-6 extension (CYLOT1 - CYLOT6). As expected the two front cylinders (1 and 6), the two back cylinders (3 and 4) and the two cylinders in the middle (2 and 5) (see Figure 1.1) move the same amount in the same time interval. The pitch angle is positive so the two front cylinders extend and the others retract making the motion base rotate up about the y axis (positive pitch).

Valve/Cylinder Model

The valve/cylinder model category illustrates the valve/cylinder combination response to a unit step as the desired cylinder extension.

```

PAGE      1      LIST VER  122084 4   11/16/88  13:47:48  SYS:0064..SRVPAR.SA
2.1970E-03 2.1970E-03 2.1970E-03 2.1970E-03 2.1970E-03 2.1970E-03
2.051 2.051 2.051 2.051 2.051 2.051
4.351 4.351 4.351 4.351 4.351 4.351
-5066. -5066. -5066. -5066. -5066. -5066.
-1.000 -1.000 -1.000 -1.000 -1.000 -1.000
1.000 1.000 1.000 1.000 1.000 1.000
-2.2700E-05 -2.2700E-05 -2.2700E-05 -2.2700E-05 -2.2700E-05 -2.2700E-05
.0000 .0000 .0000 .0000 .0000 .0000
1064. 1064. 1064. 1064. 1064. 1064.
.0000 .0000 .0000 .0000 .0000 .0000
-531.9 -531.9 -531.9 -531.9 -531.9 -531.9
-1064. -1064. -1064. -1064. -1064. -1064.
-15.30 -16.30
PAGE      1      LIST VER  122084 4   11/17/88  11:43:23  SYS:0064..VALPAR.SA
.7000 185.0 .1000 1000. .0000 .0000 .0000 .0000 7.000 210.0
1.000 .6887 2.0000E+05 500.0 50.00
1500. 1500. 1500. 1500. 1500. 1500.
6.1300E+04 6.1300E+04 6.1300E+04 6.1300E+04 6.1300E+04 6.1300E+04
487.8 487.8 487.8 487.8 487.8 487.8

```

Figure 8.11. Example of Servo and Valve/Cylinder Data Files

Figure 8.11 shows an example of a servo data file and a valve/cylinder combination data file. The values used here are for demonstration purposes only and do not represent a true valve/cylinder model or a servo.

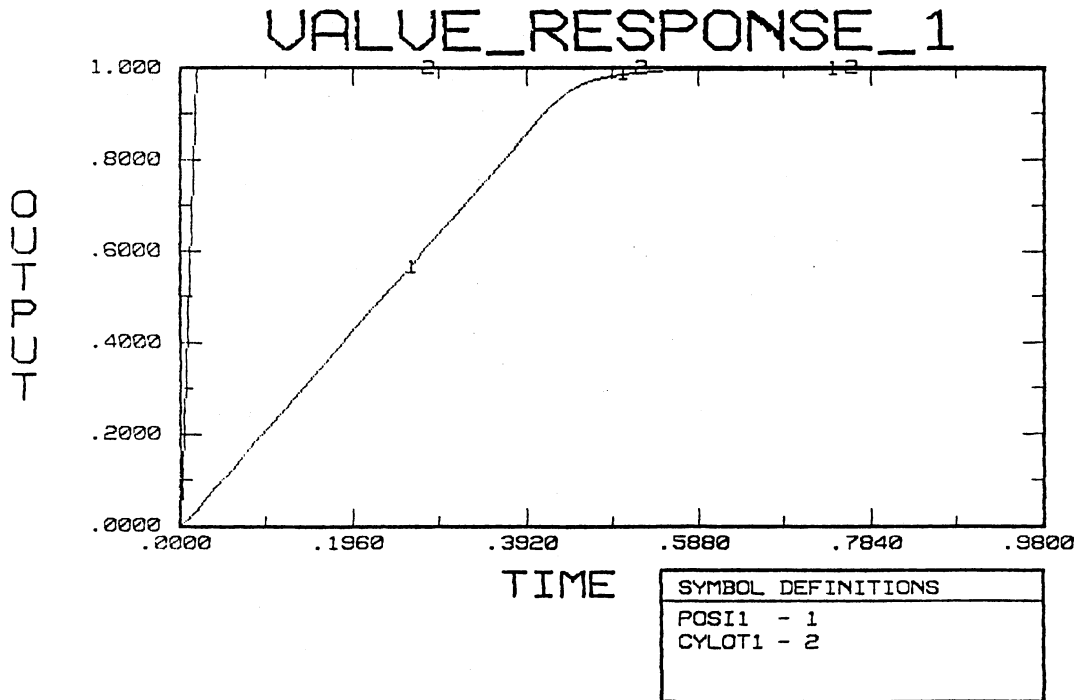


Figure 8.12. Valve/Cylinder/Servo Response 1

The figure above shows the response of the valve/cylinder model with position feedback. The purpose of this figure is to determine the settling time, about 0.5s, and also shows that the servo takes the cylinder smoothly to the desired position. The symbols are defined as:

- POSI1: the actual position of cylinder 1
- CYLOT1: the desired position of cylinder 1 (unit step)

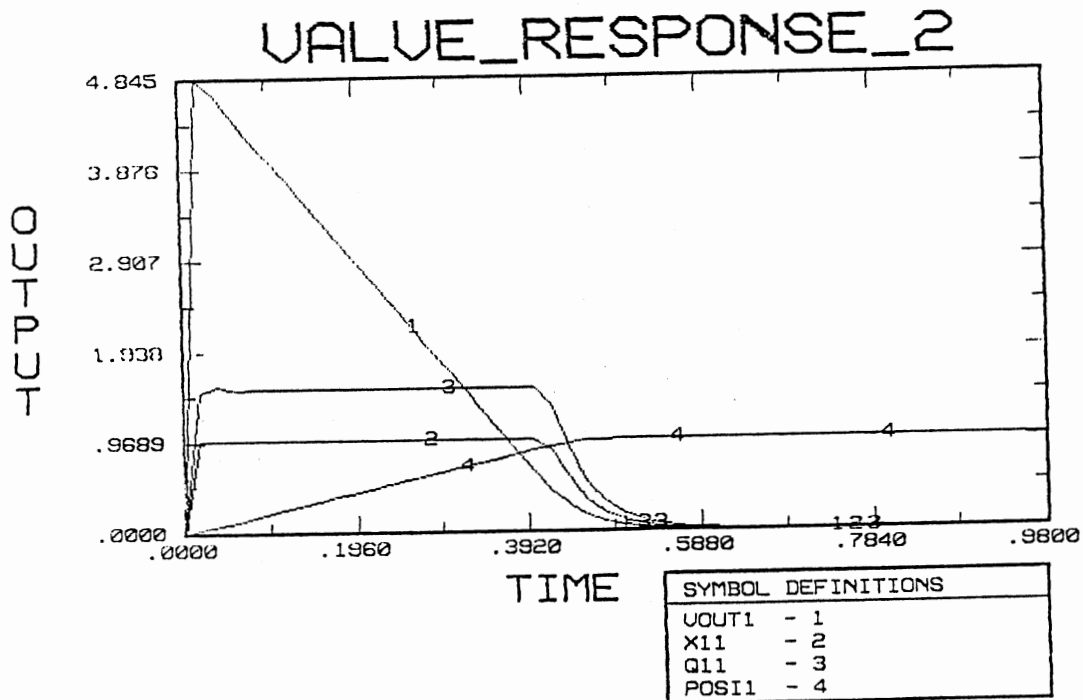


Figure 8.13. Valve/Cylinder/Servo Response 2

Figure 8.13 shows other variables in the unit step response.

VOUT1 is the voltage applied to the motor to open the valve, derived from the differential position of the cylinder. X11 is the position of the spool and it reaches the maximum at 1 inch displacement. Q11 is the flow inside the valve. All the values of these variables decrease as the actual position of the cylinder (POS11) reaches the desired position (1 in), as can be seen in the plot.

After the settling time for the response of the valve/cylinder model is obtained, an analysis of its response to a sine wave is performed. Figures 8.14 and 8.15 below show the response of the valve/cylinder model to a 0.01 Hz and 0.1 Hz sine wave respectively. A good response was obtained for both inputs even though there is some phase shift between commanded position and actual position.

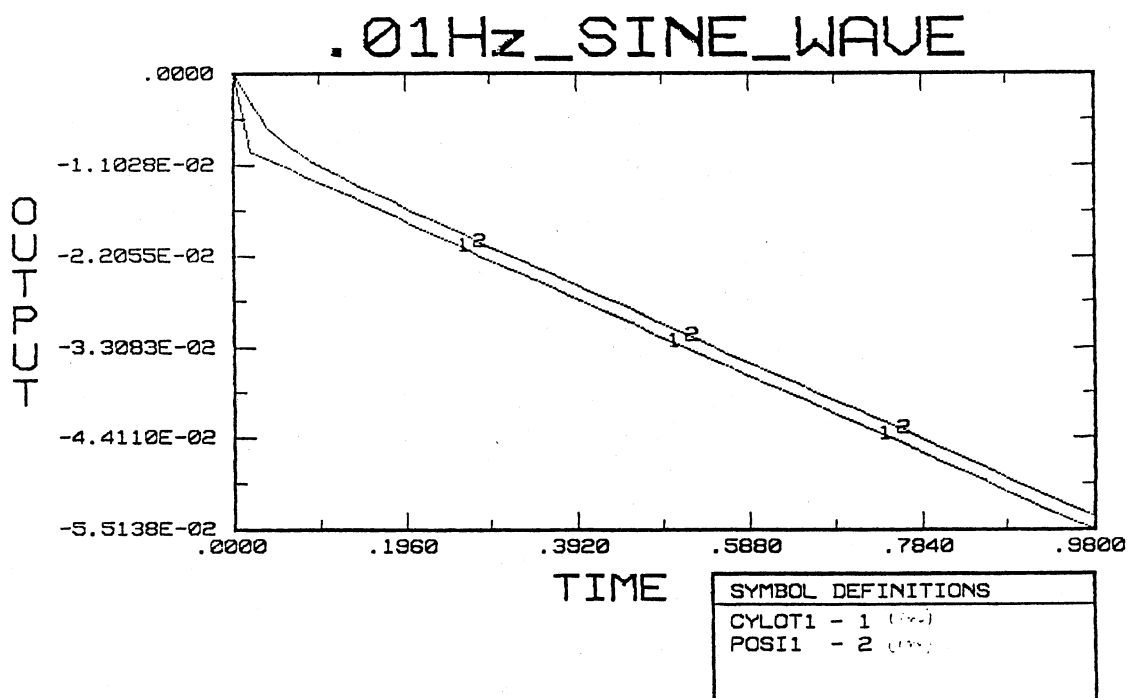


Figure 8.14. Valve/Cylinder Response to 0.01 Hz Sine Wave

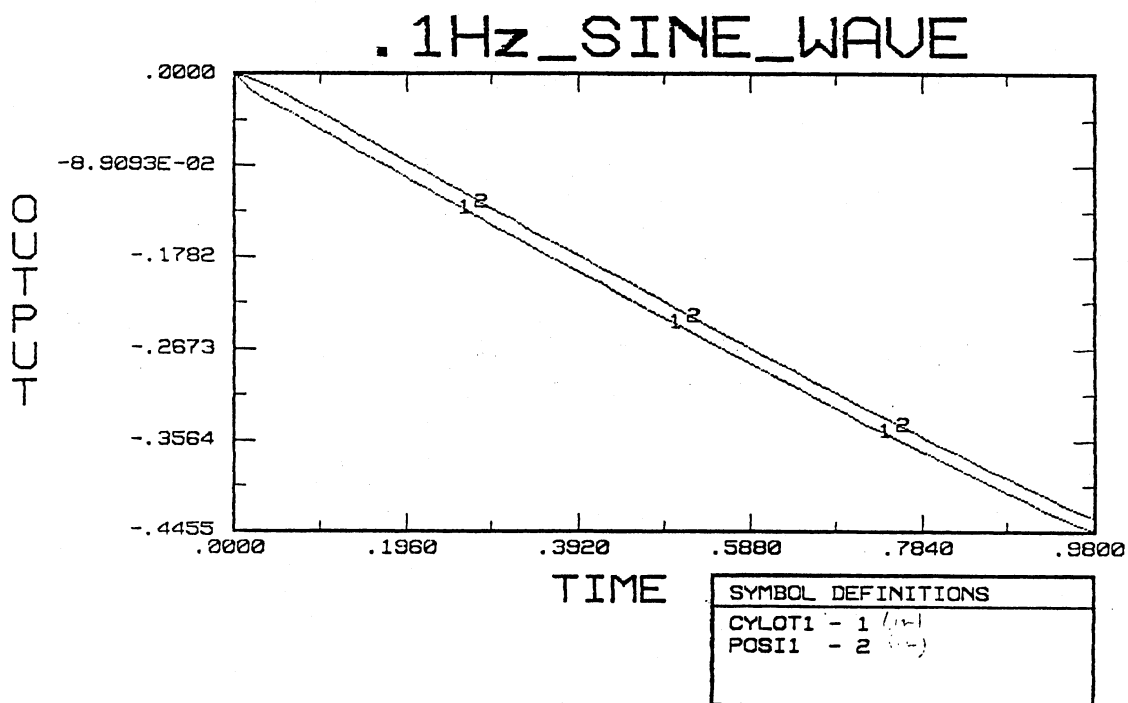


Figure 8.15. Valve/Cylinder Response to 0.1 Hz Sine Wave

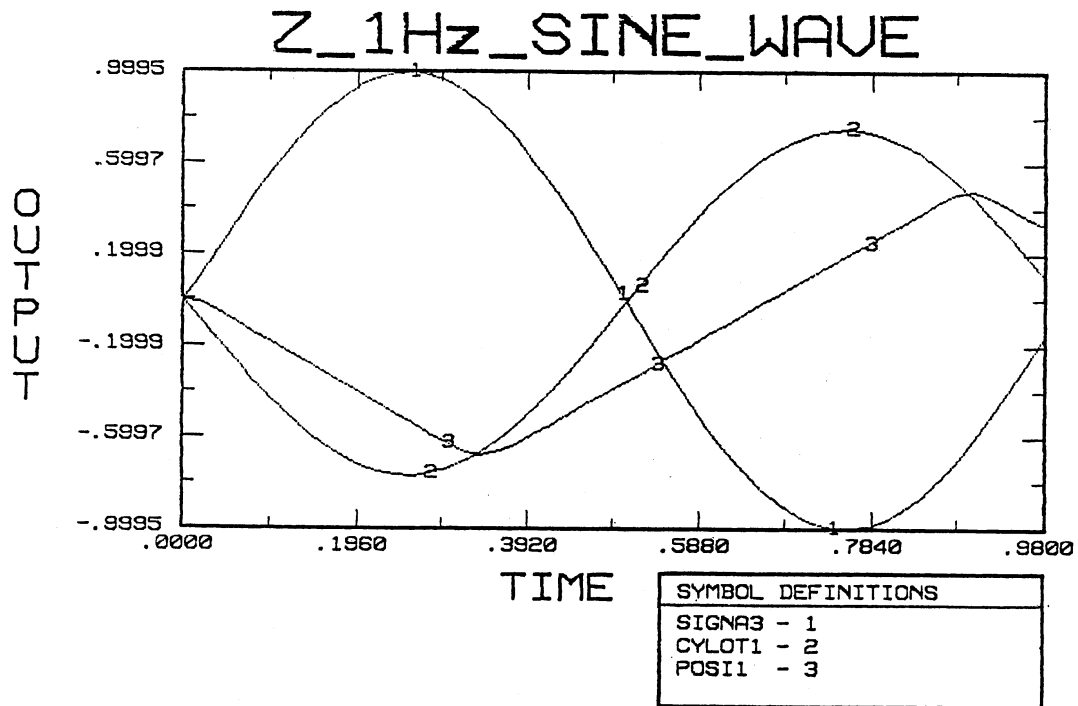


Figure 8.16. Valve/Cylinder Response to 1 Hz Sine Wave

Figure 8.16 shows the valve/cylinder model and servo response to a 1 Hz sine wave input. A bad response was obtained. SIGNA3 is the sine wave input to the z position of the motion base. CYLOT1 is the corresponding cylinder 1 extension, output of the geometric transformation and smoothing algorithm. POS11 is the actual cylinder 1 extension which is further behind the desired cylinder extension. From the figure it can be concluded that the servo is not able to track the desired cylinder extension at 1 Hz. This occurs because the frequency of the sine wave is higher than the response of the valve/cylinder model.

Inverse Geometric Transformation

The inverse geometric transformation category illustrates the inverse geometric transformation block.

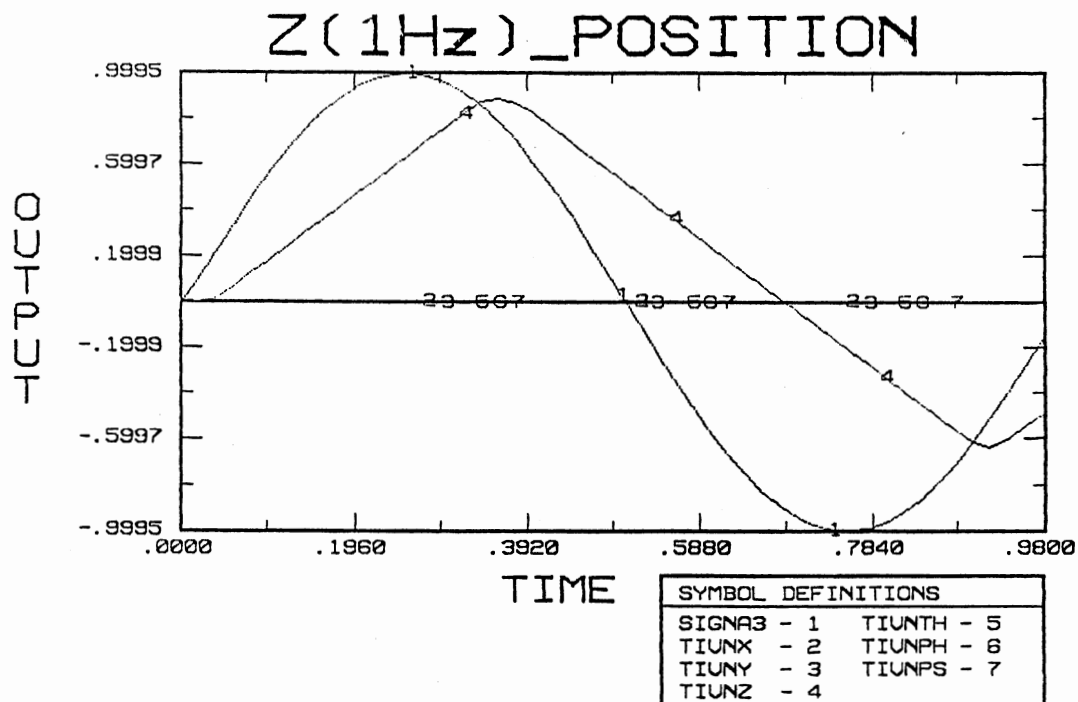


Figure 8.17. IGT of a 1 Hz Sine Wave

The figure above refers to Figure 8.16 where the servo does not track the desired cylinder position. This figure shows how the inverse transformation can provide the actual position and angular orientation of the motion base (TINVX-TINVPS). Also, the desired motion base position and angular orientation (SIGNA3) can be compared to actual values.

As an additional test, the forward geometric transformation was performed on the output of the inverse transformation. This forward transformation can be seen in Figure 8.18 below. The symbols in the figure are defined as:

- CYLOT1: desired cylinder 1 extension
- POSI1: actual cylinder 1 extension
- AFTER1: cylinder 1 extension derived from the output of the inverse geometric transformation.

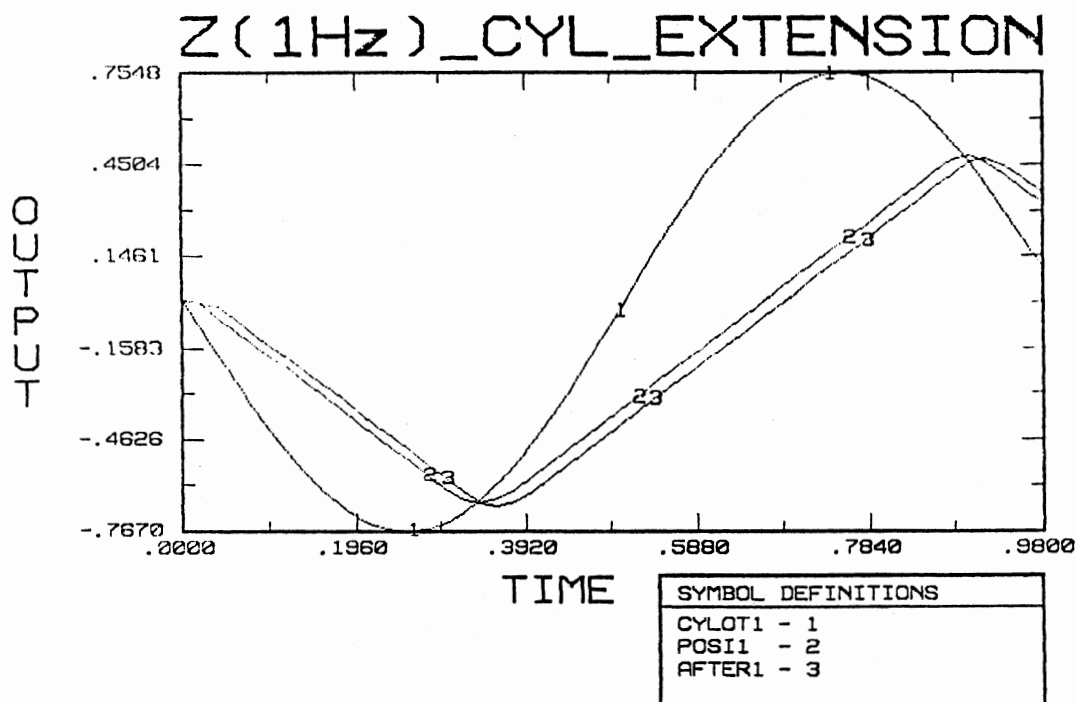


Figure 8.18. Cylinder Extensions to a 1 Hz Sine Wave

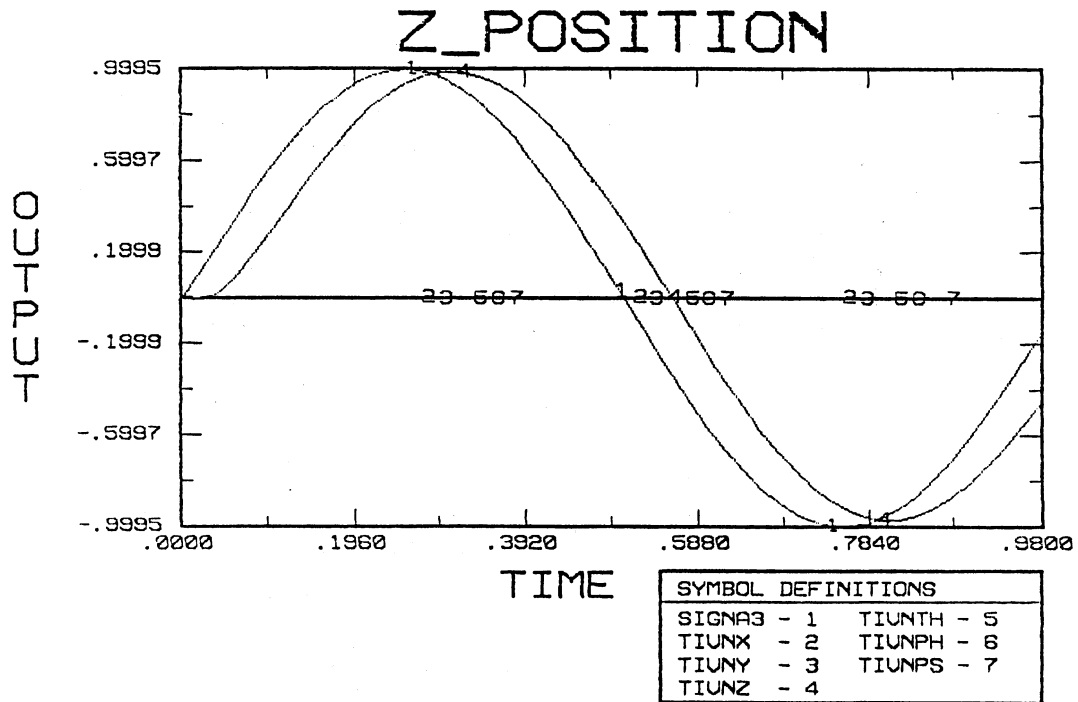


Figure 8.19. IGT Output to a Pure Z Input

Figure 8.19 shows the difference between desired and actual z position of the motion base when the servo is tracking the desired cylinder position. The difference occurs because of the phase shift described earlier. SIGNA3 is the desired z position and TINVZ is the actual z position given by the inverse geometric transformation with the actual cylinder extension. The difference between the actual cylinder extension (POSI1), the desired cylinder extension (CYLOT1) and the cylinder extension obtained from the output of the inverse geometric transformation (AFTER1) can be seen in Figure 8.20 below. The difference between actual cylinder extension (POSI) and desired cylinder extension (CYLOT) is caused by the phase shift in the servo.

The difference between actual cylinder extension (POSI) and cylinder extension obtained from the output of the inverse geometric transformation (AFTER) is due to approximations and tolerances for convergence in the algorithm for the inverse geometric transformation.

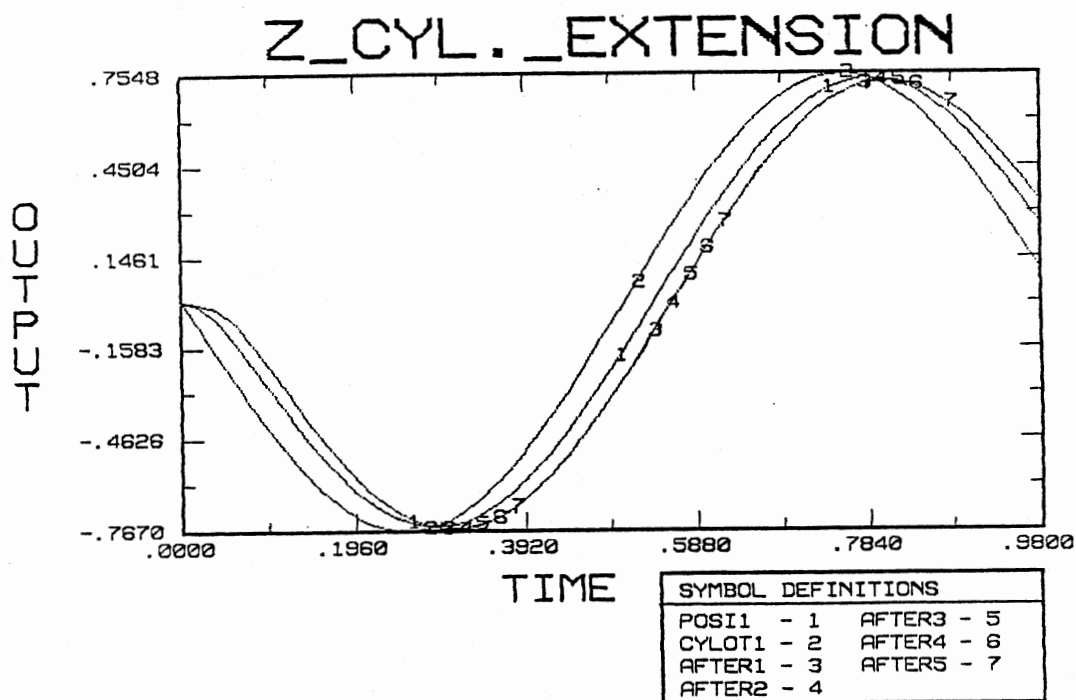


Figure 8.20. Cylinder Extension to a Pure Z Input

Another example was made to show the differences that occur between the actual and desired position and angular orientation of the motion base. The pitch angle was chosen. Figures 8.21 through 8.24 below give the same comparison plots as previous figures and include a printout showing the magnitude of the error.

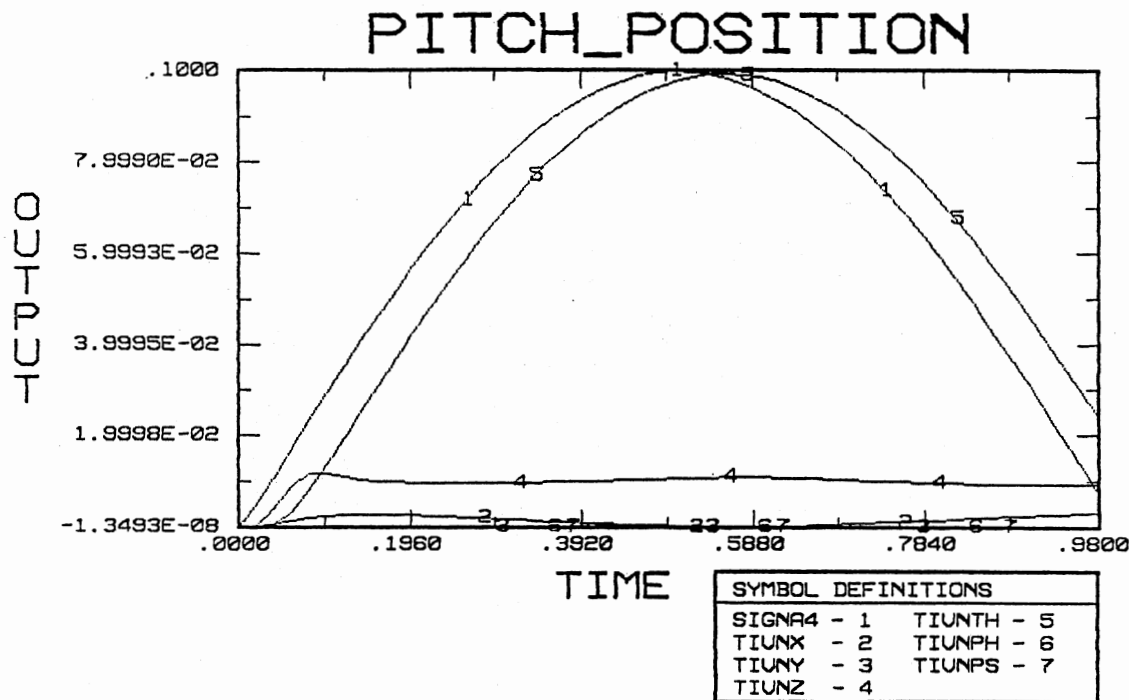


Figure 8.21. IGT Output to a Pure Pitch Input - Position

TIME	SIGNA4	TIUNX	TIUNY	TIUNZ	TIUNTH	TIUNPH	TIUNPS
0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
0.20000E-01	0.47107E-02	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
0.40000E-01	0.10973E-01	0.57682E-03	-0.60871E-08	0.40131E-02	0.65524E-03	-0.45550E-10	0.11438E-09
0.60000E-01	0.17193E-01	0.16129E-02	0.23997E-08	0.92316E-02	0.36229E-02	-0.82736E-10	0.84346E-10
0.80000E-01	0.23345E-01	0.22817E-02	-0.11335E-07	0.11757E-01	0.82719E-02	-0.57012E-10	0.16319E-09
0.10000E+00	0.29404E-01	0.26283E-02	0.40309E-07	0.11719E-01	0.13718E-01	0.11337E-09	-0.10406E-09
0.12000E+00	0.35348E-01	0.28467E-02	-0.60847E-08	0.11108E-01	0.19489E-01	0.25342E-09	-0.14373E-09
0.14000E+00	0.41152E-01	0.29435E-02	-0.12582E-07	0.10658E-01	0.25388E-01	0.64414E-10	0.21379E-09
0.16000E+00	0.46793E-01	0.29247E-02	-0.58645E-08	0.10315E-01	0.31293E-01	0.78762E-10	-0.11629E-09
0.18000E+00	0.52250E-01	0.28393E-02	-0.13493E-07	0.10048E-01	0.37126E-01	-0.13513E-09	0.15759E-10
0.20000E+00	0.57501E-01	0.27190E-02	0.26163E-08	0.98724E-02	0.42835E-01	0.17168E-10	-0.14426E-09
0.22000E+00	0.62524E-01	0.25811E-02	-0.26613E-09	0.97885E-02	0.48387E-01	-0.49334E-10	0.10388E-09
0.24000E+00	0.67301E-01	0.24170E-02	0.47249E-08	0.97504E-02	0.53753E-01	0.38820E-10	0.18879E-09
0.26000E+00	0.71813E-01	0.22432E-02	0.15583E-08	0.97504E-02	0.58909E-01	-0.60989E-10	0.78115E-10
0.28000E+00	0.76041E-01	0.20588E-02	-0.40801E-09	0.97656E-02	0.63833E-01	0.10005E-10	0.61812E-10

Figure 8.22. Printout of IGT Output to a Pure Pitch Input - Position

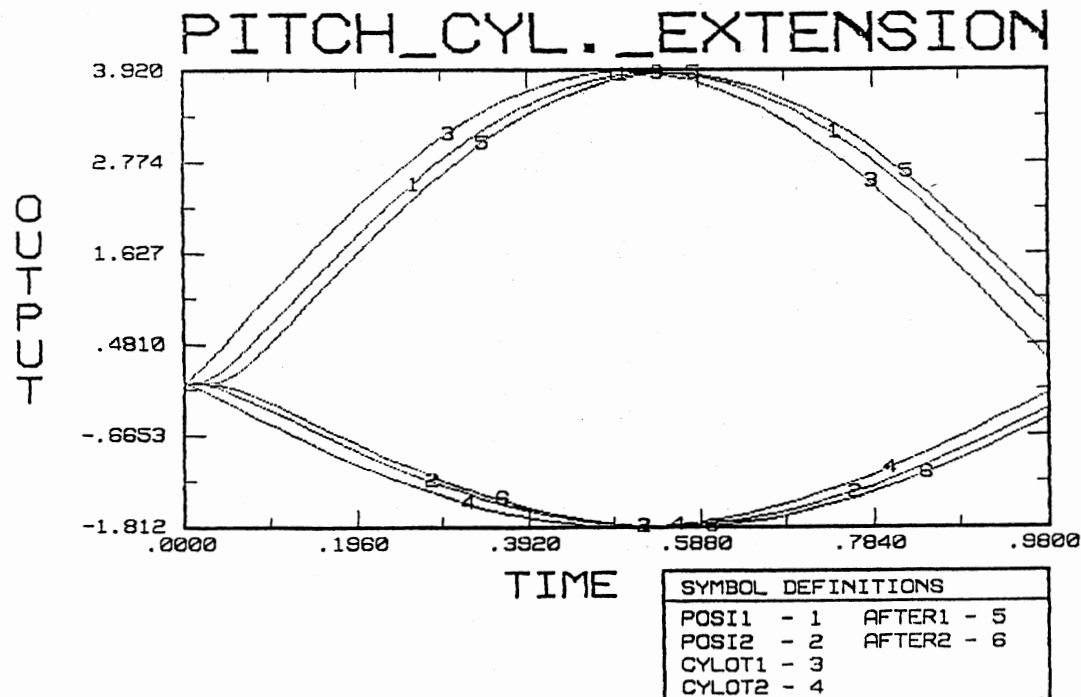


Figure 8.23. IGT Output to a Pure Pitch Input - Cylinder Extension

TIME	POS11	POS12	CYLOT1	CYLOT2	AFTER1	AFTER2
0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
0.20000E-01	0.21207E-01	-0.14114E-01	0.17593E+00	-0.90904E-01	-0.85373E-02	-0.85449E-02
0.40000E-01	0.13165E+00	-0.69791E-01	0.42132E+00	-0.20081E+00	0.14160E-01	-0.23392E-01
0.60000E-01	0.31078E+00	-0.15317E+00	0.66515E+00	-0.31041E+00	0.12657E+00	-0.79910E-01
0.80000E-01	0.52380E+00	-0.24894E+00	0.90646E+00	-0.41925E+00	0.30688E+00	-0.16376E+00
0.10000E+00	0.75045E+00	-0.35040E+00	0.11443E+01	-0.52690E+00	0.52042E+00	-0.25974E+00
0.12000E+00	0.98218E+00	-0.45461E+00	0.13776E+01	-0.63289E+00	0.74726E+00	-0.36131E+00
0.14000E+00	0.12143E+01	-0.55940E+00	0.16056E+01	-0.73679E+00	0.97904E+00	-0.46555E+00
0.16000E+00	0.14437E+01	-0.66333E+00	0.18273E+01	-0.83814E+00	0.12111E+01	-0.57032E+00
0.18000E+00	0.16682E+01	-0.76550E+00	0.20418E+01	-0.93652E+00	0.14403E+01	-0.67422E+00
0.20000E+00	0.18866E+01	-0.86526E+00	0.22482E+01	-0.10315E+01	0.16648E+01	-0.77635E+00
0.22000E+00	0.20977E+01	-0.96205E+00	0.24457E+01	-0.11227E+01	0.18830E+01	-0.87606E+00
0.24000E+00	0.23007E+01	-0.10554E+01	0.26336E+01	-0.12096E+01	0.20939E+01	-0.97279E+00
0.26000E+00	0.24945E+01	-0.11448E+01	0.28111E+01	-0.12920E+01	0.22966E+01	-0.10660E+01
0.28000E+00	0.26785E+01	-0.12299E+01	0.29774E+01	-0.13693E+01	0.24902E+01	-0.11554E+01

Figure 8.24. Printout of IGT Output to a Pure Pitch Input - Cylinder Extensions

Animation

The animation category illustrates some of the screens seen on the graphics terminal during the animation of the motion base system simulation. The fixed lower base platform is represented by a filled-in triangle, the moving upper platform is represented by an open triangle. Figure 8.25 shows the motion base in the initial neutral position from a front angle view. Figure 8.26 shows the motion base in a positive pitch angle from a straight side view. Figure 8.27 shows the motion base in a positive yaw angle from a straight top view. Figure 8.28 shows the motion base in a negative y position from a straight front view.

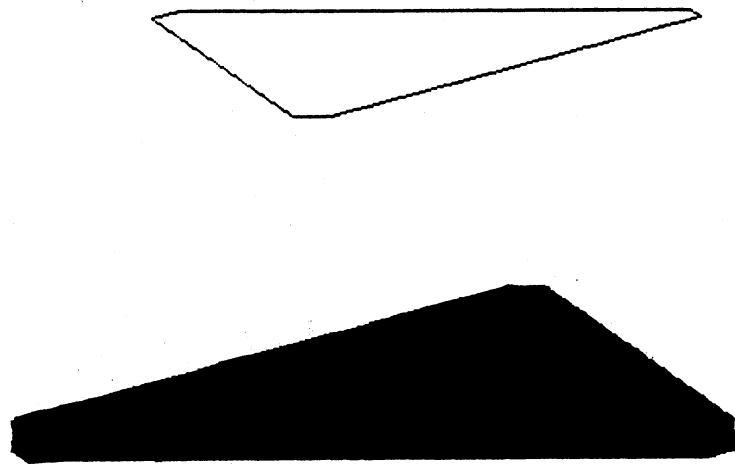


Figure 8.25. Motion Base in Initial Neutral Position - Angle View

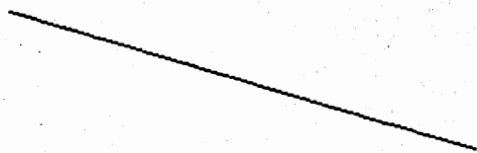


Figure 8.26. Motion Base in Pitch Angle -
Side View

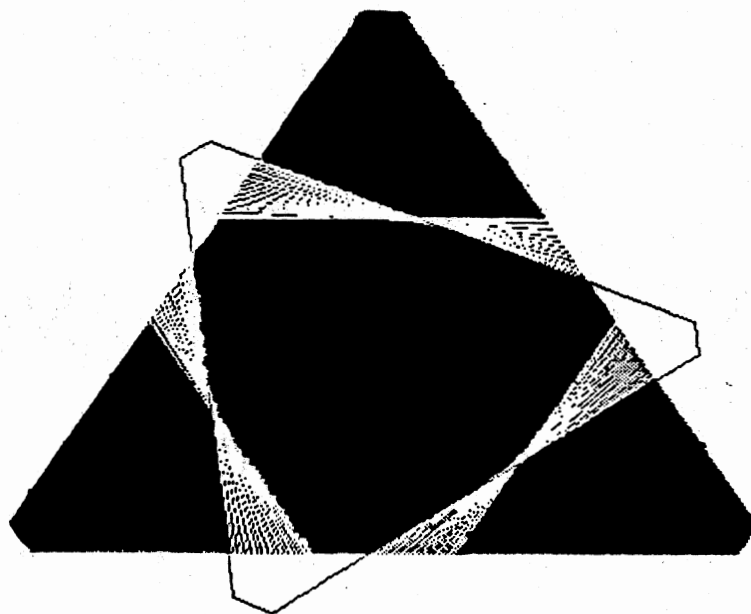


Figure 8.27. Motion Base in Yaw Angle - Top View



Figure 8.28. Motion Base in Y Displacement - Front View

This category concludes the examples of the program features. In the next chapter a conclusion is made and future improvements are suggested.

CHAPTER IX

CONCLUSION

A FORTRAN program to simulate a six degree-of-freedom motion base system for flight simulators was developed. A study of the system was performed prior to writing the program code. A general description of the system was given in Chapter I. In the following chapters all the blocks pertinent to the simulation were analyzed. A valve/cylinder model was defined in Chapter VI so the simulation would become possible. Finally, some examples were given in chapter VIII.

Currently, this type of program is not readily available to simulator designers. The program provides a means of testing the dimensions and parameter variations for a six degree-of-freedom motion base without ever building the hardware. It also permits the testing of new features of the actual motion base system software and helps engineers in the calibration process of the motion base system making it faster and less expensive. Therefore it should be helpful to most simulator designers.

In the current valve/cylinder simulation, the weight of the motion base on each cylinder is considered constant, although this is not what happens in reality. As the motion base moves the weight on the cylinders change. Further improvements can be made in the model to account for the different weights on the cylinders.

Also, a routine to enter and change the primary motion parameters might be written, making the program completely user-friendly.

Other integration methods could be made available for the spool displacement and the piston displacement calculations. Perhaps to permit the change from the continuous time system to its equivalent discrete time system.

Finally, the animation can be improved by adding the six cylinders attached to lower and upper base platforms. This allows a nicer view of the motion base system animation.

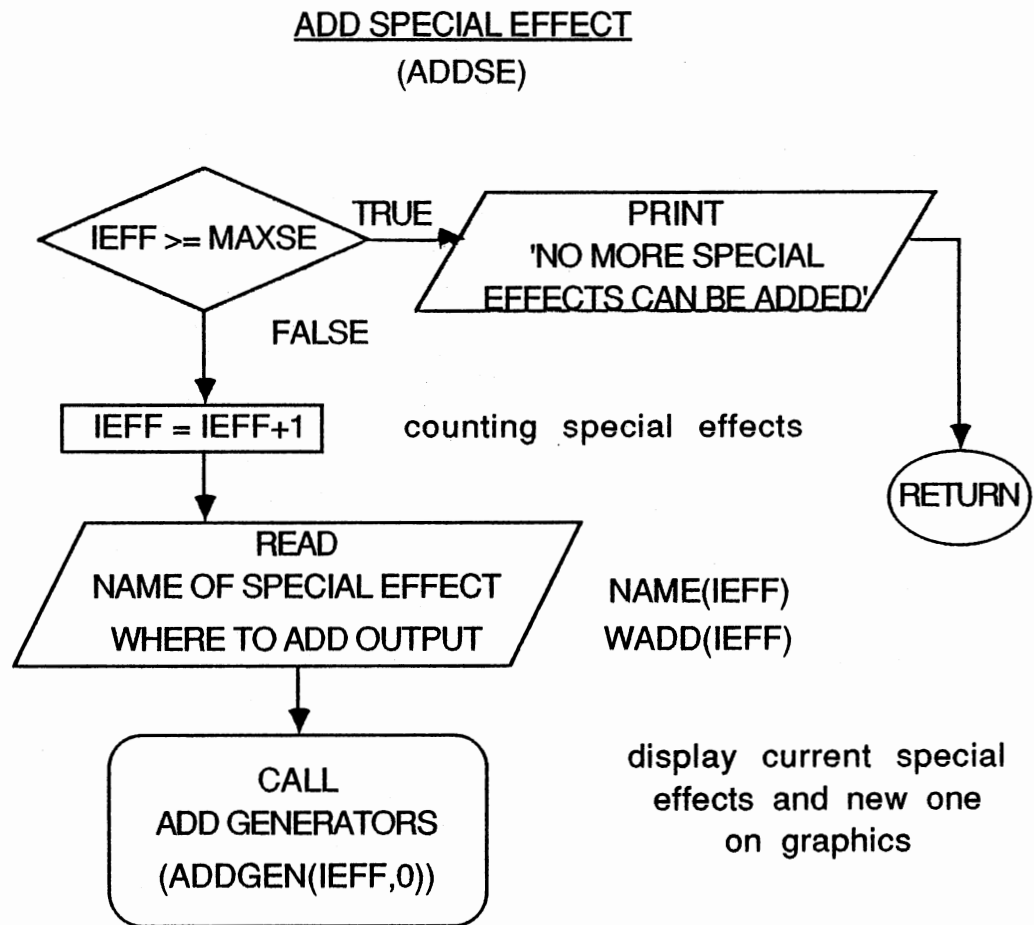
REFERENCES

- [1] J. M. Rolfe and K. J. Staples, *Flight Simulation*. Cambridge, U.K.: Cambridge University Press, 1986.
- [2] B. Friedland, C. K. Ling and M. F. Hutton, "Quasi-Optimum Design of a Six Degree of Freedom Moving Base Simulator Control System," NASA CR-2312, Oct. 1973.
- [3] S. F. Schmidt and B. Conrad, "The Calculation of Motion Drive Signals for Piloted Flight Simulators," NASA CR-73375, Oct. 1969.
- [4] S. F. Schmidt and B. Conrad, "Motion Drive Signals for Piloted Flight Simulators," NASA CR-1601, May 1970.
- [5] A. Papoulis, *Probability, Random Variables, and Stochastic Processes*. New York: McGraw-Hill, 1984.
- [6] B. C. Kuo, *Automatic Control Systems*. Englewood Cliffs, NJ: Prentice-Hall, 1987.
- [7] J. E. Dieudonne, R.V. Parrish and R. E. Bardusch, "An Actuator Extension Transformation for a Motion Simulator and an Inverse Transformation Applying Newton-Raphson's Method," NASA TN D-7067, Nov. 1972.
- [8] W. R. Ahrendt and C. J. Savant, Jr., *Servomechanism Practice*. York, PA: McGraw-Hill, 1960.
- [9] P. L. Taylor, *Servomechanisms*. London, U.K.: Longmans, 1969.
- [10] K. Ogata, *System Dynamics*. Englewood Cliffs, NJ: Prentice-Hall, 1978.
- [11] K. Ogata, *Discrete Time Control Systems*. Englewood Cliffs, NJ: Prentice-Hall, 1987.
- [12] C. F. Gerald and P. O. Wheatley, *Applied Numerical Analysis*. Menlo Park, CA: Addison-Wesley, 1984.

- [13] L.E. Scales, *Introduction to Non-Linear Optimization*. New York: Springer-Verlag New York Inc., 1985.
- [14] "Two-Stage Flow Control Servovalves." Catalog 762682. Noplace: MOOG.

APPENDIXES

APPENDIX A
ADDITIONAL FLOWCHARTS FOR SPECIAL
EFFECTS SUBROUTINES



The maximum number of special effects is 20.
MAXSE = 20

Figure A.1. Flowchart of Subroutine ADDSE

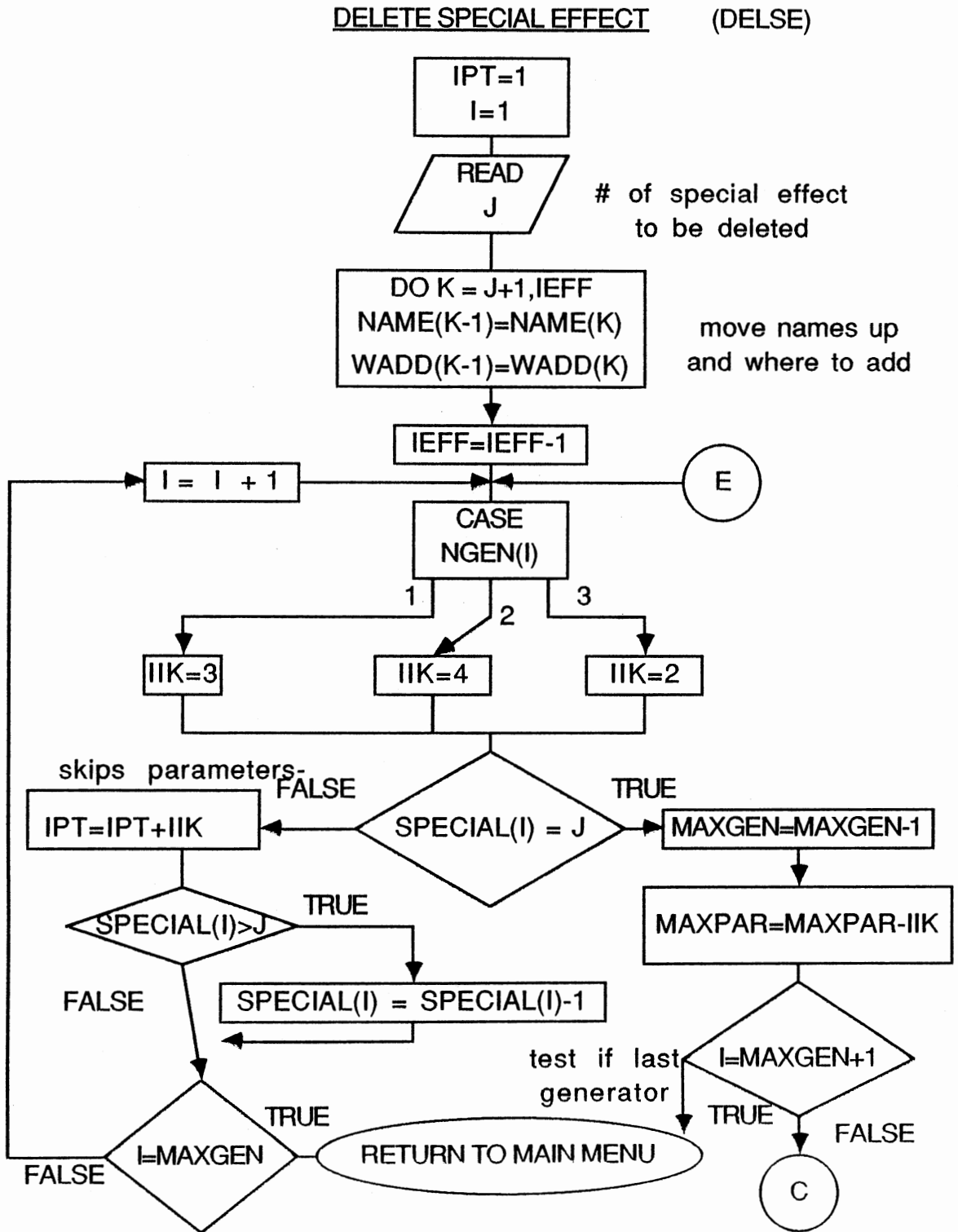


Figure A.2. Flowchart of Subroutine DELSE

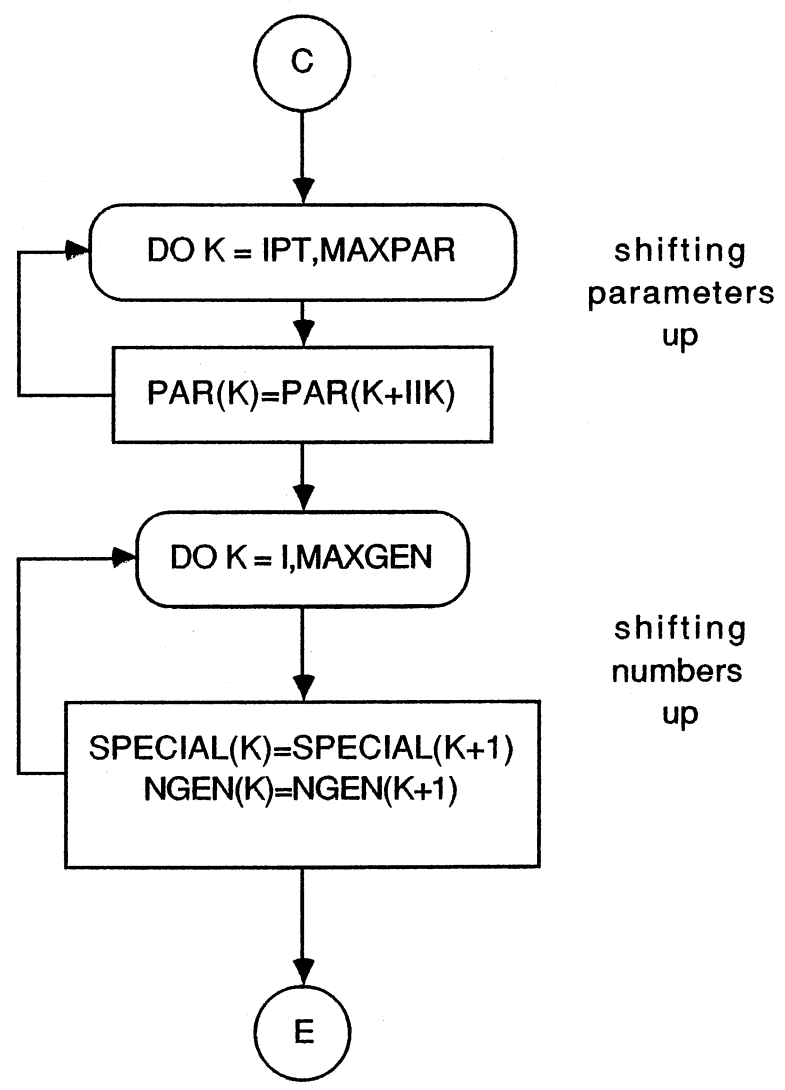


Figure A.2. (Continued)

CHANGE SPECIAL EFFECT
(CHGSE)

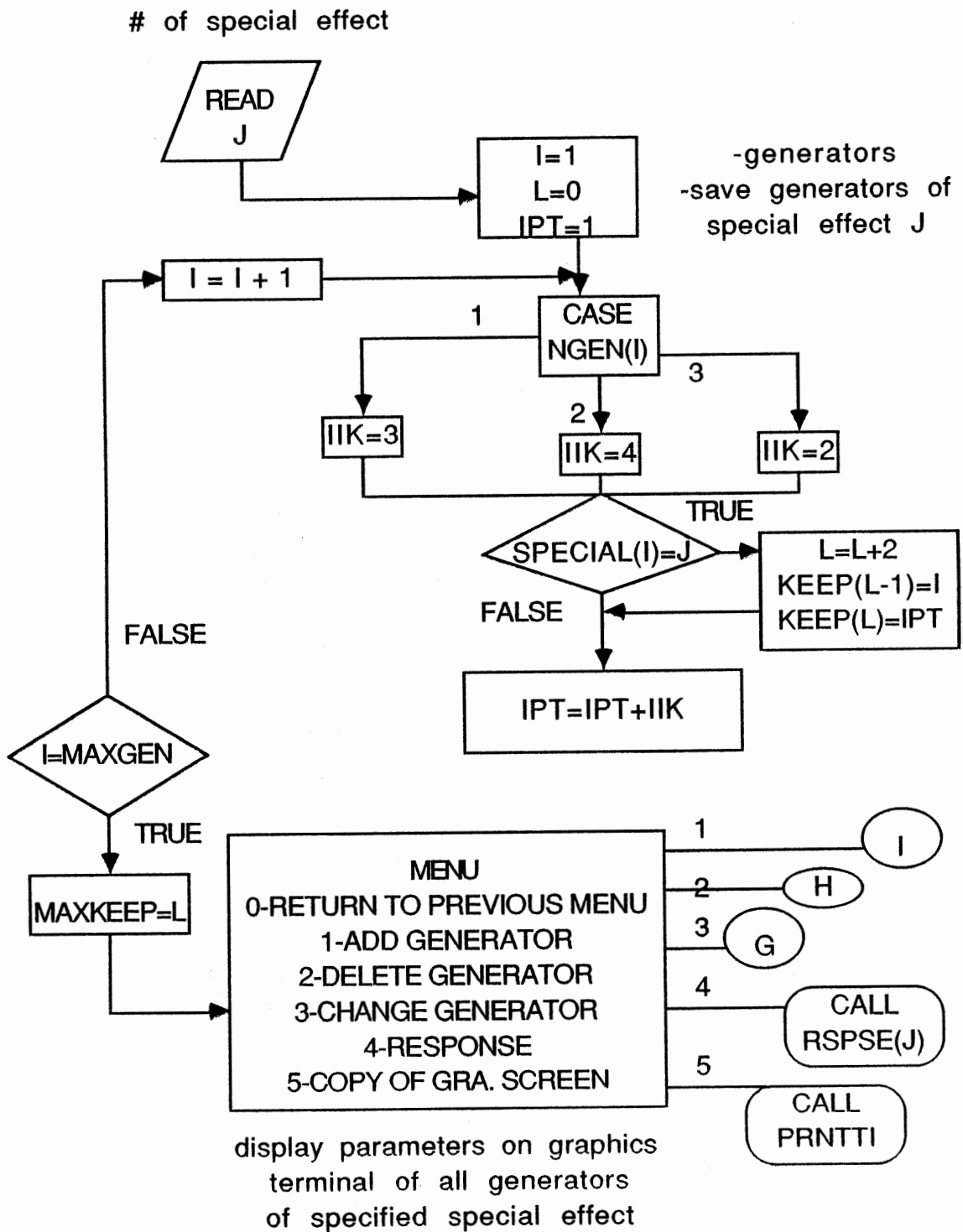


Figure A.3. Flowchart of Subroutine CHGSE

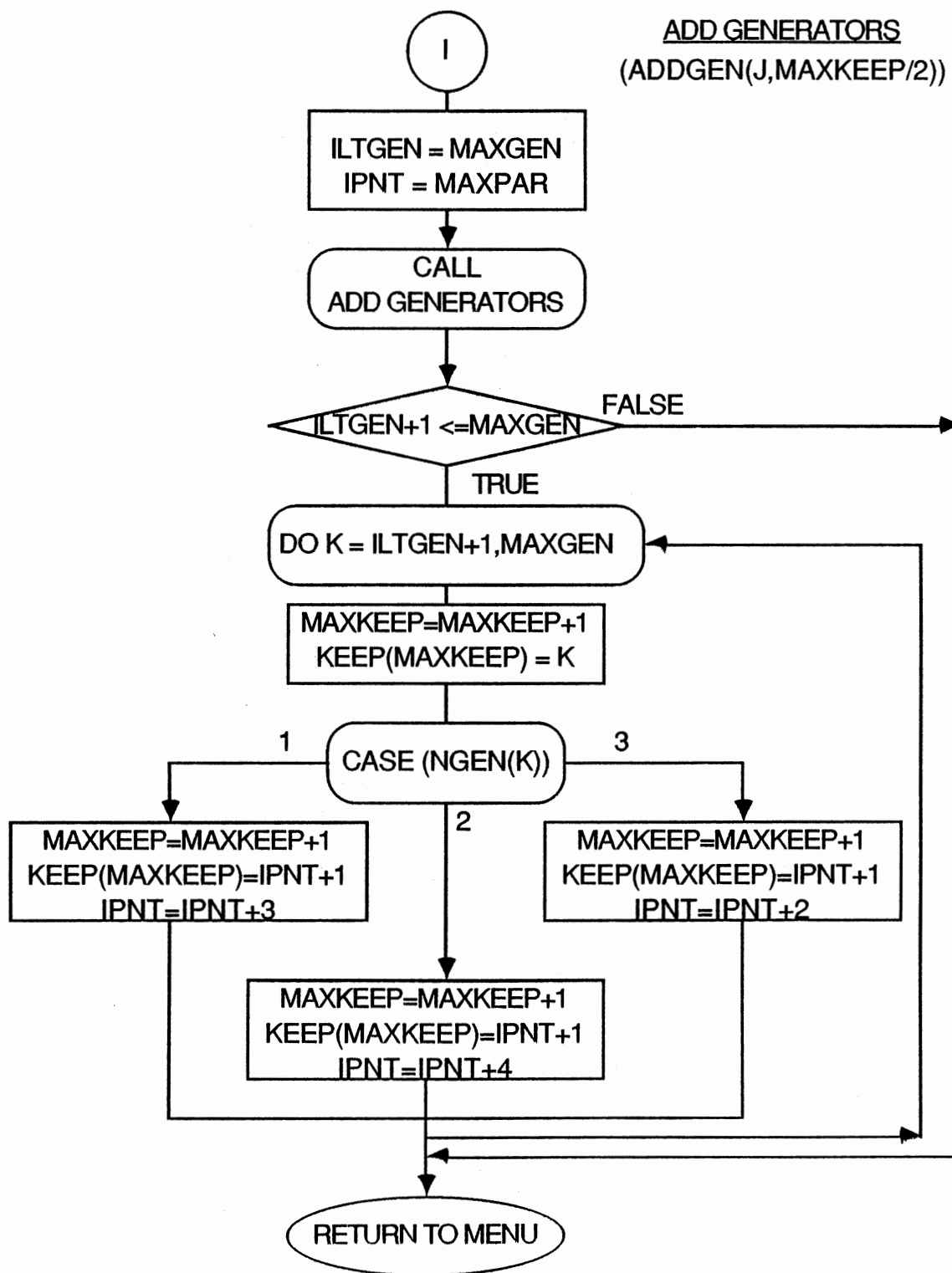


Figure A.3. (Continued)

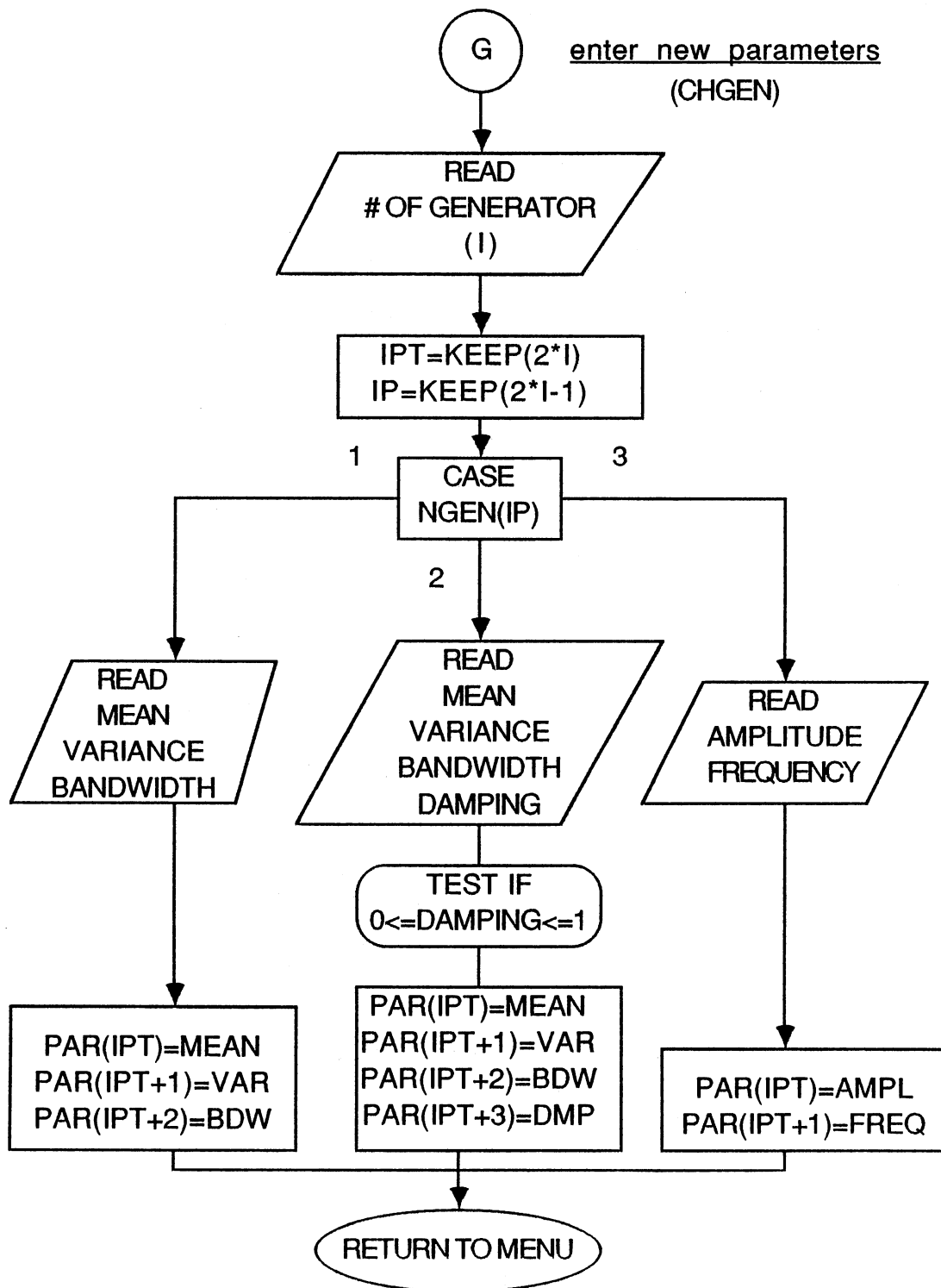


Figure A.3. (Continued)

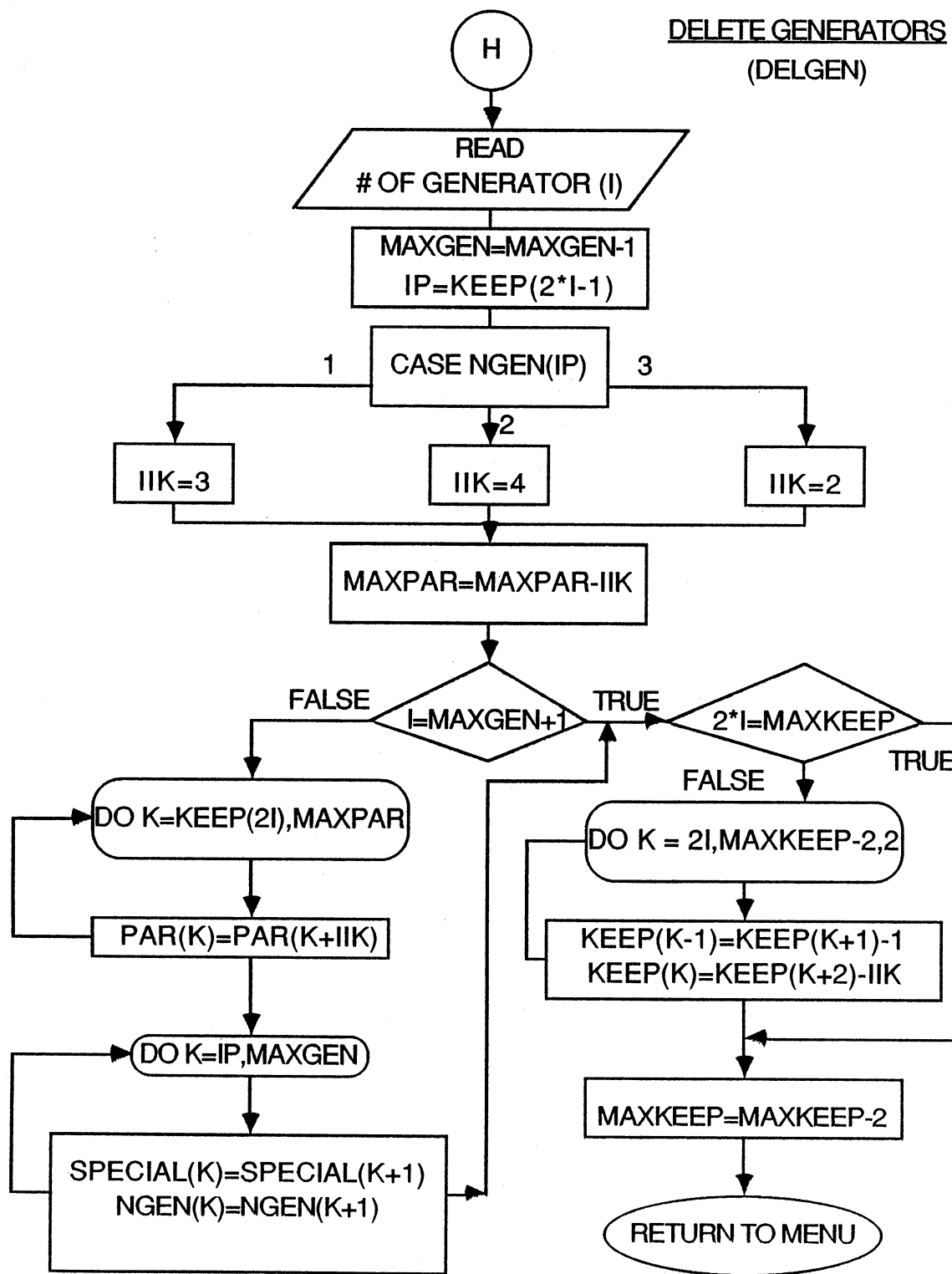


Figure A.3. (Continued)

RESPONSE OF SPECIAL EFFECT
(RSPSE(J))

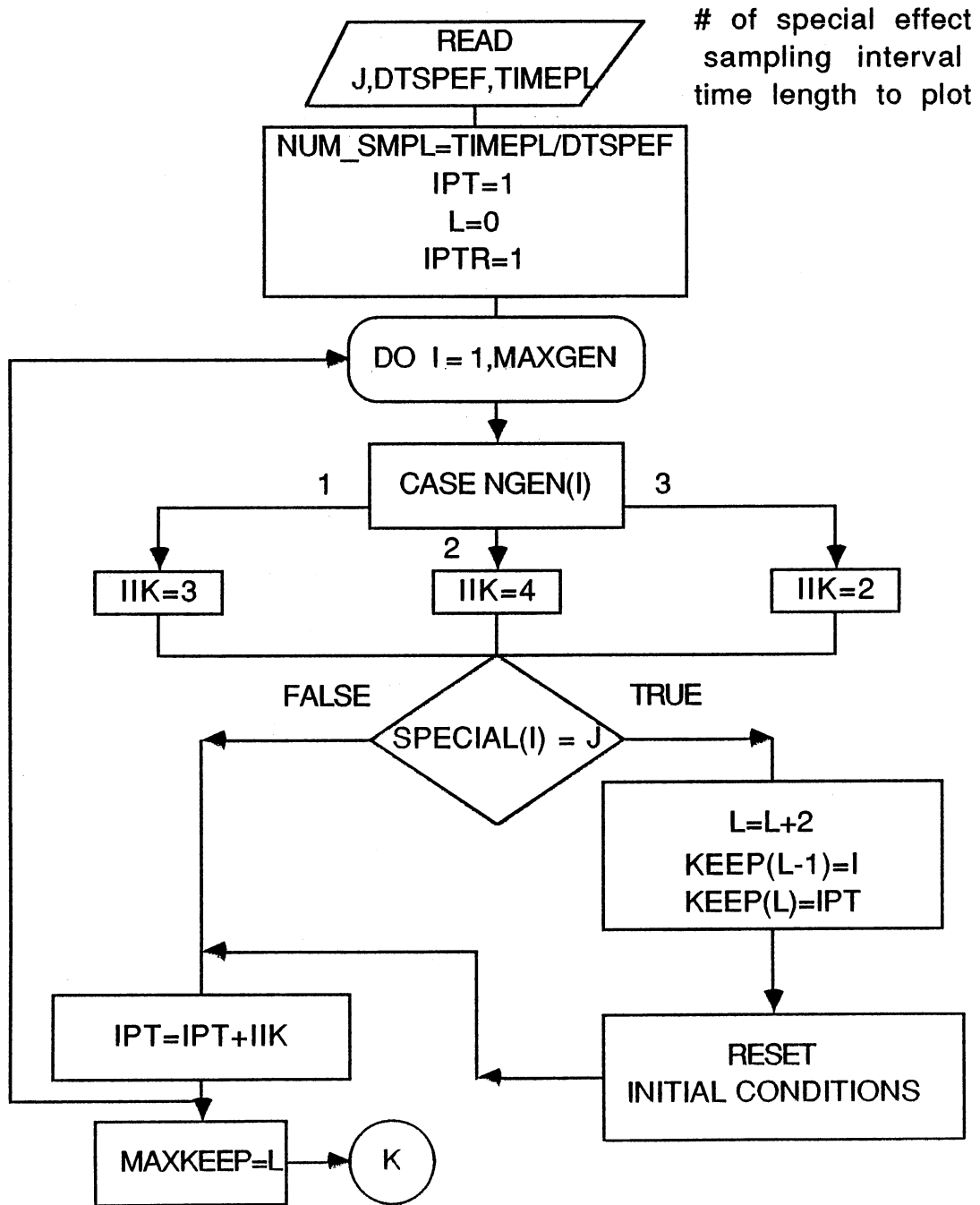


Figure A.4. Flowchart of Subroutine RSPSE

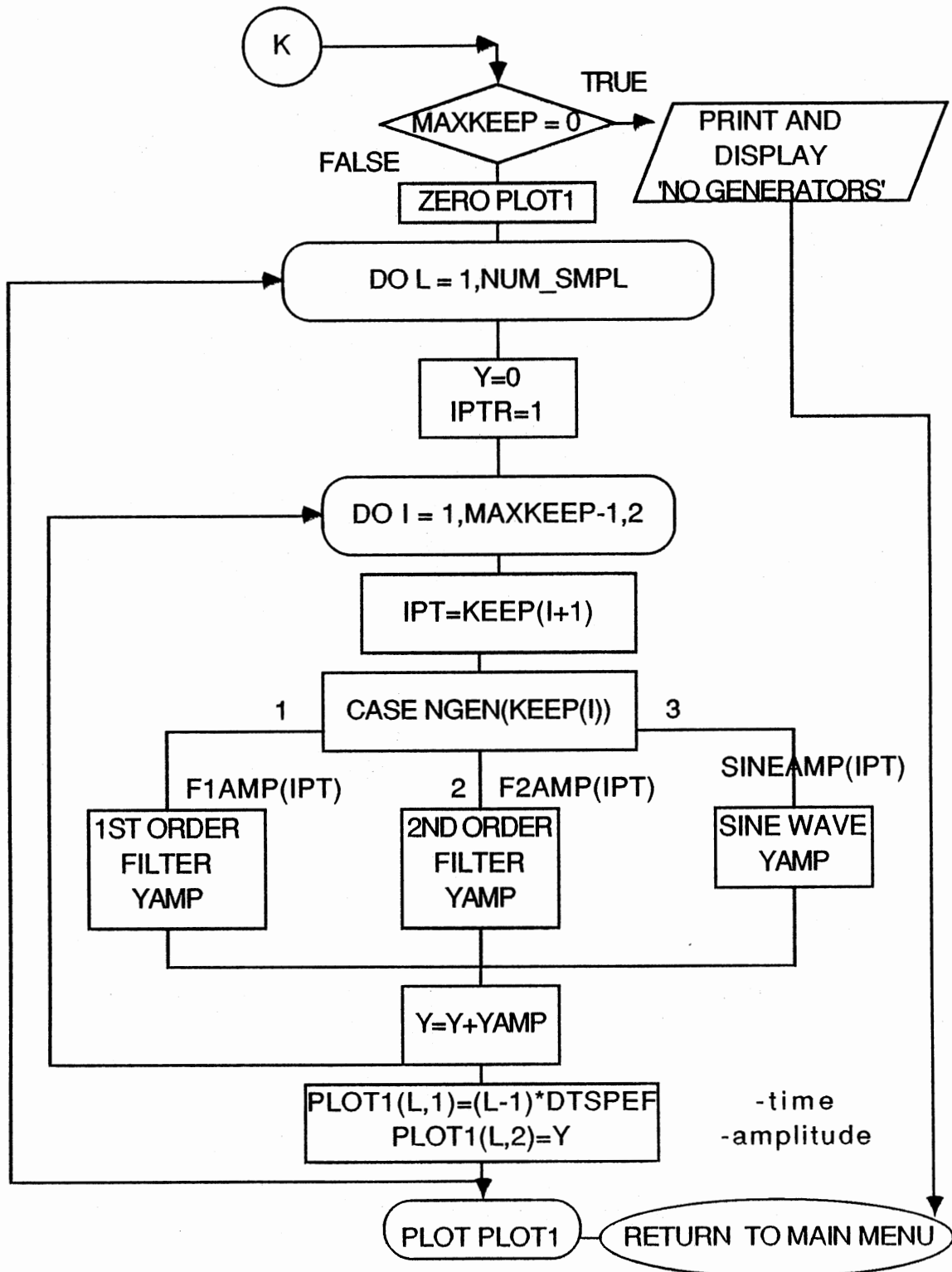
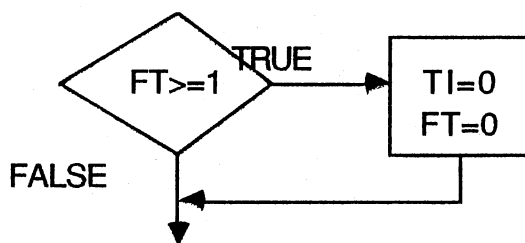


Figure A.4. (Continued)

SINE WAVE (SINEAMP(IPT))

A=PAR(IPT)
 F=PAR(IPT+1)
 IPT=IPT+2
 TI=PSTO(IPTR)
 FT=F*TI



YAMP=A*SIN(2*PI*FT)
 TI=TI+DTSPEF
 PSTO(IPTR)=TI
 IPTR=IPTR+1

WHITE NOISE GENERATOR (WHITE)

U=WHITE(M,V)

INIT=PSTO(IPTR)
 INIT=MOD(3125*INIT,65536)
 X=FLOAT(INIT)/65536.
 U=(X-0.5)*V+M
 PSTO(IPTR)=INIT

Figure A.5. Flowchart of Subroutines
 SINEAMP and WHITE

1ST ORDER FILTER (F1AMP(IPT))

```

M=PAR(IPT)
V=SQRT(12*PAR(IPT+1))
A=EXP(-DTSPEF*2*PI*PAR(IPT+2))
B=1-A
IPT=IPT+3
X1=PSTO(IPTR+1)
YAMP=X1
U=WHITE(M,V)
X1=A*X1+B*U
PSTO(IPTR+1)=X1
IPTR=IPTR+2

```

2ND ORDER FILTER

EQUATIONS I

```

AD(1,1)=(1-BW*DTSPEF)*TEMP
AD(2,1)=-SED*TEMP
AD(1,2)=-AD(2,1)*(BW**2)
AD(2,2)=(1+BW*DTSPEF)*TEMP
BD(1)=-[AD(1,1)-1+2*(Z/BW)*AD(1,2)]
BD(2)=-[AD(2,1)+2*(Z/BW)*(AD(2,2)-1)]

```

EQUATIONS II

```

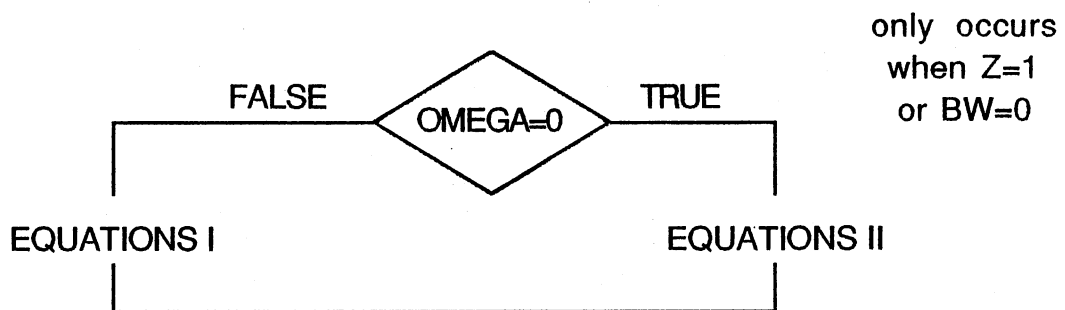
AD(1,1)=[COS(OMEGA*DTSPEF)-(ALPHA/OMEGA)*
SIN(OMEGA*DTSPEF)]*TEMP
AD(2,1)=-1/OMEGA*SIN(OMEGA*DTSPEF)*TEMP
AD(1,2)=-AD(2,1)*(BW**2)
AD(2,2)=[COS(OMEGA*DTSPEF)+(ALPHA/OMEGA)*
SIN(OMEGA*DTSPEF)]*TEMP
BD(1)=-[AD(1,1)-1+2*(ALPHA/(BW**2))*AD(1,2)]
BD(2)=-[AD(2,1)+2*(ALPHA/(BW**2))*(AD(2,2)-1)]

```

Figure A.6. Flowchart of Subroutine F1AMP and
Equations for Subroutine F2AMP

2ND ORDER FILTER (F2AMP(IPT))

M=PAR(IPT)
 V=SQRT(12*PAR(IPT+1))
 BW=2*PI*PAR(IPT+2)
 Z=PAR(IPT+3)
 IPT=IPT+4
 ALPHA=Z*BW
 OMEGA=BW*SQRT(1-Z**2)
 TEMP=EXP(-ALPHA*DTSPEF)



X1=PSTO(IPTR+1)
 X2=PSTO(IPTR+2)
 YAMP=X1
 U=WHITE(M,V)
 XU1=AD(1,1)*X1+AD(1,2)*X2+BD(1)*U
 XU2=AD(2,1)*X1+AD(2,2)*X2+BD(2)*U
 PSTO(IPTR+1)=XU1
 PSTO(IPTR+2)=XU2
 IPTR=IPTR+3

Figure A.7. Flowchart of Subroutine F2AMP

CHANGE NAME/WHERE TO ADD
SPECIAL EFFECT

(CHGWADD)

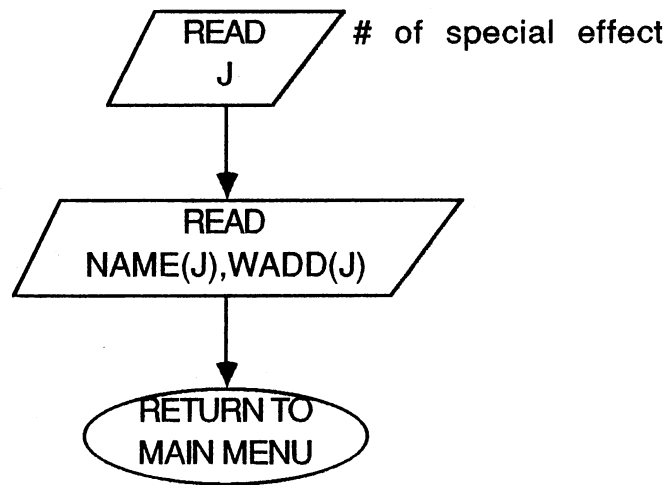


Figure A.8. Flowchart of Subroutine
CHGWADD

ADD GENERATORS
(ADDGEN(J,NUMGEN))

The maximum number of generators is:
 - 12 per effect
 - 240 overall

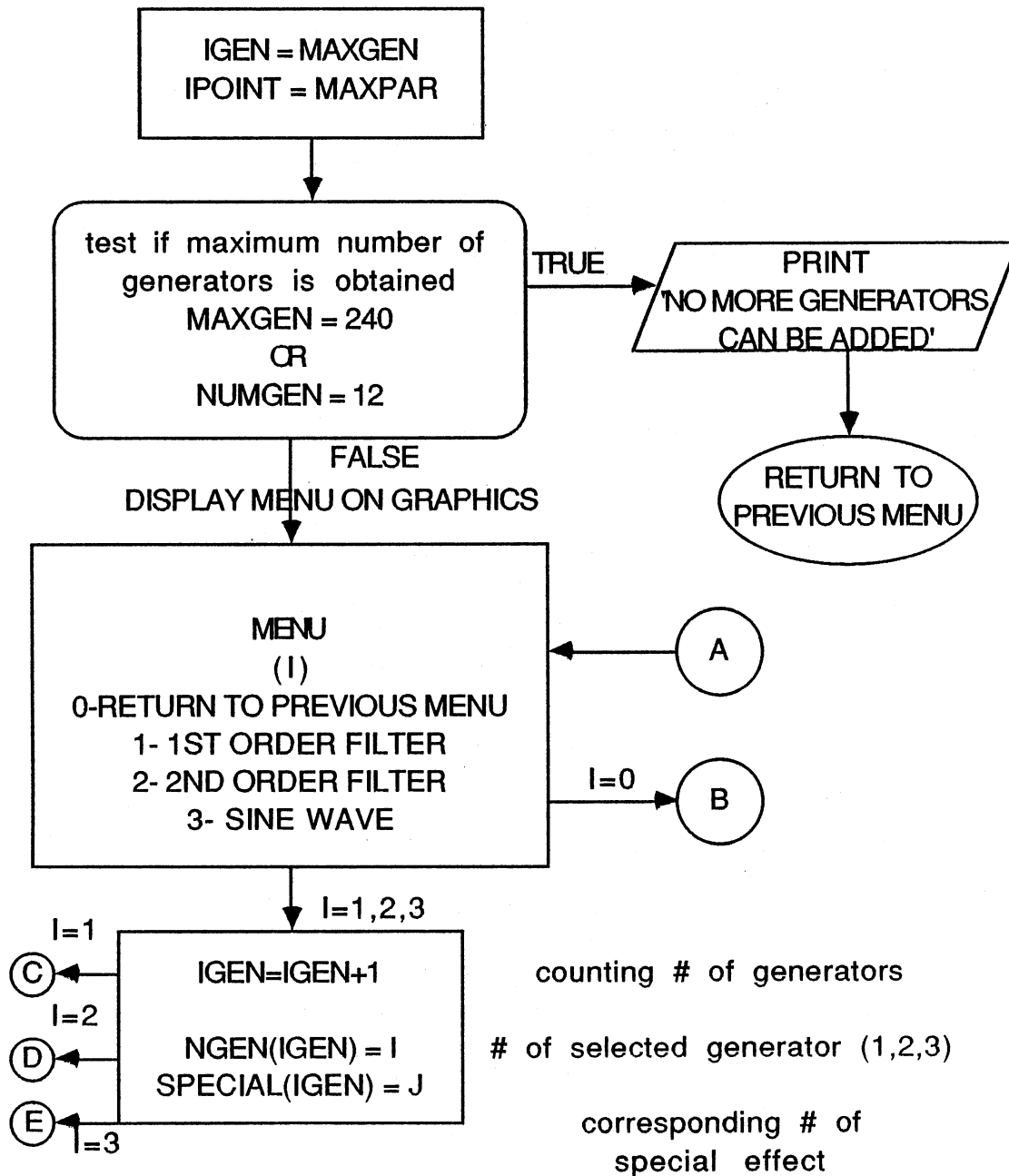


Figure A.9. Flowchart of Subroutine ADDGEN

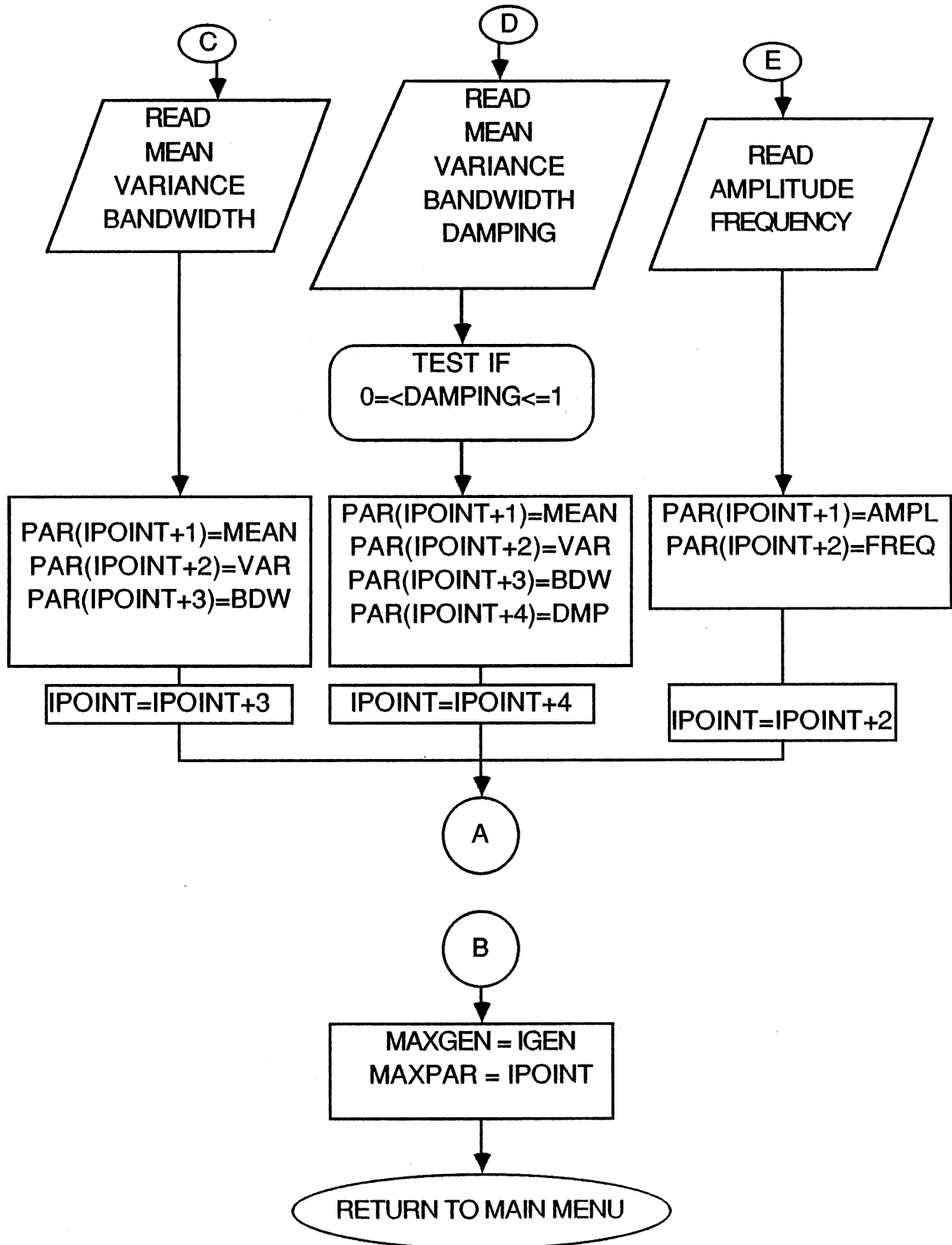


Figure A.9. (Continued)

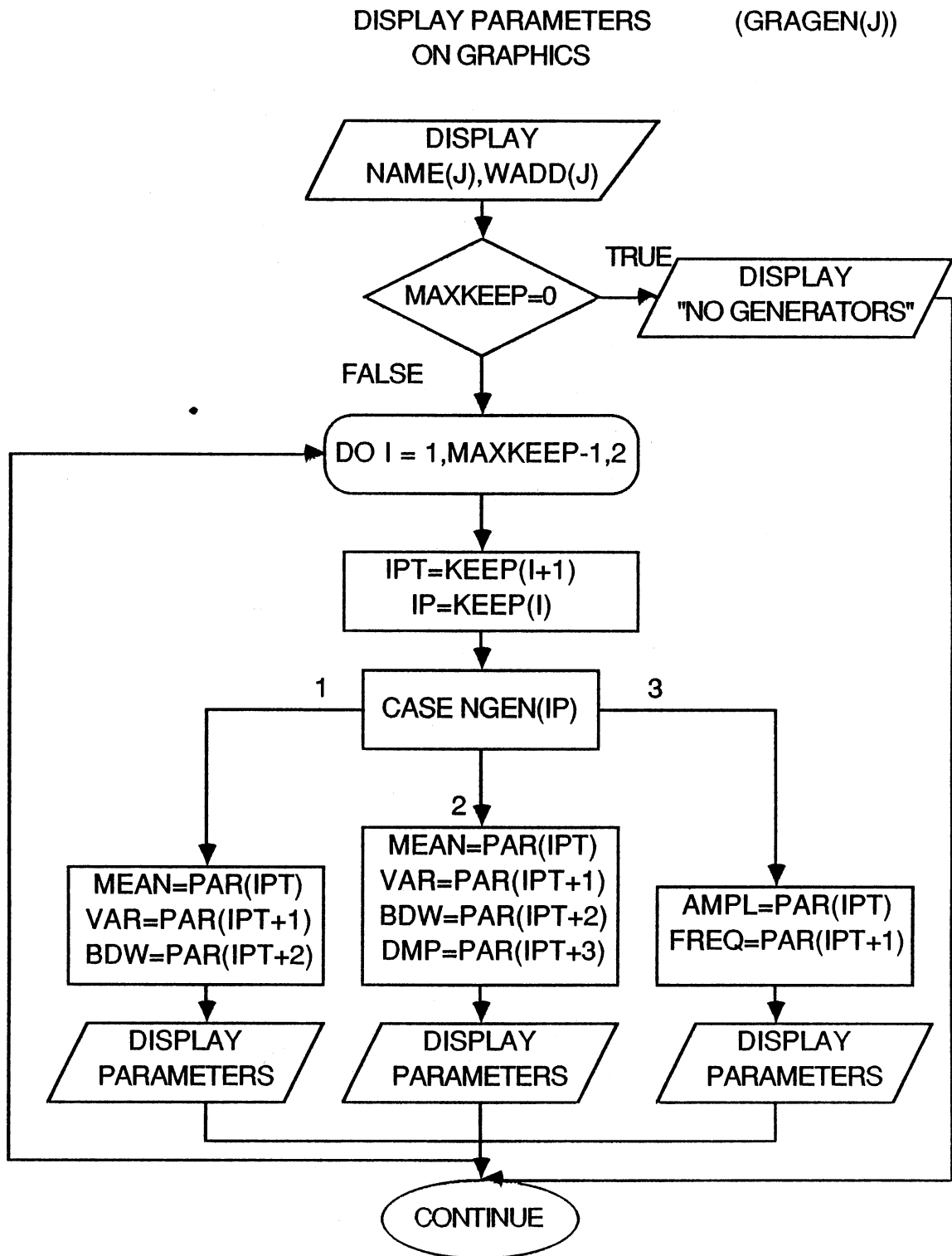


Figure A.10. Flowchart of Subroutine GRAGEN

GRAPHICS
LIST CURRENT SPECIAL EFFECTS
(GRAMENU)

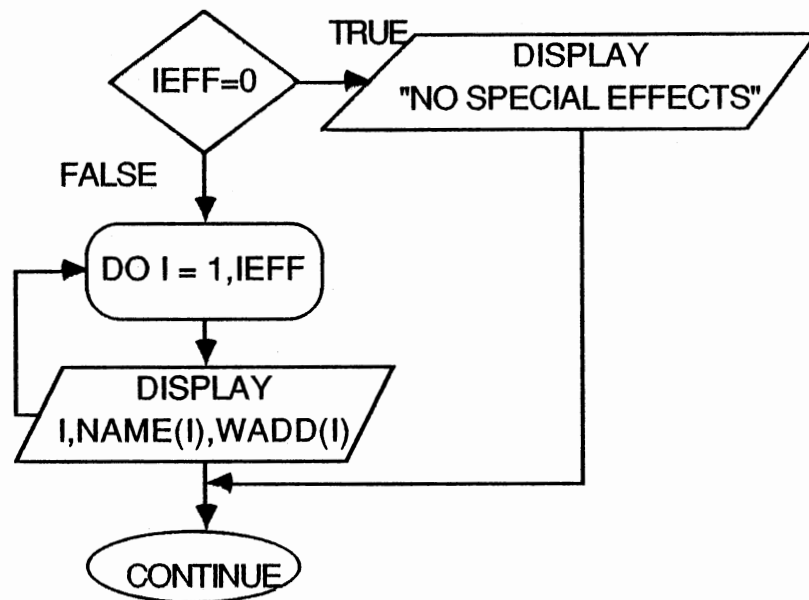


Figure A.11. Flowchart of Subroutine GRAMENU

APPENDIX B
EXAMPLE OF CALCULATION OF CONSTANT C
FOR VALVE FLOW

In this appendix an example is given on how to find the constant C of equation 6.1 (Chapter VI). The following equations are given from a two-stage flow control servovalve catalog [14]. The flow is given as a function of pressures:

$$Q = k i \sqrt{p_v} \quad (\text{B.1})$$

$$\text{So: } Q_r = k i_r \sqrt{p_s} \quad (\text{B.2})$$

where: Q - orifice flow

Q_r - rated flow

i_r - rated current

i - current

p_v - pressure drop across both orifices

$$= 2(p_s - p_1)$$

p_s - supply pressure

k - proportional constant

Dividing Q by Q_r the constant k is eliminated. Which yields:

$$\frac{Q}{Q_r} = \frac{i}{i_r} \sqrt{\frac{p_v}{p_s}} \quad (\text{B.3})$$

Replacing p_v in the above equation by $2(p_s - p_1)$ yields:

$$Q = Q_r \frac{i}{i_r} \sqrt{\frac{2(p_s - p_1)}{p_s}} \quad (\text{B.4})$$

Letting $x = k_m i$, k_m - proportional constant, yields:

$$Q = \frac{Q_r}{x_r \sqrt{p_s/2}} \sqrt{p_s - p_1} x \quad (\text{B.5})$$

Comparing equation B.5 with $Q = C \sqrt{p_s - p_1} x$ (equation 6.1)

yields:

$$C = \frac{Q_r}{x_r \sqrt{p_s/2}} \quad (\text{B.6})$$

Making: $p_s = 1000$ psi

$$Q_r = 4 \text{ gpm} = 15.4 \text{ in}^3/\text{s}$$

$$i_r = 10 \text{ mA and}$$

if $k_m = 0.1$ (for artificial position) then $x_r = 1$ in, since $x_r = k_m * i_r$.

Substituting these values in the equation B.6 the constant C is found to be $C = 0.6887 \text{ in}^2/\text{s} * (\text{psi})^{1/2}$.

The numbers used here do not necessarily correspond to a specific valve, but are used for demonstration purposes only.

APPENDIX C
PROGRAM LISTING

**** MAIN PROGRAM

**** PRIMARY MOTION COMMON BLOCKS

```

COMMON/CUEFILX/BXACCN,BAXA0,BAXA1,BAXA2,BAXA3
COMMON/CUEFILY/BYACCN,BAYA0,BAYA1,BAYA2,BAYA3
COMMON/CUEFILZ/BZACCN,BAZA0,BAZA1,BAZA2,BAZA3
COMMON/CUEFILQ/BAPITH,BQA0,BQA1,BQA2,BQA3
COMMON/CUEFILP/BAROLL,BPA0,BPA1,BPA2,BPA3
COMMON/CUEFILR/BAYAW,BRA0,BRA1,BRA2,BRA3
COMMON/USER1/BIN,NINP,INPNUM,NITER
DIMENSION BIN(2000,9),INPNUM(9)
COMMON/CTTRAN/FLTAXA,FLTAYA,FLTAZA
COMMON/CTROT/FQADOT,FPADOT,FRADOT,FQA,FPA,FRA
COMMON/GRAV1/BXALIN,BYALIN
COMMON/MPCP1/BXPOS,BYPOS,BZPOS,BTHPOS,BPHPOS,BSIPOS
COMMON/POSCON1/BMXPOS,BMYPOS,BMZPOS,BMTHP,BMPHIP,BMPSIP
COMMON/PRIM1/XENFL,YENFL,ZENFL,THENFL,PHENFL,SIENFL
COMMON/PRIM2/XGRFL,YGRFL,MPCPFL,MPLPFL
COMMON/PRIM3/BXAWTC,BYAWTC,BZAWTC,BTHWTC,BPHWTC,BSIWTC
COMMON/PRIM4/BKAX1,BKAY1,BKAZ1,BKQA1,BKPA1,BKRA1
COMMON/PRIM5/BKAX2,BKAY2,BKAZ2,BKQA2,BKPA2,BKRA2
COMMON/PRIM6/ALAGX,AKGAX,DLAGX,DKGAX,ALAGY,AKGAY,DLAGY,DKGAY
COMMON/PRIM7/BKQA4,BKPA4
COMMON/PRIM8/BLAGX,BLAGY,BLAGZ,BLAGT,BLAGP,BLAGS
INTEGER*4 XENFL,YENFL,ZENFL,THENFL,PHENFL,SIENFL
INTEGER*4 XGRFL,YGRFL,MPCPFL,MPLPFL
REAL BXAWTC,BYAWTC,BZAWTC,BTHWTC,BPHWTC,BSIWTC
REAL BKAX1,BKAY1,BKAZ1,BKQA1,BKPA1,BKRA1
REAL BKAX2,BKAY2,BKAZ2,BKQA2,BKPA2,BKRA2
REAL ALAGX,AKGAX,DLAGX,DKGAX,ALAGY,AKGAY,DLAGY,DKGAY
REAL BKQA4,BKPA4
REAL BLAGX,BLAGY,BLAGZ,BLAGT,BLAGP,BLAGS

```

**** SPECIAL EFFECTS COMMON BLOCKS

```

COMMON/SMSPE1/MAXGEN,MAXPAR,SPECIAL
COMMON/SMSPE2/IEFF,NAME,WADD
COMMON/SMSPE3/NGEN,PAR,IPOINT
COMMON/SMSPE4/MAXPSTO,IPTR,PSTO
COMMON/SMSPE5/KEEP,MAXKEEP
COMMON/SMSPE7/POX,IEFFLG

```

**** VALVE COMMON BLOCKS

```

COMMON/SMVAL1/DAMPM,BANDM,GAINM,XM1,XM2,XK,B,VRST
COMMON/SMVAL2/PS,PR
COMMON/SMVAL3/XL1,XL2,XL3,APT,VO,XLIMIT,FRC,BETA0
COMMON/SMVAL4/X,XDOT,PD,PDOT,XMOTOR,PISTON
COMMON/SMVAL5/VOU
COMMON/SMVAL6/CPRS,RPRS,POS1,Q6,Q7
COMMON/SMVAL7/Q1,Q2,Q3,Q4,Q5,V

```

**** SERVO COMMON BLOCKS

COMMON/SMSRV1/XKPM,XKP,SCLOT,XKFORC,DMPOFF,DMPON
 COMMON/SMSRV2/COMP1,COMP2,COMP3,COMP4,COMP5
 COMMON/SMSRV3/TEMP1,TEMP2,CYLOT,FORCE
 COMMON/SMSRV4/COMPN

**** SAVE COMMON BLOCKS

COMMON/SMDIS1/TMAX,NVSNPNT,NVAR,PLOTVP
 COMMON/SMDIS2/TINX,AFTER

LOTA

**** ANIMATE COMMON BLOCKS

COMMON/SMANI1/SIGNA

DIMENSION NGEN(240),PAR(1000),KEEP(1000),PSTO(1000)
 DIMENSION POSX(6),IEFFLG(20)
 INTEGER WADD(20),SPECIAL(240)
 CHARACTER NAME(20)*20
 DIMENSION X(6,2),XDOT(6,2),PD(6,4),PDOT(6,4)
 DIMENSION XMOTOR(4,5),PISTON(4,5)
 DIMENSION XM2(6),XK(6),B(6)
 DIMENSION VOUT(6)
 DIMENSION CPRS(6),RPRS(6),POSI(6),Q6(6),Q7(6)
 DIMENSION Q1(6),Q2(6),V(6,2),Q3(6),Q4(6),Q5(6)
 DIMENSION XKPM(6),XKP(6),SCLOT(6),XKFORC(6)
 DIMENSION COMP1(6),COMP2(6),COMP3(6),COMP4(6),COMP5(6)
 DIMENSION TEMP1(6),TEMP2(6),CYLOT(6),FORCE(6)
 DIMENSION NVAR(17),PLOTV(2000,18),PLOT(2000,6)
 DIMENSION SIGNA(6),COMPN(6)
 DIMENSION TINX(6),AFTER(6)
 CHARACTER CH*1

WHILE (1>0)

WRITE(9,*)

WRITE(9,*)

WRITE(9,*)

WRITE(9,(" MAIN MENU "))

WRITE(9,*)

WRITE(9,*)

WRITE(9,(" 0.END "))

CC WRITE(9,(" 1. PRIMARY MOTION (NOT AVAILABLE) "))

WRITE(9,(" 1. SPECIAL EFFECTS "))

WRITE(9,(" 2. SET UP SERVO "))

WRITE(9,(" 3. SET UP VALVE "))

WRITE(9,(" 4. SIMULATION "))

WRITE(9,(" 5. READ FILE "))

WRITE(9,(" 6. SAVE FILE "))

WRITE(9,*)

WRITE(9,*)

WRITE(9,(" ENTER YOUR SELECTION "))

WRITE(9,*)

```

WRITE(9,*)
ICH = 1000
READ(9,*) ICH
SELECT CASE (ICH)
CASE (0)
EXIT
CCC CASE (1)
CCC CH = '_'
CCC WRITE(9,('"YOU HAVE SELECTED: "PRIMARY MOTION"'))
CCC WRITE(9,('" <CR> TO RETURN - ANYTHING TO CONTINUE"'))
CCC READ(9,*) CH
CCC IF (CH.NE. '_') CALL WASHOUT2
CASE (1)
CALL SEMMENU
CASE(2)
CALL SERVO
CASE (3)
CALL VALVE
CASE (4)
CALL TSIMUL
CASE (5)
CALL FILERD
CASE (6)
CALL FILESV
CASE DEFAULT
WRITE(9,('" ILLEGAL CHOICE - SELECT AGAIN"'))
END SELECT
REPEAT
STOP
END

```

```

*****
***** SUBROUTINE FOR BASE MOVEMENT ANIMATION
*****
SUBROUTINE ANIMATE

COMMON/SMDIS1/TMAX,NVS,NPNT,NVAR,PLOTV,PLOTA

DIMENSION NVAR(17),PLOTV(2000,18),PLOTA(2000,6)

WHILE (1>0)
WRITE(9,*)
WRITE(9,*)
WRITE(9,('"          BASE ANIMATION MENU          "'))
WRITE(9,*)
WRITE(9,*)
WRITE(9,('" 0. RETURN TO PREVIOUS MENU          "'))
WRITE(9,('" 1. ANGLE VIEW OF BASE              "'))
WRITE(9,('" 2. TOP VIEW OF BASE                 "'))
WRITE(9,('"                               WRITE(9,*) 3.SIDEVIEWOFBASE  "'))
WRITE(9,('" 4. FRONT VIEW OF BASE              "'))
WRITE(9,*)
WRITE(9,*)

```

```

WRITE(9,(' ENTER YOUR SELECTION  '))
WRITE(9,*)
WRITE(9,*)

```

***** READ SELECTION

```

ICH = 1000
READ(9,*) ICH
SELECT CASE (ICH)
CASE (0)
RETURN
CASE (1)
IXVW=-15 ; IYVW=15 ; I1=-40 ; I2=0 ; I3=0
CASE (2)
IXVW=-90 ; IYVW=0 ; I1=-40 ; I2=0 ; I3=120
CASE (3)
IXVW=0 ; IYVW=90 ; I1=0 ; I2=0 ; I3=135
CASE (4)
IXVW=0 ; IYVW=0 ; I1=-40 ; I2=0 ; I3=0
CASE DEFAULT
WRITE(9,('ILLEGAL CHOICE'))
WRITE(9,('MAKE ANOTHER SELECTION'))
END SELECT

```

**** CONVERSION FACTOR TO DRAWING COORDINATES

```

CONDRW = 3.033

```

**** INITIALIZE GRAPHICS SCREEN

```

CALL PLTINIT
CALL PLOT(0)
CALL VWIDEN

```

**** VIEWER REFERENCE POINT

```

CALL VWRPT(I1,I2,I3)

```

**** VIEWER ROTATION

```

CALL VWROTX(IXVW)
CALL VWROTY(IYVW)

```

**** DRAWS LOWER BASE

**** FIRST POINT IN LOWER BASE - FRONT LEFT HAND VERTIX

```

CALL MOVE3(70,15,0)
CALL COLOR(131)

```

**** DRAW THE THICKNESS

```

DO (J = 1,20)
CALL POLYR3(6,0,0,0,348,0,0,358,0,-17,184,0,-319,164,0,-319,

```

```

+      -10,0,-17)
  CALL MDTRAN(0,1,0)
  REPEAT

  CALL PRMFIL(1)
  CALL COLOR(45)
  CALL POLYR3(6,0,0,0,348,0,0,358,0,-17,184,0,-319,164,0,-319,
+      -10,0,-17)
  CALL PRMFIL(0)

  DO (II=1, NPNT)

*** CONVERSION OF X,Y,Z TO DRAWING COORDINATES

  IX=NINT(PLOTA(II,2)*CONDRW)
  IY=NINT(-PLOTA(II,3)*CONDRW)+200
  IZ=NINT(PLOTA(II,1)*CONDRW)

  IAX=NINT(((180./3.1416)*(-PLOTA(II,4))))
  IAY=NINT(((180./3.1416)*(-PLOTA(II,6))))
  IAZ=NINT(((180./3.1416)*(-PLOTA(II,5))))

**** DRAW UPPER BASE AND ERASE IT

  CALL MDIDEN

**** (244,35,-112) CENTER OF LOWER BASE
**** (IXO,IYO,IZO) CENTER OF UPPER BASE AFTER MOVEMENT

  IXO=IX+244
  IYO=IY+35
  IZO=IZ-112
  CALL MDORG(IXO,IYO,IZO)

**** ROTATE WRT ORIGIN IN UPPER BASE

  CALL MDROTX(IAX)
  CALL MDROTY(IAY)
  CALL MDROTZ(IAZ)
  CALL MOVE3(244,35,-112) | CENTER OF LOWER BASE
  CALL MOVER3(IX,IY,IZ) | CENTER OF UPPER BASE

**** FIRST POINT IN LOWER BASE - FRONT RIGHT HAND VERTIX

  CALL MOVER3(10,0,156)
  CALL COLOR(210)
  CALL POLYR3(6,0,0,0,130,0,-226,120,0,-242,-140,0,-242,
+      -150,0,-226,-20,0,0)
  CALL MOVE3(244,35,-112)
  CALL MOVER3(IX,IY,IZ)
  CALL MOVER3(10,0,156)
  CALL COLOR(0)
  CALL POLYR3(6,0,0,0,130,0,-226,120,0,-242,-140,0,-242,

```

```

+          -150,0,-226,-20,0,0)
  CALL PRMFIL(0)
          REPEAT
REPEAT
END

*****
***** SUBROUTINE TO CHANGE PARAMETERS
*****
SUBROUTINE CHGPAR

**** DISPLAY MENU FOR CHANGE IN PARAMETERS

  WHILE (1>0)
    WRITE(9,*)
    WRITE(9,*)
    WRITE(9,("      CHANGE/VIEW PARAMETERS MENU  "))
    WRITE(9,*)
    WRITE(9,*)
    WRITE(9,("  0. RETURN TO PREVIOUS MENU  "))
CCC  WRITE(9,("    1. PRIMARY MOTION (NOT AVAILABLE)")
    WRITE(9,("    1. SPECIAL EFFECTS      "))
    WRITE(9,("    2. SERVO          "))
    WRITE(9,("    3. VALVE          "))
    WRITE(9,*)
    WRITE(9,*)
    WRITE(9,("      ENTER YOUR SELECTION  "))
    WRITE(9,*)
    WRITE(9,*)
**** READ SELECTION
    ICH = 1000
    READ(9,*) ICH
    SELECT CASE (ICH)
      CASE 0
        EXIT
CCC  CASE (1)
CCC  CALL CHGPM
    CASE (1)
    CALL GRAMENU  IGRAPHICS-MENU OF CURRENT SPECIAL EFF.
    CALL CHGSE
    CASE (2)
    CALL CHGSRV
    CASE (3)
    CALL CHGVAL
    CASE DEFAULT
    WRITE(9,("ILLEGAL CHOICE"))
    WRITE(9,("MAKE ANOTHER SELECTION"))
    END SELECT
  REPEAT
  RETURN
END

```

```
*****
```

***** SUBROUTINE TO CHANGE SERVO PARAMETERS

SUBROUTINE CHGSRV

COMMON/SMSRV1/XKPM,XKP,SCLOT,XKFORC,DMPOFF,DMPON
COMMON/SMSRV2/COMP1,COMP2,COMP3,COMP4,COMP5

DIMENSION XKPM(6),XKP(6),SCLOT(6),XKFORC(6)
DIMENSION COMP1(6),COMP2(6),COMP3(6),COMP4(6),COMP5(6)
CHARACTER CH*1

WRITE(9,('YOU HAVE SELECTED: "CHANGE SERVO PARAMETERS"'))
WRITE(9,('<CR> TO RETURN - ANYTHING TO CONTINUE'))

CH=''

READ(9,*) CH
IF (CH.EQ. '_') RETURN

WRITE(9,*)
WRITE(9,('ENTER SERVO PARAMETERS - <CR> FOR NO CHANGE'))
WRITE(9,*)

WRITE(9,('COMMANDED POSITION GAIN: '))

WRITE(9,('6E12.5')) (XKPM(I),I=1,6)

READ(9,*) (XKPM(I),I=1,6)

WRITE(9,*)

WRITE(9,('FEEDBACK POSITION GAIN: '))

WRITE(9,('6E12.5')) (XKP(I),I=1,6)

READ(9,*) (XKP(I),I=1,6)

WRITE(9,*)

WRITE(9,('SCALE FOR VALVE VOLTAGE (mV/in):'))

WRITE(9,('6E12.5')) (SCLOT(I),I=1,6)

READ(9,*) (SCLOT(I),I=1,6)

WRITE(9,*)

WRITE(9,('DIFFERENTIAL PRESSURE GAIN: '))

WRITE(9,('6E12.5')) (XKFORC(I),I=1,6)

READ(9,*) (XKFORC(I),I=1,6)

WRITE(9,*)

WRITE(9,('COMPENSATION GAINS #1: '))

WRITE(9,('6E12.5')) (COMP1(I),I=1,6)

READ(9,*) (COMP1(I),I=1,6)

WRITE(9,('COMPENSATION GAINS #2: '))

WRITE(9,('6E12.5')) (COMP2(I),I=1,6)

READ(9,*) (COMP2(I),I=1,6)

WRITE(9,('COMPENSATION GAINS #3: '))

WRITE(9,('6E12.5')) (COMP3(I),I=1,6)

READ(9,*) (COMP3(I),I=1,6)

WRITE(9,('COMPENSATION GAINS #4: '))

WRITE(9,('6E12.5')) (COMP4(I),I=1,6)

READ(9,*) (COMP4(I),I=1,6)

WRITE(9,('COMPENSATION GAINS #5: '))

WRITE(9,('6E12.5')) (COMP5(I),I=1,6)

READ(9,*) (COMP5(I),I=1,6)

WRITE(9,('2 DAMPING FADE LIMITS (HIGHER FIRST)'))

WRITE(9,('2E12.5')) DMPON,DMPOFF

READ(9,*) DMPON,DMPOFF

RETURN
END

***** SUBROUTINE TO CHANGE VALVE PARAMETERS

SUBROUTINE CHGVAL

COMMON/SMVAL1/DAMPM,BANDM,GAINM,XM1,XM2,XK,B,VRST
COMMON/SMVAL2/PS,PR
COMMON/SMVAL3/XL1,XL2,XL3,APT,VO,XLIMIT,FRC,BETAO

DIMENSION XM2(6),XK(6),B(6)
CHARACTER CH*1

WRITE(9,('YOU HAVE SELECTED: "CHANGE VALVE PARAMETERS"'))
WRITE(9,(<CR> TO RETURN ANYTHING TO CONTINUE) U2))
CH = ' _'
READ(9,*) CH
IF (CH .EQ. ' _') RETURN
WRITE(9,('ENTER VALVE PARAMETERS - <CR> FOR NO CHANGE'))
WRITE(9,('MOTOR SPECIFICATIONS'))
WRITE(9,('DAMPING: ",E11.5)') DAMPM
READ(9,*) DAMPM
WHILE ((DAMPM .LT. 0) .OR. (DAMPM .GT. 1.0))
WRITE(9,*)
WRITE(9,('ILLEGAL DAMPING RATIO'))
READ(9,*) DAMPM
REPEAT
WRITE(9,('BANDWIDTH (Hz): ",E11.5)') BANDM
READ(9,*) BANDM
WRITE(9,('GAIN (in/mA): ",E11.5)') GAINM
READ(9,*) GAINM
WRITE(9,('RESISTANCE (ohms): ",E11.5)') VRST
READ(9,*) VRST
WRITE(9,*)
WRITE(9,*)
WRITE(9,('VALVE SPECIFICATIONS'))
WRITE(9,('SUPPLY PRESSURE (psi): ",E11.5)') PS
READ(9,*) PS
WRITE(9,('RETURN PRESSURE (psi): ",E11.5)') PR
READ(9,*) PR
WRITE(9,('LEAKAGE FLOW CONSTANT (in³/(s*psi)): "'))
WRITE(9,(3E15.5)') XL1,XL2,XL3
READ(9,*) XL1,XL2,XL3
WRITE(9,('APERTURE (in²): ",E11.5)') APT
READ(9,*) APT
WRITE(9,('TOTAL EFFECTIVE VOLUME (in³): ",E11.5)') VO
READ(9,*) VO
WRITE(9,('LIMIT OF SPOOL POSITION (in): ",E11.5)') XLIMIT
READ(9,*) XLIMIT
WRITE(9,('FLOW RATE CONSTANT: ",E11.5)') FRC
READ(9,*) FRC

```

WRITE(9,*)
WRITE(9,*)
WRITE(9,('OIL SPECIFICATIONS'))
WRITE(9,('BULK MODULUS (psi): ",E11.5)') BETAO
READ(9,*) BETAO
WRITE(9,*)
WRITE(9,*)
WRITE(9,('MASS OF CYLINDER (lb): ",E11.5)') XM1
READ(9,*) XM1
WRITE(9,*)
WRITE(9,*)
WRITE(9,('MODEL OF MOTION BASE'))
WRITE(9,('MASS OF BASE FOR EACH CYLINDER (lb): "))
WRITE(9,('6E13.5)') (XM2(I),I=1,6)
READ(9,*) (XM2(I),I=1,6)
WRITE(9,('SPRING CONSTANT FOR EACH CYLINDER (lb/in): "))
WRITE(9,('6E13.5)') (XK(I),I=1,6)
READ(9,*) (XK(I),I=1,6)
WRITE(9,('DAMPING COEFF. FOR EACH CYLINDER(lb/(in/s): "))
WRITE(9,('6E13.5)') (B(I),I=1,6)
READ(9,*) (B(I),I=1,6)
RETURN
END

```

```

*****
***** SUBROUTINE TO DISPLAY RESULTS
***** PLOT SELECTED VARIABLES
*****
SUBROUTINE DISRES

COMMON/SMDIS1/TMAX,NVS,NPNT,NVAR,PLOTV,PLOTA

DIMENSION NVAR(17),PLOT1(2000,9),PLOTV(2000,18),PLOTA(2000,6)
DIMENSION IFLAG(8),VSCL(20)
CHARACTER VNAME(20)*30,VSYMBOL(20)*6
CHARACTER PNAME(8)*6,PSYMBOL(8)*1,XLABEL*4,YLABEL*6,HEADER*20

**** READ NAMES OF VARIABLES TO BE PLOTTED FROM FILE TABLE
OPEN(UNIT=17,FILE='TABLE.SA')
READ(17,*)
READ(17,*)
I = 1
WHILE (I .LE. NVS)
  READ(17,('I4,T10,A6,T20,A25,T50,F7.3)') ,END=10)
+   IA,VSYMBOL(I),VNAME(I),VSCL(I)
  IF (IA .EQ. NVAR(I)) I = I + 1
REPEAT
10 CONTINUE
CLOSE (17)

WHILE (1>0)
  WRITE(9,*)
  WRITE(9,*)

```

```

WRITE(9,*)
WRITE(9,*)
WRITE(9,(' DISPLAY RESULTS'))

*** ZERO FLAGS TO IDENTIFY VARIABLES TO BE PLOTTED

DO (I = 1,8)
  IFLAG(I) = 0
REPEAT

WRITE(9,*)
WRITE(9,(' 0. RETURN TO PREVIOUS MENU",T36,
+      "(DEFAULT)"))
+ WRITE(9,(' 1. TIME",T36,"(X AXIS)"))
DO (J = 1,NVS)
  J1=J+1
  WRITE(9,('I3,". ",A30,T36,"(",A6,")"))
+      J1,VNAME(J),VSYMBOL(J)
REPEAT
WRITE(9,*)
WRITE(9,('ENTER YOUR CHOICES (MAX 8 VARIABLES):'))
READ(9,*) (IFLAG(I),I=1,8)

IF (IFLAG(1) .EQ. 0) RETURN

**** CHOOSE TIME INTERVAL

WRITE(9,*)
WRITE(9,('ENTER TIME INTERVAL'))
WRITE(9,(' DEF = TOTAL TIME OF SIMULATION'))

**** TBEGIN: TIME OF BEGINNING
**** TEND: TIME OF END OF INTERVAL

TBEGIN = 0
TEND = TMAX
READ(9,*) TBEGIN,TEND

**** NO INTERVALS OUT OF RANGE

WHILE((TBEGIN.LT.0).OR.(TEND.GT.TMAX)
+      .OR. (TBEGIN .GE. TEND))
  WRITE(9,('INTERVAL OUT OF RANGE'))
  WRITE(9,('ENTER TIME INTERVAL AGAIN'))
  TBEGIN = 0
  TEND = TMAX
  READ(9,*) TBEGIN,TEND
REPEAT

**** CALCULATE - NPBEGIN: NUMBER OF POINT TO BEGIN AT
****      NPEND: NUMBER OF POINT TO END AT

IF ((TBEGIN .EQ. 0) .AND. (TEND .EQ. TMAX)) THEN

```

```

NPBEGIN = 1
NPEND = NPNT
ELSE
NPBEGIN = NINT(TBEGIN*NPNT/TMAX) + 1
NPEND = NINT(TEND*NPNT/TMAX)
ENDIF

```

**** NPOINT: NUMBER OF POINTS IN THE INTERVAL

```

NPOINT = NPEND - NPBEGIN + 1

```

```

NVPLT = 0      ICOUNTER OF VARIABLES TO PLOT
DO (I=1,8)
  IF (IFLAG(I) .EQ. 0) EXIT
  NVPLT = NVPLT + 1
  TEMP = 1.

```

**** SET VARIABLE NAMES TO PLOT, PRINT OR DISPLAY

```

IF ((IFLAG(I) .NE. 1) .OR. (I .NE. 1)) THEN
  RNAME(I) = VSMBOL(IFLAG(I)-1)
  PSYMBOL(I-1) = CHAR(I-1+ICHAR('0'))
  TEMP = VSCL(IFLAG(I)-1)
ENDIF

```

**** SET NEW ARRAY TO PLOT

```

IK = 1
DO (K=NPBEGIN, NPEND)
  PLOT1(IK, I) = TEMP * PLOTV(K, IFLAG(I))
  IK = IK + 1
REPEAT
REPEAT

```

**** CHOOSE TO PLOT, PRINT OR DISPLAY DATA

```

WRITE(9,*)
WRITE(9,*)
WRITE(9,*)
WRITE(9,*)
WRITE(9,*)
WRITE(9,(" 1. PLOT THE DATA (DEFAULT)"))
WRITE(9,(" 2. DISPLAY DATA ON SCREEN "))
WRITE(9,(" 3. PRINT DATA"))
WRITE(9,*)
WRITE(9,(" ENTER YOUR SELECTION "))
ICH = 1
READ(9,*) ICH
SELECT CASE (ICH)
CASE (1)
  YLABEL = 'OUTPUT'
  XLABEL = 'TIME'
  CALL NAMEPLOT(HEADER)

```

```

      CALL PLOTSIM(PLOT1,NVPLT-1,NPOINT,HEADER,XLABEL,YLABEL,
+         PNAME,PSYMBOL)
      CASE (2)
      FNMULT.                                LE5THEN
      IK = 1
      ELSE
      IK = 2
      ENDIF
      DO (IJ=1,IK)
      IJL = IJ*5 ; IJF = IJL - 4
      IF (NVPLT .LT. IJL) IJL = NVPLT
      IF (IFLAG(1) .EQ. 1) THEN
      IJF = IJ*(IJ+1)
      WRITE(9,('    TIME ',4A13))
+         (PNAME(I),I=IJF-1,IJL-1)
      DO (K=1,NPOINT)
      WRITE(9,('5E13.5')) PLOT1(K,1),(PLOT1(K,I),I=IJF,IJL)
      REPEAT
      ELSE
      WRITE(9,('5A13')) (PNAME(I),I=IJF,IJL)
      DO (K=1,NPOINT)
      WRITE(9,('5E13.5')) (PLOT1(K,I),I=IJF,IJL)
      REPEAT
      ENDIF
      WRITE(9,*)
      WRITE(9,*)
      WRITE(9,*)
      REPEAT
      CASE (3)
      NO = 18
      OPEN(NO,FILE='CN04:',STATUS='NEW')
      WRITE(NO,('A1')) CHAR(12)    IFORM FEED
      IF (IFLAG(1) .EQ. 1) THEN
      WRITE(NO,1X
+         (PNAME(I),I=1,NVPLT-1)
      ELSE
      WRITE(NO,('1X,8A13')) (PNAME(I),I=1,NVPLT)
      ENDIF
      DO (K=1,NPOINT)
      WRITE(NO,('1X,8E13.5')) (PLOT1(K,I),I=1,NVPLT)
      REPEAT
      CLOSE (NO)
      CASE DEFAULT
      CONTINUE
      END SELECT

      REPEAT
      RETURN
      END

```

***** SUBROUTINE TO INTEGRATE USING EULER'S METHOD

```

***** YYDOT = A*YY + B*U
***** YY = YY + YYDOT*XDT
*****
***** YY -> VARIABLE TO INTEGRATE
***** YYDOT -> DERIVATIVE
***** NORDER -> NUMBER OF STATES
***** AB -> MATRIX A/B
***** XDT -> SAMPLING INTERVAL
***** XINPUT -> INPUT U
***** II -> THE NUMBER CORRESPONDING TO THE CYLINDER
*****
SUBROUTINE EULER(YY,YYDOT,NORDER,AB,XDT,XINPUT,II)

DIMENSION YY(64),YYDOT(6)                A,AB(45)

DO (J=1,NORDER)
  TEMP = 0
  DO (K=1,NORDER)
    TEMP = TEMP+AB(J,K)*YY(II,K)
  REPEAT
  K = NORDER+1
  YYDOT(II,J) = TEMP+AB(J,K)*XINPUT
REPEAT
DO (J=1,NORDER)
  YY(II,J) = YY(II,J) + XDT*YYDOT(II,J)
REPEAT
RETURN
END

*****
***** SUBROUTINE TO READ DATA FROM FILE
*****
SUBROUTINE FILERD

COMMON/SMSPE1/MAXGEN,MAXPAR,SPECIAL
COMMON/SMSPE2/IEFF,NAME,WADD
COMMON/SMSPE3/NGEN,PAR,IPOINT
COMMON/SMSPE4/MAXPSTO,IPTR,PSTO
COMMON/SMVAL1/DAMPM,BANDM,GAINM,XM1,XM2,XK,B,VRST
COMMON/SMVAL2/PS,PR
COMMON/SMVAL3/XL1,XL2,XL3,APT,VO,XLIMIT,FRC,BETAO
COMMON/SMSRV1/XKPM,XKP,SCLOT,XKFORC,DMPOFF,DMPON
COMMON/SMSRV2/COMP1,COMP2,COMP3,COMP4,COMP5

DIMENSION NGEN(240),PAR(1000),PSTO(1000)
INTEGER WADD(20),SPECIAL(240)
CHARACTER NAME(20)                20
CHARACTER CH*1,FNAME*20
DIMENSION XM2(6),XK(6),B(6)
DIMENSION XKPM(6),XKP(6),SCLOT(6),XKFORC(6)
DIMENSION COMP1(6),COMP2(6),COMP3(6),COMP4(6),COMP5(6)
LOGICAL EX

```

```

EX = .FALSE.

FNAME = ' '
WRITE(9,('YOU HAVE SELECTED: "READ FILES"'))
WRITE(9,(' <CR> TO RETURN TO MAIN MENU ',
+      '- ANYTHING TO CONTINUE'))
READ(9,*) FNAME
IF (FNAME(1:1) .EQ. ' ') RETURN

**** READS INPUT FILE NAME - PRIMARY MOTION

CALL READPRIM

EX = .FALSE.

**** READS INPUT FILE NAME - SPECIAL EFFECTS

FNAME = 'SPEDATA.SA'
WRITE(9,('WHAT IS SPECIAL EFFECT DATA FILE NAME?'))
READ(9,*) FNAME

**** CHECK TO SEE IF FILE EXISTS

INQUIRE(FILE=FNAME,EXIST=EX,IOSTAT=IOS,ERR=999)
IF(.NOT.EX) THEN
  WRITE(9,('DATA FILE ',(A)," DOES NOT EXIST")) FNAME
  RETURN
ENDIF

**** OPEN FILE

OPEN(UNIT=15,FILE=FNAME)

*** READ DATA FILE
**FE                      ADSPECIAL EFFECTS DATA

READ(15,*) IEFF
IF (IEFF .GT. 0) THEN
  K = INT(IEFF/4.)
  IMOD = MOD(IEFF,4)
  IF (IMOD .NE. 0) K = K + 1
  DO (IJ = 1,K)
    IJL = IJ*4
    IJF = IJL - 3
    IF (IEFF .LT. IJL) IJL = IEFF
    READ(15,*) (NAME(J),J=IJF,IJL)
  REPEAT
  READ(15,*) (WADD(J),J=1,IEFF)
ENDIF
READ(15,*) MAXGEN
IF (MAXGEN .GT. 0) THEN
  K = INT(MAXGEN/33.)
  IMOD = MOD(MAXGEN,33)

```

```

IF (IMOD .NE. 0) K = K + 1
DO (IJ = 1,K)
  IJL = IJ*33
  IJF = IJL - 32
  IF (MAXGEN .LT. IJL) IJL = MAXGEN
  READ(15,*) (SPECIAL(J),J=IJF,IJL)
  READ(15,*) (NGEN(J),J=IJF,IJL)
REPEAT
ENDIF
READ(15,*) MAXPAR
IF (MAXPAR .GT. 0) THEN
  K = INT(MAXPAR/11.)
  IMOD = MOD(MAXPAR,11)
  IF (IMOD .NE. 0) K = K + 1
  DO (IJ = 1,K)
    IJL = IJ*11
    IF=IJL-10
    IF (MAXPAR .LT. IJL) IJL = MAXPAR
    READ(15,*) (PAR(J),J=IJF,IJL)
  REPEAT
ENDIF
READ(15,*) MAXPSTO
IF (MAXPSTO .GT. 0) THEN
  K = INT(MAXPSTO/11.)
  IMOD = MOD(MAXPSTO,11)
  IF (IMOD .NE. 0) K = K + 1
  DO (IJ = 1,K)
    IJL = IJ*11
    IJF = IJL - 10
    IF (MAXPSTO .LT. IJL) IJL = MAXPSTO
    READ(15,*) (PSTO(J),J=IJF,IJL)
  REPEAT
ENDIF
CLOSE(15)

**** READ SERVO DATA

EX = .FALSE.

**** READS INPUT FILE NAME - SERVO

FNAME = 'SERVOPAR.SA'
WRITE(9,('WHAT IS SERVO DATA FILE NAME?'))
READ(9,*) FNAME

**** CHECK TO SEE IF FILE EXISTS

INQUIRE(FILE=FNAME,EXIST=EX,IOSTAT=IOS,ERR=999)
IF(.NOT.EX) THEN
  WRITE(9,('DATA FILE ",(A)," DOES NOT EXIST')) FNAME
  RETURN
ENDIF

```


**** OPEN FILE

OPEN(UNIT=15,FILE=FNAME)

**** READ DATA FILE

READ(15,*) XJUMP
 READ(15,*) XJUMP
 READ(15,*) XJUMP
 READ(15,*) (SCLOT(I),I=1,6)
 READ(15,*) (XKP(I),I=1,6)
 READ(15,*) (XKPM(I),I=1,6)
 READ(15,*) (XKFORC(I),I=1,6)
 READ(15,*) (COMP1(I),I=1,6)
 READ(15,*) (COMP2(I),I=1,6)
 READ(15,*) (COMP3(I),I=1,6)
 READ(15,*) (COMP4(I),I=1,6)
 READ(15,*) (COMP5(I),I=1,6)
 READ(15,*) DMPON,DMPOFF

CLOSE(15)

**** READ VALVE DATA

EX = .FALSE.

**** READS INPUT FILE NAME - VALVE

FNAME = 'VALVEPAR.SA'
 WRITE(9,('WHAT IS VALVE DATA FILE NAME?'))
 READ(9,*) FNAME

**** CHECK TO SEE IF FILE EXISTS

INQUIRE(FILE=FNAME,EXIST=EX,IOSTAT=IOS,ERR=999)
 IF(.NOT.EX) THEN
 WRITE(9,('DATA FILE ',(A),' DOES NOT EXIST')) FNAME
 RETURN
 ENDIF

**** OPEN FILE

OPEN(UNIT=15,FILE=FNAME)

**** READ DATA FILE

READ(15,*) DAMPM,BANDM,GAINM,PS,PR,XL1,XL2,XL3,APT,VO
 READ(15,*)XUMT,FRCEBETAO XM1,VRST
 READ(15,*) (XM2(I),I=1,6)
 READ(15,*) (XK(I),I=1,6)
 READ(15,*) (B(I),I=1,6)

```

CLOSE(15)
RETURN

999 WRITE(9,(" ERROR CODE ",15)) IOS
RETURN
END

*****
***** SUBROUTINE TO SAVE DATA INTO A FILE
*****
SUBROUTINE FILESV

COMMON/SMSPE1/MAXGEN,MAXPAR,SPECIAL
COMMON/SMSPE2/IEFF,NAME,WADD
COMMON/SMSPE3/NGEN,PAR,IPOINT
COMMON/SMSPE4/MAXPSTO,IPTR,PSTO
COMMON/SMVAL1/DAMPM,BANDM,GAINM,XM1,XM2,XK,B,VRST
COMMON/SMVAL2/PS,PR
COMMON/SMVAL3/XL1,XL2,XL3,APT,VO,XLIMIT,FRC,BETAO
COMMON/SMSRV1/XKPM,XKP,SCLOT,XKFORC,DMPOFF,DMPON
COMMON/SMSRV2/COMP1,COMP2,COMP3,COMP4,COMP5

DIMENSION NGEN(240),PAR(1000),PSTO(1000)
INTEGER WADD(20),SPECIAL(240)
CHARACTER NAME(20)*20
CHARACTER CH*1,FNAME*20
DIMENSION XM2(6),XK(6),B(6)
DIMENSION XKPM(6),XKP(6),SCLOT(6),XKFORC(6)
DIMENSION COMP1(6),COMP2(6),COMP3(6),COMP4(6),COMP5(6)
DIMENSION XJMP1(6),XJMP2(6),XJMP3(6)
LOGICAL EX

WHILE(1>0)
EX = .TRUE.

**** READS OUTPUT FILE NAME

FNAME = ' '
WRITE(9,("YOU HAVE SELECTED: "SAVE FILES""))
WRITE(9,(" <CR> TO RETURN TO MAIN MENU -",
+ " ANYTHING TO CONTINUE"))
READ(9,*) FNAME
IF (FNAME(1:1) .EQ. ' ') RETURN

**** CHECK TO SEE IF FILE EXISTS

CCCC INQUIRE(FILE=FNAME,EXIST=EX,IOSTAT=IOS,ERR=999)
CCCC IF(EX) THEN
CCCC WRITE(9,("FILENAME IS: ",(A))) FNAME
CCCC WRITE(9,("DO YOU WANT TO WRITE OVER IT (Y/N)?"))
CCCC CH = 'N'
CCCC READ (9,*) CH

```

```
CCCC IF (CH.NE.'Y') EXIT
CCCC ENDF
```

```
CCCC OPEN(UNIT=15,FILE=FNAME,STATUS='NEW')
```

```
**** WRITES DATA TO FILE
```

```
CCCC ENFILE(15)
CCCC CLOSE(15)
EXIT
REPEAT
```

```
**** READS OUTPUT FILE NAME - SPECIAL EFFECTS
```

```
WHILE (1>0)
EX=TRU E
```

```
FNAME = 'SPEDATA.SA'
WRITE(9,('WHAT IS THE OUTPUT FILE NAME ',
+ " - SPECIAL EFFECTS?"))
READ(9,*) FNAME
```

```
**** CHECK TO SEE IF FILE EXISTS
```

```
INQUIRE(FILE=FNAME,EXIST=EX,IOSTAT=IOS,ERR=999)
IF(EX) THEN
WRITE(9,('FILENAME IS: ',(A))) FNAME
WRITE(9,('DO YOU WANT TO WRITE OVER IT (Y/N)?'))
CH = 'N'
READ (9,*) CH
IF (CH.NE.'Y') EXIT
ENDIF
```

```
*** INITIALIZE PARAMETERS FOR SPECIAL EFFECTS INITIAL CONDITIONS
```

```
ITR = 1
DO (K = 1,MAXGEN)
SELECT CASE (NGEN(K))
CASE (1)
PSTO(ITR) = 10000.
PSTO(ITR+1) = 0.
ITR = ITR + 2
CASE (2)
PSTO(ITR) = 10000.
PSTO(ITR+1) = 0.
PSTO(ITR+2) = 0.
ITR = ITR + 3
CASE (3)
PSTO(ITR) = 0.
ITR = ITR + 1
ENDSELECT
REPEAT
```

```

**** OPEN FILE

      OPEN(UNIT=15,FILE=FNAME,STATUS='NEW')

**** WRITE DATA INTO FILE
**** WRITE SPECIAL EFFECTS DATA

      WRITE(15,*) IEFF
      IF (IEFF .GT. 0) THEN
        K = INT(IEFF/4.)
        IMOD = MOD(IEFF,4)
        IF (IMOD .NE. 0) K = K + 1
        DO (IJ = 1,K)
          IJL = IJ*4
          IJF = IJL - 3
          IF (IEFF .LT. IJL) IJL = IEFF
          WRITE(15,*) (NAME(J),J=IJF,IJL)
          REPEAT
            WRITE(15,*) (WADD(J),J=1,IEFF)
          ENDIF
        ENDIF
      WRITE(15,*) MAXGEN
      IF (MAXGEN .GT. 0) THEN
        K = INT(MAXGEN/33.)
        IMOD = MOD(MAXGEN,33)
        IF (IMOD .NE. 0) K = K + 1
        DO (IJ = 1,K)
          IJL = IJ*33
          IJF = IJL - 32
          IF (MAXGEN .LT. IJL) IJL = MAXGEN
          WRITE(15,*) (SPECIAL(J),J=IJF,IJL)
          WRITE(15,*) (NGEN(J),J=IJF,IJL)
          REPEAT
            ENDIF
        ENDIF
      WRITE(15,*) MAXPAR
      XPAR
      IF (MAXPAR .GT. 0) THEN
        K = INT(MAXPAR/11.)
        IMOD = MOD(MAXPAR,11)
        IF (IMOD .NE. 0) K = K + 1
        DO (IJ = 1,K)
          IJL = IJ*11
          IJF = IJL - 10
          IF (MAXPAR .LT. IJL) IJL = MAXPAR
          WRITE(15,*) (PAR(J),J=IJF,IJL)
          REPEAT
            ENDIF
        ENDIF
      MAXPSTO = ITR - 1
      WRITE(15,*) MAXPSTO
      K = INT(MAXPSTO/11.)
      IMOD = MOD(MAXPSTO,11)
      IF (IMOD .NE. 0) K = K + 1
      DO (IJ = 1,K)
        IJL = IJ*11

```

```

    IJF = IJL - 10
    IF (MAXPSTO .LT. IJL) IJL = MAXPSTO
    WRITE(15,*) (PSTO(J),J=IJF,IJL)
    REPEAT

    ENDFILE(15)
    CLOSE(15)
    EXIT
    REPEAT

**** WRITE SERVO DATA

    WHILE (1>0)
    EX = .TRUE.

**** READS OUTPUT FILE NAME - SERVO

    FNAME = 'SERVOPAR.SA'
    WRITE(9,('WHAT IS THE OUTPUT FILE NAME - SERVO?'))
    READ(9,*) FNAME

***CHECKTOSEEFFILE                                XSTS

    INQUIRE(FILE=FNAME,EXIST=EX,IOSTAT=IOS,ERR=999)
    IF(EX) THEN
    WRITE(9,('FILENAME IS: ',(A))) FNAME
    WRITE(9,('DO YOU WANT TO WRITE OVER IT (Y/N)?'))
    CH = 'N'
    READ (9,*) CH
    IF (CH .NE. 'Y') EXIT
    ENDIF

**** OPEN FILE

    OPEN(UNIT=15,FILE=FNAME)

**** READ DATA TO WRITE OVER

    READ(15,*) (XJMP1(I),I=1,6)
    READ(15,*) (XJMP2(I),I=1,6)
    READ(15,*) (XJMP3(I),I=1,6)
    CLOSE(15)

**** OPEN FILE

    OPEN(UNIT=15,FILE=FNAME,STATUS='NEW')

**** WRITE DATA FILE

    WRITE(15,*) (XJMP1(I),I=1,6)
    WRITE(15,*) (XJMP2(I),I=1,6)
    WRITE(15,*) (XJMP3(I),I=1,6)
    WRITE(15,*) (SCLOT(I),I=1,6)

```

```

WRITE(15,*) (XKP(I),I=1,6)
WRITE(15,*) (XKPM(I),I=1,6)
WRITE(15,*) (XKFORC(I),I=1,6)
WRITE(15,*) (COMP1(I),I=1,6)
WRITE(15,*) (COMP2(I),I=1,6)
WRITE(15,*) (COMP3(I),I=1,6)
WRITE(15,*) (COMP4(I),I=1,6)
WRITE(15,*) (COMP5(I),I=1,6)
WRITE(15,*) DMPON,DMPOFF

ENDFILE(15)
CLOSE(15)
EXIT
REPEAT

**** WRITE VALVE DATA

WHILE (1>0)
  EX = .TRUE.

**** READS OUTPUT FILE NAME - VALVE

FNAME = 'VALVEPAR.SA'
WRITE(9,('WHAT IS THE OUTPUT FILE NAME - VALVE?'))
READ(9,*) FNAME

**** CHECK TO SEE IF FILE EXISTS

INQUIRE(FILE=FNAME,EXIST=EX,IOSTAT=IOS,ERR=999)
IF(EX) THEN
  WRITE(9,('FILENAME IS: ',(A))) FNAME
  WRITE(9,('DO YOU WANT TO WRITE OVER IT (Y/N)?'))
  CH = 'N'
  READ (9,*) CH
  IF (CH.NE. 'Y') EXIT
ENDIF

**** OPEN FILE

OPEN(UNIT=15,FILE=FNAME,STATUS='NEW')

**** WRITE DATA FILE

WRITE(15,*) DAMPM,BANDM,GAINM,PS,PR,XL1,XL2,XL3,APT,VO
WRITE(15,*) XLIMIT,FRC,BETAO,XM1,VRST
WRITE(15,*) (XM2(I),I=1,6)
WRITE(15,*) (XK(I),I=1,6)
WRITE(15,*) (B(I),I=1,6)

ENDFILE(15)
CLOSE(15)
EXIT
REPEAT

```

```

RETURN

999 WRITE(9,('  ERROR CODE ',I5)) IOS
RETURN
END

*****
* SUBROUTINE TO PERFORM THE GEOMETRIC TRANSFORMATIONS (VERSION #2)
* THIS VERSION IS CLOSELY RELATED TO THE ASSEMBLY LANGUAGE IMP.
*****
SUBROUTINE GTRN2(ANGLE,CEXT)

**** INPUTS

DIMENSION ANGLE(6)

**** OUTPUTS

DIMENSION CEXT(6)
DIMENSION TEMP1(6),TEMP2(6),FORCE(6)

DIMENSION CX(6),CY(6),BX(6),BY(6),BOTX(6),BOTY(6),BOTZ(6)
DIMENSION BCYLNT(6),BCYLN(6),BCYLNT1(6)

**** INITIALIZE THE DIFFERENT CONSTANTS USED

DATA (CX(I),I=1,6)/51.428,-22.931,-28.497,-28.497,-22.931,51.428/
DATA (CY(I),I=1,6)/3.214,46.146,42.931,-42.931,-46.146,-3.214/

DATA (BX(I),I=1,6)/36.891,31.324,-68.215,-68.215,31.324,36.891/
DATA (BY(I),I=1,6)/57.469,60.683,3214,-3214,-60.683,-57.469/
BZ=-65.942

**** DETERMINE THE ACTUATOR LENGTH COMPONENTS

DO (N=1,6)

TX=ANGLE(1)+CX(N)
TY=ANGLE(2)+CY(N)
TZ=ANGLE(3)

CALL ROTATE(ANGLE(5),TY,TZ)
CALL ROTATE(ANGLE(4),TZ,TX)
CALL ROTATE(ANGLE(6),TX,TY)

BOTX(N)=TX-BX(N)
BOTY(N)=TY-BY(N)
BOTZ(N)=TZ-BZ
CEXT(N)=SQRT(BOTX(N)**2+BOTY(N)**2+BOTZ(N)**2)

IF(CEXT(N).GT.104.63)CEXT(N)=104.63
IF(CEXT(N).LT.68.63)CEXT(N)=68.63

```

```

BCYLNT(N)=(CEXT(N)-86.63)/18.0001
IF (BCYLNT(N).GT.1.0) BCYLNT(N)=1.0
IF (BCYLNT(N).LT.-1.0) BCYLNT(N)=-1.0

```

**** SMOOTHING FUNCTION

```

IF (ABS(BCYLNT(N)).LT.0.8292837) THEN
  BCYLN(N)=BCYLNT(N)
ELSE
  BCYLNT1(N)=0.658707+SQRT(0.058288106-(ABS(BCYLNT(N))
+      -1.0)**2)
  IF (BCYLNT(N).LT.0.0) THEN
    BCYLN(N)=-BCYLNT1(N)
  ELSE
    BCYLN(N)=BCYLNT1(N)
  ENDF
ENDIF

CEXT(N)=BCYLN(N)*18.0001

```

REPEAT

RETURN
END

***** SUBROUTINE TO INPUT FLAGS FOR SPECIAL EFFECTS
***** AND INPUTS TO PRIMARY MOTION

SUBROUTINE INPUTS

```

COMMON/USER1/BIN,NINP,INPNUM,NITER
DIMENSION BIN(2000,9),INPNUM(9)

```

```

COMMON/SMSPE2/IEFF,NAME,WADD
COMMON/SMSPE7/POX,IEFFLG

```

```

DIMENSION POSX(6),IEFFLG(20)
DIMENSION NCE(20)
INTEGER WADD(20)
CHARACTER NAME(20)*20

```

**** SET FLAGS TO FALSE

```

DO (I=1,IEFF)
  IEFFLG(I) = 0
REPEAT

```

**** ENTER FLAGS FOR SPECIAL EFFECTS

```

WRITE(9,('YOU HAVE SELECTED: "INPUTS"'))
CALL GRAMENU

```



```
WRITE(9,('ENTER NUMBER OF SPECIAL EFFECTS TO RUN'))
WRITE(9,('<CR> TO RETURN TO PREVIOUS MENU'))
N = -1
READ(9,*) N
WHILE ((NLE-1).OR.(N.GT.IEF))
  IF (N .EQ. -1) RETURN
  N = -1
  WRITE(9,*)
  WRITE(9,(' ILLEGAL NUMBER - ENTER AGAIN'))
  READ(9,*) N
  REPEAT

**** IF N = 0 THEN NO SPECIAL EFFECTS TO RUN

IF (N .GT. 0) THEN
  WRITE(9,('ENTER NUMBER CORRESPONDING TO EACH EFFECT'))
  READ(9,*) (NCE(I),I=1,N)

**** SET FLAGS TO TRUE

DO (I=1,N)
  IEFFLG(NCE(I)) = -1
  REPEAT
ENDIF

**** SET INPUTS TO PRIMARY MOTION

WRITE(9,*)
WRITE(9,*)
WRITE(9,(' INPUT SET UP TO PRIMARY MOTION'))
WRITE(9,*)
DUM=.05
CALL PREPINP(DUM)

RETURN
END
```

***** SUBROUTINE TO SIMULATE MOTION BASE SYSTEM - SIMULATE

SUBROUTINE SIMULATE

```

COMMON/CUEFILX/BXACCN,BAXA0,BAXA1,BAXA2,BAXA3
COMMON/CUEFILY/BYACCN,BAYA0,BAYA1,BAYA2,BAYA3
COMMON/CUEFILZ/BZACCN,BAZA0,BAZA1,BAZA2,BAZA3
COMMON/CUEFILQ/BAPITH,BQA0,BQA1,BQA2,BQA3
COMMON/CUEFILP/BAROLL,BPA0,BPA1,BPA2,BPA3
COMMON/CUEFILR/BAYAW,BRA0,BRA1,BRA2,BRA3
COMMON/USER1/BIN,NINP,INPNUM,NITER
DIMENSION BIN(2000,9),INPNUM(9)
COMMON/CTTRAN/FLTAXA,FLTAYA,FLTAZA
COMMON/CTROT/FQADOT,FPADOT,FRADOT,FQA,FPA,FRA
COMMON/GRAV1/BXALIN,BYALIN
COMMON/MPCP1/BXPOS,BYPOS,BZPOS,BTHPOS,BPHPOS,BSIPOS
COMMON/POSCON1/BMXPOS,BMYPOS,BMZPOS,BMTHPEP,BMPHIP,BMPSIP
COMMON/PRIM1/XENFL,YENFL,ZENFL,THENFL,PHENFL,SIENFL
COMMON/PRIM2/XGRFL,YGRFL,MPCPFL,MPLPFL
COMMON/PRIM3/BXAWTC,BYAWTC,BZAWTC,BTHWTC,BPHWTC,BSIWTC
COMMON/PRIM4/BKAX1,BKAY1,BKAZ1,BKQA1,BKPA1,BKRA1
COMMON/PRIM5/BKAX2,BKAY2,BKAZ2,BKQA2,BKPA2,BKRA2
COMMON/PRIM6/ALAGX,AKGAX,DLAGX,DKGAX,ALAGY,AKGAY,DLAGY,DKGAY
COMMON/PRIM7/BKQA4,BKPA4
COMMON/PRIM8/BLAGX,BLAGY,BLAGZ,BLAGT,BLAGP,BLAGS
INTEGER*4 XENFL,YENFL,ZENFL,THENFL,PHENFL,SIENFL
INTEGER*4 XGRFL,YGRFL,MPCPFL,MPLPFL
REAL BXAWTC,BYAWTC,BZAWTC,BTHWTC,BPHWTC,BSIWTC
REAL BKAX1,BKAY1,BKAZ1,BKQA1,BKPA1,BKRA1
REAL BKAX2,BKAY2,BKAZ2,BKQA2,BKPA2,BKRA2
REAL ALAGX,AKGAX,DLAGX,DKGAX,ALAGY,AKGAY,DLAGY,DKGAY
REAL BKQA4,BKPA4
REAL BLAGX,BLAGY,BLAGZ,BLAGT,BLAGP,BLAGS
COMMON/SMSPE3/NGEN,PAR,IPOINT
COMMON/SMSPE4/MAXPSTO,IPTR,PSTO
COMMON/SMSPE7/POSX,IEFFLG
COMMON/SMVAL1/DAMPM,BANDM,GAINM,XM1,XM2,XK,B,VRST
COMMON/SMVAL2/PS,PR
COMMON/SMVAL4/X,XDOT,PD,PDOT,XMOTOR,PISTON
COMMON/SMVAL5/VOUT
COMMON/SMVAL6/CPRS,RPRS,POSI,Q6,Q7
COMMON/SMSRV3/TEMP1,TEMP2,CYLOT,FORCE
COMMON/SMSRV4/COMPN
COMMON/SMDIS1/TMAX,NVSNFNT,NVAR,FLOTV,FLOTA

COMMON/SMANI1/SIGNA
COMMON/SMDIS2/TIN VX,AFTER

DIMENSION XM2(6),XK(6),B(6)
DIMENSION NGEN(240),PAR(1000),PSTO(1000)
DIMENSION POSX(6),IEFFLG(20)
DIMENSION X(6,2),XDOT(6,2),PD(6,4),PDOT(6,4)
DIMENSION XMOTOR(4,5),PISTON(4,5)

```

```

DIMENSION CPRS(6),RPRS(6),POSI(6),Q6(6),Q7(6)
DIMENSION TEMP1(6),TEMP2(6),CYLOT(6),FORCE(6)
DIMENSION NVAR(17),PLOTV(2000,18),PLOTA(2000,6)
DIMENSION SIGNA(6),VOUT(6),COMPN(6)
DIMENSION TINVX(6),AFTER(6),PRIMPOS(6)
CHARACTER CH*1
DATA PI/3.1416/

**** INITIALIZE VARIABLES

      T=0 ; I1=0 ; I2=0 ; I3=0 ; I4=0 ; I5=0 ; I6=-1 ; I1=1

**** SELECT VARIABLES TO BE SAVED

      WRITE(9,('YOU HAVE SELECTED: "EXECUTE"'))
      WRITE(9,('ENTER NUMBER IN ASCENDING ORDER OF THE VARIABLE TO
+ BE SAVED (<CR> TO RETURN)'))
      WRITE(9,(' HIT <CR> AFTER EACH ONE - 0 TO CONTINUE'))
      NVS=0                                NUMBER OF VARIABLES TO SAVE
      NTEST=-1
      WHILE (NVS .LT. 17)
        WRITE(9,('ENTRY #',I3)) NVS+1
        READ(9,*) NTEST                    IREAD # OF VARIABLE TO SAVE
        IF (NTEST .EQ. -1) RETURN
        IF (NTEST .EQ. 0) EXIT
        NVS = NVS + 1                      I# OF TOTAL VARIABLES TO SAVE
        NVAR(NVS) = NTEST                  ISAVE # OF VARIABLE TO SAVE
        NTEST = -1
      REPEAT

**** ENTER RATES FOR EACH PART
*** IF RATE .LE. 0 THEN THAT PART IS NOT EXECUTED

      WRITE(9,*)
      WRITE(9,(' SET TIMING PARAMETERS'))
      WRITE(9,('ENTER RATE FOR VALVE UPDATE (in Hz)'))
      READ(9,*) RATE
      WHILE (RATE .LE. 0)
        WRITE(9,(' RATE NOT VALID - ENTER AGAIN'))
        READ(9,*) RATE
      REPEAT
      WRITE(9,('RATE WILL BE: ',E11.5,' Hz')) RATE
      DT = 1./RATE
      WRITE(9,('SAMPLING INTERVAL: ',E11.5,' s')) DT

      WRITE(9,*)
      WRITE(9,('ENTER RATE FOR PRIMARY MOTION UPDATE (in Hz)'))
      READ(9,*) RATE
      IF (RATE .LE. 0) THEN
        DTPRMO = 0.
        MCNT2 = -1 ; I2 = -1
        MCNT4 = -1 ; I4 = -1
      ELSE

```

```

DTPRMO = 1./RATE
MCNT2 = NINT(DTPRMO/DT)
MCNT4 = MCNT2
DTPRMO = MCNT2*DT
RATE = 1./DTPRMO
WRITE(9,('RATE WILL BE: ",E11.5," Hz')) RATE
WRITE(9,('SAMPLING INTERVAL: ",E11.5," s')) DTPRMO
ENDIF

```

```

WRITE(9,*)
WRITE(9,('ENTER RATE FOR SPECIAL EFFECTS UPDATE (in Hz)'))
READ(9,*) RATE
IF (RATE .LE. 0) THEN
  DTSPEF = 0.
  MCNT3 = -1 ; I3 = -1
ELSE
  DTSPEF = 1./RATE
  MCNT3 = NINT(DTSPEF/DT)
  MCNT4 = MCNT3 ; I4 = 0
  DTSPEF = MCNT3*DT
  RATE = 1./DTSPEF
  WRITE(9,('RATE WILL BE: ",E11.5," Hz')) RATE
  WRITE(9,('SAMPLING INTERVAL: ",E11.5," s')) DTSPEF
ENDIF

```

```

MCNT6 = -1
WRITE(9,*)
WRITE(9,('ENTER RATE FOR SERVO UPDATE (in Hz)'))
READ(9,*) RATE
      FRATELEQTHEN
  DTSRV = 0.
  MCNT5 = -1 ; I5 = -1 ; MCNT6 = -1
ELSE
  DTSRV = 1./RATE
  MCNT5 = NINT(DTSRV/DT)
  DTSRV = MCNT5*DT
  RATE = 1./DTSRV
  WRITE(9,('RATE WILL BE: ",E11.5," Hz')) RATE
  WRITE(9,('SAMPLING INTERVAL: ",E11.5," s')) DTSRV
  WRITE(9,*)
  WRITE(9,('DO YOU WANT THE INVERSE GEOMETRIC TRANSFORMATIONS
+ TO BE EXECUTED (Y/N)?'))

```

```

**** INVERSE GEOM. TRANSF. IS EXECUTED IF SERVO
**** AND SAVING VALUES ARE ALSO

```

```

CH = 'N'
READ(9,*) CH
IF (CH .EQ. 'Y') THEN
  MCNT6 = MCNT5 ; I6 = 0
  WRITE(9,*)
  WRITE(9,('ENTER VALUE OF TOLERANCE FOR CONVERGENCE'))
  EPSILON = 2.

```

```

READ(9,*) EPSILON
WHILE (EPSILON .LT. 2)
  WRITE(9,*)
  WRITE(9,(" VALUE NOT VALID - ENTER AGAIN"))
  READ(9,*) EPSILON
REPEAT
ENDIF
ENDIF

RATE = 0.
F( (MVS.GT.0).OR.(6NE-1)) THEN
  WRITE(9,*)
  WRITE(9,("ENTER RATE FOR SAVING VALUES (in Hz)"))
  READ(9,*) RATE
  RT1 = 1./DT
  WHILE ((RATE .GT. RT1) .AND. (RATE .GT. 0))
    WRITE(9,("RATE NOT VALID - ENTER AGAIN"))
    READ(9,*) RATE
  REPEAT
ENDIF
IF (RATE .LE. 0) THEN

**** IF SAVING VALUES IS NOT EXECUTED THEN
****   NEITHER IS INVESE GEOM. TRANSF.

  I1 = -1 ; MCNT1 = -1 ; DTSAVE = 1 ; I6 = -1 ; MCNT6 = -1
  ELSE
    DTSAVE = 1./RATE
    MCNT1 = NINT(DTSAVE/DT)
    DTSAVE = MCNT1*DT
    RATE = 1./DTSAVE
    WRITE(9,("RATE WILL BE: ",E11.5," Hz")) RATE
    WRITE(9,("SAMPLING INTERVAL: ",E11.5," s")) DTSAVE

**** RATE OF INVERSE GEOM. TRANSF. IS THE SAME AS SAVING VALUES RATE

    IF (I6 .EQ. 0) MCNT6 = MCNT1
    ENDIF
    IF (I6 .EQ. -1) THEN
      WRITE(9,*)
      WRITE(9,("INVERSE GEOMETRIC TRANSFORMATIONS WILL NOT BE",
+
      "EXECUTED"))
    ENDIF

    WRITE(9,*)
    WRITE(9,("ENTER TOTAL TIME OF SIMULATION (in sec.)"))
    READ(9,*) TMAX

**** CALCULATES NUMBER OF ITERATIONS (MITER) AND
****   APROXIMATE NUMBER OF POINTS FOR PLOT (NPNT .LT. 2000)

    NPNT = NINT(TMAX/DTSAVE)
    WHILE ((NPNT .GE. 2000) .OR. (NPNT .LE. 0))

```

```

WRITE(9,*)
WRITE(9,*)
WRITE(9,(' LENGTH NOT ACCEPTED - ENTER AGAIN'))
READ(9,*) TMAX
NPNT = NINT(TMAX/DTSAVE)
REPEAT
MITER = NINT(TMAX/DT)

```

**** MOTOR MATRIX - CONTINUOUS TIME

```

TEMP = 2*PI*BANDM IOMEGAN
XMOTOR(1,1) = 0 ; XMOTOR(1,2) = 1 ; XMOTOR(2,1) = -(TEMP**2)
XMOTOR(2,2) = -2*TEMP*DAMPM ; XMOTOR(1,3) = 0
XMOTOR(2,3) = GAINM*(TEMP**2)/VRST

```

**** PISTON MATRIX - CONSTANT PART OF CONTINUOUS TIME

```

PISTON(1,1)=0 ; PISTON(1,2)=1 ; PISTON(1,3)=0 ; PISTON(1,4)=0
PISTON(3,1)=0 ; PISTON(3,2)=0 ; PISTON(3,3)=0 ; PISTON(3,4)=1
PISTON(1,5)=0;PISTON(3,5)=0;PISTON(4,5)=0

```

**** INITIALIZING VARIABLES

```

DO (I=1,6)
DO (IJ=1,4)
PD(I,IJ) = 0.          ICYLINDER EXTENSION
PDOT(I,IJ) = 0.       ICYLINDER VELOCITY
REPEAT
X(I,1) = 0.           ISPOOL POSITION
X(I,2) = 0.
XDOT(I,1) = 0.        ISPOOL VELOCITY
XDOT(I,2) = 0.
VOUT(I) = 0.          IVOLTAGE TO VALVE
Q6(I) = 0.            IFLOW
Q7(I) = 0.            IFLOW
POSI(I) = 0.          ICYLINDER POSITION
TEMP1(I) = 0.         ISERVO INTEGRATOR
TEMP2(I) = 0.         ISERVO INTEGRATOR
COMPNI(I) = 0.        ICOMPENSATION OUTPUT
CPRS(I) = (PS+PR)/2. ICAP PRESSURE
RPRS(I) = (PS+PR)/2. IROD PRESSURE
FORCE(I) = 0.         IDIFFERENTIAL PRESSURE
POSX(I) = 0.          ISPECIAL EFFECTS OUTPUT
SIGNA(I) = 0.         ISUM PRMO+SPEF
CYLOT(I) = 0.         ICOMMANDED CYLINDER POS
TINVI(I) = 0.         IOUTPUT INV. GEOM. TRANSF.
AFTER(I) = 0.         ICYL. EXTEN. AFTER IGT
PRIMPOS(I) = 0.
REPEAT

```

**** INITIALIZING PRIMARY MOTION VARIABLES

III = 1

```

BXACCN=0.0;BXN1=0.0;BAXA0=0.0;BAXA1=0.0;BAXA2=0.0;BAXA3=0.0
BYACCN=0.0;BYN1=0.0;BAYA0=0.0;BAYA1=0.0;BAYA2=0.0;BAYA3=0.0
BZACCN=0.0;BZN1=0.0;BAZA0=0.0;BAZA1=0.0;BAZA2=0.0;BAZA3=0.0
BAROLL=0.0;BPN1=0.0;BPA0=0.0;BPA1=0.0;BPA2=0.0;BPA3=0.0
BAYAW=0.0;BSN1=0.0;BRA0=0.0;BRA1=0.0;BRA2=0.0;BRA3=0.0

```

**** INITIALIZE VARIABLES FOR SUBROUTINE CTRAN1

```

FLTAXA=0.0 ; FLTAYA=0.0 ; FLTAZA=0.0
FQADOT=0.0 ; FPADOT=0.0 ; FRADOT=0.0
FQA=0.0 ; FPA=0.0 ; FRA=0.0

```

**** INITIALIZE VARIABLES FOR SUBROUTINE GRAVAL1

```

BXALIN=0.0
BYALIN=0.0

```

**** INITIALIZE VARIABLES FOR SUBROUTINE PLATPOS1

```

BXPOS=0.0
BYPOS=0.0
BZPOS=0.0
BTHPOS=0.0
          BTFPOS=0.0
BSIPOS=0.0

```

**** INITIALIZE VARIABLES FOR SUBROUTINE POSCON1

```

BMXPOS=0.0
BMYPOS=0.0
BMZPOS=0.0
BMTHEP=0.0
BMPHIP=0.0
BMPSIP=0.0

```

**** INITIAL CONDITIONS FOR SPECIAL EFFECTS (PSTO ARRAY)

```

ITR = 1
K = 1
WHILE (ITR .LE. MAXPSTO)
  SELECT CASE (NGEN(K))
  CASE (1)
    PSTO(ITR) = 10000.
    PSTO(ITR+1) = 0.
    ITR = ITR + 2
  CASE (2)
    PSTO(ITR) = 10000.
    PSTO(ITR+1) = 0.
    PSTO(ITR+2) = 0.
    ITR = ITR + 3
  CASE (3)
    PSTO(ITR) = 0.
    ITR = ITR + 1

```

```
END SELECT
K = K + 1
REPEAT

**** SIMULATION STARTS HERE

DO (I = 1, MITER)

**** SAVE VALUES

IF (I1 .EQ. 0) THEN
  CALL SAVEVAL(T, I1)
  I1 = I1 + 1
  I1 = MCNT1
ENDIF

**** UPDATE PRIMARY MOTION

IF (I2 .EQ. 0) THEN
  CALL SUCNEP          FMO)
  I2 = I2 + 1
  PRIMPOS(1) = BMXPOS
  PRIMPOS(2) = BMYPOS
  PRIMPOS(3) = BMZPOS
  PRIMPOS(4) = BMTHEP
  PRIMPOS(5) = BMPHIP
  PRIMPOS(6) = BMPSIP
  I2 = MCNT2
ENDIF

**** UPDATE SPECIAL EFFECTS

IF (I3 .EQ. 0) THEN
  CALL SMSPEF(DTSPEF)
  I3 = MCNT3
ENDIF

IF (I4 .EQ. 0) THEN

**** ADD PRIMARY MOTION TO SPECIAL EFFECTS

DO (J=1,6)
  SIGNA(J) = POSX(J)+PRIMPOS(J)
REPEAT

**** UPDATE GEOMETRIC TRANSFORMATIONS

CALL GTRN2(SIGNA, CYLOT)
I4 = MCNT4
ENDIF

**** UPDATE SERVO
```



```

IF (I5 .EQ. 0) THEN
  CALL SMSRV(DTSRV)
  I5 = MCNT5

**** UNIT STEP INPUT TO VALVE IF SPECIAL EFFECTS AND PRIMARY MOTION
**** ARE NOT EXECUTED

  IF ((I2 .LE. -1) .AND. (I3 .LE. -1)) THEN
    DO (IIII = 1,6)
      CYLOT(IIII) = 1.
    REPEAT
      ENDF
  ENDIF

**** UPDATE VALVE

  CALL SMVALVE(DT)

**** UPDATE INVERSE GEOMETRIC TRANSFORMATIONS

  IF (I6 .EQ. 0) THEN
    CALL SMIGT(POSI,SIGNA,TINVS,EPSILON)
    CALL GTRN2(TINVS,AFTER)
    I6 = MCNT6
  ENDIF

**** UPDATE VARIABLES

  I1 = I1 - 1
  I2 = I2 - 1
  I3 = I3 - 1
  I4 = I4 - 1
  I5 = I5 - 1
  I6 = I6 - 1
  T = T + DT

  REPEAT
  NPNT = II - 1  ITOTAL NUMBER OF POINTS OF SIMULATION
  RETURN
  END

*****
***** SUBROUTINE TO ROTATE A VECTOR (2 ELEMENTS) BY THE GIVEN ANGLE:
*****
***** | VAR1 | | COS(ANGLE) | | -SIN(ANGLE) | | VAR1 |
***** |   | |   | |   |
***** | VAR2 | | SIN(ANGLE) | | COS(ANGLE) | | VAR2 |
***** |   | |   | |   |
*****
*****
SUBROUTINE ROTATE(ANGLE,VAR1,VAR2)

SINA=SIN(ANGLE)
COSA=COS(ANGLE)

```

```

TEMP1=VAR1*COSA-VAR2*SINA
VAR2=VAR1*SINA+VAR2*COSA
VAR1=TEMP1

```

```

RETURN
END

```

```

*****

```

```

***** SUBROUTINE TO SAVE VALUES OF SELECTED VARIABLES

```

```

*****

```

```

SUBROUTINE SAVEVAL(T,I)

```

```

COMMON/CUEFILX/BXACCN,BAXA0,BAXA1,BAXA2,BAXA3
COMMON/CUEFILY/BYACCN,BAYA0,BAYA1,BAYA2,BAYA3
COMMON/CUEFILZ/BZACCN,BAZA0,BAZA1,BAZA2,BAZA3
COMMON/CUEFILQ/BAPITH,BQA0,BQA1,BQA2,BQA3
COMMON/CUEFILP/BAROLL,BPA0,BPA1,BPA2,BPA3
COMMON/CUEFILR/BAYAW,BRA0,BRA1,BRA2,BRA3
COMMON/CTTRAN/FLTAXA,FLTAYA,FLTAZA
COMMON/CTROT/FQADOT,FPADOT,FRADOT,FQA,FPA,FRA
COMMON/GRAV1/BXALIN,BYALIN
COMMON/MPCP1/BXPOS,BYPOS,BZPOS,BTHPOS,BPHPOS,BSIPOS
COMMON/POSCON1/BMXPOS,BMYPOS,BMZPOS,BMTHEP,BMPHIP,BMPSIP
COMMON/SMSPEZ /POSXIEFLG
COMMON/SMVAL4/X,XDOT,PD,PDOT,XMOTOR,PISTON
COMMON/SMVAL5/VOUT
COMMON/SMVAL6/CPRS,RPRS,POSI,Q6,Q7
COMMON/SMVAL7/Q1,Q2,Q3,Q4,Q5,V
COMMON/SMSRV3/TEMP1,TEMP2,CYLOT,FORCE
COMMON/SMSRV4/COMPN
COMMON/SMDIS1/TMAX,NVS,NPNT,NVAR,PLOTV,PLOTA
COMMON/SMANI1/SIGNA
COMMON/SMDIS2/TIN VX,AFTER

```

```

DIMENSION NVAR(17),PLOTV(2000,18)
DIMENSION SAVE(500),PLOTA(2000,6)
DIMENSION POSX(6),IEFFLG(20)
DIMENSION X(6,2),XDOT(6,2),PD(6,4),PDOT(6,4)
DIMENSION XMOTOR(4,5),PISTON(4,5)
DIMENSION VOUT(6)
DIMENSION CPRS(6),RPRS(6),POSI(6),Q6(6),Q7(6)
DIMENSION Q1(6),Q2(6),V(6,2),Q3(6),Q4(6),Q5(6)
DIMENSION TEMP1(6),TEMP2(6),CYLOT(6),FORCE(6)
DIMENSION SIGNA(6),COMPN(6)
DIMENSION TIN VX(6),AFTER(6)

```

```

**** SAVING VALUES

```

```

DO (J=1,6)

```

```

**** VALUES TO ANIMATE

```

```

PLOTA(I,J) = TIN VX(J)

```

**** OTHER VARIABLES

SAVE(J)=POSX(J)	SPECIAL EFFECTS OUTPUT	T
SAVE(J+6) = PD(J,1)	ICYLINDER POSITION	
SAVE(J+12) = PDOT(J,1)	ICYLINDER VELOCITY	
SAVE(J+18) = X(J,1)	ISPOOL POSITION	
SAVE(J+24) = XDOT(J,1)	ISPOOL VELOCITY	
SAVE(J+30) = VOUT(J)	IVOLTAGE TO VALVE	
SAVE(J+36) = CPRS(J)	ICAP PRESSURE	
SAVE(J+42) = RPRS(J)	IROD PRESSURE	
SAVE(J+48) = POSI(J)	ICYLINDER POSITION (=PD)	
SAVE(J+54) = CYLOT(J)	IOUTPUT OF GEOM. TRANSF.	
SAVE(J+60) = FORCE(J)	ICOMP. DIFF. FORCE (PRES)	
SAVE(J+66) = Q6(J)	ICOMPRESSIBILITY FLOW	
SAVE(J+72) = Q7(J)	ICOMPRESSIBILITY FLOW	
SAVE(J+78) = SIGNA(J)	ISPEFF + PRIMOT	
SAVE(J+84) = COMPN(J)	ISERVO COMPENSATION	
SAVE(J+90) = Q1(J)	ISPOOL FLOW	
SAVE(J+96) = Q2(J)	ISPOOL FLOW	W
SAVE(J+102) = V(J,1)	IVOLUME OF PISTON (CAP)	
SAVE(J+108) = V(J,2)	IVOLUME OF PISTON (ROD)	
SAVE(J+114) = Q3(J)	ILEAKAGE FLOW	
SAVE(J+120) = Q4(J)	ILEAKAGE FLOW	
SAVE(J+126) = Q5(J)	ILEAKAGE FLOW	
SAVE(J+132) = CPRS(J)-RPRS(J)	IDIFFERENTIAL PRESSURE	
SAVE(J+138) = TINVX(J)	IINVERSE TRANSF. OUTPUT	
SAVE(J+144) = AFTER(J)	IEXTEN. AFTER INV.TRANSF.	
REPEAT		
SAVE(151) = FLTAXA	IX ACC. INPUT	
SAVE(152) = FLTAYA	IY ACC. INPUT	
SAVE(153) = FLTAZA	IZ ACC. INPUT	
SAVE(154) = FQA	IPITCH RATE INPUT	
SAVE(155) = FPA	IROLL RATE INPUT	
SAVE(156) = FRA	IYAW RATE INPUT	
SAVE(157) = FQADOT	IPITCH ACC. INPUT	
SAVE(158) = FPADOT	IROLL ACC. INPUT	
SAVE(159) = FRADOT	IYAW ACC. INPUT	
	SAVE(160) = BXACCN	IXCENT.ACC.
SAVE(161) = BYACCN	IY CENT. ACC.	
SAVE(162) = BZACCN	IZ CENT. ACC.	
SAVE(163) = BAROLL	IROLL CENT. ACC.	
SAVE(164) = BAYAW	IYAW CENT. ACC.	
SAVE(165) = BAXA2	IX OUTPUT OF WASHOUT	
SAVE(166) = BAYA2	IY OUTPUT OF WASHOUT	
SAVE(167) = BAZA2	IZ OUTPUT OF WASHOUT	
SAVE(168) = BPA2	IROLL OUTPUT OF WASHOUT	
SAVE(169) = BRA2	IYAW OUTPUT OF WASHOUT	
SAVE(170) = BXALIN	IX GRAVITY ALING.	
SAVE(171) = BYALIN	IY GRAVITY ALING.	
SAVE(172) = BXPOS	IX PLATF. POS.	
SAVE(173) = BYPOS	IY PLATF. POS.	
SAVE(174) = BZPOS	IZ PLATF. POS.	

SAVE(175) = BTHPOS	IPITCH PLATF. POS.
SAVE(176) = BPHPOS	IROLL PLATF. POS
SAVE(177) = BSIPOS	IYAW PLATF. POS.
SAVE(178) = BMMPOS	IX OUTPUT OF PRIM.MOTION
SAVE(179) = BMYPOS	IY OUTPUT OF PRIM. MOTION
SAVE(180) = BMZPOS	IZ OUTPUT OF PRIM. MOTION
SAVE(181) = BMTHEP	IPITCH OUTPUT OF PRIM. MOTION
SAVE(182) = BMPHIP	IROLL OUTPUT OF PRIM. MOTION
SAVE(183) = B MPSIP	IYAW OUTPUT OF PRIM. MOTION
SAVE(184) = BAXA0	IX ACC WASHOUT
SAVE(185) = BAYA0	IY ACC WASHOUT
SAVE(186) = BAZA0	IZ ACC WASHOUT
SAVE(187) = BPA0	IROLL RATE WASHOUT
SAVE(188) = BRA0	IYAW RATE WASHOUT
SAVE(189) = BAXA1	IX VEL WASHOUT
SAVE(190) = BAYA1	IY VEL WASHOUT
SAVE(191) = BAZA1	IZ VEL WASHOUT
SAVE(192) = BPA1	IROLL WASHOUT
SAVE(193) = BRA1	IYAW WASHOUT
SAVE(194) = BAXA3	IX INTER. WASHOUT
SAVE(195) = BAYA3	IY INTER. WASHOUT
SAVE(196) = BAZA3	IZ INTER.WASHOUT
SAVE(197) = BPA3	IROLL INTER. WASHOUT
SAVE(198) = BRA3	IYAW INTER. WASHOUT

IF (NVS .GT. 0) THEN

**** SAVING TIME TO PLOT

PLOTV(I,1) = T

**** SAVING SELECTED VARIABLES TO PLOT

```

DO (J=1,NVS)
  PLOTV(I,J+1) = SAVE(NVAR(J))
REPEAT
ENDIF
RETURN
END

```

 ***** SUBROUTINE TO SET UP SERVO
 ***** INPUT SERVO PARAMETERS

SUBROUTINE SERVO

COMMON/SMSRV1/XKPM,XKP,SCLOT,XKFORC,DMPOFF,DMPON
 COMMON/SMSRV2/COMP1,COMP2,COMP3,COMP4,COMP5

DIMENSION XKPM(6),XKP(6),SCLOT(6),XKFORC(6)
 DIMENSION COMP1(6),COMP2(6),COMP3(6),COMP4(6),COMP5(6)

WRITE(9,('YOU HAVE SELECTED: "SET UP SERVO"'))

```

WRITE(9,*)
WRITE(9,("ENTER SERVO PARAMETERS"))
WRITE(9,*)
WRITE(9,("COMMANDED POSITION GAIN (<CR> TO RETURN):"
XKPM(1) = 0
READ(9,*) (XKPM(I),I=1,6)
IF (XKPM(1) .EQ. 0) RETURN
WRITE(9,*)
WRITE(9,("FEEDBACK POSITION GAIN: "))
READ(9,*) (XKP(I),I=1,6)
WRITE(9,*)
WRITE(9,("SCALE FOR VALVE VOLTAGE (mV/in):"))
READ(9,*) (SCLOT(I),I=1,6)
WRITE(9,*)
WRITE(9,("DIFFERENTIAL PRESSURE GAIN: "))
READ(9,*) (XKFORC(I),I=1,6)
WRITE(9,*)
WRITE(9,("COMPENSATION GAINS #1: "))
READ(9,*) (COMP1(I),I=1,6)
WRITE(9,("COMPENSATION GAINS #2: "))
READ(9,*) (COMP2(I),I=1,6)
WRITE(9,("COMPENSATION GAINS #3: "))
READ(9,*) (COMP3(I),I=1,6)
WRITE(9,("COMPENSATION GAINS #4: "))
READ(9,*) (COMP4(I),I=1,6)
WRITE(9,("COMPENSATION GAINS #5: "))
READ(9,*) (COMP5(I),I=1,6)
WRITE(9,("2 DAMPING FADE LIMITS (HIGHER FIRST)"))
READ(9,*) DMPON,DMPOFF
RETURN
END

```

```

*****
***** SUBROUTINE TO EXECUTE INVERSE TRANSFORMATIONS
***** FROM CYLINDER LENGTHS (CEXT) IT CALCULATES
***** POSITION AND ANGULAR ORIENTATION OF UPPER PLATFORM (TIN VX)
***** USES MARQUAROT ALGORITHM FOR CONVERGENCE
***** TIN VXI: INITIAL CONDITION VECTOR
***** EPSILON AND TOL: TOLERANCE FOR CONVERGENCE
*****
SUBROUTINE SMIGT(CEXT,TIN VXI,TIN VX,EPSILON)

**** INPUT AND OUTPUT OF TRANSFORMATION - TIN VX
**** X,Y,Z,THETA,PHI,PSI OF UPPER PLATFORM

DIMENSION TIN VX(6),CEXT(6),TIN VXI(6)
DIMENSION F(6),DF(6,6),DFINV(6,6),DECTIV(6)
DIMENSION TIN VXN(6),TIN VXL(6)
DIMENSION CX(6),CY(6),BX(6),BY(6),XL(6),FF(6)
DIMENSION FI(6,6),DFT(6,6),H(6),HTH(6,6),DFI(6,6)

**** INITIALIZE THE DIFFERENT CONSTANTS USED

```

DATA V,TOL/10.,0.00001/

DATA (CX(I),I=1,6)/51.428,-22.931,-28.497,-28.497,-22.931,51.428/

DATA (CY(I),I=1,6)/3.214,46.146,42.931,-42.931,-46.146,-3.214/

DATA(B X(I),I=1,6)/36.891,31.324,68.215,68.215,31.324,36.891/

DATA (BY(I),I=1,6)/57.469,60.683,3.214,-3.214,-60.683,-57.469/

BZ=65.942

RMU = 0.01

**** FI IS THE IDENTITY MATRIX

```
DO (I=1,6)
  DO (J=1,6)
    IF (I.EQ. J) THEN
      FI(I,J) = 1.
    ELSE
      FI(I,J) = 0.
    ENDIF
  REPEAT
REPEAT
```

**** REARRANGE INPUT VECTOR - INITIAL CONDITION

```
TINVXN(1) = TINVXI(1)
TINVXN(2) = TINVXI(2)
TINVXN(3) = TINVXI(3)-BZ
TINVXN(4) = TINVXI(6)
TINVXN(5) = TINVXI(4)
TINVXN(6) = TINVXI(5)
```

**** CALCULATE TOTAL LENGTH OF VECTORS L

```
DO (I=1,6)
  XL1 = CX(I) - BX(I)
  XL2 = CY(I) - BY(I)
  XL3 = BZ
  XL(I) = SQRT(XL1**2+XL2**2+XL3**2)
  XL(I) = XL(I) + CEXT(I)
REPEAT
```

WHILE (1>0)

**** MAKE NEW PARAMETERS EQUAL OLD PARAMETERS

```
DO (I=1,6)
  TINVXL(I) = TINVXN(I)
REPEAT
```

```
T11=COS(TINVXL(4))*COS(TINVXL(5))
T12 = SIN(TINVXL(4))*COS(TINVXL(5))
T13 = -1.*SIN(TINVXL(5))
T21 = COS(TINVXL(4))*SIN(TINVXL(5))*SIN(TINVXL(6))
```

```

+   -SIN(TINVXL(4))*COS(TINVXL(6))
T22 = SIN(TINVXL(4))*SIN(TINVXL(5))*SIN(TINVXL(6))
+   +COS(TINVXL(4))*COS(TINVXL(6))
T23 = COS(TINVXL(5))*SIN(TINVXL(6))
T31 = COS(TINVXL(4))*SIN(TINVXL(5))*COS(TINVXL(6))
+   +SIN(TINVXL(4))*SIN(TINVXL(6))
T32 = SIN(TINVXL(4))*SIN(TINVXL(5))*COS(TINVXL(6))
+   -COS(TINVXL(4))*SIN(TINVXL(6))
T33 = COS(TINVXL(5))*COS(TINVXL(6))

DO (I=1,6)
  TX=CX(I)
  TY=CY(I)
  TZ=0

  CALL ROTATE(TINVXL(6),TY,TZ)
  CALL ROTATE(TINVXL(5),TZ,TX)
  CALL ROTATE(TINVXL(4),TX,TY)

  XL1=TX-BX(I)+TINVXL(1)
  XL2=TY-BY(I)+TINVXL(2)
  XL3=TZ+TINVXL(3)
  TEMP=XL1**2+XL2**2+XL3**2
  F(I) = TEMP - XL(I)**2

DF(I,1)=2*(TINVXL(1)+CX(I)*T11+CY(I)*T
21-BX(I))
DF(I,2) = 2*(TINVXL(2)+CX(I)*T12+CY(I)*T22-BY(I))
DF(I,3) = 2*(TINVXL(3)+CX(I)*T13+CY(I)*T23)
DF(I,4) = -2*(TINVXL(1)-BX(I))*(CX(I)*T12+CY(I)*T22)
+   +2*(TINVXL(2)-BY(I))*(CX(I)*T11+CY(I)*T21)
DF(I,5) = 2*(TINVXL(1)-BX(I))*(-CX(I)*SIN(TINVXL(5))*
+   COS(TINVXL(4))+CY(I)*SIN(TINVXL(6)))*
+   COS(TINVXL(5))*COS(TINVXL(4))
+   +2*(TINVXL(2)-BY(I))*(-CX(I)*SIN(TINVXL(5))
+   *SIN(TINVXL(4))+CY(I)*SIN(TINVXL(6)))*
+   COS(TINVXL(5))*SIN(TINVXL(4))-2*TINVXL(3)*(CX(I)
+   *COS(TINVXL(5))+CY(I)*SIN(TINVXL(6))
+   *SIN(TINVXL(5)))
DF(I,6) = 2*(TINVXL(1)-BX(I))*CY(I)*T31
+   +2*(TINVXL(2)-BY(I))*CY(I)*T32
+   +2*TINVXL(3)*CY(I)*T33

  REPEAT

**** CALCULATE THE NORM OF F

  SUM = 0.
  DO (I=1,6)
    SUM = SUM + F(I)**2
  REPEAT
  EFRO =SUM

**** CALCULATE TRANSPOSE OF DF: DFT

```

```

CALL MM_TRP(DF,DFT,6)

**** H = DFT*F

CALL MVV_MUL(DFT,F,H,6)

**** CALCULATE THE NORM OF H

SUM = 0.
DO (I=1,6)
  SUM = SUM + H(I)**2
REPEAT
RNORM = SQRT(SUM)

**** TEST IF TOLERANCE IS REACHED

IF (RNORM .LE. EPSILON) EXIT
RMU = RMU/(V**2)

ERRN = 2.*ERRO
WHILE (ERRN .GT. ERRO)
  RMU = RMU*V

**** HTH = DFT*DF

CALL MMM_MUL(DFT,DF,HTH,6)

**** DFI = DFT*DF + RMU*FI (RMU IS SCALAR)

CALL MMM_SUM(HTH,FI,DFI,RMU,6)

**** DFINV: INVERSE OF MATRIX DFI

CALL MAT_INV(DFI,DFINV,6,RCOND)

IF (RCOND .EQ. 0) CYCLE

**** DFINV*H=DECTIV (DECREMENT IN PARAMETER VECTOR TINVX)

CALL MVV_MUL(DFINV,H,DECTIV,6)

**** DECREMENT TINVX (POSITION AND
**** ANGULAR ORIENTATION OF UPPER PLATFORM)
**** AND CALCULATE ERROR FROM LAST DECREMENT (DELTA)

DO I=1, 6
  TINVXN(I) = TINVXL(I) - DECTIV(I)
REPEAT

DO (I=1,6)
  TX=CX(I)
  TY=CY(I)

```


TZ=0

CALL ROTATE(TINVXN(6),TY,TZ)
 CALL ROTATE(TINVXN(5),TZ, TX)
 CALL ROTATE(TINVXN(4),TX, TY)

XL1=TX-BX(I)+TINVXN(1)
 XL2=TY-BY(I)+TINVXN(2)
 XL3=TZ+TINVXN(3)
 TEMP=XL1**2+XL2**2+XL3**2
 FF(I) = TEMP - XL(I)**2
 REPEAT

**** CALCULATE SUM OF SQUARES OF FF

SUM = 0.
 DO (I=1,6)
 SUM = SUM + FF(I)**2
 REPEAT
 ERRN = SUM

REPEAT

**** CALCULATE SUM OF SQUARES OF DECTIV

SUM = 0.
 DO (I=1,6)
 SUM = SUM + DECTIV(I)**2
 REPEAT

IF (SUM .LE. TOL) EXIT

RMU = RMU*V

REPEAT

**** REARRANGE OUTPUT

TINVX(1) = TINVXL(1)
 TINVX(2) = TINVXL(2)
 TINVX(3) = TINVXL(3)+BZ
 TINVX(4) = TINVXL(5)
~~TINVX(5)~~ = ~~TINVXL(6)~~
 TINVX(6) = TINVXL(4)

RETURN
 END

 ***** SUBROUTINE FOR THE RESPONSE OF A SPECIAL EFFECT

SUBROUTINE SMSPEF(DTSE)

```

COMMON/SMSPE1/MAXGEN,MAXPAR,SPECIAL
COMMON/SMSPE2/IEFF,NAME,WADD
COMMON/SMSPE3/NGEN,PAR,IPOINT
COMMON/SMSPE4/MAXPSTO,IPTR,PSTO
COMMON/SMSPE5/KEEP,MAXKEEP
COMMON/SMSPE6/YAMP,DTSPEF
COMMON/SMSPE7/POSX,IEFFLG

```

```

DIMENSION NGEN(240),PAR(1000),KEEP(1000),PSTO(1000)
DIMENSION POSX(6),IEFFLG(20)
INTEGER WADD(20),SPECIAL(240)
CHARACTER NAME(20)*20
DIMENSION POSX(6),IFLGEN(240)

```

```
DTSPEF = DTSE
```

```
**** ZERO ELEMENTS OF OUTPUT
```

```

DO (I = 1,6)
  POSX(I) = 0.
REPEAT

```

```
**** TEST FOR GENERATORS
```

```
IF (MAXGEN .EQ. 0) RETURN
```

```
**** SET FLAGS TO FALSE
```

```

DO (I = 1,MAXGEN)
  IFLGEN(I) = 0
REPEAT

```

```
***SETFLAGSFORGENE
```

```
FATORSOFCORRESPONDINGSPECIALEFFECT
```

```

DO (J = 1,IEFF)
  IF (IEFFLG(J) .EQ. -1) THEN
    DO (I = 1,MAXGEN)
      IF (SPECIAL(I) .EQ. J) THEN
        IFLGEN(I) = -1
      ENDIF
    REPEAT
  ENDIF
REPEAT

```

```
**** INITIALIZE COUNTERS
```

```

IPTR = 1
IPT = 1

```

```
**** LOOP THROUGH ALL GENERATORS
```

```
DO (I = 1,MAXGEN)
```

```

**** TEST IF GENERATOR IS ON

      IF (IFLGEN(I) .EQ. -1) THEN

**** SELECT GENERATOR TYPE AND CALCULATE AMPLITUDE

      SELECT CASE (NGEN(I))
      CASE (1)
        CALL F1AMP(IPT)
      CASE (2)
        CALL F2AMP(IPT)
      CASE (3)
        CALL SINEAMP(IPT)
      END SELECT

**** WHERE TO ADD OUTPUT OF GENERATOR

      POSX(WADD(SPECIAL(I))) = POSX(WADD(SPECIAL(I))) + YAMP
      ELSE

**** SKIP PARAMETERS AND RESET PSTO VECTOR
      SELECT CASE (NGEN(I))
      CASE (1)
        IIK = 3
        PSTO(IPTR) = 10000.
        PSTO(IPTR+1) = 0.
      CASE (2)
        IIK = 4
        PSTO(IPTR) = 10000.
        PSTO(IPTR+1) = 0.
        PSTO(IPTR+2) = 0.
      CASE (3)
        IIK = 2
        PSTO(IPTR) = 0.
      END SELECT

**** INCREMENT POINTERS

      IPT = IPT + IIK
      IPTR = IPTR + IIK - 1
      ENDIF
      REPEAT

      RETURN
      END

*****
***** SUBROUTINE TO SIMULATE SERVO
*****
      SUBROUTINE SMSRV(DTSRV)

      COMMON/SMVAL3/XL1,XL2,XL3,APT,VO,XLIMIT,FRC,BETA0
      COMMON/SMVAL5/VOU

```

```

COMMON/SMVAL6/CPRS,RPRS,POSI,Q6,Q7
COMMON/SMSRV1/XKPM,XKP,SCLOT,XKFORC,DMPOFF,DMPON
COMMON/SMSRV2/COMP1,COMP2,COMP3,COMP4,COMP5
COMMON/SMSRV3/TEMP1,TEMP2,CYLOT,FORCE
COMMON/SMSRV4/COMPN

```

```

DIMENSION VOUT(6)
DIMENSION CPRS(6),RPRS(6),POSI(6),Q6(6),Q7(6)
DIMENSION XKPM(6),XKP(6),SCLOT(6),XKFORC(6)
DIMENSION COMP1(6),COMP2(6),COMP3(6),COMP4(6),COMP5(6)
DIMENSION TEMP1(6),TEMP2(6),CYLOT(6)
DIMENSION FORCE(6),COMPN(6)

```

```
DO (I = 1,6)
```

```
**** CALCULATE DIFFERENTIAL FORCE
```

```
FORCE(I) = (CPRS(I)-RPRS(I))*APT
```

```
**** COMPENSATION
```

```

COMPN(I) = TEMP2(I) + COMP3(I)*FORCE(I)*XKFORC(I)
IF (POSI(I) .GT. DMPON) THEN
  TMP = 1.
ELSE
  IF (POSI(I) .LT. DMPOFF) THEN
    TMP = 0.
  ELSE
    TMP = (POSI(I)-DMPOFF)/(DMPON-DMPOFF)
  ENDIF
ENDIF
TMP = COMPN(I)*TMP
DELTAY = CYLOT(I)*XKPM(I) + POSI(I)*XKP(I) + TMP

```

```
**** VOLTAGE TO VALVE
```

```
VOUT(I) = -SCLOT(I)*DELTAY
```

```
**** INTEGRATING IN THE COMPENSATION LOOP
```

```

XDOT1 = COMP1(I)*XKFORC(I)*FORCE(I)
+ COMP4(I)*COMPN(I)
XDOT2 = COMP2(I)*XKFORC(I)*FORCE(I)
+ COMP5(I)*COMPN(I) + TEMP1(I)
TEMP1(I) = TEMP1(I) + XDOT1*DTSRV
TEMP2(I) = TEMP2(I) + XDOT2*DTSRV
REPEAT

```

```

RETURN
END

```

```
*****
```

```
***** SUBROUTINE TO SIMULATE VALVE
```

```

*****
SUBROUTINE SMVALVE(DT)

COMMON/SMVAL1/DAMPM,BANDM,GAINM,XM1,XM2,XK,B,VRST
COMMON/SMVAL2/PS,PR
COMMON/SMVAL3/XL1,XL2,XL3,APT,VO,XLIMIT,FRC,BETAO
COMMON/SMVAL4/X,XDOT,PD,PDOT,XMOTOR,PISTON
COMMON/SMVAL5/VOUT
COMMON/SMVAL6/CPRS,RPRS,POSI,Q6,Q7
COMMON/SMVAL7/Q1,Q2,Q3,Q4,Q5,V

DIMENSION XM2(6),XK(6),B(6)
DIMENSION X(6,2),XDOT(6,2),PD(6,4),PDOT(6,4)
DIMENSION XMOTOR(4,5),PISTON(4,5),PISTOND(4,5)
DIMENSION VOUT(6)
DIMENSION CPRS(6),RPRS(6),POSI(6)
DIMENSION Q1(6),Q2(6),Q3(6),Q4(6),Q5(6),Q6(6),Q7(6),V(6,2)

DO (I=1,6)

**** SOLVE MOTOR EQUATION

CALL EULER(X,XDOT,2,XMOTOR,DT,VOUT(I),I)

***CHECKFORSATURATIONOFSPOOL                                POSITION

IF (X(I,1) .LT. -1.*XLIMIT) THEN
  X(I,1) = -1.*XLIMIT
  X(I,2) = 0
ENDIF
IF (X(I,1) .GT. XLIMIT) THEN
  X(I,1) = XLIMIT
  X(I,2) = 0
ENDIF

**** CALCULATE FLOW RATES

IF (X(I,1) .GE. 0.) THEN
  Q1(I) = FRC*SQRT(PS-CPRS(I))*X(I,1)
  Q2(I) = FRC*SQRT(RPRS(I)-PR)*X(I,1)
ELSE
  Q1(I) = FRC*SQRT(CPRS(I)-PR)*X(I,1)
  Q2(I) = FRC*SQRT(PS-RPRS(I))*X(I,1)
ENDIF

**** CALCULATE LEAKAGE FLOW

Q3(I) = XL1*(CPRS(I)-RPRS(I))
Q4(I) = XL2*(CPRS(I)-PR)
Q5(I) = XL3*(RPRS(I)-PR)

**** PISTON MATRIX - CONTINUOUS TIME (VARIABLE COEFFICIENTS)

```

```

PISTON(2,1)=-XK(I)/XM1 ; PISTON(2,2)=-B(I)/XM1
PISTON(2,3)=-PISTON(2,1) ; PISTON(2,4)=-PISTON(2,2)
PISTON(4,1)=XK(I)/XM2(I) ; PISTON(4,2)=B(I)/XM2(I)
PISTON(4,3)=-PISTON(4,1) ; PISTON(4,4)=-PISTON(4,2)
PISTON(2,5)= APT/XM1

```

```

***MULTPLYNGT                                HEWHOLEMATRIXBYG(GRAVITY)

```

```

**** BECAUSE OF MASS GIVEN IN lb

```

```

DO (IJ1=1,5)
  PISTON(2,IJ1) = PISTON(2,IJ1)*32.2*12
  PISTON(4,IJ1) = PISTON(4,IJ1)*32.2*12
REPEAT

```

```

**** CALCULATE PISTON DISPLACEMENT
**** INPUT TO PISTON EQUATION - DIFFERENTIAL PRESSURE

```

```

UIN = CPRS(I)-RPRS(I)
CALL EULER(PD,PDOT,4,PISTON,DT,UIN,I)

```

```

**** CALCULATE VOLUMES AND COMPRESSIBILITY FLOW

```

```

V(I,1) = VO/2. + APT*PD(I,1)
V(I,2) = VO/2. - APT*PD(I,1)
Q6(I) = Q1(I) - Q3(I) - Q4(I) - APT*PD(I,2)
Q7(I) = Q3(I) - Q2(I) - Q5(I) + APT*PD(I,2)

```

```

**** CALCULATE NEW PRESSURES

```

```

CPRS(I) = CPRS(I) + (Q6(I)/V(I,1))*BETAO*DT
RPRS(I) = RPRS(I) + (Q7(I)/V(I,2))*BETAO*DT

```

```

**** CHECK FOR SATURATION OF PRESSURES

```

```

IF (CPRS(I) .GT. PS) CPRS(I) = PS
IF (CPRS(I) .LT. PR) CPRS(I) = PR
IF (RPRS(I) .GT. PS) RPRS(I) = PS
IF (RPRS(I) .LT. PR) RPRS(I) = PR

```

```

**** NEW CYLINDER LENGTHS

```

```

POS = PD(I)

```

```

REPEAT
RETURN
END

```

```

*****
***** SUBROUTINE MENU TO TOTAL SIMULATION
*****

```

```

SUBROUTINE TSMUL

```

**** DISPLAY MENU FOR TOTAL SIMULATION

```

WHILE (1>0)
  WRITE(9,*)
  WRITE(9,*)
  WRITE(9,('          SIMULATION MENU  '))
  WRITE(9,*)
  WRITE(9,*)
  WRITE(9,('0. RETURN TO PREVIOUS MENU  '))
  WRITE(9,('1. INPUTS                    '))
  WRITE(9,('2. EXECUTE                    '))
  WRITE(9,('3. BASE MOVEMENT ANIMATION  '))
  WRITE(9,('4. DISPLAY RESULTS          '))
  WRITE(9,('5. CHANGE/VIEW PARAMETERS  '))
  WRITE(9,*)
  WRITE(9,*)
  WRITE(9,('ENTER YOUR SELECTION  '))
  WRITE(9,*)
  WRITE(9,*)

```

****FEAD

SELECTION

```

ICH = 1000
READ(9,*) ICH
SELECT CASE (ICH)
  CASE (0)
    EXIT
  CASE (1)
    CALL INPUTS
  CASE (2)
    CALL SIMULATE
  CASE (3)
    CALL ANIMATE
  CASE (4)
    CALL DISRES
  CASE (5)
    CALL CHGPAR
  CASE DEFAULT
    WRITE(9,('ILLEGAL CHOICE'))
    WRITE(9,('MAKE ANOTHER SELECTION'))
END SELECT
REPEAT
RETURN
END

```

***** SUBROUTINE TO ENTER VALVE PARAMETERS

SUBROUTINE VALVE

```

COMMON/SMVAL1/DAMPM,BANDM,GAINM,XM1,XM2,XK,B,VRST
COMMON/SMVAL2/PS,PR
COMMON/SMVAL3/XL1,XL2,XL3,APT,VO,XLIMIT,FRC,BETAO

```

```

DIMENSION XM2(6),XK(6),B(6)

WRITE(9,('"YOU HAVE SELECTED: "SET UP VALVE"'))
WRITE(9,('"ENTER VALVE PARAMETERS"'))
WRITE(9,('MOTORS SPECIFICATIONS'))
WRITE(9,('"DAMPING (<CR> TO RETURN): "'))
DAMPM = -1
READ(9,*) DAMPM
WHILE ((DAMPM .LT. 0) .OR. (DAMPM .GT. 1.0))
  IF (DAMPM .EQ. -1) RETURN
  DAMPM = -1
  WRITE(9,*)
  WRITE(9,('"ILLEGAL DAMPING RATIO"'))
  READ(9,*) DAMPM
REPEAT
WRITE(9,('"BANDWIDTH (Hz):"'))
READ(9,*) BANDM
WRITE(9,('"GAIN (in/mA):"'))
READ(9,*) GAINM
WRITE(9,('"RESISTANCE (ohms):"'))
READ(9,*) VRST
WRITE(9,*)
WRITE(9,*)
WRITE(9,('"VALVE SPECIFICATIONS"'))
WRITE(9,('"SUPPLY PRESSURE (psi):"'))
READ(9,*) PS
WRITE(9,('"RETURN PRESSURE (psi):"'))
READ(9,*) PR
WRITE(9,('"LEAKAGE FLOW CONSTANTS (in3/(s*psi):"'))
READ(9,*) XL1,XL2,XL3
WRITE(9,('"AREA OF PISTON (in2):"'))
READ(9,*) APT
WRITE(9,('"TOTAL EFFECTIVE VOLUME (in3):"'))
READ(9,*) VO
WRITE(9,('"LIMIT OF SPOOL POSITION (in):"'))
READ(9,*) XMIT
WRITE(9,('"FLOW RATE CONSTANT:"'))
READ(9,*) FRC
WRITE(9,*)
WRITE(9,*)
WRITE(9,('"OIL SPECIFICATIONS"'))
WRITE(9,('"BULK MODULUS (psi):"'))
READ(9,*) BETAO
WRITE(9,*)
WRITE(9,*)
WRITE(9,('"MASS OF CYLINDER (lb):"'))
READ(9,*) XM1
WRITE(9,*)
WRITE(9,*)
WRITE(9,('"MODEL OF MOTION BASE"'))
WRITE(9,('"MASS OF BASE FOR EACH CYLINDER (lb):"'))
READ(9,*) (XM2(I),I=1,6)

```



```
WRITE(9,('SPRING CONSTANT FOR EACH CYLINDER (lb/in):'))
READ(9,*) (XK(I),I=1,6)
WRITE(9,('DAMPING COEFF. FOR EACH CYLINDER (lb/(in/s)):'))
READ(9,*) (B(I),I=1,6)
RETURN
END
```

```
*****
```

```
**** INCLUDE ROUTINES FOR GRAPHICS TERMINAL
```

```
INCLUDE GRAPHLIB.SA
```

```
**** INCLUDE SPECIAL EFFECTS SET UP ROUTINES
```

```
INCLUDE UFSPEFF.SA
```

```
**** INCLUDE MATRIX OPERATIONS ROUTINES
```

```
INCLUDE MVUTIL.SA
```

```
INCLUDE LINPAC.SA
```

```
**** INCLUDE PRIMARY MOTION SUBROUTINES
```

```
INCLUDE SYS:65..PRIMFOR.SA
```

```

*****
***** PURPOSE: USER FRIENDLY FOR SPECIAL EFFECTS OF
***** DIGITAL MOTION BASE SYSTEM
*****
***** SUBROUTINE TO ADD GENERATORS
*****
SUBROUTINE ADDGEN (J,NUMGEN)

**** J DEFINES NUMBER OF SPECIAL EFFECT

COMMON/SMSPE1/MAXGEN,MAXPAR,SPECIAL
COMMON/SMSPE3/NGEN,PAR,IPOINT
INTEGER SPECIAL(240)
DIMENSION NGEN(240),PAR(1000)
CHARACTER CH*1

**** GENERATOR POINTER

IGEN = MAXGEN
XGEN = MAXGEN

**** PARAMETERS POINTER

IPOINT = MAXPAR

**** TEST IF MAXIMUM NUMBER OF GENERATORS IS OBTAINED

IF ((MAXGEN .GE. 240) .OR. (NUMGEN .GE. 12)) THEN
WRITE(9,*)
WRITE(9,("NO MORE GENERATORS CAN BE ADDED"))
WRITE(9,(" <CR> TO CONTINUE"))
PAUSE
WRITE(9,*)
RETURN
ENDIF

**** DISPLAY MENU FOR TYPE OF GENERATOR

WHILE (1>0)
WRITE(9,*)
WRITE(9,*)
WRITE(9,(" GENERATOR TYPE SELECTION MENU    "))
WRITE(9,*)
WRITE(9,*)
WRITE(9,("    0. RETURN TO PREVIOUS MENU    "))
WRITE(9,(" 1.FILTERED WHITENOISE(1ST ORDER)"))
WRITE(9,("    2. FILTERED WHITE NOISE (2ND ORDER)"))
WRITE(9,("    3. SINE WAVE                    "))
WRITE(9,*)
WRITE(9,*)
WRITE(9,(" ENTER YOUR SELECTION    "))
WRITE(9,*)

```

```
WRITE(9,*)
**** DISPLAY MENU ON GRAPHICS

CALL GRAPHADD(J)

**** READ SELECTION

I = 1000
READ(9,*) I

**** TYPE OF GENERATOR SELECTION

SELECT CASE (I)
CASE (0)

**** UPDATE MAX. PARAMETERS AND MAX. GENERATORS

MAXGEN = IGEN
MAXPAR = IPOINT
EXIT
CASE (1)

**** BLINK FIRST ORDER FILTER ON GRAPHICS

CALL BLINKX(64,0,0,0,10,10)

**** INPUT PARAMETERS FOR FIRST ORDER FILTER

CALL F1ADD(IGEN,J)

**** STOP BLINKING

CALL BLINKX(64,0,0,0,0,0)
CASE (2)

**** BLINK SECOND ORDER FILTER ON GRAPHICS

CALL BLINKX(23,0,0,0,10,10)

****INPUTPARAMETER                                SFORSECONDORDERFILTER

CALL F2ADD(IGEN,J)

**** STOP BLINKING

CALL BLINKX(23,0,0,0,0,0)
CASE (3)

**** BLINK SINE WAVE ON GRAPHICS

CALL BLINKX(11,0,0,0,10,10)
```

**** INPUT PARAMETERS FOR SINE WAVE

CALL SINEADD(IGEN,J)

**** STOP BLINKING

```
CALL BLINKX(11,0,0,0,0)
CASE DEFAULT
WRITE(9,('ILLEGAL CHOICE'))
WRITE(9,('MAKE ANOTHER SELECTION'))
END SELECT
```

**** UPDATE NUMGEN

```
IF (XGEN .NE. IGEN) THEN
XGEN = XGEN + 1
NUMGEN = NUMGEN + 1
ENDIF
```

```
IF (NUMGEN .GE. 12) THEN
WRITE(9,*)
WRITE(9,('NO MORE GENERATORS CAN BE ADDED'))
WRITE(9,(' <CR> TO CONTINUE'))
PAUSE
WRITE(9,*)
```

**** UPDATE MAX. PARAMETERS AND MAX. GENERATORS

```
MAXGEN = IGEN
MAXPAR = IPOINT
EXIT
ENDIF

REPEAT

RETURN
END
```

 ***** SUBROUTINE TO ADD A SPECIAL EFFECT

SUBROUTINE ADDSE

```
COMMON/SMSPE2/IEFF,NAME,WADD
INTEGER WADD(20)
CHARACTER NAME(20)*20,C*20
MAXSE = 20
```

**** TEST MAXIMUM NUMBER OF SPECIAL EFFECTS

```
IF (IEFF .GE. MAXSE) THEN
WRITE(9,*)
WRITE(9,('NO MORE SPECIAL EFFECTS CAN BE ADDED'))
WRITE(9,(' <CR> TO CONTINUE'))
PAUSE
```

```

WRITE(9,*)
RETURN
ENDIF

```

**** INPUT NAME OF SPECIAL EFFECT

```

WRITE(9,*)
WRITE(9,*)
WRITE(9,*)
WRITE(9,('YOU HAVE SELECTED: "ADD A SPECIAL EFFECT"'))
WRITE(9,(' SPECIAL EFFECT NUMBER: ",I3)') IEFF+1
WRITE(9,(' ENTER NAME OF SPECIAL EFFECT (MAXIMUM 20 CHARACT
+ERS): "'))
WRITE(9,('1__5__0__5__0 (<CR> TO RETURN TO SPECIAL E
+FFECTS MENU)'))
C= 0
READ(9,*) C
IF (C(1:1) .EQ. '0') THEN
RETURN
ELSE
IEFF = IEFF + 1
NAME(IEFF) = C
ENDIF
WRITE(9,*)
WRITE(9,*)
WRITE(9,(' WHERE TO ADD OUTPUT OF SPECIAL EFFECT'))
WRITE(9,*)
WRITE(9,(' 1. POSITION IN X AXIS'))
WRITE(9,(' 2. POSITION IN Y AXIS'))
WRITE(9,(' 3. POSITION IN Z AXIS'))
WRITE(9,(' 4. PITCH ANGLE'))
WRITE(9,(' 5. ROLL ANGLE'))
WRITE(9,(' 6. YAW ANGLE'))
WRITE(9,*)
WRITE(9,*)
WRITE(9,(' ENTER SELECTION'))
WADD(IEFF) = 10
READ(9,*) WADD(IEFF)
WHILE ((WADD(IEFF) .LT. 1) .OR. (WADD(IEFF) .GT. 6))
WRITE(9,*)
WRITE(9,('WRONG SELECTION - SELECT AGAIN'))
READ(9,*) WADD(IEFF)
REPEAT

```

**** ADD GENERATORS FOR SPECIFIED SPECIAL EFFECT

```

CALL ADDGEN (IEFF,0)
RETURN
END

```

***** SUBROUTINE TO CHANGE PARAMETERS OF A GENERATOR

SUBROUTINE CHGEN

```

COMMON/SMSPE3/NGEN,PAR,IPOINT
COMMON/SMSPE5/KEEP,MAXKEEP
DIMENSION NGEN(240),PAR(1000),KEEP(1000)

WRITE(9,*)
WRITE(9,*)
WRITE(9,*)
WRITE(9,('YOU HAVE SELECTED: "CHANGE A GENERATOR"'))
WRITE(9,('ENTER NUMBER OF GENERATOR TO CHANGE:'))
WRITE(9,(' <CR> TO RETURN TO PREVIOUS MENU'))
I = 0

```

**** TEST IF GENERATORS EXISTS

```

READ(9,*) I
WHILE ((I .LE. 0) .OR. (I .GT. MAXKEEP/2))
  IF (I .EQ. 0) RETURN
  I = 0
  WRITE(9,*)
  WRITE(9,*)
  WRITE(9,('WRONG SELECTION - SELECT AGAIN'))
  READ(9,*) I
REPEAT

```

**** INITIALIZE POINTERS

```

IPT = KEEP(2*I)
IP = KEEP(2*I-1)
SELECT CASE (NGEN(IP))
CASE (1)

```

**** FILTERED WHITE NOISE (1ST ORDER) - INPUT PARAMETERS

```

WRITE(9,*)
WRITE(9,*)
WRITE(9,('INPUT PARAMETERS FOR FILTERED WHITE NOISE (1ST
+ORDER) GENERATOR'))
WRITE(9,(' <CR> FOR NO CHANGE'))
WRITE(9,*)
WRITE(9,(' MEAN OF WHITE NOISE'))
READ(9,*) PAR(IPT)
WRITE(9,*)
WRITE(9,(' VARIANCE OF WHITE NOISE '))
READ(9,*) PAR(IPT+1)
WRITE(9,*)
WRITE(9,(' BANDWIDTH OF FILTER (in Hz)'))
READ(9,*) PAR(IPT+2)
WRITE(9,*)
CASE (2)

```

**** FILTERED WHITE NOISE (2ND ORDER) - INPUT PARAMETERS

```

WRITE(9,*)
WRITE(9,*)
WRITE(9,('INPUT PARAMETERS FOR FILTERED WHITE NOISE (2ND
+ORDER) GENERATOR'))
WRITE(9,(' <CR> FOR NO CHANGE'))
WRITE(9,*)
WRITE(9,(' MEAN OF WHITE NOISE'))
READ(9,*) PAR(IPT)
WRITE(9,*)
WRITE(9,(' VARIANCE OF WHITE NOISE'))
READ(9,*) PAR(IPT+1)
WRITE(9,*)
W                                     WRITE(9,(' BANDWIDTH OF FILTER(nHz)'))
READ(9,*) PAR(IPT+2)
WRITE(9,*)
WRITE(9,(' DAMPING OF FILTER'))
READ(9,*) PAR(IPT+3)
WHILE ((PAR(IPT+3) .LT. 0) .OR. (PAR(IPT+3) .GT. 1))
  WRITE(9,*)
  WRITE(9,(' INVALID DAMPING - ENTER AGAIN'))
  READ(9,*) DMP
REPEAT
CASE (3)

```

**** SINE WAVE - INPUT PARAMETERS

```

WRITE(9,*)
WRITE(9,*)
WRITE(9,('INPUT PARAMETERS FOR SINE WAVE GENERATOR'))
WRITE(9,(' <CR> FOR NO CHANGE'))
WRITE(9,*)
WRITE(9,(' AMPLITUDE OF SINE WAVE'))
READ(9,*) PAR(IPT)
WRITE(9,*)
WRITE(9,(' FREQUENCY OF SINE WAVE'))
READ(9,*) PAR(IPT+1)
WRITE(9,*)
END SELECT
RETURN
END

```

***** SUBROUTINE TO CHANGE A SPECIAL EFFECT

SUBROUTINE CHGSE

```

COMMON/SMSPE1/MAXGEN,MAXPAR,SPECIAL
COMMON/SMSPE2/IEFF,NAME,WADD
COMMON/SMSPE3/NGEN,PAR,IPOINT
COMMON/SMSPE5/KEEP,MAXKEEP
DIMENSION NGEN(240),PAR(1000)

```

```

DIMENSION KEEP(1000)
INTEGER SPECIAL(240),WADD(20)
CHARACTER NAME(20)*20,CH*1

```

```

**** READ NUMBER OF SPECIAL EFFECT

```

```

WRITE(9,*)
WRITE(9,*)
WRITE(9,*)
WRITE(9,('YOU HAVE SELECTED: "CHANGE/VIEW A SPECIAL EFFECT'
+      '"'))
WRITE(9,('ENTER NUMBER OF SPECIAL EFFECT TO CHANGE/VIEW'))
WRITE(9,(' <CR> TO RETURN TO PREVIOUS MENU'))
J = 0
READ(9,*) J

```

```

**** TEST IF SPECIAL EFFECT EXISTS

```

```

WHILE ((J .LE. 0) .OR. (J .GT. IEFF))
  IF (J .EQ. 0) RETURN
  J = 0
  WRITE(9,*)
  WRITE(9,*)
  WRITE(9,('WRONG SELECTION - SELECT AGAIN'))
  READ(9,*) J
REPEAT

```

```

**** INITIALIZING

```

```

I = 1
L = 0
IPT = 1

```

```

WHILE MAX          GEN(0)

```

```

**** SELECTING INCREMENT TO POINTER

```

```

SELECT CASE (NGEN(I))
  CASE (1)
    IIK = 3
  CASE (2)
    IIK = 4
  CASE (3)
    IIK = 2
END SELECT

```

```

**** TEST IF GENERATOR BELONGS TO SPECIAL EFFECT

```

```

IF (SPECIAL(I) .EQ. J) THEN

```

```

**** IF TRUE STORE POINTERS OF GENERATOR
**** AND INCREMENT INDEX

```



```

      L = L + 2

****   INDEX OF GENERATOR

      KEEP(L-1) = I

****   POINTER TO PARAMETERS

      KEEP(L) = IPT
      ENDIF

**** INCREMENT POINTER

      IPT = IPT + IIK

**** TEST IF LAST GENERATOR

      IF (I .EQ. MAXGEN) THEN
          EXIT
      ELSE

**** IF NOT INCREMENT POINTER

          I = I + 1
          ENDIF
      REPEAT

**** STORE MAXIMUM NUMBERS OF GENERATORS IN SPECIAL EFFECT

      MAXKEEP = L

      WHILE (1>0)
          WRITE(9,*)
          WRITE(9,*)
          WRITE(9,*)
          WRITE(9,*)
      WRITE(9,*) MENU TO CHANGE V                               E WAS SPECIAL EFFECT ))
          WRITE(9,*)
          WRITE(9,*)
          WRITE(9,*)(" 0. RETURN TO PREVIOUS MENU    ")
          WRITE(9,*)(" 1. ADD A GENERATOR          ")
          WRITE(9,*)(" 2. DELETE A GENERATOR         ")
          WRITE(9,*)(" 3. CHANGE A GENERATOR        ")
          WRITE(9,*)(" 4. RESPONSE OF THIS SPECIAL EFFECT)")
          WRITE(9,*)(" 5. COPY OF GRAPHICS SCREEN   ")
          WRITE(9,*)
          WRITE(9,*)
          WRITE(9,*)(" ENTER YOUR SELECTION      ")
          WRITE(9,*)
          WRITE(9,*)

**** LIST PARAMETERS OF GENERATORS ON GRAPHICS SCREEN

      CALL GRAGEN (J)

```

```

ICH = 100
READ(9,*) ICH
SELECT CASE (ICH)
  CASE (0)
    EXIT
  CASE (1)

**** STORE MAXGEN AND MAXPAR BEFORE ADDING GENERATORS

      ILTGEN = MAXGEN
      IPNT = MAXPAR

**** ADD GENERATORS

      CALLADDGEN(J,MAXK)          EEP/2

**** TEST IF ANY GENERATOR WAS ADDED

      IF (ILTGEN+1 .LE. MAXGEN) THEN

**** STORE POINTERS OF GENERATORS ADDED

      DO (K = ILTGEN+1,MAXGEN)
        MAXKEEP = MAXKEEP + 1
        KEEP(MAXKEEP) = K
        SELECT CASE (NGEN(K))
          CASE (1)
            MAXKEEP = MAXKEEP + 1
            KEEP(MAXKEEP) = IPNT + 1
            IPNT = IPNT + 3
          CASE (2)
            MAXKEEP = MAXKEEP + 1
            KEEP(MAXKEEP) = IPNT + 1
            IPNT = IPNT + 4
          CASE (3)
            MAXKEEP = MAXKEEP + 1
            KEEP(MAXKEEP) = IPNT + 1
            IPNT = IPNT + 2
        END SELECT
      REPEAT
    ENDIF
  CASE (2)
    CALL DELGEN
  CASE (3)
    CALL CHGEN
  CASE (4)
    CALL RSPSE (J)
  CASE (5)
    CH = '_'
    WRITE(9,("YOU HAVE SELECTED: "COPY GRAPHICS SCREEN"))
+   )
    WRITE(9,(" <CR> TO RETURN - ANYTHING TO CONTINUE"))
    READ(9,*) CH

```

```

      IF (CH .NE. '_') CALL PRNTTI
      CASE DEFAULT
        WRITE(9,('ILLEGAL CHOICE'))
        WRITE(9,('MAKE ANOTHER SELECTION'))
      END SELECT
    REPEAT
  RETURN
END

```

```
*****
```

```
***** SUBROUTINE TO CHANGE NAME/WHERE TO ADD SPECIAL EFFECT
```

```
*****
```

```
SUBROUTINE CHGWADD
```

```

COMMON/SMSPE1/MAXGEN,MAXPAR,SPECIAL
COMMON/SMSPE2/IEFF,NAME,WADD
INTEGER SPECIAL(50),WADD(20)
CHARACTER NAME(20)*20

```

```
**** INPUT NUMBER OF SPECIAL EFFECT TO CHANGE
```

```

WRITE(9,*)
WRITE(9,*)
WRITE(9,*)
WRITE(9, 'YOU HAVE SELECTED: "CHANGE NAME WHERE TO ADD SPECIAL EFFECT"')
+L EFFECT"')
WRITE(9,('ENTER NUMBER OF SPECIAL EFFECT TO CHANGE'))
WRITE(9,(' <CR> TO RETURN TO SPECIAL EFFECTS MENU'))
J = 0
READ(9,*) J

```

```
**** TEST IF SPECIAL EFFECT EXISTS
```

```

WHILE ((J .LE. 0) .OR. (J .GT. IEFF))
  IF (J .EQ. 0) RETURN
  J = 0
  WRITE(9,*)
  WRITE(9,(' ILLEGAL SELECTION - SELECT AGAIN'))
  READ(9,*) J
REPEAT

```

```
**** INPUT CORRECT NAME OF SPECIAL EFFECT
```

```

WRITE(9,*)
WRITE(9,(' ENTER NAME OF SPECIAL EFFECT (MAXIMUM 20 CHARACTERS): '))
WRITE(9,('1__5__0__5__0 (<CR> FOR NO CHANGE)'))
READ(9,*) NAME(J)
WRITE(9,*)
WRITE(9,*)
WRITE(9,(' WHERE TO ADD OUTPUT OF SPECIAL EFFECT'))
WRITE(9,(' 1. POSITION IN X AXIS'))
WRITE(9,(' 2. POSITION IN Y AXIS'))

```

```

WRITE(9,(' 3. POSITION IN Z AXIS"))
WRITE(9,(' 4.PITCHANGLE)
WRITE(9,(' 5. ROLL ANGLE"))
WRITE(9,(' 6. YAW ANGLE"))
WRITE(9,*)
WRITE(9,*)
WRITE(9,(' ENTER SELECTION"))
WRITE(9,(' <CR> FOR NO CHANGE"))
WADD(J) = 10
READ(9,*) WADD(J)
WHILE ((WADD(J) .LT. 1) .OR. (WADD(J) .GT. 6))
  WRITE(9,*)
  WRITE(9,('WRONG SELECTION - SELECT AGAIN"))
  READ(9,*) WADD(J)
REPEAT
RETURN
END

```

***** SUBROUTINE TO DELETE A GENERATOR

SUBROUTINE DELGEN

```

COMMON/SMSPE1/MAXGEN,MAXPAR,SPECIAL
COMMON/SMSPE3/NGEN,PAR,IPOINT
COMMON/SMSPE5/KEEP,MAXKEEP
DIMENSION NGEN(240),PAR(1000)
DIMENSION KEEP(1000)
INTEGER SPECIAL(240)

```

**** ENTER GENERATOR TO BE DELETED

```

WRITE(9,*)
WRITE(9,*)
WRITE(9,*)
WRITE(9,('YOU HAVE SELECTED: "DELETE A GENERATOR"'))
WRITE(9,('ENTER NU          MEER OF GENERATOR TO DELETE))
WRITE(9,(' <CR> TO RETURN TO PREVIOUS MENU"))
I = 0

```

**** TEST IF GENERATOR EXISTS

```

READ(9,*) I
WHILE ((I .LE. 0) .OR. (I .GT. MAXKEEP/2))
  IF (I .EQ. 0) RETURN
  I = 0
  WRITE(9,*)
  WRITE(9,*)
  WRITE(9,('WRONG SELECTION - SELECT AGAIN"))
  READ(9,*) I
REPEAT

```

**** DECREMENT NUMBER OF GENERATORS

```

MAXGEN = MAXGEN - 1

**** POINTER OF GENERATOR

IP = KEEP(2*I-1)

**** SELECT DECREMENT OF PARAMETERS

SELECT CASE (NGEN(IP))
CASE (1)
  IIK = 3
CASE (2)
  IIK = 4
CASE (3)
  IIK = 2
END SELECT
MAXPAR = MAXPAR - IIK

**** TEST IF LAST GENERATOR

IF (I .NE. MAXGEN+1) THEN

**** IF NOT MOVE PARAMETERS UP

  DO (K = KEEP(2*I),MAXPAR)
    PAR(K) = PAR(K+IIK)
  REPEAT
  DO (K = IP,MAXGEN)
    SPECIAL(K) = SPECIAL(K+1)
  NGEN(K) = NGEN(K+1)
  REPEAT
ENDIF

**** TEST IF LAST GENERATOR

IF (2*I .NE. MAXKEEP) THEN

**** IF NOT MOVE PARAMETERS UP
DO (K = 2*I,MAXKEEP-2,2)
  KEEP(K-1) = KEEP(K+1) - 1
  KEEP(K) = KEEP(K+2) - IIK
REPEAT
ENDIF

**** DECREMENT NUMBER OF PARAMETERS STORED FOR GENERATOR

MAXKEEP = MAXKEEP - 2
RETURN
END

```

```

*****
***** SUBROUTINE TO DELETE A SPECIAL EFFECT
*****

```

```

SUBROUTINE DELSE

COMMON/SMSPE1/MAXGEN,MAXPAR,SPECIAL
COMMON/SMSPE2/IEFF,NAME,WADD
COMMON/SMSPE3/NGEN,PAR,IPOINT
DIMENSION NGEN(240),PAR(1000)
INTEGER SPECIAL(240),WADD(20)
CHARACTER NAME(20)*20

**** INITIALIZE POINTER

IPT = 1
I = 1

**** READ NUMBER OF SPECIAL EFFECT

WRITE(9,*)
WRITE(9,*)
WRITE(9,('YOU HAVE SELECTED: "DELETE A SPECIAL EFFECT"'))
WRITE(9,('ENTER NUMBER OF SPECIAL EFFECT TO DELETE'))
WRITE(9,(' <CR> TO RETURN TO SPECIAL EFFECTS MENU'))
J = 0
READ(9,*) J

**** TEST IF SPECIAL EFFECT EXISTS

WHILE ((J .LE. 0) .OR. (J .GT. IEFF))
  IF (J .EQ. 0) RETURN
  J = 0
  WRITE(9,*)
  WRITE(9,*)
  WRITE(9,('WRONG SELECTION - SELECT AGAIN'))
  READ(9,*) J
  REPEAT

**** MOVE NAMES AND WHERE TO ADD UP

DO (K = J+1,IEFF)
  NAME(K-1) = NAME(K)
  WADD(K-1) = WADD(K)
REPEAT

**** DECREMENT NUMBER OF SPECIAL EFFECTS

IEFF = IEFF - 1

WHILE (1>0)

**** SELECT DECREMENT OR INCREMENT IN NUMBER OF PARAMETERS

SELECT CASE (NGEN(I))
CASE (1)
  IIK = 3

```

```

CASE (2)
  IIK = 4
CASE (3)
  IIK = 2
END SELECT

****TEST IF GENERATOR BELONGS TO SPECIAL EFFECT SPECIFIED

  IF (SPECIAL(I) .EQ. J) THEN

****IF TRUE DECREMENT NUM          BEER OF GENERATORS

      MAXGEN = MAXGEN - 1

**** DECREMENT NUMBER OF PARAMETERS

      MAXPAR = MAXPAR - IIK

**** TEST IF LAST GENERATOR

      IF (I .EQ. MAXGEN+1) THEN
        EXIT
      ELSE

**** IF NOT TRUE MOVE PARAMETERS UP

          DO (K = IPT,MAXPAR)
            PAR(K) = PAR(K+IIK)
          REPEAT
          DO (K = 1,MAXGEN)
            SPECIAL(K) = SPECIAL(K+1)
            NGEN(K) = NGEN(K+1)
          REPEAT
        ENDIF
      ELSE

**** IF NOT TRUE SKIP PARAMETERS
**** INCREMENT POINTER

          IPT = IPT + IIK

**** TEST IF BELONGS TO A GREATER VALUE OF SPECIAL EFFECT

          IF (SPECIAL(I) .GT. J) THEN

**** SUBTRACT TO MAKE IT BELONG TO CORRECT SPECIAL EFFECT

              SPECIAL(I) = SPECIAL(I) - 1
            ENDIF

**** TEST IF LAST GENERATOR

          IF (I .EQ. MAXGEN) THEN

```

```

EXIT
ELSE

***NCR                                EVENTPONTERRFORGENERATORS

      I = I + 1
    ENDIF
  ENDIF
REPEAT
RETURN
END

*****
***** SUBROUTINE TO INPUT PARAMETERS FOR
***** FIRST ORDER FILTER GENERATOR
*****
      SUBROUTINE F1ADD (IGEN,J)

      COMMON/SMSPE1/MAXGEN,MAXPAR,SPECIAL
      COMMON/SMSPE3/NGEN,PAR,IPOINT
      DIMENSION NGEN(240),PAR(1000)
      INTEGER SPECIAL(240)
      REAL MEAN

**** INPUT PARAMETERS

      WRITE(9,*)
      WRITE(9,*)
      WRITE(9,('YOU HAVE SELECTED: "FILTERED WHITE NOISE (1ST ORDER
+ ) GENERATOR"'))
      WRITE(9,('INPUT PARAMETERS (<CR> TO RETURN TO PREVIOUS MENU)
+      '))
      WRITE(9,*)
      WRITE(9,(' MEAN OF WHITE NOISE'))
      MEAN = 1000
      READ(9,*) MEAN
      IF (MEAN .EQ. 1000) RETURN
      PAR(IPOINT+1) = MEAN
      WRITE(9,*)
      WRITE(9,(' VARIANCE OF WHITE NOISE'))
      READ(9,*) PAR(IPOINT+2)
      WRITE(9,*)
      WRITE(9,(' BANDWIDTH OF FILTER (in Hz)'))
      READ(9,*) PAR(IPOINT+3)
      WRITE(9,*)
      IPOINT = IPOINT + 3

**** INCREMENT NUMBER OF GENERATORS

      IGEN = IGEN + 1

**** SPECIFY WHICH SPECIAL EFFECT IT BELONGS TO

```


SPECIAL(IGEN) = J

**** TYPE OF GENERATOR

NGEN(IGEN) = 1
RETURN
END

***** SUBROUTINE TO CALCULATE AMPLITUDE FOR
***** FIRST ORDER FILTER GENERATOR

SUBROUTINE F1AMP (IPT)

COMMON/SMSPE3/NGEN,PAR,IPOINT
COMMON/SMSPE4/MAXPSTO,IPTR,PSTO
COMMON/SMSPE6/YAMP,DTSPEF
DIMENSION NGEN(240),PAR(1000)
DIMENSION PSTO(1000)
REAL M
DATA PI/3.1416/

**** MEAN OF WHITE NOISE

M = PAR(IPT)

**** VARIANCE OF WHITE NOISE

V = SQRT(12*PAR(IPT+1))

**** DECAY

A = EXP(-DTSPEF*2*PI*PAR(IPT+2))
B=1-A

**** INCREMENT POINTER

IPT = IPT + 3

**** GET LAST VALUE CALCULATED

X1 = PSTO(IPTR+1)

**** AMPLITUDE

YAMP = X1

**** CALCULATE WHITE NOISE

CALL WHITE (U,M,V)

**** CALCULATE UPDATE VALUE FOR FIRST ORDER FILTER

$X1 = A * X1 + B * U$

**** STORE LAST VALUE CALCULATED

PSTO(IPTR+1) = X1

**** INCREMENT POINTER

IPTR = IPTR + 2

RETURN

END

 ***** SUBROUTINE TO INPUT PARAMETERS FOR
 ***** SECOND ORDER FILTER GENERATOR

SUBROUTINE F2ADD (IGEN,J)

COMMON/SMSPE1/MAXGEN,MAXPAR,SPECIAL

COMMON/SMSPE3/NGEN,PAR,IPOINT

DIMENSION NGEN(240),PAR(1000)

INTEGER SPECIAL(240)

REAL MEAN

**** INPUT PARAMETERS

WRITE(9,*)

WRITE(9,*)

WRITE(9,('YOU HAVE SELECTED: "FILTERED WHITE NOISE (2ND ORDER
 +) GENERATOR"'))

WRITE(9,INPUTPARAMETE

RS (<CR> TO RETURN TO PREVIOUS MENU)

+ ")')

WRITE(9,*)

WRITE(9,(' MEAN OF WHITE NOISE'))

MEAN = 1000

READ(9,*) MEAN

IF (MEAN .EQ. 1000) RETURN

PAR(IPOINT+1) = MEAN

WRITE(9,*)

WRITE(9,(' VARIANCE OF WHITE NOISE'))

READ(9,*) PAR(IPOINT+2)

WRITE(9,*)

WRITE(9,(' BANDWIDTH OF FILTER (in Hz)'))

READ(9,*) PAR(IPOINT+3)

WRITE(9,*)

WRITE(9,(' DAMPING OF FILTER'))

READ(9,*) DMP

WHILE ((DMP .LT. 0) .OR. (DMP .GT. 1))

WRITE(9,*)

WRITE(9,(' INVALID DAMPING - ENTER AGAIN'))

READ(9,*) DMP

REPEAT

```
PAR(IPOINT+4) = DMP  
IPOINT = IPOINT + 4
```

```
**** INCREMENT NUMBER OF GENERATORS
```

```
IGEN = IGEN + 1
```

```
**** SPECIFY WHICH SPECIAL EFFECT IT BELONGS TO
```

```
SPECIAL(IGEN) = J
```

```
**** TYPE OF GENERATOR
```

```
NGEN(IGEN) = 2  
RETURN  
END
```

```

*****
***** SUBROUTINE TO CALCULATE AMPLITUDE FOR
***** SECOND ORDER FILTER GENERATOR
*****
SUBROUTINE F2AMP (IPT)

COMMON/SMSPE3/NGEN,PAR,IPOINT
COMMON/SMSPE4/MAXPSTO,IPTR,PSTO
COMMON/SMSPE6/YAMP,DTSPEF
DIMENSION NGEN(240),PAR(1000)
DIMENSION PSTO(1000)
DIMENSION AD(2,2),BD(2)
REAL M
DATA PI/3.1416/

**** MEAN OF WHITE NOISE

M = PAR(IPT)

**** VARIANCE OF WHITE NOISE

V = SQRT(12*PAR(IPT+1))

**** BANDWIDTH

BW = 2*PI*PAR(IPT+2)

**** DAMPING

Z = PAR(IPT+3)

**** INCREMENT POINTER

IPT = IPT + 4

ALPHA = Z*BW
OMEGA = BW*SQRT(1-Z**2)
TEMP = EXP(-ALPHA*DTSPEF)

**** COEFFICIENTS FOR SECOND ORDER FILTER

IF (OMEGA .NE. 0) THEN
  AD(1,1)=(COS(OMEGA*DTSPEF)
+   -(ALPHA/OMEGA)*SIN(OMEGA*DTSPEF))*TEMP
  AD(2,1)=-(1/OMEGA)*SIN(OMEGA*DTSPEF)*TEMP
  AD(1,2)=-AD(2,1)*(BW**2)
  AD(2,2)=(COS(OMEGA*DTSPEF)
+   +(ALPHA/OMEGA)*SIN(OMEGA*DTSPEF))*TEMP
  BD(1)=-AD(1,1)-1+2*(ALPHA/(BW**2))*AD(1,2)
  BD(2)=-AD(2,1)+2*(ALPHA/(BW**2))*(AD(2,2)-1))
ELSE
  AD(1,1)=(1-BW*DTSPEF)*TEMP
  AD(2,1)=-DTSPEF*TEMP

```

```

AD(1,2)=-AD(2,1)*(BW**2)
AD(2,2)=(1+BW*DTSPEF)*TEMP
BD(1)=-AD(1,1)-1+2*(Z/BW)*AD(1,2)
BD(2)=-AD(2,1)+2*(Z/BW)*(AD(2,2)-1)
ENDIF

```

```

**                               **GETLASTVALUECALCULATED

```

```

X1 = PSTO(IPTR+1)
X2 = PSTO(IPTR+2)

```

```

**** AMPLITUDE

```

```

YAMP = X1

```

```

**** CALCULATE WHITE NOISE

```

```

CALL WHITE (U,M,V)

```

```

**** CALCULATE UPDATE VALUE FOR SECOND ORDER FILTER

```

```

XU1 = AD(1,1)*X1 + AD(1,2)*X2 + BD(1)*U
XU2 = AD(2,1)*X1 + AD(2,2)*X2 + BD(2)*U

```

```

**** STORE LAST VALUE CALCULATED

```

```

PSTO(IPTR+1) = XU1
PSTO(IPTR+2) = XU2

```

```

**** INCREMENT POINTER

```

```

IPTR = IPTR + 3
RETURN
END

```

```

*****
***** SUBROUTINE TO DISPLAY PARAMETERS OF
***** GENERATORS ON GRAPHICS
*****

```

```

SUBROUTINE GRAGEN (J)

```

```

COMMON/SMSPE2/IEFF,NAME,WADD
COMMON/SMSPE3/NGEN,PAR,IPOINT
COMMON/SMSPE5/KEEP,MAXKEEP
DIMENSION NGEN(240),PAR(1000)
DIMENSION KEEP(1000)
CHARACTER NAME(20)*20,CK*4,CKT*2,TEMP*31,CM*12
CHARACTER TWADD(6)*10
REAL MEAN
INTEGER WADD(20)

```

```

DATANCV,IXSIZE,XX/13,420,1040

```

```

**** INITIALIZE TABLE TWADD

```

```
TWADD(1) = 'POS X AXIS'  
TWADD(2) = 'POS Y AXIS'  
TWADD(3) = 'POS Z AXIS'  
TWADD(4) = 'PITCH'  
TWADD(5) = 'ROLL'  
TWADD(6) = 'YAW'
```

```
CALL PLTINIT  
CALL COLOR(180)  
CALL SMOVE(10,450)
```

**** DISPLAY SPECIAL EFFECT NAME AND WHERE TO ADD

```
CALL TEXT(NAME(J),0,0,20)  
CALL SMOVE(10,435)  
CALL COLOR(197)  
TEMP = 'ADD OUTPUT AT: '//TWADD(WADD(J))  
CALL TEXT(TEMP,0,0,15)  
CALL COLOR(180)  
CALL SMOVE(0,433)  
CALL SDRAW(630,433)
```

**** TEST FOR GENERATORS

```
IF (MAXKEEP .EQ. 0) THEN  
  CALL COLOR(104)  
  CALL SMOVE(0,250)  
  CALL TEXT('NO GENERATORS',0,0,20)  
ELSE
```

**** DISPLAY PARAMETERS OF GENERATORS

```
DO (I = 1,MAXKEEP-1,2)  
  K = (I+1)/2  
  J1 = (-1)**K  
  IF (J1 .LT. 0) THEN
```

**** ODD J - COLOR (GREEN)

```
  ICOL = 104  
  ELSE
```

**** EVEN J - COLOR (BLUE)

```
  ICOL = 101  
  ENDIF  
  CALL COLOR(ICOL)
```

**** INITIALIZE POINTERS

```
  IPT = KEEP(I+1)  
  IP = KEEP(I)
```

```

SELECT CASE (NGEN(IP))
CASE (1)

**** TEST IF END OF GRAPHICS LINE

      IF ((IY-4*IYC) .LE. -12) THEN

**** IF TRUE LIST PARAMETERS ON RIGHT HALF OF SCREEN

      IX = 319
      IXX = 359
      IY = 420
      ENDIF

**** DISPLAY PARAMETERS

      MEAN = PAR(IPT)
      VAR = PAR(IPT+1)
      BDW = PAR(IPT+2)
      CALL ITOASC(K,CK)
      CKT = CK(3:4)
      TEMP = CKT//'. FILT. WHITE NOISE-1ST ORD'
      CALL SMOVE(IX,IY)
      CALL TEXT(TEMP,0,0,ISIZE)
      IY = IY - IYC
      CALL REALTO_ASCII(MEAN,CM)
      TEMP = 'MEAN = '//CM
      CALL SMOVE(IX,IY)
      CALL TEXT(TEMP,0,0,ISIZE)
      IY = IY - IYC
      CALL REALTO_ASCII(VAR,CM)
      TEMP = 'VARIANCE = '//CM
      CALL SMOVE(IXX,IY)
      CALL TEXT(TEMP,0,0,ISIZE)
      IY = IY - IYC
      CALL REALTO_ASCII(BDW,CM)
      TEMP = 'BANDWIDTH = '//CM
      CALL SMOVE(IXX,IY)
      CALL TEXT(TEMP,0,0,ISIZE)
      IY = IY - IYC - 4
      CASE(2)

**** TEST IF END OF GRAPHICS LINE

      IF ((IY-5*IYC) .LE. -12) THEN

**** IF TRUE LIST PARAMETERS ON RIGHT HALF OF SCREEN

      IX = 319
      IXX = 359
      IY = 420
      ENDIF

```

**** DISPLAY PARAMETERS

```

    MEAN = PAR(IPT)
    VAR = PAR(IPT+1)
    BDW = PAR(IPT+2)
    DMP = PAR(IPT+3)
    CALL ITOASC(K,CK)
    CKT = CK(3:4)
    TEMP=CKT/
    FLT.WHITENOISE2NDORD
    CALL SMOVE(IX,IY)
    CALL TEXT(TEMP,0,0,ISIZE)
    IY = IY - IYC
    CALL REALTO_ASCII(MEAN,CM)
    TEMP = 'MEAN = ' //CM
    CALL SMOVE(IXX,IY)
    CALL TEXT(TEMP,0,0,ISIZE)
    IY = IY - IYC
    CALL REALTO_ASCII(VAR,CM)
    TEMP = 'VARIANCE = ' //CM
    CALL SMOVE(IXX,IY)
    CALL TEXT(TEMP,0,0,ISIZE)
    IY = IY - IYC
    CALL REALTO_ASCII(BDW,CM)
    TEMP = 'BANDWIDTH = ' //CM
    CALL SMOVE(IXX,IY)
    CALL TEXT(TEMP,0,0,ISIZE)
    IY = IY - IYC
    CALL REALTO_ASCII(DMP,CM)
    TEMP = 'DAMPING = ' //CM
    CALL SMOVE(IXX,IY)
    CALL TEXT(TEMP,0,0,ISIZE)
    IY = IY - IYC - 4
    CASE (3)

```

**** TEST IF END OF GRAPHICS LINE

```

    F((Y310)LE .-12) THEN

```

**** IF TRUE LIST PARAMETERS ON RIGHT HALF OF SCREEN

```

    IX = 319
    IXX = 359
    IY = 420
    ENDIF

```

**** DISPLAY PARAMETERS

```

    AMPL = PAR(IPT)
    FREQ = PAR(IPT+1)
    CALL ITOASC(K,CK)
    CKT = CK(3:4)
    TEMP = CKT//'. SINE WAVE'
    CALL SMOVE(IX,IY)

```



```

CALL TEXT(TEMP,0,0,ISIZE)
IY = IY - IYC
CALL REALTO_ASCII(AMPL,CM)
TEMP = 'AMPLITUDE = '//CM
CALL SMOVE(IXX,IY)
CALL TEXT(TEMP,0,0,ISIZE)
IY = IY - IYC
CALL REALTO_ASCII(FREQ,CM)
TEMP = 'FREQUENCY = '//CM
CALL SMOVE(IXX,IY)
CALL TEXT(TEMP,0,0,ISIZE)
IY = IY - IYC - 4
END SELECT
REPEAT
ENDIF
RETURN
END

```

```

*****
***** SUBROUTINE TO LIST CURRENT SPECIAL EFFECTS ON GRAPHICS
*****

```

```

SUBROUTINE GRAMENU

```

```

COMMON/SMSPE2/IEFF,NAME,WADD
CHARACTER NAME(20)*20,TEMP*35,CI*4,CIT*2,TWADD(6)*5
INTEGER WADD(20)

```

```

**** INITIALIZE TABLE TWADD

```

```

TWADD(1) = 'POS X'
TWADD(2) = 'POS Y'
TWADD(3) = 'POS Z'
TWADD(4) = 'PITCH'
TWADD(5) = 'ROLL'
TWADD(6) = 'YAW '

```

```

**** CLEAR SCREEN

```

```

CALL PLTINIT

```

```

**** TEST IF THERE ARE ANY SPECIAL EFFECTS

```

```

IF (IEFF .EQ. 0) THEN
CALL COLOR(104)
CALL SMOVE(10,250)
CALL TEXT('NO CURRENT SPECIAL EFFECTS',0,0,20)
ELSE

```

```

**** DISPLAY CURRENT SPECIAL EFFECTS

```

```

CALL COLOR(179)
CALL SMOVE(30,430)
CALL TEXT('CURRENT SPECIAL EFFECTS',0,0,20)

```

```

CALL SMOVE(10,420)
CALL SDRAW(610,420)
CALL SMOVE(10,419)
CALL SDRAW(610,419)
CALL SMOVE(10,418)
CALL SDRAW(610,418)

IY = 390
CALL COLOR(104)
DO (I = 1,IEFF)
  CALL ITOASC(I,CI)
  CIT = CI(3:4)
  CALL SMOVE(20,IY)
  TEMP = CIT//'. '//NAME(I)//'AT: '//TWADD(WADD(I))
  CALL TEXT(TEMP,0,0,15)
  IY = IY - 20
REPEAT
ENDIF
RETURN
END

```

```
*****
```

```
***** MENU FOR GRAPHICS TO ADD GENERATORS
```

```
*****
```

```
SUBROUTINE GRAPHADD (J)
```

```

COMMON/SMSPE2/IEFF,NAME,WADD
CHARACTER NAME(20)*20,TEMP*36
INTEGER WADD(20)

```

```
**** DISPLAYS MENU FOR TYPE OF GENERATOR ON GRAPHICS MONITOR
```

```
**** CLEAR SCREEN
```

```
CALL PLTINIT
```

```

CALL COLOR(180)
CALL SMOVE(100,420)
CALL TEXT('ADD GENERATORS',0,0,20)

```

```
**** WRITE NAME OF SPECIAL EFFECT THAT IS ADDING GENERATORS
```

```

CALL COLOR(209)
CALL SMOVE(100,390)
TEMP = 'SPECIAL EFFECT: '//NAME(J)
CALL TEXT(TEMP,0,0,15)

```

```
**** DRAW A RECTANGLE
```

```

CALL PRMFIL(0)
CALL COLOR(31)
CALL SMOVE(0,145)
CALL SRECT(550,350)
CALL SMOVE(1,146)
CALL SRECT(549,349)

```

CALL SMOVE(2,147)
CALL SRECT(548,348)

**** DRAW A RECTANGLE FOR FILTERED WHITE NOISE (1ST ORDER)

CALL SMOVE(10,300)
CALL COLOR(179)
CALL TEXT('1. ',0,0,10)
CALL SMOVE(40,200)
CALL COLOR(64)
CALL SRECT(140,300)
CALL SMOVE(41,201)
CALL SRECT(139,299)

**** DRAWS A UNIT STEP RESPONSE

CALL COLOR(179)
CALL SMOVE(46,211)
CALL SDRAWR(0,78)
CALL SMOVE(46,221)
CALL SDRAWR(88,0)
CALL SMOVE(46,221)
DO (IT = 0,88)
 Y = EXP(-0.1*IT)
 IY = 221 + NINT(Y*68)
 IX = 46 + IT
 CALL SDRAW(IX,IY)
REPEAT

**** TITLE OF ABOVE RECTANGLE

CALL COLOR(215)
CALL SMOVE(50,180)
CALL TEXT('FILTERED',0,0,10)
CALL SMOVE(35,168)
CALL TEXT('WHITENoise',0,0,10)
CALL SMOVE(45,156)
CALL TEXT('1ST ORDER',0,0,10)

**** DRAW A RECTANGLE FOR FILTERED WHITE NOISE (2ND ORDER)

CALL SMOVE(190,300)
CALL COLOR(179)
CALL TEXT('2. ',0,0,10)
CALL SMOVE(220,200)
CALL COLOR(23)
CALL SRECT(320,300)
CALL SMOVE(221,201)
CALL SRECT(319,299)

**** DRAWS A UNIT STEP RESPONSE

CALL COLOR(179)

```

CALL SMOVE(226,211)
CALL SDRAWR(0,78)
CALL SMOVE(226,250)
CALL SDRAWR(88,0)
CALL SMOVE(226,250)
DO (IT = 0,88)
  Y = EXP(-0.05*IT)*COS(2*3.1416*.1*IT)
  IY = 250 + NINT(Y*39)
  IX = 226 + IT
  CALL SDRAW(IX,IY)
REPEAT

```

**** TITLE OF ABOVE RECTANGLE

```

CALL COLOR(215)
CALL SMOVE(230,180)
CALL TEXT('FILTERED',0,0,10)
CALL SMOVE(215,168)
CALL TEXT('WHITE NOISE',0,0,10)
CALL SMOVE(225,156)
CALL TEXT('2ND ORDER',0,0,10)

```

**** DRAW A RECTANGLE FOR SINE WAVE

```

CALL SMOVE(370,300)
CALL COLOR(179)
CALL TEXT('3.',0,0,10)
CALL SMOVE(400,200)
CALL COLOR(11)
CALL SRECT(500,300)
CALL SMOVE(401,201)
CALL SRECT(499,299)

```

**** DRAWS A SINE WAVE

```

CALL COLOR(179)
CALL SMOVE(406,211)
CALL SDRAWR(0,78)
CALL SMOVE(406,250)
CALL SDRAWR(88,0)
CALL SMOVE(406,250)
DO (IT = 0,88)
  Y = SIN(2*3.1416*0.05*IT)
  IY = 250 + NINT(Y*39)
  IX = 406 + IT
  CALL SDRAW(IX,IY)
REPEAT

```

**** TITLE OF ABOVE RECTANGLE

```

CALL COLOR(215)
CALL SMOVE(405,168)
CALL TEXT('SINE WAVE',0,0,10)

```

```
CALL PRMFIL(1)
RETURN
END
```

```
*****
```

```
[B*
```

```
***** ROUTINE TO READ IN SAMPLING RATE
```

```
*****
```

```
***** READS IN FREQ, THEN CALCULATES TIMER2,PRESCA2,DTF
```

```
***** DTF HAS THE FIRST POSSIBLE VALUE GREATER THAN DT
```

```
*****
```

```
*****
```

```
SUBROUTINE_ 1FREQ,DT,TIMER,PRESCA,IA_FLG)
```

```
INTEGER*1 TIMER,PRESCA
```

```
CHARACTER CHF*1
```

```
INTEGER PS,PSX
```

```
* enter the # of interrupt cycles, repetition rate (main count &
* prescaler). Rate= 1.23 MHz/ (Maincount*Prescaler)
```

```
*
```

```
* maximum main count=255
```

```
* prescaler= 4 for psch=1
```

```
* =10 =2
```

```
* =16 =3
```

```
* =50 =4
```

```
* =64 =5
```

```
* =100 =6
```

```
* =200 =7
```

```
IF(IA_FLG.EQ.1)THEN
```

```
WRITE(9,(' ENTER DESIRED ITERATION RATE IN Hz (EX.1000)'))
```

```
FREQ=1.0/DT
```

```
READ(9,*)FREQ
```

```
DT=1/(FREQ)
```

```
ENDIF
```

```
DTF=0
```

```
PRESCA=1
```

```
ITIME=0
```

```
WHILE(DT-DTF.GT.1.5E-6)
```

```
ITIME=ITIME+1 ! INCREMENT MAIN COUNTER
```

```
IF(ITIME.EQ.256)THEN IMANCOUNTEROVERFLOWED,
```

```
RESETIT
```

```
ITIME=1 !
```

```
PRESCA=PRESCA+1 ! INCREMENT TIMER
```

```
IF(PRESCA.EQ.8)THEN
```

```
WRITE(9,('CAN NOT HAVE SUCH A SLOW SAMPLING RATE'))
```

```
IF(IA_FLG.EQ.1)THEN
```

```

        GOTO 50
    ELSE
        TIMER=0
        PRESCA=0
        RETURN
    ENDIF
ENDIF
ENDIF
PSX=PRESCA

IF(PSX.EQ.1) PS=4
IF(PSX.EQ.2) PS=10
IF(PSX.EQ.3) PS=16
IF(PSX.EQ.4) PS=50
IF(PSX.EQ.5) PS=64
IF(PSX.EQ.6) PS=100
IF(PSX.EQ.7) PS=200

DTF=ITIME*PS/1.23E+6

REPEAT

DT=DTF
TIMER=ITIME
FREQ=1/(DT)

IF(IA_FLG.EQ.1)THEN
    WRITE(9,(' SAMPLING RATE",G12.4," Hz"))FREQ
    WRITE(9,(' DT",G12.4," SEC"))DT
WRIT                                     EQ('TIMER/PRESCA',25)TIMER/PRESCA
    WRITE(9,(' PRESS <CR> TO CONTINUE OR "R" TO RE-ENTER FREQ
+      "'))
    CHF=' '
    READ(9,*)CHF
    IF((CHF.EQ.'R').OR.(CHF.EQ.'r')) GOTO 50
ENDIF

RETURN

END

*****
***** SUBROUTINE FOR THE RESPONSE OF A SPECIAL EFFECT
*****
SUBROUTINE RSPSE (J)

*** J DEFINES NUMBER OF SPECIAL EFFECT,
*** IF ZERO THEN SPECIAL EFFECT IS NOT CHOSEN YET

COMMON/SMSPE1/MAXGEN,MAXPAR,SPECIAL
COMMON/SMSPE2/IEFF,NAME,WADD
COMMON/SMSPE3/NGEN,PAR,IPOINT
COMMON/SMSPE4/MAXPSTO,IPTR,PSTO

```

```

COMMON/SMSPE5/KEEP,MAXKEEP
COMMON/SMSPE6/YAMP,DTSPEF
DIMENSION NGEN(240),PAR(1000)
DIMENSION PSTO(1000),PLOT1(2000,2),KEEP(1000)
INTEGER SPECIAL(240),WADD(20)
CHARACTER NAME(20)*20,CH*1
CHARACTER VNAME*8,HEADER*20,XLABEL*4,Y
                                LABEL*6,VSMBOL*1

```

**** ENTER NUMBER OF SPECIAL EFFECT TO SEE OUTPUT

```

WRITE(9,*)
WRITE(9,*)
WRITE(9,*)
WRITE(9,('YOU HAVE SELECTED: "RESPONSE OF A SPECIAL EFFECT"
+      "))
IF (J .EQ. 0) THEN
  WRITE(9,('ENTER NUMBER OF SPECIAL EFFECT YOU WANT TO SEE
+      "))
  WRITE(9,(' <CR> TO RETURN TO PREVIOUS MENU"))
  READ(9,*) J

```

**** TEST IF SPECIAL EFFECT EXISTS

```

WHILE ((J .LE. 0) .OR. (J .GT. IEFF))
  IF (J .EQ. 0) RETURN
  J = 0
  WRITE(9,*)
  WRITE(9,*)
  WRITE(9,('WRONG SELECTION - SELECT AGAIN"))
  READ(9,*) J
  REPEAT
ENDIF

```

**** SEE IF SAMPLING INTERVAL IS CORRECT

```

WRITE(9,('SAMPLING INTERVAL IS: ",E11.5," sec")) DTSPEF
WRITE(9,(' IS IT CORRECT (Y/N)?"))
CH = 'N'
READ(9,*) CH
IF (CH .NE. 'Y') CALL R_1FREQ(DTSPEF,SETIM,SEPC,1)
WRITE(9,('ENTER TIMELENGTH (in Sec
                                )TO BE PLOTTED))
READ(9,*) TIMEPL

```

**** CALCULATES NUMBER OF SAMPLES

```

NUM_SMPL = NINT(TIMEPL/DTSPEF)
WHILE ((NUM_SMPL .GT. 2000) .OR. (NUM_SMPL .LE. 0))
  WRITE(9,*)
  WRITE(9,*)
  WRITE(9,(' LENGTH IS TOO BIG - ENTER AGAIN"))
  READ(9,*) TIMEPL
  NUM_SMPL = NINT(TIMEPL/DTSPEF)
REPEAT

```

**** INITIALIZE COUNTERS

IPT = 1
L = 0
IPTR = 1

**** LOOP THROUGH ALL GENERATORS

DO (I = 1,MAXGEN)

**** SELECT INCREMENT OF PARAMETERS

SELECT CASE (NGEN(I))
CASE (1)
IIK = 3
CASE (2)
IIK = 4
CASE (3)
IIK = 2
END SELECT

**** TEST FOR WHICH GENERATOR BELONGS TO SPECIAL EFFECT SELECTED

IF (SPECIAL(I) .EQ. J) THEN

**** IF TRUE STORE POINTERS

L = L + 2

**** INDEX OF GENERATOR

KEEP(L-1) = I

**** POINTER OF PARAMETER ARRAY PAR

KEEP(L) = PT

**** SET INITIAL CONDITIONS

SELECT CASE (NGEN(I))
CASE (1)
PSTO(IPTR) = 10000.
PSTO(IPTR+1) = 0.
CASE (2)
PSTO(IPTR) = 10000.
PSTO(IPTR+1) = 0.
PSTO(IPTR+2) = 0.
CASE (3)
PSTO(IPTR) = 0.
END SELECT

**** INCREMENT POINTER (PSTO)


```

        IPTR = IPTR + IIK - 1
    ENDIF

**** INCREMENT POINTER (PAR)

        IPT = IPT + IIK
    REPEAT

**** STORE NUMBER OF GENERATORS FOR SPECIAL EFFECT SELECTED

        MAXKEEP = L

**** TEST FOR GENERATORS

    IF (MAXKEEP .EQ. 0) THEN
        CALL CLS(0)
        CALL SMOVE(20,250)
        CALL TEXT('NO GENERATORS',0,0,20)
        WRITE(9,*)
        WRITE(9,*)
        WRITE(9,('NO GENERATORS - RETURN TO CONTINUE'))
        PAUSE
        RETURN
    ENDIF

**** ZERO ELEMENTS OF OUTPUT

DO I=1,          NUM_SMPL)
    PLOT1(I,2) = 0.
    REPEAT

**** CALCULATE AMPLITUDE OF SPECIAL EFFECT

    DO (L = 1,NUM_SMPL)
        Y = 0.

**** POINTER FOR STORAGE VARIABLE

        IPTR = 1
        DO (I = 1,MAXKEEP-1,2)
            IPT = KEEP(I+1)

**** SELECT TYPE OF GENERATOR

        SELECT CASE (NGEN(KEEP(I)))
            CASE (1)
                CALL F1AMP (IPT)
            CASE (2)
                CALL F2AMP (IPT)
            CASE (3)
                CALL SINEAMP (IPT)

```

```

        END SELECT
        Y = Y + YAMP
    REPEAT
        PLOT1(L,1) = (L - 1)*DTSPEF
        PLOT1(L,2) = Y
    REPEAT

**** PLOT YOUT ON GRAPHICS SCREEN

    HEADER = NAME(J)
    XLABEL = 'TIME'
    YLABEL = 'OUTPUT'
    VNAME = 'RESPSE'
    VSYMBOL = '1'

    CALL PLOTSIM (PLOT1,1,NUM_SMPL,HEADER,XLABEL,YLABEL,VNAME,
+               VSYMBOL)

    CALL PLTINIT
    RETURN
    END

*****
***                                     ***MANMENUFORSPECIALAFFECTS
*****

SUBROUTINE SEMMENU

COMMON/SMSPE1/MAXGEN,MAXPAR,SPECIAL
COMMON/SMSPE2/IEFF,NAME,WADD
COMMON/SMSPE3/NGEN,PAR,IPOINT
COMMON/SMSPE4/MAXPSTO,IPTR,PSTO
COMMON/SMSPE5/KEEP,MAXKEEP
COMMON/SMSPE6/YAMP,DTSPEF
DIMENSION NGEN(240),PAR(1000)
DIMENSION PSTO(1000),PLOT1(2000,2),KEEP(1000)
INTEGER SPECIAL(240),WADD(20)
CHARACTER NAME(20)*20,CH*1
CHARACTER VNAME*8,HEADER*20,XLABEL*4,YLABEL*6,VSYMBOL*1

**** TEST IF FILE WAS READ

IF ((IEFF .LT. 0) .OR. (IEFF .GT. 20)) THEN
    WRITE(9,*)
    WRITE(9,*)
    WRITE(9,(' ARRAY BOUNDARY ERROR '))
    RETURN
ENDIF

WHILE (1>0)
    WRITE(9,*)
    WRITE(9,*)
    WRITE(9,*)
    WRITE(9,(' SPECIAL EFFECTS '))

```

```

WRITE(9,('          MAIN MENU          '))
WRITE(9,*)
WRITE(9,*)
                                WRITE(9,(' 0.RETURN TOPREVIOUSMENU  '))
WRITE(9,(' 1. ADD A SPECIAL EFFECT      '))
WRITE(9,(' 2. DELETE A SPECIAL EFFECT     '))
WRITE(9,(' 3. CHANGE/VIEW A SPECIAL EFFECT  '))
WRITE(9,(' 4. RESPONSE OF A SPECIAL EFFECT  '))
WRITE(9,(' 5. CHANGE NAME/WHERE TO ADD SPECIAL EFFECT
+      '))
WRITE(9,(' 6. COPY OF GRAPHICS SCREEN   '))
WRITE(9,*)
WRITE(9,*)
WRITE(9,('          ENTER YOUR SELECTION    '))
WRITE(9,*)
WRITE(9,*)

**** LIST CURRENT SPECIAL EFFECTS ON GRAPHICS SCREEN

CALL GRAMENU

**** SELECT FROM MAIN MENU

ICH = 1000
READ(9,*) ICH
SELECT CASE (ICH)
CASE (0)
  EXIT
CASE (1)
  CALL ADDSE
CASE (2)
  CALL DELSE
CASE (3)
  CALL CHGSE
CASE (4)
                                U=0
  CALL RSPSE (IJ)
CASE (5)
  CALL CHGWADD
CASE (6)
  CH = ' '
  WRITE(9,('YOU HAVE SELECTED: "COPY GRAPHICS SCREEN"'))
+  )
  WRITE(9,(' <CR> TO RETURN - ANYTHING TO CONTINUE'))
  READ(9,*) CH
  IF (CH.NE. ' ') CALL PRNTTI
CASE DEFAULT
  WRITE(9,('ILLEGAL CHOICE'))
  WRITE(9,('MAKE ANOTHER SELECTION'))
END SELECT
REPEAT
RETURN
END

```

```

*****
***** SUBROUTINE TO INPUT PARAMETERS FOR
***** SINE WAVE GENERATOR
*****
      SUBROUTINE SINEADD (IGEN,J)

      COMMON/SMSPE1/MAXGEN,MAXPAR,SPECIAL
      COMMON/SMSPE3/NGEN,PAR,IPOINT
      DIMENSION NGEN(240),PAR(1000)
      INTEGER SPECIAL(240)

**** INPUT PARAMETERS

      WRITE(9,*)
      WRITE(9,*)
      WRITE(9,*)YOUHAVESELECTED:'SINEWAVEGENERATOR'
      WRITE(9,*)('INPUT PARAMETERS (<CR> TO RETURN TO PREVIOUS MENU
+)')
      WRITE(9,*)
      WRITE(9,*)(' AMPLITUDE OF SINE WAVE')
      AMP = 1000
      READ(9,*) AMP
      IF (AMP .EQ. 1000) RETURN
      PAR(IPOINT+1) = AMP
      WRITE(9,*)
      WRITE(9,*)(' FREQUENCY OF SINE WAVE')
      READ(9,*) PAR(IPOINT+2)
      IPOINT = IPOINT + 2

**** INCREMENT NUMBER OF GENERATORS

      IGEN = IGEN + 1

**** SPECIFY WHICH SPECIAL EFFECT IT BELONGS TO

      SPECIAL(IGEN) = J

**** TYPE OF GENERATOR

      NGEN(IGEN) = 3
      RETURN
      END

*****
***** SUBROUTINE TO CALCULATE AMPLITUDE
***** OF SINE WAVE GENERATOR
*****
      SUBROUTINE SINEAMP (IPT)

      COMMON/SMSPE3/NGEN,PAR,IPOINT
      COMMON/SMSPE4/MAXPSTO,IPTR,PSTO

```

```

COMMON/SMSPE6/YAMP,DTSPEF
DIMENSION NGEN(240),PAR(1000)
DIMENSION PSTO(1000)
DATA P3141          6

**** AMPLITUDE OF SINE WAVE

  A = PAR(IPT)

**** FREQUENCY OF SINE WAVE

  F = PAR(IPT+1)

**** INCREMENT POINTER

  IPT = IPT + 2

**** GET LAST VALUE OF TIME

  TI = PSTO(IPTR)
  FT = F*TI

**** RESETS TIME AFTER ONE CYCLE

  IF (FT .GE. 1) THEN
    TI = 0.
    FT = 0.
  ENDIF

**** CALCULATES AMPLITUDE

  YAMP = A*SIN(2*PI*FT)

**** UPDATE TIME

  TI = TI + DTSPEF

**** STORE UPDATED TIME

  PSTO(IPTR) = TI

**** INCREMENT POINTER

  IPTR = IPTR + 1
  RETURN
END

*****
***** WHITE NOISE GENERATOR
*****
SUBROUTINE WHITE (U,M,V)

COMMON/SMSPE4/MAXPSTO,IPTR,PSTO

```

```
DIMENSION PSTO(1000)
REAL M

INIT = PSTO(IPTR)
INIT = MOD(3125*INIT,65536)
X = FLOAT(INIT)/65536.
U = (X - 0.5)*V + M
PSTO(IPTR) = INIT
RETURN
EN D
```

***** ROOT SUBROUTINE FOR IMPLEMENTATION OF
 ***** VERSION #1 PRIMARY MOTION

SUBROUTINE OSUONE(DTPRMO,ITR)

**** COMMON BLOCKS USED IN SUBROUTINES CUEFIL1,SETINP,SETPLOT

COMMON/CUEFILX/BXACCN,BAXA0,BAXA1,BAXA2,BAXA3
 COMMON/CUEFILY/BYACCN,BAYA0,BAYA1,BAYA2,BAYA3
 COMMON/CUEFILZ/BZACCN,BAZA0,BAZA1,BAZA2,BAZA3
 COMMON/CUEFILQ/BAPITH,BQA0,BQA1,BQA2,BQA3
 COMMON/CUEFILP/BAROLL,BPA0,BPA1,BPA2,BPA3
 COMMON/CUEFILR/BAYAW,BRA0,BRA1,BRA2,BRA3

**** COMMON BLOCKS USED IN SUBROUTINES PREPINP,SETINP

COMMON/USER1/BIN,NINP,INPNUM,NITER
 DIMENSION BIN(2000,9),INPNUM(9)

**** COMMON BLOCKS USED IN SUBROUTINE CTRAN1

COMMON/CTTRAN/FLTAXA,FLTAYA,FLTAZA
 COMMON/CTROT/FQADOT,FPADOT,FRADOT,FQA,FPA,FRA

**** COMMON BLOCK USED IN SUBROUTINE GRAVAL1

COMMON/GRAV1/BXALIN,BYALIN

**** COMMON BLOCK USED IN SUBROUTINE PLATPOS1

COMMON/MPCP1/BXPOS,BYPOS,BZPOS,BTHPOS,BPHPOS,BSIPOS

**** COMMON BLOCK USED IN SUBROUTINE POSCON1

COMMON/POSCON1/BMXPOS,BMYPOS,BMZPOS,BMTHEP,BMPHIP,BMPSIP

**** COMMON BLOCK USED IN SUBROUTINE READPRIM

COMMON/PRIM1/XENFL,YENFL,ZENFL,THENFL,PHENFL,SIENFL
 COMMON/PRIM2/XGRFL,YGRFL,MPCPFL,MPLPFL
 COMMON/PRIM3/BXAWTC,BYAWTC,BZAWTC,BTHWTC,BPHWTC,BSIWTC
 COMMON/PRIM4/BKAX1,BKAY1,BKAZ1,BKQA1,BKPA1,BKRA1
 COMMON/PRIM5/BKAX2,BKAY2,BKAZ2,BKQA2,BKPA2,BKRA2
 COMMON/PRIM6/ALAGX,AKGAX,DLAGX,DKGAX,ALAGY,AKGAY,DLAGY,DKGAY
 COMMON/PRIM7/BKQA4,BKPA4
 COMMON/PRIM8/BLAGX,BLAGY,BLAGZ,BLAGT,BLAGP,BLAGS

INTEGER*4 XENFL,YENFL,ZENFL,THENFL,PHENFL,SIENFL
 INTEGER*4 XGRFL,YGRFL,MPCPFL,MPLPFL
 REAL BXAWTC,BYAWTC,BZAWTC,BTHWTC,BPHWTC,BSIWTC

```

REAL BKAX1,BKAY1,BKAZ1,BKQA1,BKPA1,BKRA1
REAL BKAX2,BKAY2,BKAZ2,BKQA2,BKPA2,BKRA2
REAL ALAGX,AKGAX,DLAGX,DKGAX,ALAGY,AKGAY,DLAGY,DKGAY
REAL BKQA4,BKPA4
REAL BLAGX,BLAGY,BLAGZ,BLAGT,BLAGP,BLAGS

```

*

**** MAIN LOOP - PRIMARY MOTION

*

**** SET AIRCRAFT ACCELERATIONS FROM PREPARED INPUT

CALL SETINP(ITR)

**** PERFORM CENTROID TRANSFORMATIONS

CALL CTRAN1

**** PERFORM WASHOU T(VERSION#1)

CALL CUEFIL1(DTPRMO)

**** PERFORM GRAVITY ALIGNMENT (VERSION #1)

CALL GRAVAL1

**** PERFORM MOTION PLATFORM COMMENDED POSITIONS (VERSION #1)

CALL PLATPOS1

**** PERFORM MOTION POSITION CONTROL (VERSION #1)

CALL POSCON1

RETURN

END

***** MOTION ONSET CUE FILTERS SUBROUTINE

SUBROUTINE CUEFIL1(FIC20)

COMMON/CUEFILX/BXACCN,BAXA0,BAXA1,BAXA2,BAXA3

COMMON/CUEFILY/BYACCN,BAYA0,BAYA1,BAYA2,BAYA3

COMMON/CUEFILZ/BZACCN,BAZA0,BAZA1,BAZA2,BAZA3

COMMON/CUEFILQ/BAPITH,BQA0,BQA1,BQA2,BQA3

COMMON/CUEFILP/BAROLL,BPA0,BPA1,BPA2,BPA3

COMMON/CUEFILR/BAYAW,BRA0,BRA1,BRA2,BRA3

COMMON/PRIM1/XENFL,YENFL,ZENFL,THENFL,PHENFL,SIENFL

COMMON/PRIM3/BXAWTC,BYAWTC,BZAWTC,BTHWTC,BPHWTC,BSIWTC
COMMON/PRIM4/BKAX1,BKAY1,BKAZ1,BKQA1,BKPA1,BKRA1
COMMONPR ~~M5BKAX2BKAY2BKAZ2BKQA2BKPA2BKRA2~~

INTEGER*4 XENFL,YENFL,ZENFL,THENFL,PHENFL,SIENFL
REAL BXAWTC,BYAWTC,BZAWTC,BTHWTC,BPHWTC,BSIWTC
REAL BKAX1,BKAY1,BKAZ1,BKQA1,BKPA1,BKRA1
REAL BKAX2,BKAY2,BKAZ2,BKQA2,BKPA2,BKRA2

*
**** LINEAR THIRD ORDER WASHOUT FILTER FOR THE LATERAL AXIS (X)
*

ALPHA=BXAWTC ; A=BKAX2+ALPHA ; B=BKAX1+BKAX2*ALPHA
C=BKAX1*ALPHA ; D=BKAX1

BAXA0=D*BXACCN-A*BAXA1-B*BAXA2-C*BAXA3
BAXA1=BAXA1+FIC20*BAXA0
BAXA2=BAXA2+FIC20*BAXA1
BAXA3=BAXA3+FIC20*BAXA2

*
**** LINEAR THIRD ORDER WASHOUT FILTER FOR THE LATERAL AXIS (Y)
*

ALPHA=BYAWTC ; A=BKAY2+ALPHA ; B=BKAY1+BKAY2*ALPHA
C=BKAY1*ALPHA ; D=BKAY1

BAYA0=D*BYACCN-A*BAYA1-B*BAYA2-C*BAYA3
BAYA1=BAYA1+FIC20*BAYA0
BAYA2=BAYA2+FIC20*BAYA1
BAYA3=BAYA3+FIC20*BAYA2

*
**** LINEAR THIRD ORDER WASHOUT FILTER FOR THE VERTICAL AXIS (Z)
*

ALPHA=BZAWTC ; A=BKAZ2+ALPHA ; B=BKAZ1+BKAZ2*ALPHA
C=BKAZ1*ALPHA ; D=BKAZ1

BAZA0=D*BZACCN-A*BAZA1-B*BAZA2-C*BAZA3
BAZA1=BAZA1+FIC20*BAZA0
BAZA2=BAZA2+FIC20*BAZA1
BAZA3=BAZA3+FIC20*BAZA2

*
**** LINEAR THIRD ORDER WASHOUT FILTER FOR THE PITCH AXIS (Q)
* (DISABLED)

* ALPHA=BTHWTC ; A=BKQA2+ALPHA ; B=BKQA1+BKQA2*ALPHA
* C=BKQA1*ALPHA ; D=BKQA1
*

```

*   BQA0=D*BAPITH-A*BQA1-B*BQA2-C*BQA3
*   BQA1=BQA1+FIC20*BQA0
*   BQA2=BQA2+FIC20*BQA1
***** BQA3=BQA3+FIC20*BQA2

*
***** LINEAR THIRD ORDER WASHOUT FILTER FOR THE ROLL AXIS (P)
*

ALPHA=BPHWTC ; A=BKPA2+ALPHA ; B=BKPA1+BKPA2*ALPHA
C=BKPA1*ALPHA ; D=BKPA1

BPA0=D*BAROLL-A*BPA1-B*BPA2-C*BPA3
BPA1=BPA1+FIC20*BPA0
BPA2=BPA2+FIC20*BPA1
BPA3=BPA3+FIC20*BPA2

*
**** LINEAR THIRD ORDER WASHOUT FILTER FOR THE YAW AXIS (R)
*

ALPHA=BSIWTC ; A=BKRA2+ALPHA ; B=BKRA1+BKRA2*ALPHA
C=BKRA1*ALPHA ; D=BKRA1

BRA0=D*BAYAWA-BRA1-B*BRA2-C*B          RA3
BRA1=BRA1+FIC20*BRA0
BRA2=BRA2+FIC20*BRA1
BRA3=BRA3+FIC20*BRA2

RETURN
END

*****
*****
***** SUBROUTINE TO EXECUTE THE CENTROID TRANSFORMATIONS
*****

SUBROUTINE CTRAN1

COMMON/CUEFILX/BXACCN,BAXA0,BAXA1,BAXA2,BAXA3
COMMON/CUEFILY/BYACCN,BAYA0,BAYA1,BAYA2,BAYA3
COMMON/CUEFILZ/BZACCN,BAZA0,BAZA1,BAZA2,BAZA3
COMMON/CUEFILQ/BAPITH,BQA0,BQA1,BQA2,BQA3
COMMON/CUEFILP/BAROLL,BPA0,BPA1,BPA2,BPA3
COMMON/CUEFILR/BAYAW,BRA0,BRA1,BRA2,BRA3

COMMON/CTTRAN/FLTAXA,FLTAYA,FLTAZA
COMMON/CTROT/FQADOT,FPADOT,FRADOT,FQA,FPA,FRA

**** DEFINE THE CONSTANTS (LATER ALLOW TO BE CHANGED BY USER)

FRX=10. ; FRY=0. ; FRZ=0.

```

FDCOSL3=0. ;FDCOSM3=0. ; FDCOSN3=0.0 ; G=32.174

*

**** THE TRANSFORMATIONS

*

**** LONGITUDINAL ACCELERATION

BXACCN= FLTAXA - (FQA**2+FRA**2)*FRX
 1 + (FOA*FPA -FRADOT)*FRY
 1 + (FRA*FPA+FQADOT)*FRZ
 1 + FDCOSL3*G

**** LATERAL ACCELERATION

BYACCN= FLTAYA + (FPA*FQA+FRADOT)*FRX
 1 - (FPA**2+FRA**2)*FRY
 1 + (FRA*FQA-FPADOT)*FRZ
 1 + FDCOSM3*G

**** VERTICAL ACCELERATION

BZACCN= FLTAZA + (FPA*FRA-FQADOT)*FRX
 1 + (FQA*FRA+FPADOT)*FRY
 1 - (FPA**2+FQA**2)*FRZ
 1 + FDCOSN3*G

**** SELECT TO PASS ANGULAR RATES (NOT ACCELERATIONS) TO WASHOUT

CC BAPITH=FQA

BAROLL=FPA

BAYAW=FRA

RETURN

END

***** GRAVITY ALIGNMENT SUBROUTINE

SUBROUTINE GRAVAL1

COMMON/CUEFILX/BXACCN,BAXA0,BAXA1,BAXA2,BAXA3

COMMON/CUEFILI/BYACCN,BAYA0,BAYA1,BAYA2,BAYA3

COMMON/CUEFLZEZ ACCNBAZA0,BAZA1,BAZA2,BAZA3

COMMON/CUEFILQ/BAPITH,BQA0,BQA1,BQA2,BQA3

COMMON/CUEFILP/BAROLL,BPA0,BPA1,BPA2,BPA3

COMMON/CUEFILR/BAYAW,BRA0,BRA1,BRA2,BRA3

COMMON/GRAV1/BXALIN,BYALIN

COMMON/PRIM2/XGRFL,YGRFL,MPCPFL,MPLPFL

COMMON/PRIM6/ALAGX,AKGAX,DLAGX,DKGAX,ALAGY,AKGAY,DLAGY,DKGAY

```

INTEGER*4 XGRFL,YGRFL,MPCPFL,MPLPFL
REAL ALAGX,AKGAX,DLAGX,DKGAX,ALAGY,AKGAY,DLAGY,DKGAY

```

```

**** GRAVITY ALIGN LONGITUDINAL ACCELERATION

```

```

IF (BXACCN.GT.0.0) THEN
  FLAGP=ALAGX
  BKGAP=AKGAX
ELSE
  FLAGP=DLAGX
  BKGAP=DKGAX
ENDIF
BXALIN=BXALIN+FLAGP*(BKGAP*BXACCN-BXALIN)

```

```

**** GRAVITY ALIGN LATERAL ACCELERATION

```

```

IF (BYACCN.GT.0.0) THEN
  FLAGY=ALAGY
  BKGAY=AKGAY
ELSE
  FLAGY=DLAGY
  BKGAY=DKGAY
ENDIF
BYALIN=BYALIN+FLAGY*(BKGAY*BYACCN-BYALIN)

```

```

RETURN
END

```

```

*****

```

```

*****

```

```

****

```

```

MOTIONPLATFORMCOMMANDEDPOSITIONSSUBROUTINE

```

```

*****

```

```

SUBROUTINE PLATPOS1

```

```

COMMON/CUEFILX/BXACCN,BAXA0,BAXA1,BAXA2,BAXA3
COMMON/CUEFILI/BYACCN,BAYA0,BAYA1,BAYA2,BAYA3
COMMON/CUEFILZ/BZACCN,BAZA0,BAZA1,BAZA2,BAZA3
COMMON/CUEFILQ/BAPITH,BQA0,BQA1,BQA2,BQA3
COMMON/CUEFILP/BAROLL,BPA0,BPA1,BPA2,BPA3
COMMON/CUEFILR/BAYAW,BRA0,BRA1,BRA2,BRA3

```

```

COMMON/GRAV1/BXALIN,BYALIN

```

```

COMMON/MPCP1/BXPOS,BYPOS,BZPOS,BTHPOS,BPHPOS,BSIPOS

```

```

COMMON/PRIM7/BKQA4,BKPA4
REAL BKQA4,BKPA4

```

```

**** INITIALIZE THE CONSTANTS

```

BKXPOS=0.037
BKYPOS=0.037
BKZPOS=0.037

BKTHP=0.037
BKPIP=0.037
BKSIP=0.037

**** SET ALL SPECIAL EFFECTS TO ZERO

BSPEFX=0.0
BSPEFY=0.0
BTURBW=0.0

FSINT=0.0
FSINPH=0.0

BSPEFQ=0.0
BSPEFP=0.0
BSPEFR=0.0

**** LONGITUDINAL

BXPOS=BKXPOS*BAXA2+BSPEFX

**** LATERAL

BYPOS=BKYPOS*BAYA2+BSPEFY

**** VERTICAL

BZPOS=BKZPOS*BAZA2+BTURBW

**** PITCH

BTHPOS=BKTHP*BQA2+BKQA4*FSINT+BXALIN+BSPEFQ

**** ROLL

BPHPOS=BKPIP*BPA2+BKPA4*FSINPH+BYALIN+BSPEFP

**** YAW

BSIPOS=BKSIP*BRA2+BSPEFR

RETURN
END

***** MOTION POSITION CONTROL SUBROUTINE

```

SUBROUTINE POSCON1

COMMON/MPCP1/BXPOS,BYPOS,BZPOS,BTHPOS,BPHPOS,BSIPOS

COMMON/POSCON1/BMXPOS,BMYPOS,BMZPOS,BMTHEP,BMPHIP,BMPSIP

COMMON/PRIM2/XGRFL,YGRFL,MPCPFL,MPLPFL
COMMON/PRIM8/BLAGX,BLAGY,BLAGZ,BLAGT,BLAGP,BLAGS

INTEGER*4 XGRFL,YGRFL,MPCPFL,MPLPFL
REAL BLAGX,BLAGY,BLAGZ,BLAGT,BLAGP,BLAGS

**** POSITION CONTROL OUTPUTS (THE SIX POSITIONS IN INCHES )

BMXPOS=BMXPOS+(BXPOS*12.-BMXPOS)*BLAGX
BMYPOS=BMYPOS+(BYPOS*12.-BMYPOS)*BLAGY
BMZPOS=BMZPOS+(BZPOS*12.-BMZPOS)*BLAGZ

BMTHEP=BMTHEP+(BTHPOS-BMTHEP)*BLAGT
BMPHIP=BMPHIP+(BPHPOS-BMPHIP)*BLAGP
BMPSIP=BMPSIP+(BSIPOS-BMPSIP)*BLAGS

RETURN
END

*****
***** ROUTINE TO READ THE PRIMARY MOTION PARAMETERS FROM A FILE
*****
SUBROUTINE READPRIM

COMMON/PRIM1/XENFL,YENFL,ZENFL,THENFL,PHENFL,SIENFL
COMMON/PRIM2/XGRFL,YGRFL,MPCPFL,MPLPFL
COMMON/PRIM3/BXAWTC,BYAWTC,BZAWTC,BTHWTC,BPHWTC,BSIWTC
COMMON/PRIM4/BKAX1,BKAY1,BKAZ1,BKQA1,BKPA1,BKRA1
COMMON/PRIM5/BKAX2,BKAY2,BKAZ2,BKQA2,BKPA2,BKRA2
COMMON/PRIM6/ALAGX,AKGAX,DLAGX,DKGAX,ALAGY,AKGAY,DLAGY,DKGAY
COMMON/PRIM7/BKQA4,BKPA4
COMMON/PRIM8/BLAGX,BLAGY,BLAGZ,BLAGT,BLAGP,BLAGS

INTEGER*4 XENFL,YENFL,ZENFL,THENFL,PHENFL,SIENFL
INTEGER*4 XGRFL,YGRFL,MPCPFL,MPLPFL
REAL BXAWTC,BYAWTC,BZAWTC,BTHWTC,BPHWTC,BSIWTC
REAL BKAX1,BKAY1,BKAZ1,BKQA1,BKPA1,BKRA1
REAL BKAX2,BKAY2,BKAZ2,BKQA2,BKPA2,BKRA2
REAL ALAGX,AKGAX,DLAGX,DKGAX,ALAGY,AKGAY,DLAGY,DKGAY
REAL BLAGX,BLAGY,BLAGZ,BLAGT,BLAGP,BLAGS

CHARACTER MOTFNAM*16
LOGICAL EX
EX = .FALSE.
MOTFNAM = 'PRIMPAR.SA'
WRITE(9,*) ('WHAT IS PRIMARY MOTION DATA FILE NAME?')

```

```

READ(9,*) MOTFNAM
INQUIRE(FILE=MOTFNAM,EXIST=EX,IOSTAT=IOS,ERR=1000)
IF(.NOT. EX) THEN
  WRITE(9,('DATA FILE ",(A)," DOES NOT EXIST')) MOTFNAM
  STOP
ENDIF
OPEN(UNIT=10,FILE=MOTFNAM)

READ(10,*)XENFL,YENFL,ZENFL,THENFL,PHENFL,SIENFL
READ(10,*)XGRFL,YGRFL,MPCPFL,MPLPFL
READ(10,*)BXAWTC,BYAWTC,BZAWTC,BTHWTC,BPHWTC,BSIWTC
READ(10,*)BKAX1,BKAY1,BKAZ1,BKQA1,BKPA1,BKRA1
READ(10,*)BKAX2,BKAY2,BKAZ2,BKQA2,BKPA2,BKRA2
READ(10,*)ALAGX,AKGAX,DLAGX,DKGAX,ALAGY,AKGAY,DLAGY,DKGAY
READ(10,*)BKQA4,BKPA4
READ(10,*)BLAGX,BLAGY,BLAGZ,BLAGT,BLAGP,BLAGS

RETURN
1000 WRITE(9,(' ERROR READING THE FILE '))
RETURN
END

*****
*****
***** SUBROUTINE TO PREPARE THE INPUT BASED ON USER REQUIREMENT
*****

SUBROUTINE PREPINP(FIC20)

COMMON/USER1/BIN,NINP,INPNUM,NITER
DIMENSION BIN(2000,9),INPNUM(9)

CALL INIT_PROG_VARS

DO (I=1,9)
  INPNUM(I)=0
REPEAT

WRITE(9,(' ENTER NUMBER OF ITERATIONS '))
WRITE(9,(' ENTER 0 FOR NO INPUT'))
NITER = 0
READ(9,*)NITER
IF (NITER .EQ. 0) RETURN
DO (I=1,10)
  WRITE(9,*)
REPEAT
WRITE(9,(' INPUT VARIABLES '))
WRITE(9,*)
WRITE(9,(' 1. LONGITUDINAL ACCELERATION (FLTAXA) '))
WRITE(9,(' 2. LATERAL ACCELERATION (FLTAYA) '))
WRITE(9,(' 3. VERTICAL ACCELERATION (FLTAZA) '))
WRITE(9,(' 4. PITCH ACCELERATION (FQADOT) '))
WRITE(9,(' 5. ROLL ACCELERATION (FPADOT) '))

```

```

WRITE(9,(' 6. YAW ACCELERATION      (FRADOT ")')
WRITE(9,(' 7. PITCH VELOCITY      (FPA) ")')
WRITE(9,(' 8. ROLL VELOCITY      (FPA ")')
WRITE(9,(' 9. YAW VELOCITY      (FRA ")')
WRITE(9,*)
WRITE(9,(' ENTER VARIABLES ")')
READ(9,*)(INPNUM(I),I=1,9)

```

```

**** DETERMINE NUMBER OF INPUTS

```

```

I=1
WHILE((INPNUM(I).GE.1).AND.(INPNUM(I).LE.9))
  I=I+1
  IF(I.EQ.10) EXIT
REPEAT
NINP=I-1

```

```

**** CONSTRUCT INPUT

```

```

DO (I=1,NINP)

```

```

**** LONGITUDINAL ACCELERATION

```

```

IF (INPNUM(I).EQ.1) THEN
  WRITE(9,(' FOR THE LONGITUDINAL ACCELERATION "))
  CALL SETBIN(1,FIC20)

```

```

**** LATERAL ACC

```

```

ELSEIF (INPNUM(I).EQ.2) THEN
  WRITE(9,(' FOR THE LATERAL ACCELERATION "))
  CALL SETBIN(2,FIC20)

```

```

**** VERTICAL ACCELERATION

```

```

ELSEIF (INPNUM(I).EQ.3) THEN
  WRITE(9,(' FOR THE VERTICAL ACCELERATION "))
  CALL SETBIN(3,FIC20)

```

```

**** PITCH ACCELERATION

```

```

ELSEIF (INPNUM(I).EQ.4) THEN
  WRITE(9,(' FOR THE PITCH ACCELERATION "))
  CALL SETBIN(4,FIC20)

```

```

**** ROLL ACCELERATION

```

```

ELSEIF (INPNUM(I).EQ.5) THEN
  WRITE(9,(' FOR THE ROLL ACCELERATION "))
  CALL SETBIN(5,FIC20)

```

```

**** YAW ACCELERATION

```



```

ELSEIF (INPNUM(I).EQ.6) THEN
  WRITE(9,(' FOR THE YAW ACCELERATION '))
  CALL SETBIN(6,FIC20)

**** PITCH VELOCITY

ELSEIF (INPNUM(I).EQ.7) THEN
  WRITE(9,(' FOR THE PITCH VELOCITY '))
  CALL SETBIN(7,FIC20)

**** ROLL VELOCITY

ELSEIF (INPNUM(I).EQ.8) THEN
  WRITE(9,(' FOR THE ROLL VELOCITY '))
  CALL SETBIN(8,FIC20)

**** YAW VELOCITY

ELSEIF (INPNUM(I).EQ.9) THEN
  WRITE(9,(' FOR THE YAW VELOCITY '))
  CALL SETBIN(9,FIC20)
ENDIF
REPEAT

RETURN
END

*****
*****
***** SUBROUTINETOSETUPARRAYBIN
*****
SUBROUTINE SETBIN(M,FIC20)

COMMON/USER1/BIN,NINP,INPNUM,NITER
DIMENSION BIN(2000,9),INPNUM(9)

DIMENSION BRKPT(10),AMP(10)

WRITE(9,*)
WRITE(9,(' SELECT INPUT SIGNAL TYPE '))
WRITE(9,*)
WRITE(9,(' 1- STAIR STEP      '))
WRITE(9,(' 2- SINE WAVE         '))
WRITE(9,(' 3- READ FROM A FILE   '))
WRITE(9,*)
READ(9,*)ISEL

IF (ISEL.EQ.1) THEN

  WRITE(9,(' ENTER # INPUT AMPLITUDE CHANGES'))
  READ(9,*)NUMCHG
  DO (J=1,NUMCHG)

```

```

WRITE(9,(' ENTER BREAK POINT AND AMPLITUDE "))
READ(9,*)BRKPT(J),AMP(J)
REPEAT
DO (K=1,NITER)
DO (JJ=1,NUMCHG-1)
IF ((K.GE.BRKPT(JJ)).AND.(K.LT.BRKPT(JJ+1)))
1   BIN(K,M)=AMP(JJ)
REPEAT
IF (K.LT.BRKPT(1)) BIN(K,M)=0.0
IF (K.GE.BRKPT(NUMCHG)) BIN(K,M)=AMP(NUMCH
REPEAT

ELSEIF(ISEL.EQ.2) THEN

WRITE(9,(' ENTER THE AMPLITUDE & FREQ OF WAVE "))
READ(9,*)AAMP,FREQ

**** SIN WAVE WITH FIG20

DO (K=1,NITER)
BIN(K,M)=AAMP*SIN(2.*3.1415927*FREQ*FLOAT(K)*FIG20)
REPEAT

ENDIF

RETURN
END
*****
*****
***** SUBROUTINE TO SET THE DIFFERENT INPUTS IN EACH ITERATION.
***** THE ARRAY BIN IS USED TO SET THE PROPER INPUT VALUE FOR THE
***** RIGHT VARIABLE.
*****
SUBROUTINE SETINP(IT)

COMMON/CTTRAN/FLTAXA,FLTAYA,FLTAZA
COMMON/CTROT/FQADOT,FPADOT,FRADOT,FQA,FPA,FRA

COMMON/USER1/BIN,NINP,INPNUM,NITER
DIMENSION BIN(2000,9),INPNUM(9)

FLTAXA=BIN(IT,1)
FLTAYA=BIN(IT,2)
FLTAZA=BIN(IT,3)
FQADOT=BIN(IT,4)
FPADOT=BIN(IT,5)
FRADOT=BIN(IT,6)
FQA=BIN(IT,7)
FPA=BIN(IT,8)
FRA=BIN(IT,9)

RETURN
END

```

```
*****
*****
***** SUBROUTINE TO INITIALIZE THE PROGRAM VARIABLES
*****

SUBROUTINE INIT_PROG_VARS

COMMON/USER1/BIN,NINP,INPNUM,NITER
DIMENSION BIN(2000,9),INPNUM(9)

DO (J=1,9)
  DO (I=1,2000)
    BIN(I,J)=0.0
  REPEAT
REPEAT

RETURN
END

*****
```

NUMBER	SYMBOL	NAME - DESCRIPTION	SCALE
1	POSX	SPECIAL EFF - X AXIS	1.0
2	POSY	SPECIAL EFF - Y AXIS	1.0
3	POSZ	SPECIAL EFF - Z AXIS	1.0
4	POSTHE	SPECIAL EFF - PITCH	1.0
5	POSPHI	SPECIAL EFF - ROLL	1.0
6	POSPSI	SPECIAL EFF - YAW	1.0
7	PD11	PISTON1 DISPLACEMENT	1.0
8	PD21	PISTON2 DISPLACEMENT	1.0
9	PD31	PISTON3 DISPLACEMENT	1.0
10	PD41	PISTON4 DISPLACEMENT	1.0
11	PD51	PISTON5 DISPLACEMENT	1.0
12	PD61	PISTON6 DISPLACEMENT	1.0
13	PDOT11	PISTON1 VELOCITY	1.0
14	PDOT21	PISTON2 VELOCITY	1.0
15	PDOT31	PISTON3 VELOCITY	1.0
16	PDOT41	PISTON4 VELOCITY	1.0
17	PDOT51	PISTON5 VELOCITY	1.0
18	PDOT61	PISTON6 VELOCITY	1.0
19	X11	SPOOL1 DISPLACEMENT	1.0
20	X21	SPOOL2 DISPLACEMENT	1.0
21	X31	SPOOL3 DISPLACEMENT	1.0
22	X41	SPOOL4 DISPLACEMENT	1.0
23	X51	SPOOL5 DISPLACEMENT	1.0
24	X61	SPOOL6 DISPLACEMENT	1.0
25	XDOT11	SPOOL1 VELOCITY	1.0
26	XDOT21	SPOOL2 VELOCITY	1.0
27	XDOT31	SPOOL3 VELOCITY	1.0
28	XDOT41	SPOOL4 VELOCITY	1.0
29	XDOT51	SPOOL5 VELOCITY	1.0
30	XDOT61	SPOOL6 VELOCITY	1.0
31	VOUT1	VOLTAGE TO VALVE1	0.001
32	VOUT2	VOLTAGE TO VALVE2	1.0
33	VOUT3	VOLTAGE TO VALVE3	1.0
34	VOUT4	VOLTAGE TO VALVE4	1.0
35	VOUT5	VOLTAGE TO VALVE5	1.0
36	VOUT6	VOLTAGE TO VALVE6	1.0
37	CPRS1	CAP PRESSURE1	0.002
38	CPRS2	CAP PRESSURE2	1.0
39	CPRS3	CAP PRESSURE3	1.0
40	CPRS4	CAP PRESSURE4	1.0
41	CPRS5	CAP PRESSURE5	1.0
42	CPRS6	CAP PRESSURE6	1.0
43	RPRS1	ROD PRESSURE1	0.002
44	RPRS2	ROD PRESSURE2	1.0
45	RPRS3	ROD PRESSURE3	1.0
46	RPRS4	ROD PRESSURE4	1.0
47	RPRS5	ROD PRESSURE5	1.0
48	RPRS6	ROD PRESSURE6	1.0
49	POSI1	CYLINDER1 LENGTH	1.0
50	POSI2	CYLINDER2 LENGTH	1.0
51	POSI3	CYLINDER3 LENGTH	1.0

52	POS14	CYLINDER4 LENGTH	1.0
53	POS15	CYLINDER5 LENGTH	1.0
54	POS16	CYLINDER6 LENGTH	1.0
55	CYLOT1	COMM CYL1 LENGTH	1.0
56	CYLOT2	COMM CYL2 LENGTH	1.0
57	CYLOT3	COMM CYL3 LENGTH	1.0
58	CYLOT4	COMM CYL4 LENGTH	1.0
59	CYLOT5	COMM CYL5 LENGTH	1.0
60	CYLOT6	COMM CYL6 LENGTH	1.0
61	FORCE1	DIFFERENTIAL FORCE1	1.0
62	FORCE2	DIFFERENTIAL FORCE2	1.0
63	FORCE3	DIFFERENTIAL FORCE3	1.0
64	FORCE4	DIFFERENTIAL FORCE4	1.0
65	FORCE5	DIFFERENTIAL FORCE5	1.0
66	FORCE6	DIFFERENTIAL FORCE6	1.0
67	Q61	COMPRESS. FLOW1	1.0
68	Q62	COMPRESS. FLOW2	1
69	Q63	COMPRESS. FLOW3	1.0
70	Q64	COMPRESS. FLOW4	1.0
71	Q65	COMPRESS. FLOW5	1.0
72	Q66	COMPRESS. FLOW6	1.0
73	Q71	COMPRESS. FLOW1	0.1
74	Q72	COMPRESS. FLOW2	1.0
75	Q73	COMPRESS. FLOW3	1.0
76	Q74	COMPRESS. FLOW4	1.0
77	Q75	COMPRESS. FLOW5	1.0
78	Q76	COMPRESS. FLOW6	1.0
79	SIGNA1	SPEFX+PRIMOX	1.0
80	SIGNA2	SPEFY+PRIMOY	1.0
81	SIGNA3	SPEFZ+PRIMOZ	1.0
82	SIGNA4	SPEFTH+PRIMOTHE	1.0
83	SIGNA5	SPEFPHI+PRIMOPHI	1.0
84	SIGNA6	SPEFPSI+PRIMOPSI	1.0
85	COMP1	COMPENSATION 1	1.0
86	COMP2	COMPENSATION 2	1.0
87	COMP3	COMPENSATION 3	1.0
88	COMP4	COMPENSATION 4	1.0
89	COMP5	COMPENSATION 5	1.0
90	COMP6	COMPENSATION 6	1.0
91	Q11	FLOW11	0.1
92	Q12	FLOW12	1.0
93	Q13	FLOW13	1.0
94	Q14	FLOW14	1.0
95	Q15	FLOW15	1.0
96	Q16	FLOW16	1.0
97	Q21	FLOW21	1.0
98	Q22	FLOW22	1.0
99	Q23	FLOW22	1.0
100	Q24	FLOW25	1.0
101	Q25	FLOW24	1.0
102	Q26	FLOW26	1.0
103	V11	CAP VOLUME1	1.0
104	V12	CAPVOLUME2	1.0

105	V13	CAP VOLUME3	1.0
106	V14	CAP VOLUME4	1.0
107	V15	CAP VOLUME5	1.0
108	V16	CAP VOLUME6	1.0
109	V21	ROD VOLUME1	1.0
110	V22	ROD VOLUME2	1.0
111	V23	ROD VOLUME3	1.0
112	V24	ROD VOLUME4	1.0
113	V25	ROD VOLUME5	1.0
114	V26	ROD VOLUME6	1.0
115	Q31	LEAKAGE FLOW31	1.0
116	Q32	LEAKAGE FLOW32	1.0
117	Q33	LEAKAGE FLOW33	1.0
118	Q34	LEAKAGE FLOW34	1.0
119	Q35	LEAKAGE FLOW35	1.0
120	Q36	LEAKAGE FLOW36	1.0
121	Q41	LEAKAGE FLOW41	1.0
122	Q42	LEAKAGE FLOW42	1.0
123	Q43	LEAKAGE FLOW43	1.0
124	Q44	LEAKAGE FLOW44	1.0
125	Q45	LEAKAGE FLOW45	1.0
126	Q46	LEAKAGE FLOW46	1.0
127	Q51	LEAKAGE FLOW51	1.0
128	Q52	LEAKAGE FLOW52	1.0
129	Q53	LEAKAGE FLOW53	1.0
130	Q54	LEAKAGE FLOW54	1.0
131	Q55	LEAKAGE FLOW55	1.0
132	Q56	LEAKAGE FLOW56	1.0
133	UIN1	DIFFERENCIAL PRESS1	0.01
134	UIN2	DIFFERENCIAL PRESS2	1.0
135	UIN3	DIFFERENCIAL PRESS3	1.0
136	UIN4	DIFFERENCIAL PRESS4	1.0
137	UIN5	DIFFERENCIAL PRESS5	1.0
138	UIN6	DIFFERENCIAL PRESS6	1.0
139	TINX	INV. TRANSF. X	1.0
140	TINY	INV. TRANSF. Y	1.0
141	TINZ	INV. TRANSF. Z	1.0
142	TINVTH	INV. TRANSF. THE	1.0
143	TINVPH	INV. TRANSF. PHI	1.0
144	TINVPS	INV. TRANSF. PSI	1.0
145	AFTER1	CEXT AFTER INVTRANS	1.0
146	AFTER2	CEXT AFTER INVTRANS	1.0
147	AFTER3	CEXT AFTER INVTRANS	1.0
148	AFTER4	CEXT AFTER INVTRANS	1.0
149	AFTER5	CEXT AFTER INVTRANS	1.0
150	AFTER6	CEXT AFTER INVTRANS	1.0
151	FLTAXA	X ACC. INPUT	1.0
152	FLTAYA	Y ACC. INPUT	1.0
153	FLTAZA	Z ACC. INPUT	1.0
154	FQA	PITCH RATE INPUT	1.0
155	FPA	ROLL RATE INPUT	1.0
156	FRA	YAW RATE INPUT	1.0
157	FQADOT	PITCH ACC. INPUT	1.0

158	FPADOT	ROLL ACC. INPUT	1.0
159	FRADOT	YAW ACC. INPUT	1.0
160	BXACCN	X CENT. ACC.	1.0
161	BYACCN	Y CENT. ACC.	1.0
162	BZACCN	Z CENT. ACC.	1.0
163	BAROLL	ROLL CENT. ACC.	1.0
164	BAYAW	YAW CENT. ACC.	1.0
165	BAXA2	X OUTPUT OF WASHOUT	1.0
166	BAYA2	Y OUTPUT OF WASHOUT	1.0
167	BAZA2	Z OUTPUT OF WASHOUT	1.0
168	BPA2	ROLL OUTPUT OF WASHOUT	1.0
169	BRA2	YAW OUTPUT OF WASHOUT	1.0
170	BXALIN	X GRAVITY ALIGN.	1.0
171	BYALIN	Y GRAVITY ALING.	1.0
172	BXPOS	X PLATF. POS.	1.0
173	BYPOS	Y PLATF. POS.	1.0
174	BZPOS	Z PLATF. POS.	1.0
175	BTHPOS	PITCH PLATF. POS.	1.0
176	BPHPOS	ROLL PLATF. POS.	1.0
177	BSIPOS	YAW PLATF. POS.	1.0
178	BMXPOS	X OUTPUT OF PRIM. MOTION	1.0
179	BMYPOS	Y OUTPUT OF PRIM. MOTION	1.0
180	BMZPOS	Z OUTPUT OF PRIM. MOTION	1.0
181	BMTHEP	PITCH OUTPUT PRIM. MOTION	1.0
182	BMPHIP	ROLL OUTPUT PRIM. MOTION	1.0
183	BMP SIP	YAW OUTPUT PRIM. MOTION	1.0
184	BAXA0	X ACC WASHOUT	1.0
185	BAYA0	Y ACC WASHOUT	1.0
186	BAZA0	Z ACC WASHOUT	1.0
187	BPA0	ROLL RATE WASHOUT	1.0
188	BRA0	YAW RATE WASHOUT	1.0
189	BAXA1	X VEL WASHOUT	1.0
190	BAYA1	Y VEL WASHOUT	1.0
191	BAZA1	Z VEL WASHOUT	1.0
192	BPA1	ROLL WASHOUT	1.0
193	BRA1	YAW WASHOUT	1.0
194	BAXA3	X INT WASHOUT	1.0
195	BAYA3	Y INT WASHOUT	1.0
196	BAZA3	Z INT WASHOUT	1.0
197	BPA3	ROLL INT WASHOUT	1.0
198	BRA3	YAW INT WASHOUT	1.0

VITA ²

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Master of Science

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SIX-DEGREE-OF-FREEDOM MOTION BASE
SYSTEM FOR FLIGHT SIMULATORS**

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